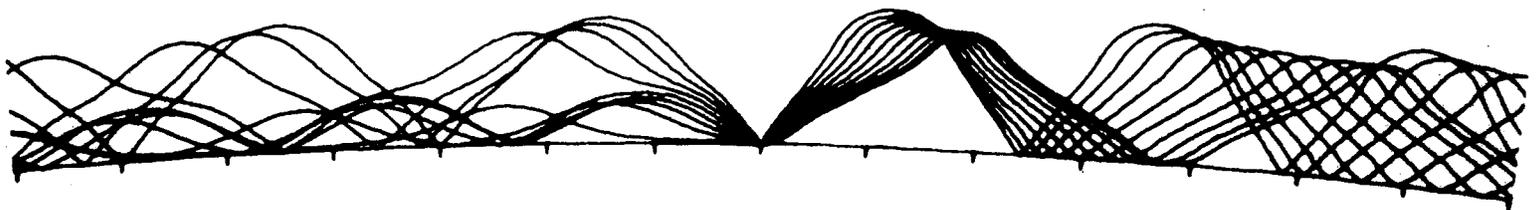


# HARPA

## A Versatile Three-Dimensional Hamiltonian Ray-Tracing Program for Acoustic Waves in the Atmosphere Above Irregular Terrain

R. Michael Jones  
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U.S. DEPARTMENT OF COMMERCE  
National Oceanic and Atmospheric Administration  
Environmental Research Laboratories

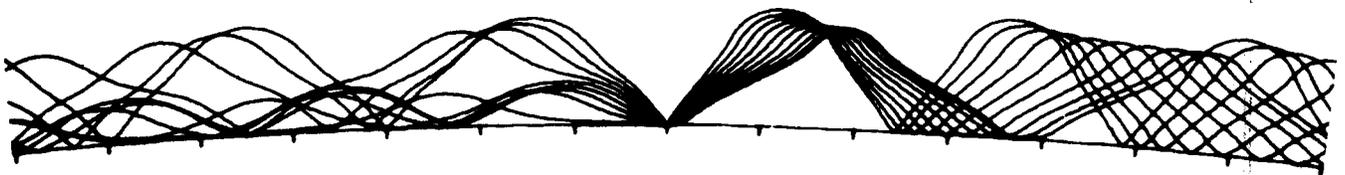


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R. Michael Jones  
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Wave Propagation Laboratory  
Boulder, Colorado  
August 1986



U.S. DEPARTMENT OF COMMERCE  
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## APPENDIX E. ERRATA FOR HARPA REPORT

HARPA: A versatile Three-Dimensional Hamiltonian Ray-Tracing Program for Acoustic Waves in the Atmosphere Above Irregular Terrain" by R. Michael Jones, J. P. Riley, and T. M. Georges

2 February 1987

- Page xi: change line 12 to:  
Table 7.23 Definitions of the parameters in common block /HDRC/....157
- Page 21: Following "The profile:" circle the units "km" in the columns labeled  $z_i$  and  $\delta_i$ .
- Page 31 and 199: At mid-page, change "stop frequency stepping" to "stop elevation-angle stepping," and change W30, W31, and W32 to W278, W279, and W280, respectively.
- Page 33 and 221: Change the Model Check Number from 3.0 to 2.0.
- Page 50: Change "Phase path, km" to Phase time, sec" and "Group path, km" to "Pulse travel time, sec."
- Page 59: In Table 4.1, change "NPABS" to "NPABSR".
- Page 69: Change the last two lines to read:  
\*\*\* Format type 1 implies format number A (see Table 5.3).  
\*\*\* Format type 2 implies format number 1, 2, or 3 (see Table 5.3).
- Page 79: Change description following W(21) to read "Set = 1 to stop elevation-angle increment when the ray goes out of bounds."
- Page 94-98: Add the following to the captions for Figures 6.1 through 6.5:  
"Circled block numbers correspond to program statement numbers."
- Page 98: Change the comment near the lower branch of the "Test Mode" block to read: "MODE = 4 and  $Y_{i,1} \neq 0$ ".
- Page 101: In the last sentence of Section 6.4 change the table mentioned from Table 7.9 to Table 7.17.
- Page 102: In the second line of the first full paragraph change the equation mentioned from Eq. (4.1) to Eq. (6.30).
- Page 126 and 128: Change the captions so that the parenthetical expressions following ANWNL and AWWNL begin "(Acoustic, No Winds..." and "(Acoustic, With Winds...").
- Page 127: Change the name of PROGRAM NITIAL to PROGRAM RAYTRC in the second block down.

Page 136: Change the first note in the caption of Figure 7.10 to read: "\*  
See Equation (6.83) to estimate the time of nearest closest approach to  
the specified surface."

Page 155: Add the variable names NDEVGRP and NDEVBIN to Table 7.19.

Page 158: Replace Table 7.23 by:

Table 7.23--Definitions of the parameters in common block /HDRC/

Position in common	Variable name	Definition
1	INITID	Character string for user name and phone number identifier for graphics output
2	DAT	Character string for the date of the computer run
3	TOD	Character string for the time of day of the computer run

Page 168: In line 9, replace PGRKPH with PGRPH.  
In line 11, replace  $\partial g/\partial \theta$  by  $\partial g/\partial \phi$ .

Page 222: Change the Model Check Number from 2.0 to 3.0.

Make the following changes in both the source-code listing (Appendix D) and  
in the program itself:

Page 251: Following the line "UCON 30" in LOGICAL FUNCTION UCON, insert the  
line: IF(CONV.EQ.-1.0) CONV = 1.0/EARTHUR UCON305

Page 251: Replace line "UCON 38" in LOGICAL FUNCTION UCON by:  
CNVV(1,3) = -1.0 UCON380

Page 361: Replace line "TTANH554" in SUBROUTINE TTANH5 by:  
ZIM1 = Z0 TTANH554

Page 395: Replace line "RVERT 21" in SUBROUTINE RVERT by:  
DATA RECORR/3.0/ RVERT21

Add the following routine:

	FUNCTION ITOC(N)	ITOC0020
C	RETURN 7 CHARACTER STRING REPRESENTATION OF INTEGER N	ITOC0030
C	IF NUMBER IS TOO LARGE OR SMALL USE FLOATING POINT FORMAT	ITOC0040
	CHARACTER ITOC*7	ITOC0050
	IF(N.LT.-9999.OR.N.GT.99999) GO TO 100	ITOC0060
	ITOC=' '	ITOC0070
	WRITE(ITOC, '(I7)', ERR=100) N	ITOC0080
	RETURN	ITOC0090
100	WRITE(ITOC, '(2PG7.0)') FLOAT(N)	ITOC0100
	END	ITOC0110

Appendix E. Errata (17 Sep 1986) for HARPA report

3 June 2004: See the six additional errata at the end.

"HARPA: A versatile three-dimensional Hamiltonian ray-tracing program for acoustic waves in the atmosphere above irregular terrain", by R. Michael Jones, J. P. Riley, and T. M. Georges, NOAA special report, August 1986

Documentation errata

On the "form to specify input data" on pages 31 and 199, "stop frequency stepping" should be changed to "stop elevation angle stepping," and W30, W31, and W32 should be changed to W278, W279, and W280, respectively.

The model check number in the "Form to specify input data for receiver-surface model RTERR on pages 33 and 221 should be 2.0 instead of 3.0

The last two lines on page 69 should read:

\*\*\* Format type 1 implies format number A (see Table 5.3).  
\*\*\* Format type 2 implies format number 1, 2, or 3 (see Table 5.3).

The figure captions for Figures 6.1 through 6.5 on pages 94 through 98 should have the following added:

Circled block numbers correspond to program statement numbers.

In Figure 6.5 on page 98, the lower branch on "Test mode." should read:

```
MODE = 4  
and y    is not = 0  
    i,1
```

The last sentence in Section 6.4 on page 101 should refer to Table 7.17 instead of 7.9.

The second line of the first full paragraph on page 102 should refer to equation (6.30) rather than (4.1).

The first note in the caption to Figure 7.10 on page 136 should read:

\* See Equation (6.83) to estimate the time of the nearest closest approach to the specified surface.

The model check number in the "Form to specify input data for receiver-surface model RVERT on page 222 should be 3.0 instead of 2.0

(plus at least 3 more errata that Tom Georges knows about)

Program errata (17 September 1986)

Following line "UCON 30" in LOGICAL FUNCTION UCON on page 251, insert the line:

```
IF(CONV.EQ.-1.0) CONV = 1.0/EARTHTR                                UCON305
```

Line "UCON 38" in LOGICAL FUNCTION UCON on page 251 should be replaced by:  
CNVV(1,3) = -1.0 UCON380

Line "RVERT 21" in SUBROUTINE RVERT on page 395 should be replaced by:  
DATA RECORR/3.0/ RVERT21

NOTICE: The HARPO report (Appendix E, pp 449-450) has a later (2 February 1987) and more complete errata for the HARPA report.

Except for the following errata:

Documentation errata

3 June 2004:

The calculation of absorption in the sample printout and sample raysets on pages 177 through 196 is incorrect. The correct values are in the files dinp.sam and punch.sam

29 October 2003:

page 200: The sentence "Superimpose these raypath plots on the graph of the previous sunset:" should read "Superimpose these raypath plots on the graph of the next sunset:"

3 June 2004:

The model check number in the "Form to specify input data for receiver-surface model RTERR on page 221 should be 2.0 instead of 3.0

Program errata

17 December 2002:

page 329: The variable OWI in line ANWWL 70 in SUBROUTINE ANWWL should be OW.

6 May 2003:

page 332: The variable OW in line AWWWL 76 in SUBROUTINE AWWWL should be OWI.

17 October 2003:

page 344: Line WGAUSS18 in SUBROUTINE WGAUSS2 should be

DATA RECOGU/8.0/

WGAUSS18

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## ACKNOWLEDGMENTS

Part of the organization of this program into subroutines follows that of the program of Dudziak (1961). Also, the coordinate transformation in subroutine PRINTR and the method for data input via the W array are taken from the program of Dudziak (1961). The term "rayset," the idea of outputting computer-readable results of each hop for each ray trace, and the idea of automatically plotting raypaths come from the program of Croft and Gregory (1963). Subroutine RKAM1 is a modification of subroutine RKAMSUB, written by G. J. Lastman, and is available through the CDC CO-OP library (the CO-OP identification is D2 UTEX RKAMSUB). Subroutine GAUSEL was written by L. David Lewis, NOAA Space Environment Laboratory. Judith Stephenson wrote much of the code for the original ionospheric ray-tracing program, upon which HARPA is based. Richard Lindzen devised the method upon which models TTANH5, CSTANH, and GTANH are based. We also thank the many users of earlier versions of the program who provided helpful feedback. Special thanks go to the Editorial Staff of Publication Services for extensive help in clarifying the expression of our ideas, and to Ms. Mildred Birchfield for her excellent typing and layout of the manuscript.



# HARPA -- A VERSATILE THREE-DIMENSIONAL HAMILTONIAN RAY-TRACING PROGRAM FOR ACOUSTIC WAVES IN THE ATMOSPHERE ABOVE IRREGULAR TERRAIN

R. Michael Jones, J. P. Riley, and T. M. Georges

## ABSTRACT

HARPA stands for Hamiltonian Acoustic Ray-tracing Program for the Atmosphere. This FORTRAN computer program traces the three-dimensional paths of acoustic rays through model atmospheres by numerically integrating Hamilton's equations, which are a differential expression of Fermat's principle. The user specifies an atmospheric model by writing closed-form formulas for its three-dimensional wind and temperature (or sound-speed) distribution, and by defining the height of the reflecting terrain as a function of geographic latitude and longitude. Some general-purpose models are provided, or users can easily design their own.

Because it uses continuous models, the Hamiltonian method avoids the false caustics and discontinuous raypath properties encountered in conventional ray-tracing methods, which use layers or cells where each acoustic-raypath segment can be computed in closed form. Furthermore, computational speed can be traded for accuracy, without changing the model of the medium, by specifying the maximum allowable integration error per step.

In addition to computing the geometry of each raypath, the program can calculate pulse travel time, phase time, Doppler shift (if the medium varies in time), absorption, and geometrical path length. Amplitude is not explicitly computed, but the contributions by absorption, reflection losses, and focusing are separately available for each ray. Only geometrical effects are accounted for; that is, no diffraction or partial-reflection corrections are applied. The program prints out a step-by-step account of each ray's progress, and it can plot the

projection of a set of rays on any vertical plane or on the ground. Furthermore, it can output each ray's properties in machine-readable form for further processing (amplitude calculations, for example).

This report describes the ray-tracing equations and the structure of the program and provides complete instructions for using it, illustrated by a sample case. The program is modular and can be adapted to model propagation through other media by changing the routine that defines the medium's dispersion relation.

# PART I: WHAT THIS RAY-TRACING PROGRAM CAN DO

## 1. Introduction to Hamiltonian Ray Tracing

### 1.1 Rationale

Many practical problems in atmospheric acoustics submit to a straightforward application of geometrical acoustics, or ray theory. No other propagation-modeling tool provides such an intuitive and graphic portrayal of the paths that acoustic energy follows through inhomogeneous media. Even in situations where ray theory does not strictly apply, a picture of the acoustic raypaths often provides a useful first look at the way the waves and the medium interact, and it gives insight into where higher order computations are required. Some calculations cannot be easily made in any other way, for example, computing multipath pulse travel time or showing which parts of the medium affect each pulse arrival.

Yet most of the ray-tracing computer programs in common use fail to take full advantage of the power of geometrical acoustics. Many are essentially automated versions of graphical techniques that patch together closed-form raypath solutions for layers or cells with simple refractive-index gradients (Roberts, 1974; Cornyn, 1973). In such models, gradient discontinuities at cell boundaries can introduce false caustics and cause discontinuous behavior of ray properties as launch angle varies (Pederson, 1961). Furthermore, it is difficult to extend such models to three-dimensional media, to account for winds, and to compute reflections from complicated terrain models.

This report describes a general-purpose atmospheric acoustic ray-tracing program called HARPA -- for Hamiltonian Acoustic Ray-tracing Program for the Atmosphere -- that we have designed to overcome these limitations. It computes acoustic raypaths by numerically integrating Hamilton's equations, which are a differential expression of Fermat's principle. The user defines an atmospheric model by writing closed-form expressions for its temperature (or sound-speed) and wind distribution in three dimensions, and by defining the terrain height as a function of latitude and longitude. Several simple but generally useful models with user-definable parameters are described in this report; users can pattern their own models after them.

HARPA is the companion to a similar program we have developed for the ocean, known as HARPO. The main differences between the two programs are in the models available for the two media, in provisions for reflections from an upper boundary (in the ocean case), and in the program module that describes the media dispersion relations. HARPO is documented in a separate report (Jones et al., 1986).

## 1.2 What Is Ray Tracing?

Although ray tracing has a long history, many people outside the field do not know what ray tracing is or what it can do. In ray theory, waves are treated like particles (photons of light, phonons of sound) that travel along geometric trajectories called rays. In material media, the particles travel at a speed determined by the medium's "refractive index." Gradients in refractive index bend rays, giving rise to the problem of computing ray trajectories through a known spatial distribution of refractive index. Ray tracing is any method, graphical or numerical, for solving that problem.

Originally, lensmakers used ray tracing to find out how light rays travel through optical systems. They used graphical techniques based on Snell's law to compute the bending that light rays suffer when they encounter abrupt changes in refractive index, as at the surface of a lens. By constructing bundles of such rays, lensmakers could simulate the magnification, reduction, and focusing of their lens designs without actually building them.

Modern ray-tracing applications, whether acoustic or electromagnetic, serve basically the same function: they allow one to simulate the propagation of waves through media whose refractive-index structure varies in a complicated way, without actually performing the physical measurement. Modern ray-tracing computations are usually performed by programs written for digital computers that can graphically display the results of their computations in various informative ways.

Today's ray-tracing programs do much more than compute the bending of rays as they cross interfaces; they can model media whose refractive index varies continuously in space and even with time. In dissipative media, they integrate absorption along the raypath. They can also integrate phase and

pulse travel time, as well as wave amplitude. In time-varying media, they can integrate the rate of change of phase, or Doppler shift. Some programs (including HARPA) produce machine-readable output so that the results of many raypath computations can be processed by other programs to display field observables, such as amplitude.

The most advanced applications of ray-tracing computer programs have been to the fields of ionospheric radio propagation, seismic wave propagation, and the propagation of acoustic or sound waves in the ocean and the atmosphere. In the Hamiltonian formalism, the ray-tracing equations for acoustic, seismic, and electromagnetic waves are identical. General-purpose programs can thus be constructed in which only the modules that describe the wave dispersion relation and how the medium varies in space need be changed to go from one kind of ray-tracing program to another.

### 1.3 What Approximations Are Involved in Ray Tracing?

Solving a wave equation with arbitrary boundary conditions is still an impractical task, even for the most modern computers. Therefore, practical problems in wave propagation are often solved by making simplifying approximations to the wave equation. Examples of such approximations are the parabolic-equation (P.E.) method (Tappert, 1977), normal-mode theory (Tolstoy and Clay, 1966; Pierce, 1965), fast-field methods for numerical integration of the wave equation in range-independent environments (Raspet et al., 1985), and ray theory.

Ray theory, sometimes called the WKB or eikonal method, results from making a high-frequency approximation in the solution of arbitrary elliptic or hyperbolic partial differential equations (Budden, 1961). Ray tracing is related to the "method of characteristics" for solving such equations because the raypaths are the bi-characteristic rays of the differential equations in the infinite frequency, infinite wave-number limits. In some fields, ray tracing is called the "shooting method" because (as with shooting a gun) the location of the end point is found by trial and error while the initial conditions of a ray are varied.

In the case of the wave equation, the approximation gives rise to the fields of geometrical acoustics or geometrical optics, which are concerned

with the trajectories of bundles of acoustic or electromagnetic energy radiated in infinitesimal angular beams. Such rays experience no diffraction but produce sharp shadow boundaries when they encounter solid objects. Ray theory can be extended to include the effects of diffraction, for example, by using the Geometrical Theory of Diffraction (GTD) (Keller, 1962).

In ray theory, one assumes conservation of energy within a bundle of rays called a flux tube so that wave intensity is inversely proportional to the cross-sectional area of the flux tube. When that cross-sectional area becomes zero, ray theory predicts infinite energy density. At such "caustics," higher order corrections to ray theory can give more accurate field estimates when needed. For example, the field near a surface caustic can be calculated in terms of Airy functions (Ludwig, 1966; White and Pedersen, 1981).

Without such corrections, ray tracing accounts only for refraction by large-scale gradients in the medium and not for diffraction and scattering by changes in the medium over scales that are small compared to a Fresnel zone. Even so, ray theory provides a useful first look at many complicated propagation problems and gives a kind of graphical insight lacking in other propagation models.

#### 1.4 When Should You Use Ray Tracing?

Ray tracing is best suited to modeling acoustic propagation in environments where the medium's refractive index can be described deterministically in one, two, or three dimensions, and where changes in refractive index are small in the WKB sense (roughly speaking, within an acoustic Fresnel zone). (This means that ray models are most accurate at high frequencies.) In such environments, ray tracing gives accurate information about the geometrical paths followed by acoustic rays (energy), about shadow boundaries and reflections from surfaces, and about phase, intensity, pulse travel time, absorption and Doppler shift (for time-varying media) integrated along those paths.

In environments where multiple rays reach a receiver location of interest, additional computations, external to the ray tracing, may be required to combine field information from multiple rays. When the number of multipath rays becomes large, alternative formulations of the problem (P.E. or normal-mode

theory, for example) are more appropriate for continuous-wave amplitude calculations. For pulse transmissions, ray theory is useful for describing the distinct geometric paths corresponding to each pulse arrival and for computing multipath travel times.

In situations where the applicability of ray theory is doubtful, a raypath picture can tell which regions must be treated with higher order methods, such as GTD or the Airy-function approximation to the field near a caustic. Furthermore, there are standard formulas to estimate how close to a caustic amplitude calculations are accurate (Budden, 1961; 1972).

Even when ray calculations of one wave quantity become inaccurate, they can give useful estimates of others. For example, when amplitude estimates break down (as at surface caustics), other information, such as travel time or phase, may still be reliable and can be tracked through caustics. Furthermore, Budden (1961, pp. 325-326) shows that the ray-computed phase must be advanced by  $90^\circ$  every time a ray passes through a line caustic.

### 1.5 What Is Hamiltonian Ray Tracing?

An alternative to cellular methods requires the medium to be modeled as a continuous three-dimensional function with continuous gradients and computes each raypath by numerically integrating Hamilton's equations with a different set of initial conditions. This method has been called Hamiltonian ray tracing. Hamilton's equations are the same for all kinds of wave propagation; only the definition of the Hamiltonian varies when going from one wave type to another.

Although Hamilton's equations are more familiar in mechanics, they have a long history of application to more general problems, including wave propagation. There, the point of view is that in a high-frequency limit, waves behave like particles and travel along rays, according to equations that exactly parallel those governing changes of position and momentum in mechanical systems (Lighthill, 1978, Sec. 4.5). Two steps show that integrating Hamilton's equations can lead to approximate solutions of a wave equation:

(1) The first step is to show that solutions to the wave equation are related to paths that satisfy a particular stationary principle, usually called

Fermat's principle. There are at least two standard methods for demonstrating that relation.

(a) First is the method of characteristics (see, for example, Courant and Hilbert, 1962; Garabedian, 1964), in which the solution is related to initial-value data chosen on some appropriate surface. Specifying a surface and constructing a solution requires first constructing the characteristic surfaces that are wave fronts of the wave. These characteristic surfaces can be constructed by first constructing bi-characteristic rays that satisfy a stationary principle. The bi-characteristic rays are the same as the geometrical raypaths whenever all terms in the wave equation are proportional to a derivative of the wave function, or in the limit of infinite frequency and wave number.

(b) Second is the path-integral method (see, for example, Feynman and Hibbs, 1965), in which a solution to the wave equation is constructed as an integral over all possible paths (not just raypaths) that connect the source and observer. Making a saddlepoint (or stationary phase) approximation to the path integral finds the paths that contribute most to the path integral. Such paths are those for which the action (phase) is stationary for variations of the path; that is, they satisfy Fermat's principle.

(2) The second step is to show that Hamilton's equations can be integrated to construct paths that satisfy a variational principle, such as Fermat's principle. This is done in standard texts (for example, Lighthill, 1978). First, the variational principle is expressed as an integral of a Lagrangian along the path (specified in terms of generalized coordinates,  $q_i$ ). This determines the form of the Lagrangian for the problem, which for the wave equation is usually some simple function of the phase refractive index. Then the generalized momenta  $p_i$  are defined, which for the wave equation correspond to components  $k_i$  of the wave number vector. Then a Hamiltonian  $H(q_i, p_i)$  is constructed from the Lagrangian. For the wave equation, the Hamiltonian is usually a function that gives the dispersion relation for the wave in question when it is set to zero. Integrating Hamilton's equations then gives a path that satisfies the variational (Fermat's) principle.

In Cartesian coordinates, Hamilton's equations take the particularly simple form (Lighthill, 1978)

$$\frac{dx_i}{d\tau} = \frac{\partial H}{\partial k_i} \quad ; \quad \frac{dk_i}{d\tau} = - \frac{\partial H}{\partial x_i} \quad , \quad i = 1 \text{ to } 3 \quad , \quad (1.1)$$

where  $\tau$  is a parameter (sometimes proportional to time) whose physical meaning depends on the how the Hamiltonian,  $H$ , is defined,  $k_i$  are the wave-number components, and  $x_i$  are the coordinates of a point on the raypath. Transforming to spherical polar coordinates complicates the equations considerably. The full set of equations for spherical coordinates can be found in Chapter 6.

To solve (1.1) for the raypath, one chooses initial values for the six quantities  $x_i$  and  $k_i$  and performs a numerical integration of the system (1.1) of six total differential equations. For acoustic waves in the atmosphere, the Hamiltonian (which is constant along a raypath) is defined as

$$H(x_i, k_j) = [\omega - \vec{k} \cdot \vec{V}(x_i)]^2 - C^2(x_i) k^2 = 0 \quad , \quad (1.2)$$

where  $\vec{V}(x_i)$  is the wind field,  $C(x_i)$  is the sound-speed field, and  $\omega$  is the angular wave frequency ( $\vec{V}$  and  $C$  may also depend on time). Thus, the effects of a three-dimensional vector-wind field are automatically included in the definition of the Hamiltonian.

There is an alternative to Hamilton's equations for a differential form of the ray equation, namely the eikonal equation (see, for example, Garabedian, 1964, p. 166; Felsen and Marcuvitz, 1973, p. 126). The eikonal equation is derived by first assuming an approximate solution to the wave equation in terms of an asymptotic series. Substituting the asymptotic series into the wave equation leads to the eikonal equation, which determines the raypaths, and a transport equation, which determines an approximate solution to the wave equation. The eikonal equation is equivalent to Hamilton's equations for determining the raypath. The transport equation is equivalent to methods mentioned above for determining an approximate solution to the wave equation.

In addition to allowing continuous three-dimensional models of the refractive-index field and two-dimensional models of reflecting surfaces, Hamiltonian ray tracing by numerical integration permits the user to trade computing speed for accuracy by specifying the maximum allowed integration error per step. In other words, you can have a fast but crude ray trace or a

slower and more accurate one. The program automatically adjusts the integration step length along the raypath to keep the error within specified bounds. In regions where the refractive index varies quickly, small steps are required, but in regions where it varies slowly, large steps save computation. If the quantity being integrated varies monotonically along the raypath, the specified relative accuracy will be preserved in integrated quantities, such as travel time.

## 1.6 What This Program Does

HARPA computes the paths of acoustic rays, one at a time, through a user-defined model of the atmosphere, given initial conditions that include the source location (latitude, longitude, and height above the ground), wave frequency, direction of transmission (elevation and azimuth), the receiver-surface model, and the maximum number of hops (intersections with the receiver surface). The input data specification forms in Chapter 2 illustrate the generality of acceptable input.

The mechanics of the raypath calculation have been completely separated from the modeling of the medium (sound-speed, wind velocity, and terrain models). This allows the user to select models from those we have developed or to develop new models simply by writing new (or altering existing) subroutines to define those models.

The modular structure of the program allows the user to extend the program easily to other types of geophysical ray tracing (underwater acoustics, for example) simply by substituting new subroutines for defining the Hamiltonian and the model of the medium.

The method for inputting data into the program is easy to learn. The user simply specifies the magnitude and units of the elements of an Input Data File which correspond to physical or mathematical quantities that tell the program what models to use, what rays to trace, and in what form to present its results. We provide input parameter forms for making sure that all the required quantities are specified.

At the user's option, HARPA produces three kinds of output: (1) The printout reproduces the input data set and gives detailed information about

each raypath computed, in columnar form, with each line corresponding to a "snapshot" of the ray's progress after a specified number of integration steps. (2) Computer-readable output permits further processing of raypath data by supplementary programs, without recomputing the raypaths. (3) The raypath plots show projections of any part of the raypaths on any vertical plane or on any part of the ground, with any desired magnification. These plots give the user a quick view of the raypath geometries.

Chapter 2 illustrates more fully what the program does by going through the setup and execution of a representative application.

### 1.7 What This Program Does Not Do

HARPA's computations lie entirely within the scope of geometrical acoustics (ray theory). It applies no corrections for diffraction or partial reflections. The atmospheric model must be deterministic, not stochastic.

There are no provisions built into HARPA for explicit computations of acoustic amplitude. This would normally be done with a supplementary program that processes HARPA's machine-readable output. Total amplitude at a receiver would be computed by combining flux-tube focusing, reflection losses, and absorption, and the user would normally decide whether to add coherently or incoherently the contributions of multipath rays. Because there are so many ways to compute amplitude, we think it is best to keep the various factors separate and let the users combine them however they wish.

Because the numerical integration of Hamilton's equations requires media models with continuous gradients, HARPA cannot presently handle refraction at discontinuities of refractive index or its gradients. If such discontinuities are included in a model, the integration routine will attempt to handle them by taking extremely small steps when a ray encounters a discontinuity, and the results may not be reliable. In general, one can approximate discontinuous functions with continuous functions to any desired accuracy, and HARPA will adjust its step length to accommodate them. Our algorithms for reflecting rays from arbitrary terrain surfaces could be generalized to compute refraction at discontinuities in refractive index.

HARPA is not currently equipped to model penetration of rays into the ground or to account for partial reflections from subsurface layers. However, the user can specify a complex (to account for phase and amplitude) ground-reflection coefficient that is a function of frequency and angle of incidence. Since reflection coefficients do not affect the raypaths, their effects can be added after raypath calculations.

HARPA cannot directly compute the raypaths that connect a specified source and receiver. To find such "eigenrays," one usually launches a fan of rays at small increments in elevation and/or azimuth angle and linearly interpolates for the rays that reach the desired receiver location (range, azimuth and height). We have developed an eigenray program that processes the "rayset" output of HARPA, interpolating in elevation angle only, and that will be documented elsewhere. Some shortcuts for finding three-dimensional eigenrays when azimuthal deflections are small are described by Georges et al. (1986).

HARPA makes no checks to see if atmospheric models satisfy physical conservation laws and boundary conditions, or that wind and temperature models are geostrophically consistent. (Accurate raypaths can be computed through physically impossible models.) Therefore, users should make their models as physically realistic as their application demands.

## 1.8 History of the Program

HARPA has a long history of development. We started by learning from the programs of Dudziak (1961) and Croft and Gregory (1963). Jones (1966) documented our first version of a three-dimensional ray-tracing program for radio waves in the ionosphere, which included anisotropy caused by the earth's magnetic field. Jones (1968) documented improvements in the original program. Georges (1971) converted the ionospheric radio program to trace raypaths for acoustic-gravity waves in an atmosphere with winds and changed the ray-tracing equations into Hamiltonian form. Jones and Stephenson (1975) documented further significant improvements in the ionospheric program. Jones et al. (1982) documented a Hamiltonian acoustic ray-tracing program for an atmosphere over a spherical earth.

Through its history, HARPA and its predecessors have found application in the propagation of radio waves through the ionosphere (Georges, 1967; 1970;

Georges and Stephenson, 1968; Stephenson and Georges, 1969), acoustic propagation through the atmosphere (Georges, 1972; Georges and Beasley, 1977) and acoustic propagation in the ocean (Georges et al., 1986; Jones et al., 1984). In extending the utility of ray theory, Jones (1970) has treated ray propagation in lossy media (ray tracing in complex space), bending of rays in random, inhomogeneous media (Jones, 1981a), and the frequency shift suffered by pulses propagating in dispersive media (Jones, 1981b). Jones (1983) has also surveyed existing techniques for underwater acoustic ray tracing.

HARPA combines the improvements made by Jones and Stephenson with the acoustic-wave capability and atmospheric models developed by Georges. Although it does not include the capability for tracing acoustic-gravity-wave raypaths, it includes modularity features that make it easier to convert the program to trace rays in other media. It also includes algorithms developed by Jones (1982) for reflecting rays from arbitrary terrain surfaces. In addition, we have developed real-time graphics routines and facilitated operation from time-share graphics terminals as that technology has advanced.

### 1.9 Scope of This Report

This report documents only the ray-tracing program HARPA, its supporting subroutines, and its various forms of input and output. The main intent of this report is to show what HARPA can do and to explain how to use it. We illustrate its capabilities with a comprehensive sample case. We also show how to extend and modify the program to the user's specific needs.

Not documented here are supplementary programs that we have designed to plot properties of the atmospheric models and to process the computer-readable output of HARPA. Examples of such programs are packages to plot range vs. elevation angle of transmission, range vs. travel time, and amplitude calculations (Jones et al., 1984). We have not documented here our programs for editing input to HARPA or our procedure files for running it on our computer. Nevertheless, the package documented here is self-contained and has everything needed to compute and display raypaths through arbitrary three-dimensional model atmospheres.

Figure 1.1 shows an organization chart of HARPA in relation to its supporting modules. The dotted line encloses the portion documented in this

report. Separate reports will document the remaining modules, which are the same for both HARPA and HARPO.

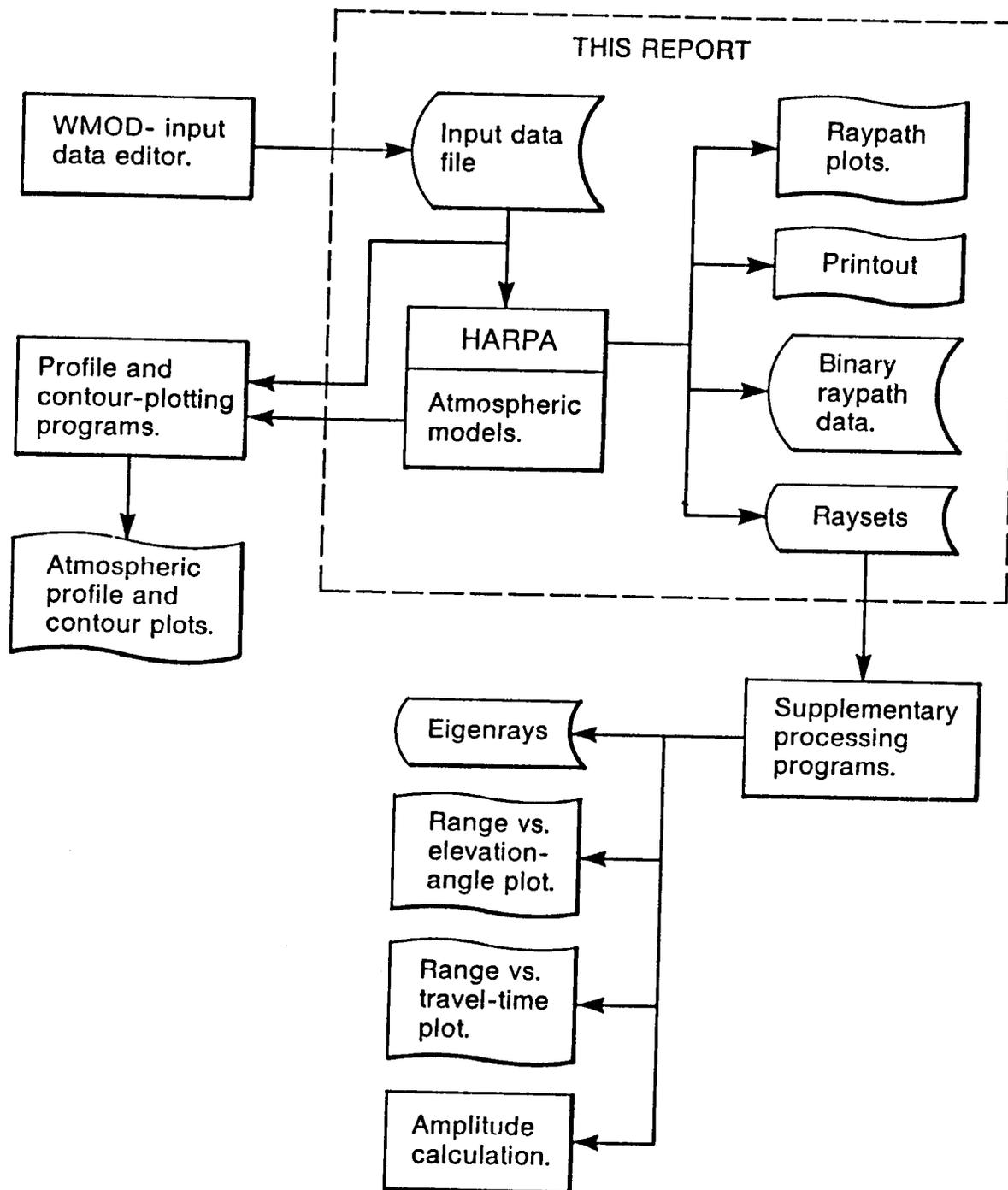


Figure 1.1. Relation of HARPA to its inputs and outputs, as well as its supporting and supplementary programs. The dashed line shows the scope of this report.

## 2. A Sample Run Illustrating an Application of HARPA

A sample case serves several purposes: it introduces new users to the capabilities of the program in terms of physical models they can understand; it shows new users how to set up and run the program and what output to expect; and it provides a comprehensive test case to exercise the program and make sure everything works on a new machine. New users should run the sample case (provided with the program) first and make sure that the program's output is identical to that shown in this report. Varying the input parameters, one by one, from the sample case is an instructive way to explore the program's capabilities.

The usual procedure for defining models is to fill out "order forms" corresponding to the wind, sound speed, temperature, molecular weight, viscosity/conductivity and terrain models you want to use, then create an "Input Data File" from the information on the order forms. Models can be selected from the general-purpose ones we have created, or you can design your own. The following pages show filled-out forms for the models used by the sample case; blank order forms for all our models are supplied in Appendix B. Using these forms is recommended, even for advanced users, because they make sure that you specify all the required model parameters. They also help you keep track of the models you create.

### 2.1 The Atmospheric Model for the Sample Case

The atmospheric model described here is designed more to exercise features of the program than to represent any physically realistic situation. It combines a three-dimensional wind and temperature field with a terrain model containing a Lorentzian-shaped ridge. The sample case also includes a simple absorption model based on models of atmospheric viscosity and thermal conductivity.

Refer now to the FORM TO SPECIFY AN ATMOSPHERIC MODEL (Figure 2.1). This form is filled in with the names of all the subroutines required to specify the atmospheric model, for the sample case, including the terrain model,

viscosity/ conductivity model and receiver-surface model. Data-set ID numbers uniquely identify the particular set of parameter values used by each subroutine for the sample case. The entire set of models and parameters that constitute the atmospheric model for the sample case is also given a unique ID number, which is S03. The references to W followed by numbers in these forms correspond to specific input data parameters, as described in Section 5.3.

The first subroutine name on this form specifies the acoustic-wave dispersion relation to be used. In the sample case, we specify AWWWL, which means "Acoustic, With Winds, With Losses." This means that we will use a model atmosphere with winds and will calculate acoustic absorption. More efficient versions of the dispersion relation should be selected when wind or absorption models are not used. The remaining subroutine names filled in on this form refer to the atmospheric model subroutines, to be discussed next.

Refer next to the FORM TO SPECIFY INPUT DATA FOR WIND VELOCITY MODEL ULOGZ2 (Figure 2.2). This wind-field model represents a wind profile for the atmospheric boundary layer, neglecting Coriolis forces. The wind has only an eastward component whose magnitude depends only on height above the terrain surface, according to the formula given on the ULOGZ2 order form.

ULOGZ2 requires the user to specify three parameters,  $z_0$ ,  $u_*$ , and  $k$ . For the sample case, we choose  $k=0.35$ ,  $z_0=1.0$  km, and  $u_*=5.0$  m/s. The resulting profile of wind speed is shown in Figure 2.1a. (The program that provided this plot is part of a set of peripheral programs that will be documented in another report.) Because we use no wind-perturbation model, we select the do-nothing wind-perturbation NPWIND.

Refer next to the FORM TO SPECIFY SOUND-SPEED MODEL GAMRTDM (Figure 2.3). We use this sound-speed model because we want to specify a background temperature distribution instead of a sound-speed model directly. GAMRTDM requires no input parameters, but it requires a molecular weight model, discussed next.

Refer next to the FORM TO SPECIFY INPUT DATA FOR ATMOSPHERIC MOLECULAR WEIGHT MODEL MCONST (Figure 2.4). For the sample case, we select the simplest possible model, namely a constant value of 29. Molecular weight is required to convert temperature to sound speed when temperature models are specified.

FORM TO SPECIFY AN ATMOSPHERIC MODEL  
(including terrain model)

Name GEORGES RB3 X6437

Date 2-10-86

Atmospheric ID (3 characters) 503

Coordinates of the north pole of the computational coordinate system:

North geographic latitude: 90 rad, km, deg (W24)

East geographic longitude: 0 rad, km, deg (W25)

Models:

	Subroutine Name	Data set ID
Dispersion relation	<u>AWWWL</u>	
Wind velocity	<u>ULOGZ2</u>	<u>3.0</u> (W102)
Wind-velocity perturbation	<u>NPWIND</u>	<u>0.0</u> (W127)
Sound speed	<u>GAMRTDM</u>	<u>0.0</u> (W152)
Sound-speed perturbation	<u>CBLOB2</u>	<u>2.0</u> (W177)
Temperature	<u>TTANH5</u>	<u>1.0</u> (W202)
Temperature perturbation	<u>TBLOB2</u>	<u>2.0</u> (W227)
Molecular weight	<u>MCONST</u>	<u>29.0</u> (W252)
Terrain	<u>GLORENZ</u>	<u>2.0</u> (W302)
Terrain perturbation	<u>NPTERR</u>	<u>0.0</u> (W327)
Viscosity/conductivity	<u>MUARDC</u>	<u>1.0</u> (W502)
Viscosity/conductivity perturbation	<u>NPABSR</u>	<u>0.0</u> (W527)
Pressure	<u>PEXP</u>	<u>1.0</u> (W552)
Pressure perturbation	<u>NPPRES</u>	<u>0.0</u> (W557)
Receiver surface*	<u>RTERR</u>	
Plot-annotation model*	<u>FULANN</u>	

\*The receiver-surface model and plot-annotation model are not considered part of the atmospheric ID

Figure 2.1. Sample of completed form to specify an atmospheric model (including terrain model).

FORM TO SPECIFY INPUT DATA  
FOR WIND-VELOCITY MODEL ULOGZ2

A logarithmic wind profile of the atmospheric boundary layer neglecting Coriolis forces. The eastward wind is given by

$$u_{\phi} = \frac{u_*}{k} \ln \frac{z}{z_0} \quad \text{for} \quad z > z_0 e$$

$$u_{\phi} = \frac{u_*}{k} \frac{z}{z_0 e} \quad \text{for} \quad z \leq z_0 e$$

where  $z = G(r, \theta, \phi)$  is determined by the terrain model and is the height above or some kind of distance from the terrain, depending on the terrain model, and  $r$  is the radial coordinate of the ray point.

Specify--

the model check for ULOGZ2 = 6.0 (W100)

the input data-format code = \_\_\_\_\_ (W101)

an input data-set identification number = 3.0 (W102)

an 80-character description of the wind velocity profile:

LOGARITHMIC EASTWARD WIND PROFILE,  $U^* = .5$  M/S,  $Z_0 = 1$  KM

the reference wind speed,  $u_* =$  5 km/s, (m/s) (W103)

von Kármán's constant,  $k =$  .35 (W104) (.35 recommended)

the roughness height,  $z_0 =$  1 km (W105)

OTHER MODELS REQUIRED: Any wind-perturbation model. Use NPWIND if no perturbation is desired.

( $\overline{uw} = -u_*^2$  is the surface stress at the ground.)

Figure 2.2. Sample of completed form to specify input data for wind-velocity model ULOGZ2.

FORM TO SPECIFY  
SOUND-SPEED MODEL GAMRTDM

This model specifies sound speed in terms of a background temperature model using

$$c^2 = \frac{\gamma RT}{M} ,$$

where  $\gamma = 1.4$ , R is the universal gas constant, T is the absolute temperature in Kelvins, and  $M(r, \theta, \phi)$  is a model of the mean molecular weight of the atmosphere. See Sec. 6.3 for further description of this model.

Specify --

The model check for GAMRTDM = 1.0 (W150)

OTHER MODELS REQUIRED: Any background temperature model; any molecular weight model.

Figure 2.3. Sample of completed form to specify sound-speed model GAMRTDM.

FORM TO SPECIFY INPUT DATA FOR  
ATMOSPHERIC MOLECULAR-WEIGHT MODEL MCONST

A constant molecular weight (independent of height, longitude, latitude,  
and time)

Specify--

the model check for MCONST = 1.0 (W250)

the input data-format code = \_\_\_\_\_ (W251)

an input data-set identification number = 29 (W252)

an 80-character description of the molecular weight:

MOLECULAR WEIGHT = 29

the value of the constant molecular weight, M = 29 (W253)

OTHER MODELS REQUIRED: none.

Figure 2.4. Sample of completed form to specify input data for  
atmospheric molecular-weight model MCONST.

FORM TO SPECIFY INPUT DATA FOR  
TEMPERATURE MODEL TTANH5

This model represents the temperature profile by a sequence of linear segments that are smoothly joined by hyperbolic functions:

$$T = T_0 + \frac{c_1}{2} (z-z_0) + \sum_{i=1}^n \delta_i \left( \frac{c_{i+1} - c_i}{2} \right) \ln \left( \frac{\cosh \left( \frac{z-z_i}{\delta_i} \right)}{\cosh \left( \frac{z_i-z_0}{\delta_i} \right)} \right) + \frac{c_{n+1}}{2} (z-z_0)$$

$$\frac{dT}{dz} = c_1 + \sum_{i=1}^n \left( \frac{c_{i+1} - c_i}{2} \right) \left\{ \tanh \left( \frac{z-z_i}{\delta_i} \right) + 1 \right\}$$

$$c_i = (T_i - T_{i-1}) / (z_i - z_{i-1})$$

$z = r - r_e$ , where  $r_e$  is the Earth radius, and  $r$  is the radial coordinate of the ray point. Thus,  $\delta_i$  is the half-thickness of a region centered at approximately  $z_i$  km, in which  $dT/dz$  changes from  $c_i$  to  $c_{i+1}$ . Start by drawing a profile using linear segments and get  $T_i$  and  $z_i$  from the corners. Then select  $\delta_i$  to round the corners. The final profile will not go through  $(T_i, z_i)$ .

Specify--

the model check for TTANH5 = 7.0 (W200)

the input data-format code = \_\_\_\_\_ (W201)

an input data-set identification number = 1.0 (W202)

an 80-character description of the model with parameters:

U.S. STANDARD ATMOSPHERE 1962 TEMPERATURE PROFILE

and the profile values:

the number of points in the profile -2 = n = 4

the profile:	i	$z_i$ (km,m)	$T_i$ (°K)	$\delta_i$ (km,m)
	0	0	288	0
	1	15	190.5	10
	2	52	320	7.5
	3	95	191	10
	4	165	1451	50
	5	300	1586	0

OTHER MODELS REQUIRED: Any temperature-perturbation model. Use NPTEMP if no perturbations are desired. FUNCTION ALCOSH.

Figure 2.5. Sample of completed form to specify input data for temperature model TTANH5.

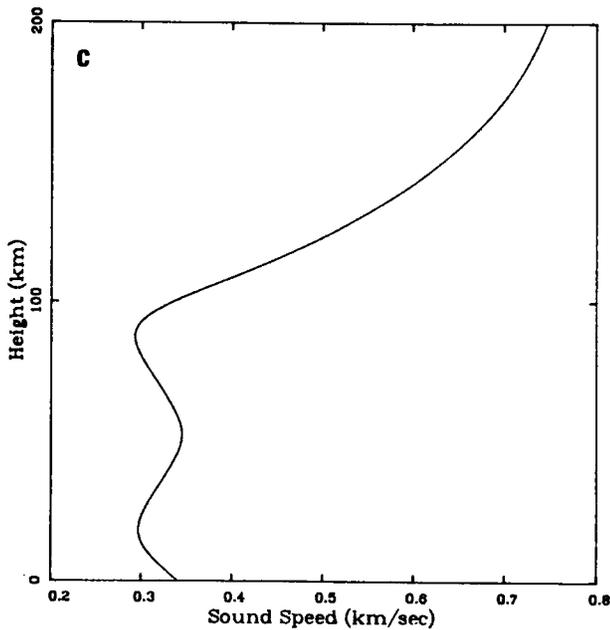
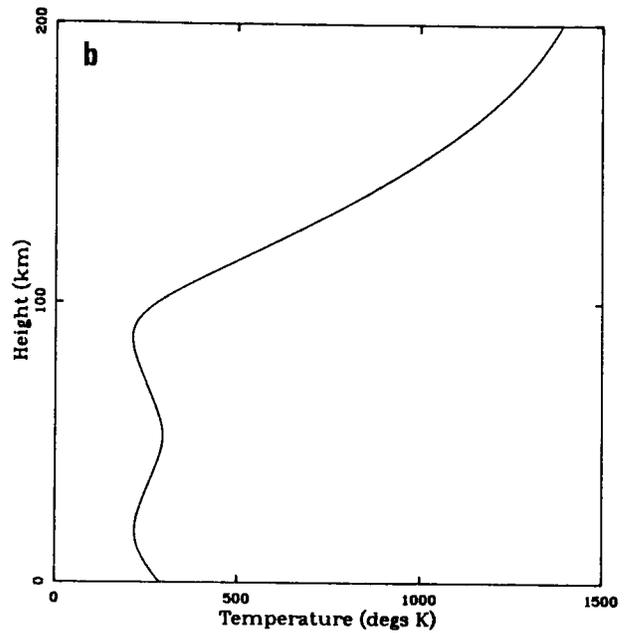
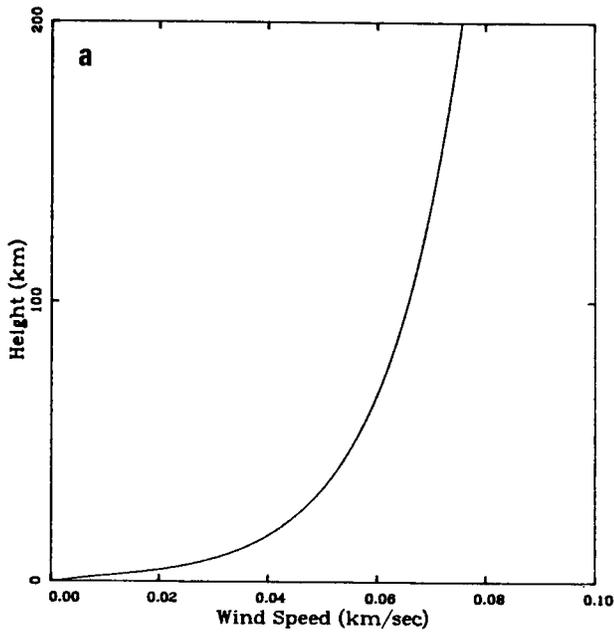


Figure 2.6. Profiles of background (a) eastward wind speed, (b) temperature, and (c) sound speed used in the sample case. The program for plotting these profiles is not supplied with HARPA but is part of a set of supplementary programs documented elsewhere.

Refer next to the FORM TO SPECIFY INPUT DATA FOR TEMPERATURE MODEL TTANH5 (Figure 2.5). This "background" temperature model is a continuous approximation to the 1962 U.S. Standard Atmosphere (USSA) temperature profile (Valley, 1965). The model's parameters, shown on the TTANH5 form, have been selected to give a smooth representation of the USSA profile, which actually has "corners." Figures 2.6b and 2.6c show the resulting temperature and sound-speed profiles. TTANH5 is a very flexible model that can be used to match virtually any temperature profile with linear segments that join smoothly.

Superimposed on the height-dependent background temperature model (TTANH5) are two "perturbations." One is expressed as a temperature perturbation (TBLOB2), and the other is expressed as a sound-speed perturbation (CBLOB2).

Refer now to the FORM TO SPECIFY INPUT DATA FOR ATMOSPHERIC TEMPERATURE-PERTURBATION MODEL TBLOB2 (Figure 2.7). This temperature-perturbation model is in general a three-dimensional blob with Gaussian cross sections in all three dimensions, centered at any latitude, longitude, and height. The formula is given on the TBLOB2 order form.

For the sample case, we suppress the vertical temperature dependence (by setting  $W_z=0$ ), making the perturbation a vertical cylinder with Gaussian cross sections in the two horizontal dimensions. For the sample case, we locate the cylinder at longitude 50 km east and latitude 105 km north, and set its E-W (zonal) Gaussian width at 25 km and its N-S (meridional) width at 50 km. Its maximum fractional temperature perturbation is 0.5 (50%). Notice that the form allows us to specify some of the model parameters in various units (such as latitude in kilometers); the program will automatically convert to the units (radians, in this example) it uses for computations.

Refer next to the FORM TO SPECIFY INPUT DATA FOR SOUND-SPEED PERTURBATION MODEL CBLOB2 (Figure 2.8). This sound-speed perturbation model is of the same form as TBLOB2, and its formula is shown on the CBLOB2 order form. For the sample case, we center a 50% increase in sound speed at 125 km height, longitude 250 km east, and latitude 335 km north. The Gaussian widths are 25 km in height, 50 km N-S, and 25 km E-W.

Figure 2.9 shows sound-speed contours in a horizontal slice at 125 km height, and Figure 2.10 shows sound-speed contours in a vertical slice near the centers of the two perturbations. (The contour-plotting routine is also part of the supplementary program set.)

The final part of the atmospheric model specifies the method used to compute acoustic absorption parameters required by the dispersion-relation subroutine AWWWL. In the sample case, we use a viscosity/conductivity subroutine called MUARDC, which requires a model of pressure.

FORM TO SPECIFY INPUT DATA FOR  
ATMOSPHERIC TEMPERATURE-PERTURBATION MODEL TBLOB2

An increase (or decrease) in temperature in a localized region that decays in a Gaussian manner in all three spatial directions.

$$T(r, \theta, \phi) = T_0(r, \theta, \phi) \left\{ 1 + \Delta \exp \left[ - \left( \frac{z-z_0}{W_z} \right)^2 - \left( \frac{\theta-\theta_0}{W_\theta} \right)^2 - \left( \frac{\phi-\phi_0}{W_\phi} \right)^2 \right] \right\}$$

$T_0(r, \theta, \phi)$  is the temperature specified by a temperature model.  $(r, \theta, \phi)$  are the coordinates of the ray point in an Earth-centered spherical polar coordinate system.  $\theta_0 = \pi/2 - \lambda_0$  and  $z = r - r_e$ , where  $r_e$  is the Earth radius.

Specify--

the model check for subroutine TBLOB2 = 2.0 (W225)

the input data-format code = \_\_\_\_\_ (W226)

an input data-set identification number = 2.0 (W227)

an 80-character description for the temperature-perturbation model, including description of parameter values:

50% CYLINDRICAL INCREASE IN TEMPERATURE AT 105 KM N., 105 KM W

the strength of the increase (or decrease),  $\Delta =$  0.5 (W228)

the height of maximum effect,  $z_0 =$  100 km (W229)

the latitude of maximum effect,  $\lambda_0 =$  105 rad, deg, (km) N (W230)

the longitude of maximum effect,  $\phi_0 =$  -105 rad, deg, (km) E (W231)

the Gaussian width in height of the effect,  $W_z =$  0 km (W232)\*

the meridional width of the effect,  $W_\theta =$  50 rad, deg, (km) (W233)\*

the zonal width of the effect,  $W_\phi =$  25 rad, deg, (km) (W234)\*

OTHER MODELS REQUIRED: none.

\* Setting  $W_z$ ,  $W_\theta$ , or  $W_\phi =$  zero results in no space variation in that direction.

Figure 2.7. Sample of completed form to specify input data for atmospheric temperature perturbation model TBLOB2.

FORM TO SPECIFY INPUT DATA FOR SOUND-SPEED  
PERTURBATION MODEL CBLOB2

An increase (or decrease) in sound speed in a localized region that decays in a Gaussian manner in all three spatial directions.

$$C^2(r, \theta, \phi) = C_0^2(r, \theta, \phi) \left( 1 + \Delta \exp \left\{ - \left( \frac{z-z_0}{W_z} \right)^2 - \left( \frac{\theta-\theta_0}{W_\theta} \right)^2 - \left( \frac{\phi-\phi_0}{W_\phi} \right)^2 \right\} \right)$$

$C_0^2(r, \theta, \phi)$  is the square of the sound speed specified by a sound-speed model.  $(r, \theta, \phi)$  are the coordinates of the ray point in an Earth-centered spherical polar-coordinate system.  $\theta_0 = \pi/2 - \lambda_0$  and  $z = r - r_e$ , where  $r_e$  is the Earth radius.

Specify--

the model check for subroutine CBLOB2 = 2.0 (W175)

the input data-format code = \_\_\_\_\_ (W176)

an input data-set identification number = 2.0 (W177)

an 80-character description for the sound-speed perturbation model, including description of parameter values:

50% INCREASE IN SQ. SOUND SPEED AT 125 KM HT, 335 KM N, 125 KM E

the strength of the fractional increase (or decrease),  $\Delta =$  0.5 (W178)

the height of maximum effect,  $z_0 =$  125 km (W179)

the latitude of maximum effect,  $\lambda_0 =$  335 rad, deg, (km) N (W180)

the longitude of maximum effect,  $\phi_0 =$  125 rad, deg, (km) E (W181)

the Gaussian width in height of the effect,  $W_z =$  25 km (W182)\*

the meridional width of the effect,  $W_\theta =$  50 rad, deg, (km) (W183)\*

the zonal width of the effect,  $W_\phi =$  25 rad, deg, (km) (W184)\*

OTHER MODELS REQUIRED: none.

\* Setting  $W_z$ ,  $W_\theta$ , or  $W_\phi =$  zero results in no space variation in that direction.

Figure 2.8. Sample of completed form to specify input data for sound-speed perturbation model CBLOB2.

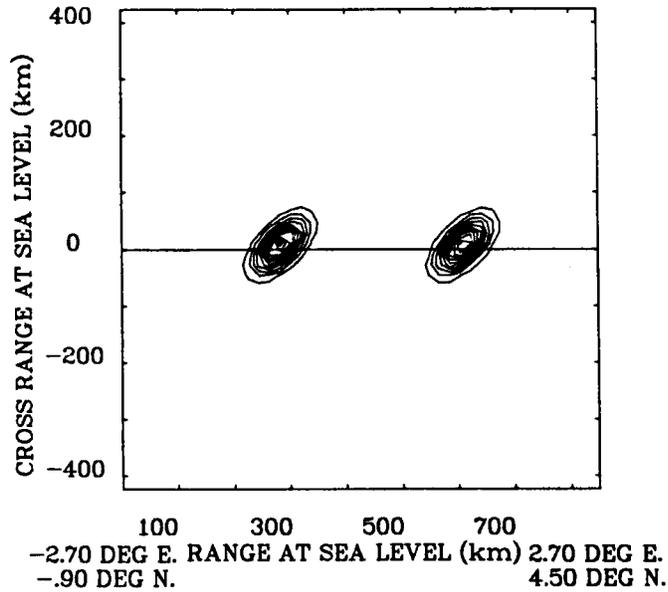


Figure 2.9. A plan view of the sound-speed contours in a horizontal slice through the sample-case atmospheric model at an altitude of 125 km above sea level. The contours show the perturbations caused by TBLOB2 (left) and CBLOB2 (right). The horizontal line across the center of the plot corresponds to the line L-R in Figure 2.18.

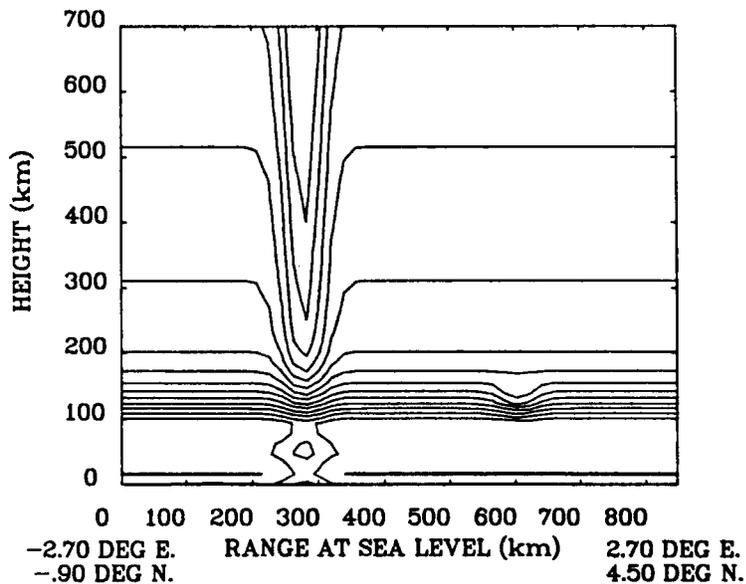


Figure 2.10. Sound-speed contours in a vertical slice through the sample-case model, showing the perturbations caused by models TBLOB2 (left) and CBLOB2 (right) to an otherwise horizontally stratified atmosphere. The plane of the figure corresponds to the line L-R in Figure 2.18.

Refer next to the FORM TO SPECIFY INPUT DATA FOR VISCOSITY/CONDUCTIVITY MODEL MUARDC (Figure 2.11). This model gives a formula (shown on the form) devised by the Air Research and Development Command (ARDC) (NOAA et al., 1976) for atmospheric viscosity and thermal conductivity. Its variable parameters are viscosity constant ( $\beta$ ), Sutherland's constant (S), and Prandtl number ( $P_n$ ). For the sample case,  $\beta = 1.45 \times 10^{-6}$ ,  $S = 110.4$ , and  $P_n = .733$ .

Refer next to the FORM TO SPECIFY INPUT DATA FOR PRESSURE MODEL PEXP (Figure 2.12). This model specifies an exponential decrease of pressure with height. The variable parameters are the pressure  $p_0$  at sea level (in Newtons per square meter) and the pressure scale height H (in kilometers). For the sample case,  $p_0 = 1.01328 \times 10^5$ , and  $H=8.5$  km.

Refer next to the FORM TO SPECIFY INPUT DATA FOR TERRAIN MODEL GLORENZ (Figure 2.13). This terrain model superimposes a Lorentzian-shaped ridge on a spherical earth. The ridge, defined by the formula on the GLORENZ order form, runs along a latitude line chosen to be the equator for the sample case. The half width of the ridge is 30 km, and its height is 2 km.

This completes the specification of the atmosphere (and terrain) model for the sample case. Now we specify what raypaths we want to calculate through this model.

## 2.2 The Ray-Tracing Order Form for the Sample Case

Refer now to the FORM TO SPECIFY INPUT DATA FOR A THREE-DIMENSIONAL RAYPATH CALCULATION (Figure 2.14). The form has been filled out with the values for the sample case. We want to transmit rays from a height 13 km above the earth's surface (as specified in the terrain model), at a latitude of 200 km north, and longitude of zero. The acoustic frequency is 0.05 Hz (infrasound), with no stepping in frequency. The azimuth angle of transmission is 45° (northeastward), with no stepping in azimuth. The elevation angle is stepped from -20° to +140° in steps of 5°. (If azimuth and frequency stepping were used, elevation-angle stepping would be performed first, then azimuth angle, then frequency.)

We want to keep track of ray intersections with a receiver surface 5 km above the terrain, and we want to stop tracing rays that go above 500 km alti-

FORM TO SPECIFY INPUT DATA FOR  
VISCOSITY/CONDUCTIVITY MODEL MUARDC

This subroutine calculates the atmospheric molecular viscosity using the ARDC formula for viscosity and calculates atmospheric thermal conductivity from the value of viscosity using a Prandtl number specified by the user. This model is used only to calculate acoustic absorption when either ANWWL or ANWWL is used.

The ARDC formula for viscosity is (U.S. Standard Atmosphere, 1976, p. 19, NOAA, NASA, USAF, U.S. Government Printing Office, Washington, D.C., October 1976)

$$\mu = \beta T^{3/2}/(S+T) ,$$

where T is the atmospheric temperature in Kelvins.

The atmospheric thermal conductivity using the Prandtl approximation (e.g., Francis Weston Sears, Thermodynamics, Addison-Wesley, 1956, pp. 287-9) is

$$\kappa = \gamma R\mu/((\gamma-1)M Pr) ,$$

where  $\gamma$  is the ratio specific heats = 1.4,  
R is the universal gas constant,  
and M is the mean atmospheric molecular weight.

Specify --

the model check for subroutine MUARDC = 1.0 (W500)

the input data-format code = \_\_\_\_\_ (W501)

an input data-set identification number = 1.0 (W502)

an 80-character description for the absorption model, including description of parameter values:

ARDC VISCOSITY/THERMAL CONDUCTIVITY MODEL

the viscosity constant,  $\beta = \underline{1.458 \times 10^{-6}}$  kg s<sup>-1</sup> m<sup>-1</sup> K<sup>-1/2</sup> (W503)

( $1.458 \times 10^{-6}$  kg s<sup>-1</sup> m<sup>-1</sup> K<sup>-1/2</sup> suggested)

Sutherland's constant, S = 110.4 Kelvins (W504)

(110.4 Kelvins suggested)

Prandtl number, Pr = .733 (W505) (0.733 suggested)

OTHER MODELS REQUIRED: Any atmospheric temperature model and any atmospheric molecular weight model.

Figure 2.11. Sample of completed form to specify input data for viscosity/conductivity model MUARDC.

FORM TO SPECIFY INPUT DATA FOR  
PRESSURE MODEL PEXP

This model is used only to calculate absorption when either AWWWL or ANWWL is used. The pressure is given by

$$P = P_0 \exp(-z/H),$$

where  $z$  is the height above sea level.

Specify --

the model check for subroutine PEXP = 1.0 (W550)

the input data-format code = \_\_\_\_\_ (W551)

an input data-set identification number = 1.0 (W552)

an 80-character description for the pressure model, including description of parameter values:

EXPONENTIAL PRESSURE MODEL, SCALE HEIGHT = 8.5 KM

the pressure at sea level,  $P_0 =$  101328 Newtons/m<sup>2</sup> (W553)

( $1.01328 \times 10^5$  Newtons/m<sup>2</sup> suggested)

the pressure scale height,  $H =$  8.5 (km) m (W554)

OTHER MODELS REQUIRED: Any pressure-perturbation model. Use NPPRES if no perturbation is desired.

Figure 2.12. Sample of completed form to specify input data for pressure model PEXP.

FORM TO SPECIFY INPUT DATA FOR  
TERRAIN MODEL GLORENZ

An east-west Lorentzian-shaped ridge.

$$g(r, \theta, \phi) = h - z ,$$

where  $h = r - r_e ,$

$$z = z_0 / (1 + ((\theta - \theta_0) / \Delta\theta)^2) + z_B ,$$

$$\theta_0 = \pi/2 - \lambda_0 ,$$

and  $r_e$  is the radius of the Earth.

Specify--

the model check number for GLORENZ = 4.0 (W300)

the input data-format code number = \_\_\_\_\_ (W301)

the input data-set identification number = 2.0 (W302)

an 80-character description of the model including parameters:

RIDGE 2-KM HIGH, 30-KM WIDE ALONG EQUATOR

the height of the ridge,  $z_0 =$  2 km, m (W303)

the latitude of the ridge center,  $\lambda_0 =$  0 rad, deg, km (W304)

the half-width of the ridge,  $\Delta\theta =$  30 rad, deg, km (W305)

base of the ridge (negative if below sea level)  $z_B =$  0 m, km (W306)

OTHER MODELS REQUIRED: Any terrain-perturbation model. Use NPERR if no perturbation is desired.

Figure 2.13. Sample of completed form to specify input data for terrain model GLORENZ.



tude, 1 km below the terrain (all rays should reflect from the terrain surface, however), or beyond 1000-km range. We want to stop the ray trace after 3 hops, a hop being defined as an intersection with the receiver surface.

Because we have selected a receiver surface at a fixed height above the terrain, we also fill out the FORM TO SPECIFY INPUT DATA FOR RECEIVER-SURFACE MODEL RTERR, as shown in Figure 2.15.

We set the maximum number of steps per hop to 1000 (usually a large number that we don't expect to be exceeded under normal conditions but which guards against accidents). We set the maximum allowable integration error per step to  $10^{-6}$ , which means that integrated quantities (that vary monotonically) are computed with at least that relative accuracy. We want to integrate and print phase path, path length, and absorption, but not to calculate Doppler shift (zero for the sample case, which has no time-dependent models). The printed output will display the raypath status every 50th step, in addition to printing at special events, such as reflections, apogees (turnovers), and perigees. Machine-readable "raysets" will also be produced.

### 2.3 Rayplot Order Form for the Sample Case

Two kinds of raypath plots are available and are specified for the sample case on the FORM TO SPECIFY INPUT PARAMETERS FOR PLOTTING A PROJECTION OF THE RAYPATH (Figures 2.16 and 2.17). The same form is used twice: once for a projection of raypaths on a vertical plane and once for a projection on a horizontal plane.

The vertical plane is specified by the geographic coordinates of its left and right edges and the height above ground of the bottom of the graph. In the sample case, we want the left edge to be at latitude -100 km (south) and longitude -300 km (west); the right edge is to be at latitude 500 km (north), longitude 300 km (east). Thus, the plane of the vertical projection coincides with the plane of initial ray transmission. The bottom of the graph is to be at ground level. We specify tick marks every 100 km, and we want registration marks (the top of the graph) at 300 km height.

The horizontal projection plane is specified by the location of the centers of its left and right edges. For the sample case, we select the left and

FORM TO SPECIFY INPUT DATA  
FOR RECEIVER-SURFACE MODEL RTERR

A receiver-surface model in which the receiver surface is a fixed height above the terrain surface.

$$f(r, \theta, \phi) = g(r, \theta, \phi) + z_R$$

$$\frac{\partial f}{\partial r} = \frac{\partial g}{\partial r}, \quad \frac{\partial f}{\partial \theta} = \frac{\partial g}{\partial \theta}, \quad \frac{\partial f}{\partial \phi} = \frac{\partial g}{\partial \phi},$$

where  $g(r, \theta, \phi)$  and its derivatives are specified in common block /GG/ by the terrain model.

Specify--

2.0

the model check number for subroutine RTERR = ~~8.0~~ (W275)

the input data-format code number = \_\_\_\_\_ (W276)

an 80-character description of the model including parameters:  
RECEIVER SURFACE 5 KM ABOVE TERRAIN

the height of the receiver surface above the terrain,  $z_R =$  5 km (W20)

OTHER MODELS REQUIRED: Any terrain model.

Figure 2.15. Sample of completed form to specify input data for receiver-surface model RTERR.

FORM TO SPECIFY INPUT PARAMETERS FOR PLOTTING A  
PROJECTION OF THE RAYPATH

Model ID: S03

Plot directly during raypath calculations ✓, or  
plot from precomputed raypaths \_\_\_\_\_  
in disk file \_\_\_\_\_

Normal or apogee plots: Normal ✓ (W80=0.0)  
Plot apogees only \_\_\_\_\_ (W80=1.0)

Projection:

Vertical plane, polar plot, rectangular expansion ✓ (W81=1.0)  
Horizontal plane, lateral expansion \_\_\_\_\_ (W81=2.0)  
Vertical plane, polar plot, radial expansion \_\_\_\_\_ (W81=3.0)  
Vertical plane, rectangular plot \_\_\_\_\_ (W81=4.0)

Superimpose these raypath plots on the graph of the previous sunset:

Yes \_\_\_\_\_ (W81 negative.)  
No ✓ (W81 positive.)

Vertical or lateral expansion factor 1 (W82)

Coordinates of the left edge of the graph:

Latitude = -100 (rad, deg, km) north (W83)  
Longitude = -300 (rad, deg, km) east (W84)

Coordinates of the right edge of the graph:

Latitude = 500 (rad, deg, km) north (W85)  
Longitude = 300 (rad, deg, km) east (W86)

Distance between horizontal tick marks = 100 rad, deg, km (W87)

Height above sea level of bottom of graph = 0 km (W88)

Height above sea level of top of graph = 300 km (W89)

Distance between vertical tick marks = 100 km (W96)

Figure 2.16. Sample of completed form to specify input parameters  
for plotting a projection of the raypath.

FORM TO SPECIFY INPUT PARAMETERS FOR PLOTTING A  
PROJECTION OF THE RAYPATH

Model ID: S03

Plot directly during raypath calculations  , or  
plot from precomputed raypaths \_\_\_\_\_  
in disk file \_\_\_\_\_

Normal or apogee plots: Normal  (W80=0.0)  
Plot apogees only \_\_\_\_\_ (W80=1.0)

Projection:

Vertical plane, polar plot, rectangular expansion \_\_\_\_\_ (W81=1.0)  
Horizontal plane, lateral expansion  \_\_\_\_\_ (W81=2.0)  
Vertical plane, polar plot, radial expansion \_\_\_\_\_ (W81=3.0)  
Vertical plane, rectangular plot \_\_\_\_\_ (W81=4.0)

Superimpose these raypath plots on the graph of the previous sunset:

Yes \_\_\_\_\_ (W81 negative.)  
No  \_\_\_\_\_ (W81 positive.)

Vertical or lateral expansion factor 3 (W82)

Coordinates of the left edge of the graph:

Latitude = -100 (rad, deg, km) north (W83)  
Longitude = -300 (rad, deg, km) east (W84)

Coordinates of the right edge of the graph:

Latitude = 500 (rad, deg, km) north (W85)  
Longitude = 300 (rad, deg, km) east (W86)

Distance between horizontal tick marks = 100 rad, deg, km (W87)

Height above sea level of bottom of graph = \_\_\_\_\_ km (W88)

Height above sea level of top of graph = \_\_\_\_\_ km (W89)

Distance between vertical tick marks = \_\_\_\_\_ km (W96)

Figure 2.17. Sample of completed form to specify input parameters  
for plotting a projection of the raypath.

right edges of the horizontal plot to coincide with the coordinates of the left and right edges of the vertical plot, as specified above.

Figure 2.18 shows a plan view of the region of the earth's surface near latitude zero, longitude zero, including the transmitter location, the ray-launch azimuth, the locations of the centers of the CBLOB2 and TBLOB2 perturbations, the ridge along the equator, and the locations of the left and right edges of the two plot projections.

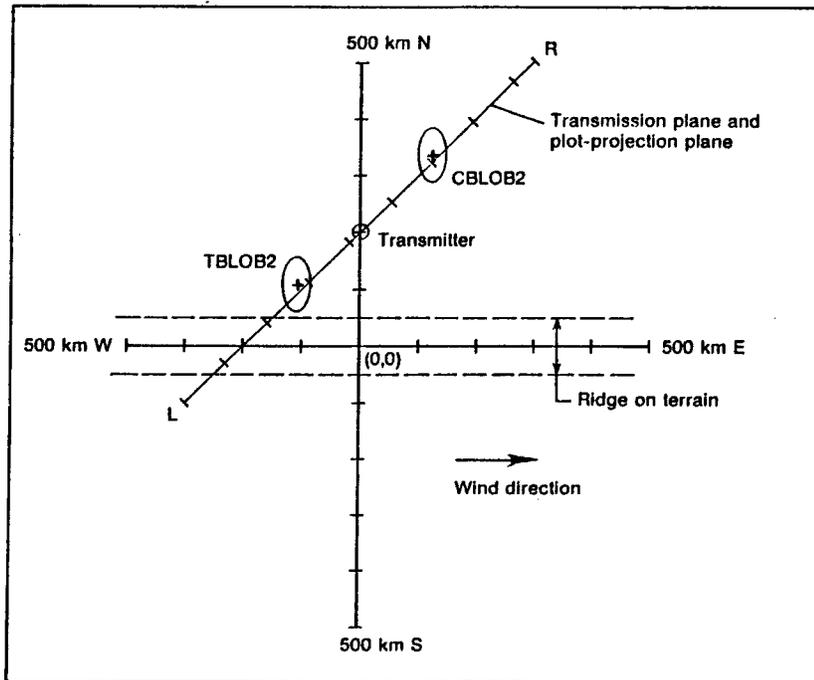


Figure 2.18. Plan view of the major features of the sample-case model, the transmitter location, the transmission direction, and the plot-projection plane.

#### 2.4 Setting Up the Input Data File (W Array) for the Sample Case

Now that we have defined all the parameters needed to specify the atmospheric model, the raypaths desired, as well as the printed, plotted and machine-readable output, we can look at the form in which these input data are communicated to HARPA. To run HARPA, you have to create a file like the one shown for the sample case in Figure 2.19. (Such a file for the sample case comes with the program.) HARPA reads this file into an array named  $W(n)$ , where  $n$ , the array subscript, is the first value on each line (columns 1-3), and  $W(n)$  is the second value on each line (columns 4-17).

The values of  $n$  corresponding to each input parameter are indicated on each of the input parameter forms we have just looked at. You will notice that not all values of  $n$  are listed in the input table for the sample case; those not explicitly defined in the Input Data File assume an initial value that is usually (but not always) zero. The initialization scheme is explained in Section 5.3.1.

Besides the values of  $n$  and  $W(n)$ , the figure contains in columns 18-24 provisions for unit conversion on input, that is, for entering data in various units. For example, the notation AN KM means that angular data has been entered in kilometers and will be converted to radians by the program. For  $W(3)$ , the height of the transmitter, a T in column 17 converts the height specified to height above the terrain model. Finally, in columns 25-80, descriptive comments identify the data for easy data entry.

There are special values of  $n$  (such as zero or negative values) that contain instructions for reading what follows. They will be described in detail in Chapter 5. A negative number in columns 1-3 indicates that tabular or text data follow. A zero in columns 1-3 indicates the end of tabular data or the end of a "run set," the name we give to the input data for a set of ray calculations. For example, the rays for one run set will all appear on a single rayplot. A new run set is necessary to create different plots or to change model parameters. In Figure 2.19, new run sets start with the lines that begin with "S03." For the sample case, each of the two run sets generates a different plot projection of the raypaths through the same atmospheric model. Only the  $W$  values that change from the previous run set need be specified; the others remain unchanged.

For now, you need only be aware of this tabular procedure for entering data into HARPA; it would also be instructive to verify that the values entered into the order forms for the sample case correspond to the entries in the  $W(n)$  Input Data File.

When you run the program with this input data set, three kinds of output will be produced: a step-by-step printed account of each ray's progress, plots of the raypaths on vertical and horizontal planes, and machine-readable data, including "raysets."

col. 1-3 n	col. 4-17 W(n)	col. 18-24 UNITS	col. 25-80 DESCRIPTION
GEORGES	RB3	X6437	
S03-1	SAMPLE	CASE FOR HARPA DOCUMENTATION	REV. 2-10-86
1	6370.		EARTH RADIUS, KM (6370.)
3	13.		TTRANSMITTER HEIGHT, KM (T=ABOVE TERRAIN)
4	200.	AN KM	N. TRANSMITTER LATITUDE, KM
5	0.	AN KM	E. TRANSMITTER LONGITUDE, KM
7	.05	FQ HZ	INITIAL FREQUENCY, HZ
11	45.	AN DG	INITIAL AZIMUTH ANGLE, DEG
15	-20.	AN DG	INITIAL ELEVATION ANGLE, DEG
16	140.	AN DG	FINAL ELEVATION ANGLE, DEG
17	5.	AN DG	STEP IN ELEVATION ANGLE, DEG
20	5.		RECEIVER HEIGHT, KM
22	3.		MAXIMUM NUMBER OF HOPS (1.0)
23	1000.		MAXIMUM NUMBER OF STEPS PER HOP (1000.)
26	500.		MAXIMUM RAY HEIGHT, KM (500.)
27	-1.		MINIMUM RAY HEIGHT, KM
28	1000.		MAXIMUM RANGE, KM
29	0000100.		DO: EIGRAY/RNG-TIM/RNG-ELV/NEW-PROJ/RAYTRC/CONT/PROF
33	999.999		MAXIMUM ABSORPTION, DB (999.999)
42	1.0E-6		SINGLE-STEP INTEGRATION ERROR (1.0E-4)
44	.1		INITIAL INTEGRATION STEP SIZE, KM (1.0)
57	2.		PHASE PATH (0=NO; 1=INTEGRATE; 2=INTEGRATE/PRINT)
58	2.		ABSORPTION (0=NO; 1=INTEGRATE; 2=INTEGRATE/PRINT)
60	2.		PATH LENGTH (0=NO; 1=INTEGRATE; 2=INTEGRATE/PRINT)
71	50.		NUMBER OF INTEGRATION STEPS PER PRINT [1.E31]
72	1.		OUTPUT RAYSETS (1=YES; 0=NO)
73	0.		DIAGNOSTIC PRINTOUT (1=YES; 0=NO)
74	0.		PRINT RAY STEPS (0=YES; 1=NO)
75	.15		FULANN LETTER HEIGHT [0.15 IN]
76	0.		BINARY RAY OUTPUT (1=YES; 0=NO)
77	57.		LINES PER PAGE IN PRINTOUT (66.)
81	1.		RAYPLOT PROJECTION (1=VERT; 2=HORIZ) PLANE
82	1.		PLOT-EXPANSION FACTOR [1.0]
83	-100.	AN KM	N. LATITUDE OF LEFT PLOT EDGE, KM
84	-300.	AN KM	E. LONGITUDE OF LEFT PLOT EDGE, KM
85	500.	AN KM	N. LATITUDE OF RIGHT PLOT EDGE, KM
86	300.	AN KM	E. LONGITUDE OF RIGHT PLOT EDGE, KM
87	100.	AN KM	DISTANCE BETWEEN TIC MARKS, KM
88	0.		HEIGHT ABOVE SEA LEVEL OF BOTTOM OF GRAPH, KM
89	300.		HEIGHT ABOVE SEA LEVEL OF TOP OF GRAPH, KM
96	100.		DISTANCE BETWEEN VERTICAL TIC MARKS, KM
100	6.		ULOGZ2 WIND MODEL CHECK NUMBER
102	3.		BACKGROUND WIND DATA SET ID
103	5.	LN M	REFERENCE WIND SPEED, M/S
104	35		VON KARMAN'S CONSTANT
105	1.		ROUGHNESS HEIGHT, KM
150	1.		GAMRTDM SOUND SPEED MODEL CHECK NUMBER
175	2.		CBLOB2 MODEL CHECK NUMBER
177	2.		SOUND SPEED PERTURBATION DATA SET ID
178	.5		FRACTIONAL INCREASE OF SQUARED SOUND SPEED

Figure 2.19. Input Data File for the sample case.

```

179      125.          HEIGHT OF MAXIMUM INCREASE, KM
180      335.      AN KM  N. LATITUDE OF MAXIMUM INCREASE, KM
181      125.      AN KM  E. LONGITUDE OF MAXIMUM INCREASE, KM
182      25.          GAUSSIAN WIDTH IN HEIGHT OF INCREASE, KM
183      50.      AN KM  N-S WIDTH OF THE INCREASE, KM
184      25.      AN KM  E-W WIDTH OF THE INCREASE, KM
200      7.          TTANH5 TEMPERATURE MODEL CHECK NUMBER
202      1.          BACKGROUND TEMPERATURE DATA SET ID
225      2.          TBLOB2 MODEL CHECK NUMBER
227      2.          TEMPERATURE PERTURBATION DATA SET ID
228      .5         FRACTIONAL TEMPERATURE INCREASE
229      0.          HEIGHT OF MAXIMUM INCREASE, KM
230      105.     AN KM  N. LATITUDE OF MAXIMUM INCREASE, KM
231     -105.     AN KM  E. LONGITUDE OF MAXIMUM INCREASE, KM
232      0.          GAUSSIAN WIDTH IN HEIGHT OF INCREASE, KM
233      50.      AN KM  N-S WIDTH OF THE INCREASE, KM
234      25.      AN KM  E-W WIDTH OF THE INCREASE, KM
250      1.          MCONST MOLECULAR WEIGHT MODEL CHECK NUMBER
252      29.          MOLECULAR WEIGHT DATA SET ID
253      29.          MOLECULAR WEIGHT
275      2.          RTERR RECEIVER MODEL CHECK NUMBER
300      4.          GLORENZ TERRAIN MODEL CHECK NUMBER
302      2.          TERRAIN MODEL DATA SET ID
303      2.          HEIGHT OF THE RIDGE, KM
304      0.          N. LATITUDE OF THE RIDGE CENTER
305      30.     AN KM  HALF-WIDTH OF THE RIDGE, KM
325      0.          NPTErr NO TERRAIN PERTURBATION
500      1.          MUARDC VISC/COND MODEL CHECK NUMBER
502      1.          VISC/COND MODEL DATA SET ID
503      1.458E-06  VISCOSITY COEFFICIENT BETA
504      110.4     SUTHERLAND'S CONSTANT, KELVINS
505      .733     PRANDTL NUMBER
525      0.          NPABS NO VISC/COND PERTURBATION
550      1.          PEXP PRESSURE MODEL CHECK NUMBER
552      1.          BACKGROUND PRESSURE MODEL DATA SET ID
553      101328.   PRESSURE AT SEA LEVEL, N/SQ.M.
554      8.5     PRESSURE SCALE HEIGHT, KM
575      0.          NPPRES NO PRESSURE PERTURBATION
-1          DATA SUBSET FOR BACKGROUND WIND MODEL
A LOGARITHMIC EASTWARD WIND PROFILE, U*=.5 M/S, Z0=1 KM
0          RETURN TO W ARRAY DATA SET
-2          DATA SUBSET FOR WIND PERTURBATION MODEL
A NO WIND PERTURBATION
0          RETURN TO W ARRAY DATA SET
-3          DATA SUBSET FOR BACKGROUND SOUND-SPEED MODEL
A SOUND SPEED IN TERMS OF TEMPERATURE MODEL
0          RETURN TO W ARRAY DATA SET
-4          DATA SUBSET FOR SOUND-SPEED PERTURBATION MODEL
A 50% INCREASE IN SQ. SOUND SPEED AT 125KM HT, 335KM N, 125KM E
0          RETURN TO W ARRAY DATA SET
-5          DATA SUBSET FOR TEMPERATURE MODEL
A U.S. STANDARD ATMOSPHERE 1962 TEMPERATURE PROFILE
3          999.0
LN KM          LN KM
0.            288.000      0.

```

Figure 2.19. Input Data File (continued).

```

15.0000      190.500      10.0000
52.0000      320.000      7.50000
95.0000      191.000      10.0000
165.0000     1451.000     50.0000
300.0000     1586.000      0.
999.0000
0      RETURN TO W ARRAY DATA SET
-6      DATA SUBSET FOR TEMPERATURE PERTURBATION MODEL
A 50% CYLINDRICAL INCREASE IN TEMPERATURE AT 105KM N., 105 KM W
0      RETURN TO W ARRAY DATA SET
-7      DATA SUBSET FOR MOLECULAR WEIGHT MODEL
A MOLECULAR WEIGHT = 29
0      RETURN TO W ARRAY DATA SET
-8      DATA SUBSET FOR RECEIVER SURFACE MODEL
A RECEIVER SURFACE 5 KM ABOVE TERRAIN
0      RETURN TO W ARRAY DATA SET
-9      DATA SUBSET FOR TERRAIN MODEL
A RIDGE 2-KM HIGH, 30-KM WIDE ALONG EQUATOR
0      RETURN TO W ARRAY DATA SET
-10     DATA SUBSET FOR TERRAIN PERTURBATION MODEL
A NO TERRAIN PERTURBATION
0      RETURN TO W ARRAY DATA SET
-17     DATA SUBSET FOR VISC/COND MODEL
A ARDC VISCOSITY AND THERMAL CONDUCTIVITY MODEL
0      RETURN TO W ARRAY DATA SET
-18     DATA SUBSET FOR VISC/COND PERTURBATION MODEL
A NO VISCOSITY/CONDUCTIVITY PERTURBATION
0      RETURN TO W ARRAY DATA SET
-19     DATA SUBSET FOR BACKGROUND PRESSURE MODEL
A EXPONENTIAL PRESSURE MODEL, SCALE HEIGHT = 8.5 KM
0      RETURN TO W ARRAY DATA SET
-20     DATA SUBSET FOR PRESSURE PERTURBATION MODEL
A NO PRESSURE PERTURBATION
0      RETURN TO W ARRAY DATA SET
0
0      ***** END OF RUN SET NUMBER 1 *****
S03-2   SAMPLE CASE FOR HARPA DOCUMENTATION      REV. 2-10-86
71      0.      NUMBER OF INTEGRATION STEPS PER PRINT
72      0.      OUTPUT RAYSETS (1=YES; 0=NO)
73      1.      DIAGNOSTIC PRINTOUT (1=YES; 0=NO)
81      2.      RAYPLOT PROJECTION (1=VERT; 2=HORIZ) PLANE
82      3.      PLOT-EXPANSION FACTOR
0      ***** END OF RUN SET NUMBER 2 *****

```

Figure 2.19. Input Data File (continued).

## 2.5 Printed Output for the Sample Case

Appendix A shows the complete printed output, or "printout," for the sample case. Sections 2.5.1 and 2.5.2 define the terms and quantities used in the printout.

Page 1 of the printout contains the program title block and a list of all the models used for the first run set. The model list includes subroutine names, a number identifying the set of parameters defining that particular model, and comments describing each model.

Pages 2-4 of the printout reproduce the Input Data File for run set number 1.

Page 5 of the printout is a list of  $n$  and  $W(n)$  for all nonzero  $W(n)$ . The values of  $W(n)$  have been converted to the units used by the program; for example, angles (like latitude and longitude) input in kilometers have been converted to radians. The standard set of units used by the program are: angles in radians, distances in kilometers, and frequency in radians per second.

Pages 6-10 of the printout are in a columnar format that gives a step-by-step account of each ray's progress, with each line showing important raypath quantities at user-specified intervals along the raypath. The meanings of the quantities printed out are explained in Section 2.5.1. The user can specify how often along the ray a line is printed (we specified every 50 integration steps). In addition, a line is printed out every time a ray experiences a "special event," such as a ground reflection, a turnover (apogee) or turnunder (perigee), crosses the receiver height, or a few other events. Section 2.5.2 explains the exact meanings of all the special events.

Each ray calculation terminates when one of the termination conditions is met, such as the maximum number of hops, maximum range, or maximum number of integration steps, whichever occurs first. In the sample case, all of the rays terminate either because they reached the maximum number of hops specified (3) or because the absorption reached the maximum specified. At the end of each ray calculation, the printout shows how much CPU time was used for that ray computation (2.009 s, in this case).

Look at page 1 of the printout in Appendix A. Verify that the models indicated at the bottom of the page coincide with those we specified as input. Verify that the wave frequency and initial azimuth and elevation angles on page 6 are what we want. Look down the first (ERROR) column of the tabular printout (page 6) and verify that none of the numbers in this column exceeds the maximum allowable single-step integration error,  $W(42)$ , which for the sample case is  $10^{-6}$ . This means that the numerical integration is proceeding correctly.

Look at the first entries in the ELEVATION columns and verify that the ray starts at the correct height above the terrain (13.00 km in this case), as well as the correct height above sea level (slightly more than 13 km in this case, because of the terrain model). The RANGE column should begin with zero range from the transmitter and indicate the range from the transmitter with successive steps.

A general idea of the sequence of events along this ray can be read in the EVENT column. These notations mark the special events along the raypath, which cause printout regardless of the step number. Reading down this column, we see that this ray begins at the transmitter (XMTR), then crosses the receiver (RCVR) height at 5 km altitude above the terrain, then reflects from the ground (GRND REF), passes through the receiver (RCVR) height once again, then executes an APOGEE, or turnover, and stops when it reaches the receiver height (RCVR) a third time. The ray stopped because we specified a maximum of three hops, or intersections with the receiver height (MAX HOPS).

The numbers in the AZIMUTH DEVIATION columns indicate that the ray deviates from the azimuth of transmission because of the wind. The ELEVATION ANGLE columns show changes in the local wave-normal direction and the elevation of the ray point measured from the transmitter.

PULSE TIME gives the time for a pulse or wave packet to reach that point, and PHASE TIME gives the time for a wave phase front to reach that point. The wave phase can be derived from PHASE TIME by multiplying by the wave frequency in appropriate units (cycles per second to get wave phase in cycles, etc.) and removing the integer part. The PATH LENGTH gives the physical length of the ray path.

The second run set shown in the sample-case printout uses the same initial ray conditions, but it changes the rayplot to a horizontal projection, and it adds diagnostic printout that can be useful for studying the details of terrain or receiver-surface intersections.

#### 2.5.1 Definitions of Quantities Listed in Printout (Appendix A)

**AZIMUTH ANGLE OF TRANSMISSION** -- Azimuth angle (degrees clockwise from north) of the initial ray-launch direction.

**ELEVATION ANGLE OF TRANSMISSION** -- Elevation angle (degrees upward) between the initial ray-launch direction and local horizontal at the transmitter.

**TRANSMITTER LATITUDE** -- East latitude of the transmitter in geographic coordinates.

**TRANSMITTER LONGITUDE** -- North longitude of the transmitter in geographic coordinates.

**FREQUENCY** -- Acoustic wave frequency in hertz.

**SINGLE-STEP ERROR** -- Maximum allowable single-step integration error.

**ERROR** -- Normalized difference between the wave number  $k$  computed by numerical integration and  $k$  computed from the dispersion relation [Eq. (6.32)].

**EVENT** -- Nature of special event along the raypath (see Sec. 2.5.2).

**HEIGHT** -- Height of the ray point above sea level (or above the terrain).

**RANGE** -- Great-circle distance, measured at sea level between the transmitter and the ray point.

**AZIMUTH DEVIATION (XMTR)** -- Azimuth angle of the direction of transmission in degrees clockwise from the great circle between the transmitter and the ray point.

**AZIMUTH DEVIATION (LOCAL)** -- Azimuth angle of the wave normal in degrees clockwise from the great circle between the transmitter and the ray point.

**ELEVATION (XMTR)** -- Elevation angle (degrees) of the ray point from local horizontal at the transmitter.

**ELEVATION (LOCAL)** -- Elevation angle (degrees) of the wave normal from the local horizontal at the ray point.

**PULSE TIME** -- The time (seconds) required for a wave packet (pulse) to travel from the transmitter to the ray point (Sec. 6.1).

PHASE TIME -- The time (seconds) required for a wave front to travel from the transmitter to the ray point (Sec. 6.1.1).

ABSORPTION -- Decrease in acoustic intensity (dB) from the transmitter to the ray point caused by atmospheric dissipation only (Sec. 6.1.2).

PATH LENGTH -- Geometric length of the ray path (kilometers) from the transmitter to the ray point (Sec. 6.1.3).

#### 2.5.2 Meanings of Special Events Along a Raypath

XMTR -- Ray is at the transmitter.

RCVR -- Ray is at the receiver surface.

GRND REF -- Ray has reflected from the terrain surface.

APOGEE -- Ray has passed through a maximum in height.

PERIGEE -- Ray has passed through a minimum in height.

WAVE REV -- Vertical, southward, or eastward component of the wave vector has changed sign.

MAX LAT -- Ray has passed through a maximum (or minimum) in latitude.

MAX LONG -- Ray has passed through a maximum (or minimum) in longitude.

EXTINC -- Absorption has exceeded the maximum allowable.

MAX HOP -- Ray has executed the requested number of hops (receiver-surface crossings).

MAX RANG -- Ray has exceeded the maximum allowable ground range.

MAX HT -- Ray has exceeded the maximum allowable height.

MIN HT -- Ray has gone below the minimum allowable height.

MIN DIST -- Ray has made a closest approach to the receiver surface.

#### ADDITIONAL EVENTS IN DIAGNOSTIC PRINTOUT

BACK UP0 -- At call to subroutine BACKUP.

BACK UP1 -- Before each numerical integration step in subroutine BACKUP.

GRAZE 0 -- At call to ENTRY point GRAZE in subroutine BACKUP.

GRAZE 1 -- Before each numerical integration step after ENTRY point GRAZE.

BACK UP2 -- After unsuccessfully trying to find a closest approach to the receiver surface.

BACK UP3 -- Before each numerical integration step after BACK UP2.

## 2.6 Rayplots for the Sample Case

We requested two rayplots, a projection on a vertical plane and a projection on a horizontal plane. These two plots are shown in Figures 2.20 and 2.21. Because we selected the FULANN (full annotation) option in W(75), we have produced a plot with publication-quality lettering. This capability requires the DISSPLA plotting package.

Rayplots are often the most useful output from a ray-tracing program, particularly when the medium is complicated. Depending on the user's plotting and display facilities, rayplots can be produced on paper, microfilm, or video displays.

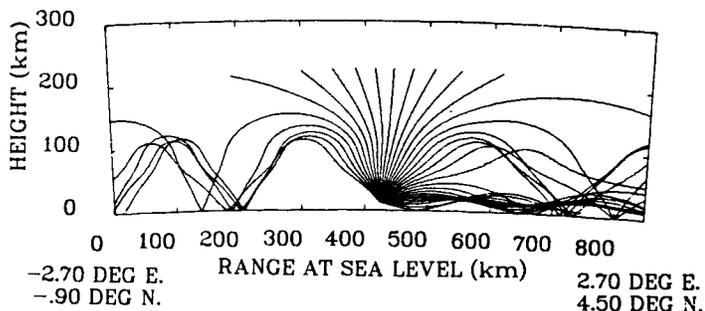
Because the atmospheric and terrain models used in the sample case cause the acoustic raypaths to behave in complicated ways, a few features of the two rayplot projections call for some explanation. Figure 2.18 shows how the planes of these plots are related to the transmitter location and the features of the atmospheric and terrain models. The letters L and R show the locations of the left and right edges of the two plots; the line connecting the L and R represents the plane of the vertical projection (Figure 2.20) as well as the line across the center of the horizontal projection (Figure 2.21).

The two rayplots show the gross refracting features of this atmospheric model, namely that the temperature gradient bends upgoing rays back toward the ground, and that the eastward wind deflects rays generally downwind. The wind direction is to the right in Figure 2.20 (though not in the plane of the plot) and is down and to the right in Figure 2.21. In the absence of wind, the rays shown in Figure 2.21 would all be coplanar and so would appear as a single straight, horizontal line in that projection, and the plot of Figure 2.20 would exhibit left-right symmetry. By comparing corresponding rays in Figures 2.20 and 2.21, one can get a rough three-dimensional perspective of the raypaths.

The effects of the ridge in the terrain model are not evident in the scales of these plots because the ridge is only 2 km high. The peak of the

1 SAMPLE CASE FOR HARPA DOCUMENTATION REV. 2-10-86  
 MODEL = S03 ,FREQ = .050 HZ, AZ = 45.000 DEG  
 EL = -20.00 DEG TO 140.00 DEG, STEP = 5.00 DEG  
 XMTR HT = 13.04 KM ,LAT = 1.80 DEG, LONG = .00 DEG  
 ACOUSTIC WAVE \*\*\* WITH WIND \*\*\*\*\* WITH LOSSES

MODELS  
 ULOGZ2 3.0  
 NPWIND .0  
 GAMRTDM .0  
 CBLOB2 2.0  
 TTANH5 1.0  
 TBLOB2 2.0  
 MCONST 29.0  
 GLORENZ 2.0  
 NPERR .0  
 MUARDC 1.0  
 NPABSR .0  
 PEXP 1.0  
 NPPRES .0  
 RTERR .0

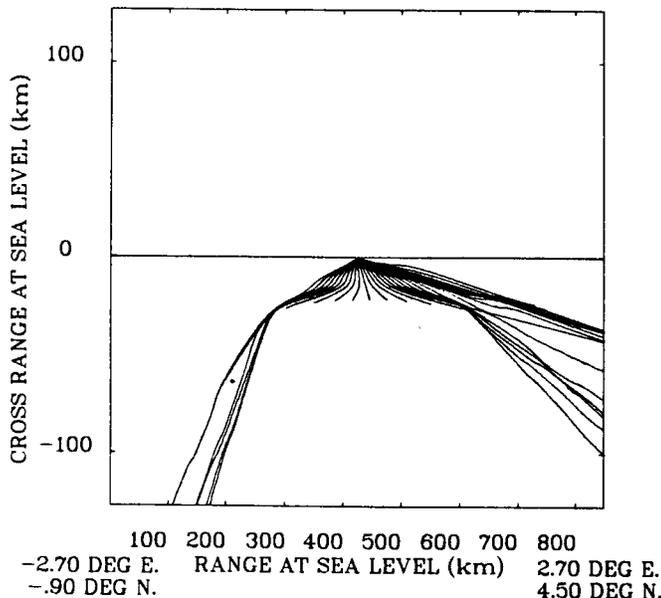


86/03/21. 17.34

Figure 2.20. Projection of the rays of the sample case onto the vertical plane shown in Figure 2.18.

2 SAMPLE CASE FOR HARPA DOCUMENTATION REV. 2-10-86  
 MODEL = S03 ,FREQ = .050 HZ, AZ = 45.000 DEG  
 EL = -20.00 DEG TO 140.00 DEG, STEP = 5.00 DEG  
 XMTR HT = 13.04 KM ,LAT = 1.80 DEG, LONG = .00 DEG  
 ACOUSTIC WAVE \*\*\* WITH WIND \*\*\*\*\* WITH LOSSES

MODELS  
 ULOGZ2 3.0  
 NPWIND .0  
 GAMRTDM .0  
 CBLOB2 2.0  
 TTANH5 1.0  
 TBLOB2 2.0  
 MCONST 29.0  
 GLORENZ 2.0  
 NPERR .0  
 MUARDC 1.0  
 NPABSR .0  
 PEXP 1.0  
 NPPRES .0  
 RTERR .0



86/03/21. 17.34

Figure 2.21. Projection of the rays of the sample case onto a horizontal plane whose axis (the horizontal line across the middle of the plot) is shown in Figure 2.18.

ridge intersects the plane of the vertical projection at about 300 km to the left of the transmitter, and rays launched between about 120 and 130 deg elevation reflect from the terrain near the peak of the ridge. They can be observed in detail by launching a dense fan of rays between 120 and 130 deg elevation and magnifying the vertical-projection plot in the vicinity of the ridge. This could be done with just a few modifications of the Input Data File and will be left as an exercise for the user.

## 2.7 Machine-Readable Output for the Sample Case

HARPA produces two kinds of machine-readable output. One form is called "raysets," which summarize in compressed form some useful ray parameters at each special event (as defined above) along the raypath. The other form of machine-readable output is called "binary raypath data," which permits a complete reconstruction of the raypaths by a supplementary processing program. When stored in machine-readable form (punched cards, magnetic tape, disk files), raysets (as a file named PUNCH) and binary raypath data (as a file named TAPE6) form the input to supplementary processing programs and extend the utility of ray-tracing calculations. Examples are supplementary programs to plot model profiles and contours, to compute amplitude, to plot range versus elevation angle of transmission and range versus travel time, as well as programs that interpolate in elevation angle to estimate eigenrays that reach a specified range. These supplementary capabilities will be documented in another report.

Figure 2.22 shows a portion of the printout of the raysets for the sample case. The complete rayset output for the sample case is given in Appendix A. Each ray begins with a "transmitter rayset," the lines beginning with "S03" in the example. Additional 80-column lines are produced whenever a ray reflects from the terrain surface or crosses the receiver height and at the end of each ray trace. Because of the way hops are counted, two identical raysets are produced each time a ray executes a closest approach to the receiver height.

The compressed rayset format is generally meant to be read by machines, not humans, so it can be rather difficult to inspect for information.

S03-1 SAMPLE CASE FOR HARPA DOCUMENTATION REV.9-23-85  
 ULOGZ2 3.0 NPWIND .0 GAMMA RT .0 CBLOB2 2.0  
 TTANH5 1.0 TBLOB2 2.0 MCONST 29.0 NO MODL .0  
 PEXP 1.0 NPPRES .0 MUARDC 1.0 NPABSR .0  
 GLORENZ 2.0 NPTRR .0 RTERR .0 NO MODL .0

Model  
 Identification  
 Header

LOGARITHMIC EASTWARD WIND PROFILE  
 50% INCREASE IN SQUARED SOUND SPEED AT 125KM HT, 335KM N, 125KM E.  
 U.S. STANDARD ATMOSPHERE 1962 TEMPERATURE PROFILE  
 50% CYLINDRICAL INCREASE IN TEMPERATURE AT 105KM N., 105 KM W.  
 MOLECULAR WEIGHT = 29

RIDGE 2-KM HIGH, 30-KM WIDE ALONG EQUATOR										
S03	130440	1799	0	50000	3142	4500000	-2000000			
	50367	294887	-3840	-3838-12169	9196124	9196123	0	0	0	0 3T
	313	563108	-2735	-2735 10693	17228767	17228768	0	0	0	0 1R
	50270	831414	-2343	-2340 12148	25260761	25260764	0	0	0	0 2G
	50112	3073288	-4374	-4375-12129	94307633	94307634	0	0	0	0 2R
S03	130440	1799	0	50000	3142	4500000	0	0	0	0 3R
	130453	2250470	-4938	-4939 -3	68990961	68990962	0	0	0	0 3T
	130453	2250470	-4938	-4939 -3	68990961	68990962	0	0	0	0 1M
	130423	4501421	-4932	-4941 -1	137987009	137987013	0	0	0	0 2M
S03	130440	1799	0	50000	3142	4500000	2000000	0	0	0 3M
	50170	1946869	-5322	-5324-12129	59828119	59828103	0	0	0	0 1T
	152	2215510	-4860	-4863 10665	67882811	67882797	0	0	0	0 3R
	50137	2484283	-4498	-4500 12121	75937724	75937711	0	0	0	0 2G
	50070	4727741	-4790	-4799-12126	145006034	145006027	0	0	0	0 2R
S03	130440	1799	0	50000	3142	4500000	4000000	0	0	0 3R
	50103	3741414	-9536	-4137-35775	117807866	117807837	3	0	0	0 3T
	101	3814687	-9488	-4092 34998	120425195	120425167	3	0	0	0 1R
	50099	3887966	-9442	-4046 35772	123042513	123042487	3	0	0	0 2G
	50043	7937415	-10564	-5185-35793	249875267	249875381	6	0	0	0 2R
S03	130440	1799	0	50000	3142	4500000	6000000	0	0	0 3R
	50104	3788921	-10259	-3574-59417	113854747	113854834	840	0	0	0 3T
	103	3820800	-10249	-3572 58548	115617591	115617680	840	0	0	0 1R
	50102	3852681	-10240	-3563 59414	117380431	117380523	840	0	0	0 2G
	50049	7425637	-11689	-5024-59423	230295002	230295121	1573	0	0	0 2R
S03	130440	1799	0	50000	3142	4500000	8000000	0	0	0 3R
	2245590	880081	-14390	-14394 64191	50090000	500899659999999	0	0	0	0 3T
S03	130440	1799	0	50000	3142	4500000	10000000	0	0	0 1E
	2238850	451046208869	28867	65050	49890000	498899649999999	0	0	0	0 3T
S03	130440	1799	0	50000	3142	4500000	12000000	0	0	0 1E
	53003	2990950200125	978	-57476	115367955	115368106	2511	0	0	0 3T
	2797	3023605200153	553	54429	117198670	117198821	2511	0	0	0 1R
	52607	3056827200187	580	56842	119028620	119028770	2511	0	0	0 2G
	50134	5991692205807	6198	-56730	234573129	234573354	3731	0	0	0 2R
S03	130440	1799	0	50000	3142	4500000	14000000	0	0	0 3R
	58098	2555846202632	-6592	-36018	108393614	108393701	11	0	0	0 3T
	6338	2633761202904	-6666	28584	111287389	111287482	11	0	0	0 1R
	55009	2713368203173	-6406	33954	114170553	114170650	11	0	0	0 2G
	50143	5658781212816	3229	-33478	231386220	231386499	18	0	0	0 2R

Transmitter Raysets

Receiver Raysets

Figure 2.22. Rayset output for the first run set of the sample case, using an elevation-angle increment of 20°.

However, since this is occasionally necessary, Figures 2.23 and 2.24 provide the key for reading rayset printouts.

Notice that the last 3 columns preceding the hop identifier in the receiver raysets contain all zeroes for the sample case. The first of these columns is for Doppler shift, which is zero because we did not use a time-varying model atmosphere. The transverse polarization is always zero for pure acoustic waves, but is nonzero for acoustic-gravity waves (Jones et al., 1982, Sec. 4.1).

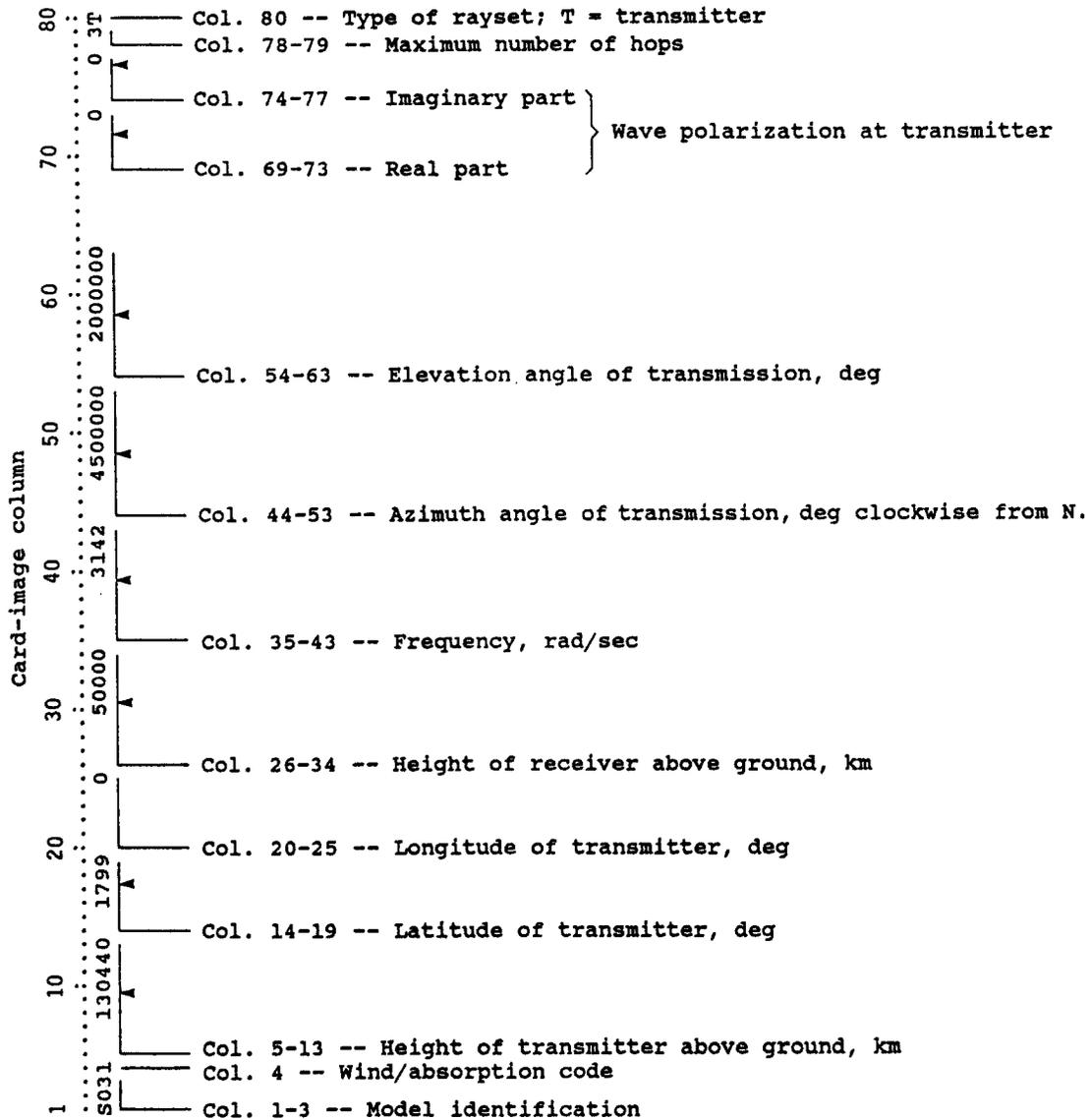


Figure 2.23. Definitions and format for a transmitter rayset. \*Wind/absorption code: 0 = no wind, no absorption; 1 = with wind, no absorption; 2 = no wind, with absorption; 3 = with wind, with absorption and ▲ = decimal point.



## PART II: HOW TO USE THIS PROGRAM

### 3. How to Get This Program Running on Your Computer

This chapter explains how to get the FORTRAN source code off the distribution tape and onto your computer, and how to get as far as running the sample case. It also deals with the machine-dependent aspects of running HARPA and suggests ways to deal with different computing environments.

#### 3.1 How To Get a Copy of the Program

The FORTRAN source code for the version of HARPA documented in this report and the Input Data File for the sample case are available on magnetic tape. For ordering information, contact the authors at the Wave Propagation Laboratory, Propagation Studies Program Area, 325 Broadway, Boulder, Colorado 80303.

The format of the distribution tape is 0.5 in x 1200 ft, 9 track, 1600 bpi, ASCII character set, block size 1600 bytes, logical record length 80 bytes, no parity.

#### 3.2 ANSI-FORTRAN 77 Compatibility

HARPA was designed to run on a Control Data Corp. (CDC) CYBER 700-800 series with a CDC FORTRAN 77 compiler. It should compile with any FORTRAN compiler that adheres to the ANSI FORTRAN 77 standard, including microcomputer FORTRAN compilers that claim such compatibility.

To ensure portability, we have made many changes in portions of the program that were written before the ANSI standard was established. However, where such changes would have been arduous, and where de facto standards that exist on many systems permit deviations from the ANSI standard, we have retained some non-ANSI code. Following are some exceptions to the ANSI standard:

- (1) Some variable and subroutine names have seven characters (six is the ANSI standard).

- (2) Some alphanumeric characters are stored eight characters per word in numeric (not character) variables and are output using A8 format.
- (3) Some machine-dependent constants are entered in nonstandard format (see the following section).
- (4) Sometimes a function is called as though it were a subroutine.
- (5) Some real variables are EQUIVALENCed to integer variables.
- (6) In some models and other subroutines, data statements are used to initialize variables contained in labeled-common blocks. For systems that do not permit this, such data statements must be put into separate BLOCK DATA modules. Sequence numbers in the source-code listing identify such statements.

### 3.2.1 Machine- and System-Dependent Code

We have tried to consolidate any machine- or operating-system-dependent code into two subroutines to make it easier to identify and adapt to new environments.

Before attempting to run HARPA, the user must modify SUBROUTINE DFCNST, which defines machine-dependent constants. The version supplied on the distribution tape is for the CYBER 700-800 series with NOS 2x. Instructions for modifying this routine for several popular machines are included as comments in SUBROUTINE DFCNST (Appendix D).

Another subroutine, DFSYS, contains some operating-system-dependent functions, such as clock and date functions and system-dependent I/O. Users should also check DFSYS and make changes appropriate to their own operating systems.

### 3.2.2 Word Length

Some problems may arise with machines that have word lengths shorter than the 60-bit word used in our CYBER 840. The numerical integration subroutine (RKAM1) uses double-precision arithmetic to accumulate numerically integrated quantities, but this is almost certainly not necessary with a 60-bit word for ordinary precision requirements. We have not investigated what errors might

occur if less precision were used. We recommend testing the precision on a different machine by running the sample case for smaller and smaller values of the single-step integration error,  $W(42)$ , and verifying that the error value in the first column of the printout maintains at least the accuracy specified by  $W(42)$ . The level where that accuracy first breaks down is probably the precision limit imposed by the computer's word length.

### 3.2.3 Execution Speed

For many applications, HARPA runs fast enough on our CYBER 840 to allow virtually interactive (machine load permitting) ray tracing using a graphics terminal for editing program input and for viewing graphical output. Although HARPA may compile and run on smaller machines, its speed may be so slow that interactive ray tracing may no longer be practical. The run times shown on the printout (Appendix A) for the sample case (at the end of each ray) allow you to compare run times between your computer and ours. Tests on a CRAY XMP-48 indicate a factor of 7 speedup over a CYBER 840.

### 3.2.4 Graphics

The graphics programs included with HARPA were designed to run on the CYBER 700-800 series computer and use the DISSPLA graphics package (by ISSCO, Inc.) and a CDC 250 Microfilm Potting Unit. However, HARPA will run regardless of the plotting facilities you have.

If you have DISSPLA, you can produce the graphic output by running the supplementary program DDSPLA, supplied as File 6 of the distribution tape. This program reads a graphics metafile called TAPE5, which HARPA produces when plots are requested (see Fig. C1).

If you don't have DISSPLA, you can still run HARPA and get the printed and machine-readable outputs, but you won't get any graphics output. Just ignore the TAPE5 file. If you have other graphics devices, you can modify the DD-prefix plotting routines to drive them. PROGRAM DDALT (file 7 of the distribution tape) provides a framework for inserting custom plot-command calls. The functions of these routines and further details about the CDC 250 plot package and the DISSPLA interface are given in Appendix C.

### 3.3 Unpacking the Program Tape and File Organization

The distribution tape contains the seven files listed in Section 3.3.1. Section 7.1 gives a list of the programs and subroutines on the distribution tape. Normally, you would transfer all tape files to punched cards or permanent disk files, depending on which medium you will use to run the program.

Although HARPA continues to evolve, the source code on the distribution tape will always correspond exactly with the version described in this report. Updates and errata will be documented separately and included in a dated update tape file.

#### 3.3.1 Files on the HARPA Distribution Tape

File #:

1. FORTRAN source code for the Sample Case, including its models, ready to compile, with common and data blocks included.
2. Input Data File for the Sample Case.
3. FORTRAN source code for the "Ray-tracing Core" programs, including plotting (graphics-write) routines.
4. FORTRAN source code for four dispersion-relation routines.
5. FORTRAN source code for all atmospheric-model routines.
6. FORTRAN source code for program DDSPLA for reading the Graphics Output File (TAPE5) for users with DISSPLA.
7. FORTRAN source code for program DDALT, a skeleton routine for reading the Graphics Output File (TAPE5), allowing users to insert plotting modules for their own plotting system.

#### 3.3.2 Setting Up a Run Module

A run module is the subset of programs that you submit to your computer to run a particular application, along with the job-control commands your computer needs to compile and/or run a program. Files 1 and 2 of the distribution tape constitute the run module (minus the job-control cards) for the sample case. It consists of a core of routines (Sec. 7.1.1) that must always be present to trace rays, and a set of selectable routines (Secs. 7.1.2 and 7.1.3) that describe the particular model (those for the sample case in this example). Figure 3.1 shows a representative run module.

Job-control statements for your computer
Ray-tracing core
One dispersion-relation routine
Selected atmospheric-model routines
Input data file

Figure 3.1. Configuration of a run module, assembled from parts consisting either of disk-file modules or punched-card decks.

The selectable part of the run module means that you select only the routines that describe the model you want to use. The run module must contain one and only one (with exceptions noted) of the following kinds of model routines:

- a dispersion-relation routine
- a background sound-speed model
- a background wind model (if you use dispersion models AWWWL or AWWNL)
- a background terrain model
- a perturbation sound-speed model (NPSPEED does nothing)
- a perturbation wind model (NPWIND does nothing) (if you use dispersion models AWWWL or AWWNL)
- a perturbation terrain model (NPTERR does nothing)
- a receiver-surface model.

In addition, you need any other models that are called by any of the above routines, for example, background and temperature-perturbation models called by a sound-speed model (such as GAMRTDM). If you are using a version of the dispersion-relation routine that includes absorption (AWWWL or ANWWL), you will also need models for viscosity/thermal conductivity and pressure, or whatever other parameters it requires. Look at the bottom of the model input parameter forms (Appendix B) to see what other models a given model needs.

### 3.3.3 If You Are Using Cards To Input Data

If you have no permanent disk storage on your computer, you can load a previously compiled version of HARPA (if you don't change the program itself) into your computer from tape each time you want to run it, and have it read the Input Data File from punched cards. For each run, you have to edit the Input Data File (Deck) by punching new cards for the data you change from a previous run. The Input Data File is arranged in an 80-column format with one input parameter per card so that the deck is easy to edit if you have the contents of the cards interpreted (printed across the card tops).

### 3.3.4 If You Are Using Permanent Disk Files

It is far more convenient to store both the program and the Input Data File in permanent disk files. A run module (Fig. 3.1) can be constructed by a batch or procedure program that selects the appropriate routines from the HARPA "library." Procedure (or batch) programs also simplify the manipulation of HARPA input and output, but because they depend on the operating system you use, you will generally have to write your own procedures.

## 4. How to Construct An Atmospheric Model

The easy way to set up an atmospheric model is to select from a general-purpose set of models we have designed (Table 4.1) and choose the model parameters that fit your needs. This requires no programming whatsoever and we encourage that choice whenever possible. Alternatively, you can design your own atmospheric models by writing a FORTRAN subroutine that defines the atmospheric property and its spatial derivatives in a form that is compatible with the rest of the program. This chapter describes both ways.

### 4.1 Choosing From the Available Atmospheric Models

We have designed some generic atmospheric models that can be adapted to represent common atmospheric structures simply by selecting the appropriate model and its parameters in the Input Data File. They are closed-form expressions for an atmospheric property as a function of geographic latitude, longitude, and height; some accept input parameters in tabular form. There are models for wind, sound-speed and temperature fields, viscosity and thermal conductivity, pressure, molecular weight and terrain surfaces. Though not strictly considered part of the atmospheric model, three models for the receiver surface are also provided. All of these models are described in Appendix B.

Most of the models come in two kinds, "background" and "perturbation." Perturbation models generally superimpose more structure on a background model. Table 4.1 lists the atmospheric models that come with HARPA. To run HARPA, you always have to specify one background model and one perturbation model for each required atmospheric property, even if the perturbation is a do-nothing version.

To put together an atmospheric model from the subroutines we have supplied, first copy the FORM TO SPECIFY AN ATMOSPHERIC MODEL from Appendix B and fill in the name of a model you want to use for each atmospheric parameter, selecting from the choices listed in Table 4.1. Full mathematical descriptions of each model can be found in Appendix B on the order form listed under the model name, and FORTRAN listings for the model subroutines can be found in Appendix D. For now, leave off the numbers of the Data Set ID column until you have selected the models' parameters.

Table 4.1--Available atmospheric models

Model type number	Start of W array parameter block	Model check number	Subroutine name	Description
1.	100	1.	WLINEAR	Background wind models: Constant upward and northerly wind, linear easterly wind profile
		6.	ULOGZ2	Logarithmic atmospheric boundary layer profile
		9.	VVORTX3	Vertical, cylindrical wind vortex
		8.	WGAUSS2	Localized (Gaussian) zonal wind field
		5.	WTIDE	Zonal and meridional profiles that are harmonic in time and height and are in quadrature
2.	125	0.	NPWIND	Wind-perturbation models: Do-nothing version
3.	150	1.	GAMRTDM	Sound-speed models: $C^2 = \gamma RT/M$
		2.	CSTANH	Profile with linear segments joined by hyperbolic functions
4.	175	0.	NPSPEED	Sound-speed perturbation models: Do-nothing version
		2.	CBLOB2	Localized (Gaussian) temperature perturbation
5.	200	0.	NTEMP	Background temperature models: Do-nothing temperature model
		1.	TLINEAR	Linear temperature profile
		6.	TTABLE	Tabular temperature profile with cubic interpolation between points
		7.	TTANH5	Profile with linear segments joined by hyperbolic functions
6.	225	0.	NPTEMP	Temperature-perturbation models: Do-nothing version
		2.	TBLOB2	Localized (Gaussian) temperature perturbation
7.	250	1.	MCONST	Molecular weight models: Constant molecular weight

Table 4.1--Available atmospheric models (continued)

Model type number	Start of W array parameter block	Model check number	Subroutine name	Description
8.	275			Receiver-surface models:
		1.	RHORIZ	A sphere concentric with the earth
		2.	RTERR	A fixed height above the terrain
		3.	RVERT	A vertical surface at a specified fixed range from a specified geographic point
9.	300			Terrain models:
		1.	GHORIZ	A sphere concentric with the earth
		3.	GTANH	A profile of linear segments joined by hyperbolic functions
		4.	GLORENZ	An east-west Lorentzian-shaped ridge
10.	325			Terrain perturbations:
		0.	NPTERR	Do-nothing version
17.	500			Viscosity/thermal conductivity:
		1.	MUARDC	ARDC viscosity model, Prandtl number for thermal conductivity
18.	525			Viscosity/conductivity perturbation:
		0.	NPABS	Do-nothing version
19.	550			Atmospheric pressure:
		1.	PEXP	Exponential profile
20.	575			Pressure perturbation:
		0.	NPPRES	Do-nothing version

Next, select and copy the blank Input Parameter Forms from Appendix B for the models you have selected and fill in the values of the variable parameters that you want. Next transfer the input parameters to a new Input Data File, either constructing one from scratch, according to the format shown in Figure 2.5, or modifying an old one. (If you use an old one, make sure that unused parameters are removed.) Remember to assign an input data-set identification number (F7.3 FORMAT), which uniquely identifies that set of input parameters for each model, and to assign an Atmospheric Identification (ID) for the entire

set of models. Put these ID numbers on the FORM TO SPECIFY AN ATMOSPHERIC MODEL and save all these forms as a record of the models you have defined.

Here are a few guidelines for selecting models. If you want a model with no temperature variation, use TLINEAR and set the gradient to zero. If you want a model with no wind, use no wind model and select a dispersion-relation routine with no wind (ANWNL or ANWWL). If you specify any temperature model, you have to use model GAMRTDM, which simply converts temperature to sound speed. If you want to specify a sound-speed field only (such as CSTANH), don't use any temperature model, in which case you don't need GAMRTDM. You can also specify a background model in terms of temperature or sound speed (but not both), and perturbations in terms of temperature or sound speed or both (as in the sample case). If you want no perturbation model for wind speed, temperature, sound speed, or terrain, use the corresponding do-nothing perturbation models NPTEMP, NPWIND, NPSPEED, or NPTERR.

If you are storing HARPA on a permanent disk file, you have to select only the subroutines that define your atmospheric model (and the correct dispersion-relation routine) and assemble them into a separate "run module" (Section 3.3.2). If you are storing the programs on punched cards, you should select and submit only the decks for the model subroutines you want to use. It is convenient to think of HARPA as consisting of a core of ray-tracing routines that are always used, and a set of selectable model-related routines from which you select the ones appropriate to the models you want. The specific routines that fall into each category are listed in Chapter 7.

#### 4.1.1 Model Check Numbers

To guard against accidentally selecting the wrong model subroutine for a run module, each model is assigned a permanent Model Check Number, which is entered on each model input data form (Appendix B). If a model subroutine is selected whose Check Number does not match that specified in the Input Data File, then the program will stop and give an error message.

Another number, called the Input Data Format Code, is not now being used or checked, but may be used in the future.

#### 4.1.2 Tabular Input to Models

Some models, like TTANH5 and TTABLE, can accept so many input parameters that it is inconvenient to specify each one as a separate line in the Input Data File, so a general provision has been made for entering data in tabular form. The use of TTANH5 in the sample case is an example. Tabular data are entered into the Input Data File in a special format illustrated by Figure 2.19 and described fully in Chapter 5.

#### 4.2 Designing Your Own Models

HARPA will accept any atmospheric model specification that provides the desired atmospheric property as a function of the earth-centered spherical-polar coordinates  $r, \theta, \phi$  and time  $t$ , as well as its spatial and temporal derivatives. There are three important considerations in writing model subroutines: (a) All spatial derivatives must be not only continuous but also analytically consistent with the formulas for the atmospheric property itself; any errors or approximations in those calculations will result in larger-than-desired integration errors, as displayed in the first column of the ray-tracing printout. (b) The input data for the models must come from the part of the W array assigned to that type of model (Table 4.1) and from the tabular-input common blocks assigned to those models (Table 4.2). (c) The output from the atmospheric model must go to the appropriate data-output common block (Table 4.3). Because the model routines are called many times, efficient programming here pays off in execution efficiency.

If you want a new model of wind, temperature, or sound speed that depends only on height, you would normally design a new background model. If you want a three-dimensional model, you could use one of the background models we have supplied and design a new perturbation model. Conceivably, you could design both a new background and a new perturbation model, but the safe way to proceed is to do one at a time.

Those designing a new model should pattern their subroutine after a similar one that comes with HARPA. We will use the model TTANH5 (Fig. 4.1), as an example and discuss its structure in detail to illustrate how to write a model subroutine. In the following paragraphs, general statements will be followed in square brackets by the specific examples from TTANH5.

Table 4.2--Allocation of common blocks for tabular input to the various atmospheric models\*

Common block name	Atmospheric model
/B1/	Wind velocity
/B2/	Perturbation to the wind velocity
/B3/	Sound speed
/B4/	Perturbations to the sound speed
/B5/	Temperature
/B6/	Perturbations to the temperature
/B7/	Molecular weight
/B8/	Receiver surface
/B9/	Terrain
/B10/	Terrain perturbation
/B17/	Viscosity/thermal conductivity
/B18/	Viscosity/conductivity perturbation
/B19/	Pressure
/B20/	Pressure perturbation

\* In the first 31 elements of each of these common blocks, each atmospheric model indicates the structure of the rest of the common block. Subroutine READW1 stores input data that it reads starting in element 32 of the common block.

Table 4.3--Allocation of common blocks for output from the various atmospheric models

Common block name	Location of description (table number)	Atmospheric model
/UU/	7.10	Wind velocity
/CC/	7.11	Sound speed
/TT/	7.12	Temperature
/MM/	7.13	Molecular weight
/RR/	7.14	Receiver surface
/GG/	7.15	Terrain
/AA/	7.16	Viscosity/thermal conductivity
/PP/	7.17	Atmospheric pressure

There are no restrictions on naming models, but it is useful to assign a name that suggests the model's function. [TTANH5 is the fifth temperature model that used TANH functions to smooth temperature profiles with linear segments. Square brackets enclose examples of parameters for the TTANH5 routine.] Each model subroutine has two entry points whose standard names are given in Table 4.4. These names must be used when designing new subroutines. The first entry point [ENTRY IPTEMP], whose name begins with an "I," is for initialization after new input data have been read in, and that entry point is called the first time the program enters the subroutine. The second entry point [ENTRY TEMP] enters the routine for subsequent computations of the atmospheric parameter [T] and its time and space derivatives [PTT, PTR, PTH, PTPH] according to the formulas given on the model order form.

The input to each subroutine (geographic coordinates  $r, \theta, \phi$ ) is through blank common, and output [temperature and its derivatives] is through the labeled common blocks [/TT/], named for each kind of model and listed in Table 4.3. If you need more input parameters than will fit in the assigned block of the Input Data Table [200-224], then you should use a tabular input format, which uses the labeled common blocks [B5] listed in Table 4.2. Tabular

	SUBROUTINE TTANH5	TTANH5 9
C	TEMPERATURE PROFILE REPRESENTED BY A SEQUENCE OF LINEAR SEGMENTS	TTANH510
C	SMOOTHLY JOINED BY HYPERBOLIC FUNCTIONS. PARAMETERS ARE INPUT	TTANH511
C	AS TABULAR DATA WITH SLOPES COMPUTED FROM TEMPERATURE DATA.	TTANH512
C	REFERENCE TEMPERATURE TO IS READ FROM TABULAR DATA.	TTANH513
	DIMENSION C(20), TM(19), Z(19), DL(19)	TTANH514
C	COMMON DECK "RKAM" INSERTED HERE	RKAMCOM2
	REAL KR, KTH, KPH	RKAMCOM4
	COMMON//R, TH, PH, KR, KTH, KPH, RKVARS(14), TPULSE, CSTEP, DRDT(20)	RKAMCOM5
C	COMMON DECK "TT" INSERTED HERE	CTT 2
	REAL MODT	CTT 4
	COMMON/TT/MODT(4), T, PTT, PTR, PTTT, PTPH	CTT 5
C	COMMON DECK "WW" INSERTED HERE	CWW 2
	PARAMETER (NWARSZ=1000)	CWW1 3
	COMMON/WW/ID(10), MAXW, W(NWARSZ)	CWW1 4
	REAL MAXSTP, MAXERR, INTYP, LLAT, LLON	CWW2 2
	EQUIVALENCE (EARTH, W(1)), (RAY, W(2)), (XMTRH, W(3)), (TLAT, W(4)),	CWW2 3
	1 (TLON, W(5)), (OW, W(6)), (FBEG, W(7)), (FEND, W(8)), (FSTEP, W(9)),	CWW2 4
	2 (AZ1, W(10)), (AZBEG, W(11)), (AZEND, W(12)), (AZSTEP, W(13)),	CWW2 5
	3 (BETA, W(14)), (ELBEG, W(15)), (ELEND, W(16)), (ELSTEP, W(17)),	CWW2 6
	8 (RCVRH, W(20)),	CWW2 7
	4 (ONLY, W(21)), (HOP, W(22)), (MAXSTP, W(23)), (PLAT, W(24)), (PLON, W(25))	CWW2 8
	5, (HMAX, W(26)), (RAYFNC, W(29)), (EXTINC, W(33)),	CWW2 9
	6 (HMIN, W(27)), (RGMAX, W(28)),	CWW2 10
	8 (INTYP, W(41)), (MAXERR, W(42)), (ERATIO, W(43)),	CWW2 11
	6 (STEP1, W(44)), (STPMAX, W(45)), (STPMIN, W(46)), (FACTR, W(47)),	CWW2 12
	7 (SKIP, W(71)), (RAYSET, W(72)), (PRTSRP, W(74)), (HITLET, W(75))	CWW2 13
	9, (BINRAY, W(76)), (PAGLN, W(77)), (PLT, W(81)), (PFACTR, W(82)),	CWW2 14
	1 (LLAT, W(83)), (LLON, W(84)), (RLAT, W(85)), (RLON, W(86))	CWW2 15
	2, (TIC, W(87)), (HB, W(88)), (HT, W(89)), (TICV, W(96))	CWW2 16
	REAL MMODEL, MFORM, MID	CWW3 2
C		CWW3 3
C	WIND 100-124	CWW3 4
	EQUIVALENCE (W(100), UMODEL), (W(101), UFORM), (W(102), UID)	CWW3 5
C		CWW3 6
C	DELTA WIND 125-149	CWW3 7
	EQUIVALENCE (W(125), DUMODEL), (W(126), DUFORM), (W(127), DUID)	CWW3 8
C		CWW3 9
C	SOUND SPEED 150-174	CWW3 10
	EQUIVALENCE (W(150), CMODEL), (W(151), CFORM), (W(152), CID)	CWW3 11
	EQUIVALENCE (W(153), REFC)	CWW3 12
C		CWW3 13
C	DELTA SOUND SPEED 175-199	CWW3 14
	EQUIVALENCE (W(175), DCMODEL), (W(176), DCFORM), (W(177), DCID)	CWW3 15
C		CWW3 16
C	TEMPERATURE 200-224	CWW3 17
	EQUIVALENCE (W(200), TMODEL), (W(201), TFORM), (W(202), TID)	CWW3 18
C		CWW3 19
C	DELTA TEMPERATURE 225-249	CWW3 20
	EQUIVALENCE (W(225), DTMODEL), (W(226), DTFORM), (W(227), DTID)	CWW3 21
C		CWW3 22
C	MOLECULAR 250-274	CWW3 23
	EQUIVALENCE (W(250), MMODEL), (W(251), MFORM), (W(252), MID)	CWW3 24
C		CWW3 25
C	RECEIVER HEIGHT 275-299	CWW3 26
	EQUIVALENCE (W(275), RMODEL), (W(276), RFORM), (W(277), RID)	CWW3 27

Figure 4.1. Listing for model temperature subroutine TTANH5.

C		CWW3	28
C	TOPOGRAPHY 300-324	CWW3	29
	EQUIVALENCE (W(300),GMODEL),(W(301),GFORM),(W(302),GID)	CWW3	30
C		CWW3	31
C	DELTA TOPOGRAPHY 325-349	CWW3	32
	EQUIVALENCE (W(325),GUMODEL),(W(326),GUFORM),(W(327),GUID)	CWW3	33
C		CWW3	34
C	UPPER SURFACE TOPOGRAPHY 350-374	CWW3	35
	EQUIVALENCE (W(350),SMODEL),(W(351),SFORM),(W(352),SID)	CWW3	36
C	PLOT ENHANCEMENTS CONTROL PARAMETERS	CWW3	37
C		CWW3	38
	EQUIVALENCE (W(490),XFQMDL),(W(491),YFQMDL)	CWW3	39
C	ABSORPTION 500-524	CWW3	40
	EQUIVALENCE (W(500),AMODEL),(W(501),AFORM),(W(502),AID)	CWW3	41
C		CWW3	42
C	DELTA ABSORPTION 525-549	CWW3	43
	EQUIVALENCE (W(525),DAMODEL),(W(526),DAFORM),(W(527),DAID)	CWW3	44
C		CWW3	45
C	PRESSURE 550-574	CWW3	46
	EQUIVALENCE (W(550),PMODEL),(W(551),PFORM),(W(552),PID)	CWW3	47
C		CWW3	48
C	DELTA PRESSURE 575-599	CWW3	49
	EQUIVALENCE (W(575),DPMODEL),(W(576),DPFORM),(W(577),DPID)	CWW3	50
C		CWW3	51
C	COMMON DECK "B5" INSERTED HERE	CB5	2
	INTEGER TMX,TNTBL,TITBL,TFRMTBL,IDST(10)	CB5	4
	COMMON/B5/TMX,TNTBL(10),TITBL(10),TFRMTBL(10),TGP(262)	CB5	5
	EQUIVALENCE (TGP,IDST),(ANT,TGP(11))	CB5	6
	EQUIVALENCE (Z0,TGP(12)),(TM,TGP(33))	TTANH519	
	EQUIVALENCE (Z,TGP(13)),(C,TGP(32)),(DL,TGP(53))	TTANH520	
C		TTANH521	
	DATA RECOGT,N/7.0,0/	TTANH522	
	DATA ANT/0.0/	TNH5BL 2	
	DATA TMX/2/	TNH5BL 3	
	DATA TNTBL/1,11,72,7*0/	TNH5BL 4	
	DATA TITBL/1,20,8*0/	TNH5BL 5	
	DATA TFRMTBL/1,2,8*0/	TNH5BL 6	
C		TTANH525	
	COSH (X) = (EXP (X) + 1. / (EXP (X))) / 2.	TTANH526	
C		TTANH527	
	ENTRY ITEMP	TTANH528	
C		TTANH529	
	CALL IPTMP	TTANH530	
C		TTANH531	
C	IF HAD PREVIOUS CALL BUT NOTHING THIS TIME, EXIT NOW	TTANH532	
C	RETAINING PREVIOUS TABULAR DATA COUNT	TTANH533	
	IF(N.GT.0 .AND. ANT.EQ.0.0) RETURN	TTANH534	
C		TTANH535	
	IF(RECOGT .NE. TMODEL)	TTANH536	
	1 CALL RERROR('TEMP ', 'WRNG MODEL',RECOGT)	TTANH537	
C		TTANH538	
	MODT(1)=7HTTANH5	TTANH539	
	MODT(2)=TID	TTANH540	
C		TTANH541	
	N=(ANT+1)/3 - 2	TTANH542	
C		TTANH543	
	IF(N.LE.0)	TTANH544	
	1 CALL RERROR('TTANH5', 'BAD N VALUE',FLOAT(N))	TTANH545	
C		TTANH546	

Figure 4.1. Listing for model temprature subroutine TTANH5 (continued).

C	ANT=0.0	TTANH547
C		TTANH548
C	CONVERT 'T' ARRAY INPUT(OVERLAYS 'C' ARRAY) TO 'C' ARRAY	TTANH549
C		TTANH550
	TO=C(1)	TTANH551
	TIM1=TO	TTANH552
	ZIM1=0.0	TTANH553
	NP1=N+1	TTANH554
	DO 10 I=1, NP1	TTANH555
	TI=TM(I)	TTANH556
	ZI=Z(I)	TTANH557
	C(I)=(TI-TIM1)/(ZI-ZIM1)	TTANH558
10	TIM1=TI	TTANH559
C	ZIM1=ZI	TTANH560
		TTANH561
	RETURN	TTANH562
C		TTANH563
	ENTRY TEMP	TTANH564
	H = R - EARTH	TTANH565
	SUM = 0.	TTANH566
C		TTANH567
C	LOOP TO SUM OVER ALL COEFFICIENTS	TTANH568
C	USE SPECIAL FUNCTION 'ALCOSH' WHICH ALLOWS FOR LARGE ARGUMENTS.	TTANH569
	DO 1 I = 1, N	TTANH570
1	SUM = SUM + DL(I) * (C(I + 1) - C(I)) / 2. * (ALCOSH((H - Z	TTANH571
	1(I)) / DL(I)) - ALCOSH((Z(I)-Z0) / DL(I)))	TTANH572
	T = TO + SUM + (C(1) + C(N + 1)) * (H - Z0) * 0.5	TTANH573
	SUM = 0.	TTANH574
	DO 2 I = 1, N	TTANH575
2	SUM = SUM + (C(I + 1) - C(I)) / 2. * (1. + TANH ((H - Z(I)) / DL	TTANH576
	1 (I)))	TTANH577
	PTT=0.0	TTANH578
	PTR = C(1) + SUM	TTANH579
	PTTH=0.0	TTANH580
	PTPH=0.0	TTANH581
C		TTANH582
	CALL PTEMP	TTANH583
	RETURN	TTANH584
	END	TTANH585
		TTANH586

Figure 4.1. Listing for model temperature subroutine TTANH5 (continued).

Table 4.4--Assignment of entry point names and input parameter blocks in the W array for the atmospheric models

Atmospheric model	Entry point names	Input parameter block in the W array
Wind	WINDR, IWINDR	100-124
Wind perturbation	PWINDR, IPWINDR	125-149
Sound-speed	SPEED, ISPEED	150-174
Sound speed perturbation	PSPEED, IPSPEED	175-199
Temperature	TEMP, ITEMP	200-224
Temperature perturbation	PTEMP, IPTEMP	225-249
Molecular weight	MOLWT, IMOLWT	250-274
Receiver surface	RECVR, IRECVR	275-299
Terrain	TOPOG, ITOPOG	300-324
Terrain perturbation	PTOPOG, IPTOPOG	325-349
Viscosity/thermal conductivity	ABSRP, IABSRP	500-524
Viscosity/thermal conductivity perturbation	PABSRP, IPABSRP	525-549
Pressure	PRES, IPRES	550-574
Pressure perturbation	PPRES, IPPRES	575-599

data are read into this common block from the Input Data File according to the format described in Chapter 5 and illustrated near the end of Figure 2.19 for the sample case.

#### 4.2.1 How To Write an Atmospheric Model Subroutine So It Can Receive Tabular Data Read Into Common Blocks by READW1

If you want to write an atmospheric model subroutine that uses tabular input data, then you have to observe some special precautions. In what follows, general statements are exemplified in square brackets for the case of the temperature subroutine TTANH5. You can use this example as a guide in developing new model subroutines that use tabular data.

Tabular [temperature] data are read into a model-related common block [/B5/] by READW1. Table 4.3 gives the names of the common blocks associated with the different model types. The format of the tabular input data can be selected by the user and is determined by a code [3] in columns 1-3 of the Input Data File (see Figure 2.19). [In the case of TTANH5, a three-column format makes sense because there are three input parameters]. READW1 interprets this code according to the formats listed in Table 5.4. The model subroutine [TTANH5] must tell READW1 how it wants the tabular input data stored in the common block [B5] in an array [TGP]. It does so by setting (in DATA statements) the values in variable TMX and in arrays TNTBL, TITBL and TFRMTBL for temperature models (or corresponding names for other model types, in which the first letter is different). The model variables [Z0, TM, C, DL] are EQUIVALENCED to elements of a GP (for general-purpose) array [called TGP for temperature models]. Table 4.5 defines the structure of common block /B5/, which transmits these variables between READW1 and TTANH5, and it explains how to set the data-block parameters.

#### 4.2.2 Designing Your Own Terrain Models

A terrain model specifies a function  $g(r, \theta, \phi)$  such that  $g=0$  on the terrain,  $g>0$  above the terrain, and  $g<0$  below the terrain. To be an allowed model,  $g$  must be continuous through second derivatives. A subroutine for a terrain model must calculate  $g$ , its three first derivatives, and its six second derivatives for any values of  $r, \theta, \phi$ . All of our present terrain models define  $g$  to be the height above the terrain, but more general definitions are allowed to handle cliffs, overhangs, and caves. To design a simple model with a few parameters, follow the example of SUBROUTINE GLORENZ. To design a more elaborate model that needs tabular input data, follow the example of SUBROUTINE GTANH. Source-Code listings for these models are in Appendix D.

**Table 4.5--Definitions of the parameters in common block /B5/\***

Position common	Variable name	Definition
1	TMX	Maximum number of data blocks in /B5/
2-11	TNTBL	An array that contains the beginning location of data blocks within the common block
2	TNTBL(1)	Beginning location (in TGP array) of data block 1
3	TNTBL(2)	Beginning location (in TGP array) of data block 2
4	TNTBL(3)	Beginning location (in TGP array) of data block 3**
12-21	TITBL	An array that contains the iteration (or cycle) length of the data in the data blocks within the common block (if there is more than one array in the data block, then this is the dimension of the arrays)
12	TITBL(1)	Cycle length of data block 1
13	TITBL(2)	Cycle length of data block 2
22-31	TFRMTBL	An array that contains the input format numbers for the data blocks within the common block
22	TFRMTBL(1)	Format type*** for data block 1
23	TFRMTBL(2)	Format type*** for data block 2
32-	TGP	An array containing TMX number of data blocks for tabular input data for atmospheric models

\* The values of the first 31 elements in /B5/ define the block structure for the array TGP, and they are defined in the atmospheric models and used in the data read-in routines READW and READW1. The common blocks /B1/, /B2/, /B3/, /B4/, /B6/, and /B7/ have the same structure as /B5/, but have different names for the variables.

\*\* Only two data blocks are now available to use; however, the beginning location of the first data block not used must be specified to indicate the length of the last data block used.

\*\*\* Format type 1 implies format number 1 (see Table 5.3).  
 Format type 2 implies format numbers 2, 3, or 4 (see Table 5.3).



## 5. How to Specify the Input Data and Set Up an Input Data File

To give HARPA an atmospheric model and to tell it what rays to trace, you have to construct an Input Data File, like the one shown in Figure 5.1 (same as Figure 2.19, reproduced here for the user's convenience) for the sample case. An Input Data File may contain one or more "run sets," each of which can specify a different atmospheric model, different plotting modes, or different initial ray conditions, but which will all be executed as a single computer run. The sample case contains two run sets. After the first run set, only the parameters whose values differ from those specified in the preceding run set need be specified.

After setting up an Input Data File, you run HARPA by combining it with other ray-tracing modules to form a "run module," as explained in Section 3.3.2. All the necessary modules to run the sample case are contained in Files 1 and 2 of the distribution tape (Sec. 3.3.1).

### 5.1 Editing the Input Data File

Because HARPA contains no built-in way to construct or edit an Input Data File, you have to use an editor of your own to do so. We have designed a specialized editor, called WMOD, for this purpose. It not only permits editing the Input Data File, but it also sets up a "run module" that includes job-submission procedures for our computer. This program, which could run on a local microcomputer, will be documented in another report.

The Input Data File can take the form of either a deck of punched cards or a disk file to be read by HARPA. Some suggestions for those using punched cards are given in Section 3.3.3. Henceforth, we will assume that the Input Data File will be created as a disk file. There are no formal differences between the two methods, however.

Rather than start from scratch, we recommend that you modify an existing Input Data File. After you have run the sample case and have verified that its output agrees with that given in Appendix A, you can modify the Input Data File for the sample case to make the raypath calculations you want.

col. 1-3 n	col. 4-17 W(n)	col. 18-24 UNITS	col. 25-80 DESCRIPTION
GEORGES	RB3	X6437	
S03-1	SAMPLE	CASE FOR HARPA DOCUMENTATION	REV. 2-10-86
1	6370.		EARTH RADIUS, KM (6370.)
3	13.		TTRANSMITTER HEIGHT, KM (T=ABOVE TERRAIN)
4	200.	AN KM	N. TRANSMITTER LATITUDE, KM
5	0.	AN KM	E. TRANSMITTER LONGITUDE, KM
7	.05	FQ HZ	INITIAL FREQUENCY, HZ
11	45.	AN DG	INITIAL AZIMUTH ANGLE, DEG
15	-20.	AN DG	INITIAL ELEVATION ANGLE, DEG
16	140.	AN DG	FINAL ELEVATION ANGLE, DEG
17	5.	AN DG	STEP IN ELEVATION ANGLE, DEG
20	5.		RECEIVER HEIGHT, KM
22	3.		MAXIMUM NUMBER OF HOPS (1.0)
23	1000.		MAXIMUM NUMBER OF STEPS PER HOP (1000.)
26	500.		MAXIMUM RAY HEIGHT, KM (500.)
27	-1.		MINIMUM RAY HEIGHT, KM
28	1000.		MAXIMUM RANGE, KM
29	0000100.		DO: EIGRAY/RNG-TIM/RNG-ELV/NEW-PROJ/RAYTRC/CONT/PROF
33	999.999		MAXIMUM ABSORPTION, DB (999.999)
42	1.0E-6		SINGLE-STEP INTEGRATION ERROR (1.0E-4)
44	.1		INITIAL INTEGRATION STEP SIZE, KM (1.0)
57	2.		PHASE PATH (0=NO; 1=INTEGRATE; 2=INTEGRATE/PRINT)
58	2.		ABSORPTION (0=NO; 1=INTEGRATE; 2=INTEGRATE/PRINT)
60	2.		PATH LENGTH (0=NO; 1=INTEGRATE; 2=INTEGRATE/PRINT)
71	50.		NUMBER OF INTEGRATION STEPS PER PRINT [1.E31]
72	1.		OUTPUT RAYSETS (1=YES; 0=NO)
73	0.		DIAGNOSTIC PRINTOUT (1=YES; 0=NO)
74	0.		PRINT RAY STEPS (0=YES; 1=NO)
75	.15		FULANN LETTER HEIGHT [0.15 IN]
76	0.		BINARY RAY OUTPUT (1=YES; 0=NO)
77	57.		LINES PER PAGE IN PRINTOUT (66.)
81	1.		RAYPLOT PROJECTION (1=VERT; 2=HORIZ) PLANE
82	1.		PLOT-EXPANSION FACTOR [1.0]
83	-100.	AN KM	N. LATITUDE OF LEFT PLOT EDGE, KM
84	-300.	AN KM	E. LONGITUDE OF LEFT PLOT EDGE, KM
85	500.	AN KM	N. LATITUDE OF RIGHT PLOT EDGE, KM
86	300.	AN KM	E. LONGITUDE OF RIGHT PLOT EDGE, KM
87	100.	AN KM	DISTANCE BETWEEN TIC MARKS, KM
88	0.		HEIGHT ABOVE SEA LEVEL OF BOTTOM OF GRAPH, KM
89	300.		HEIGHT ABOVE SEA LEVEL OF TOP OF GRAPH, KM
96	100.		DISTANCE BETWEEN VERTICAL TIC MARKS, KM
100	6.		ULOGZ2 WIND MODEL CHECK NUMBER
102	3.		BACKGROUND WIND DATA SET ID
103	5.	LN M	REFERENCE WIND SPEED, M/S
104	.35		VON KARMAN'S CONSTANT
105	1.		ROUGHNESS HEIGHT, KM
150	1.		GAMRTDM SOUND SPEED MODEL CHECK NUMBER
175	2.		CBLOB2 MODEL CHECK NUMBER
177	2.		SOUND SPEED PERTURBATION DATA SET ID
178	.5		FRACTIONAL INCREASE OF SQUARED SOUND SPEED

Figure 5.1. Input Data File (W array) for the sample case.

```

179      125.          HEIGHT OF MAXIMUM INCREASE, KM
180      335.      AN KM  N. LATITUDE OF MAXIMUM INCREASE, KM
181      125.      AN KM  E. LONGITUDE OF MAXIMUM INCREASE, KM
182      25.          GAUSSIAN WIDTH IN HEIGHT OF INCREASE, KM
183      50.      AN KM  N-S WIDTH OF THE INCREASE, KM
184      25.      AN KM  E-W WIDTH OF THE INCREASE, KM
200      7.          TTANH5 TEMPERATURE MODEL CHECK NUMBER
202      1.          BACKGROUND TEMPERATURE DATA SET ID
225      2.          TBLOB2 MODEL CHECK NUMBER
227      2.          TEMPERATURE PERTURBATION DATA SET ID
228      .5          FRACTIONAL TEMPERATURE INCREASE
229      0.          HEIGHT OF MAXIMUM INCREASE, KM
230      105.     AN KM  N. LATITUDE OF MAXIMUM INCREASE, KM
231     -105.     AN KM  E. LONGITUDE OF MAXIMUM INCREASE, KM
232      0.          GAUSSIAN WIDTH IN HEIGHT OF INCREASE, KM
233      50.      AN KM  N-S WIDTH OF THE INCREASE, KM
234      25.      AN KM  E-W WIDTH OF THE INCREASE, KM
250      1.          MCONST MOLECULAR WEIGHT MODEL CHECK NUMBER
252      29.         MOLECULAR WEIGHT DATA SET ID
253      29.         MOLECULAR WEIGHT
275      2.          RTERR RECEIVER MODEL CHECK NUMBER
300      4.          GLORENZ TERRAIN MODEL CHECK NUMBER
302      2.          TERRAIN MODEL DATA SET ID
303      2.          HEIGHT OF THE RIDGE, KM
304      0.          N. LATITUDE OF THE RIDGE CENTER
305      30.      AN KM  HALF-WIDTH OF THE RIDGE, KM
325      0.          NPERR NO TERRAIN PERTURBATION
500      1.          MUARDC VISC/COND MODEL CHECK NUMBER
502      1.          VISC/COND MODEL DATA SET ID
503      1.458E-06  VISCOSITY COEFFICIENT BETA
504      110.4      SUTHERLAND'S CONSTANT, KELVINS
505      .733      PRANDTL NUMBER
525      0.          NPABS NO VISC/COND PERTURBATION
550      1.          PEXP PRESSURE MODEL CHECK NUMBER
552      1.          BACKGROUND PRESSURE MODEL DATA SET ID
553     101328.    PRESSURE AT SEA LEVEL, N/SQ.M.
554      8.5       PRESSURE SCALE HEIGHT, KM
575      0.          NPPRES NO PRESSURE PERTURBATION
-1      DATA SUBSET FOR BACKGROUND WIND MODEL
A      LOGARITHMIC EASTWARD WIND PROFILE, U*=.5 M/S, Z0=1 KM
0      RETURN TO W ARRAY DATA SET
-2      DATA SUBSET FOR WIND PERTURBATION MODEL
A      NO WIND PERTURBATION
0      RETURN TO W ARRAY DATA SET
-3      DATA SUBSET FOR BACKGROUND SOUND-SPEED MODEL
A      SOUND SPEED IN TERMS OF TEMPERATURE MODEL
0      RETURN TO W ARRAY DATA SET
-4      DATA SUBSET FOR SOUND-SPEED PERTURBATION MODEL
A      50% INCREASE IN SQ. SOUND SPEED AT 125KM HT, 335KM N, 125KM E
0      RETURN TO W ARRAY DATA SET
-5      DATA SUBSET FOR TEMPERATURE MODEL
A      U.S. STANDARD ATMOSPHERE 1962 TEMPERATURE PROFILE
3      999.0
LN KM          LN KM
0.            288.000      0.

```

Figure 5.1. Input Data File (W array) for the sample case (continued).

```

15.0000      190.500      10.0000
52.0000      320.000      7.50000
95.0000      191.000      10.0000
165.0000     1451.000     50.0000
300.0000     1586.000      0.
999.0000
0      RETURN TO W ARRAY DATA SET
-6      DATA SUBSET FOR TEMPERATURE PERTURBATION MODEL
A 50% CYLINDRICAL INCREASE IN TEMPERATURE AT 105KM N., 105 KM W
0      RETURN TO W ARRAY DATA SET
-7      DATA SUBSET FOR MOLECULAR WEIGHT MODEL
A MOLECULAR WEIGHT = 29
0      RETURN TO W ARRAY DATA SET
-8      DATA SUBSET FOR RECEIVER SURFACE MODEL
A RECEIVER SURFACE 5 KM ABOVE TERRAIN
0      RETURN TO W ARRAY DATA SET
-9      DATA SUBSET FOR TERRAIN MODEL
A RIDGE 2-KM HIGH, 30-KM WIDE ALONG EQUATOR
0      RETURN TO W ARRAY DATA SET
-10     DATA SUBSET FOR TERRAIN PERTURBATION MODEL
A NO TERRAIN PERTURBATION
0      RETURN TO W ARRAY DATA SET
-17     DATA SUBSET FOR VISC/COND MODEL
A ARDC VISCOSITY AND THERMAL CONDUCTIVITY MODEL
0      RETURN TO W ARRAY DATA SET
-18     DATA SUBSET FOR VISC/COND PERTURBATION MODEL
A NO VISCOSITY/CONDUCTIVITY PERTURBATION
0      RETURN TO W ARRAY DATA SET
-19     DATA SUBSET FOR BACKGROUND PRESSURE MODEL
A EXPONENTIAL PRESSURE MODEL, SCALE HEIGHT = 8.5 KM
0      RETURN TO W ARRAY DATA SET
-20     DATA SUBSET FOR PRESSURE PERTURBATION MODEL
A NO PRESSURE PERTURBATION
0      RETURN TO W ARRAY DATA SET
0      ***** END OF RUN SET NUMBER 1 *****
S03-2    SAMPLE CASE FOR HARPA DOCUMENTATION      REV. 2-10-86
71      0.      NUMBER OF INTEGRATION STEPS PER PRINT
72      0.      OUTPUT RAYSETS (1=YES; 0=NO)
73      1.      DIAGNOSTIC PRINTOUT (1=YES; 0=NO)
81      2.      RAYPLOT PROJECTION (1=VERT; 2=HORIZ) PLANE
82      3.      PLOT-EXPANSION FACTOR
0      ***** END OF RUN SET NUMBER 2 *****

```

Figure 5.1. Input Data File (W array) for the sample case (continued).

The best way to be sure you have input all the required data is to fill out the forms for specifying all the model and ray parameters, as discussed for the sample case in Chapter 2. Then translate the data from those forms into the format of the Input Data File. We provide blank forms for all models and procedures in Appendix B.

## 5.2 Input Data Formats

The Input Data File is read by a FORTRAN program and so must conform to precise format specifications. Originally, the Input Data File consisted of a deck of 80-column punched cards, with one input parameter per card, so the data format is still specified in terms of data fields in card-image columns, even though cards are no longer used. Figure 5.1 for the sample case is an example of the proper format.

Looking at Figure 5.1 you will notice that the first part of the file consists of a series of lines that begin with a positive integer. Each of these lines specifies an element of a Data Input Array,  $W(n)$ . This format goes as far as the line that begins with 575. At the line beginning with -1, the data format changes to accept tabular input data. First, we will explain how to specify data to be read into  $W(n)$ ; then we will explain how to enter data in the tabular format.

## 5.3 Specifying the W-Array Input

The W-array input format consists of a single 80-column line with four data fields:  $n$ ,  $W(n)$ , unit conversion characters, and a description field.

The first three card-image columns contain the first data field in I3 format and specify the index,  $n$ , of the array  $W(n)$ . The value of  $n$  must be between 0 and 999, and if there are fewer than three digits, the entry must be right-justified, or else trailing zeroes will be appended to fill out the three columns. If two or more lines begin with the same value of  $n$ , the last one prevails.

The second field, columns 4-17, contains the value of  $W(n)$  in E14.7 format. The value can be entered in either E or F format, but if the E format is used, the exponent must be right-justified within the 14 spaces, or else zeroes will be appended.

The third field, columns 18-24, contains characters that tell the program to convert the units of the data, as input, to units used by the program. The present choices available for input in this field are given in Table 5.1; the characters must be input in exactly the columnar format shown.

Table 5.1--Units conversion on input

Units of input value*	Meaning	Conversion needed	Value stored by read-in routine
AN RD	Angle in radians	None	$V_i$
AN DG	Angle in degrees	degs to radians or deg/s to rad/s	$V_i \pi/180^{**}$
AN KM	Central earth angle in kilometers	km to rad	$V_i/r_e^{***}$
LN KM	Length in kilometers	None	$V_i$
LN M	Length in meters	m to km	$V_i/1000$
LN NM	Length in nautical miles	nmi to km	$1.852 V_i$
LN FT	Length in feet	ft to km	$3.048006096 \times 10^{-4} V_i$
FQ HZ	Frequency in hertz	Hz to rad/s	$2\pi V_i$
FQ S	Frequency expressed as a period in seconds	Period in s to frequency in rad/s	$2\pi/V_i$
T****	Transmitter height relative to terrain instead of sea level	Add terrain height to transmitter height	$V_i$ (also, a flag is set)****

\* The five characters listed are to be put in card-image columns 18 through 22 of the W-array input value to be converted, or put above the data-input column of tabular input. For three-column tabular input, for example, the five characters should be in columns 1-13, 14-26 and 27-39. The five characters are automatically put in the appropriate place when using the WMOD editor.

\*\*  $V_i$  is the input value.

\*\*\*  $r_e$  is the radius of the earth. The current value of W(1) in the W array is used for this conversion.

\*\*\*\* Applies only for input to W(3) (transmitter height). The "T" must be put in card-image column 24.

\*\*\*\*\* At the start of each ray, the status of the flag is checked. If the flag is set, then the terrain height at the longitude and latitude of the transmitter is added to the transmitter height. For general terrain models, the terrain height at a given longitude and latitude can only be estimated. For all of the presently available terrain models, the estimate gives an exact result, however, because  $\partial g/\partial r$  is constant.

The fourth field (columns 25-80) contains descriptive comments, which aid the user in setting up the table. These comments are optional and arbitrary as far as HARPA is concerned, but for  $n \geq 100$  and divisible by 25, the first word in the comment field is read when WMOD is used for editing and must be a valid model name. This convention will be described in a report about the supplementary programs. Where practical, the comments should describe the function of all acceptable values of the parameter, not just the present value, so that the comment would not have to be changed when the parameter is changed. We have included nonzero initial values in the comment field, where applicable. To make it easier to see the model groupings, we have adopted the convention of indenting the comments that describe model parameters.

### 5.3.1 Initialization of the Input Data Parameters

Before reading the Input Data File, the program initializes all of the input parameters,  $W(n)$ . Most are set to zero, but a few are given nonzero initial values that correspond to common usage. An example is the latitude of north pole of the computational coordinate system,  $W(24)$ , which usually has a value of  $\pi/2$ . Section 5.3.2 denotes those nonzero initial values by parentheses. These initial values can be overridden by the Input Data File (including a value of zero), but if no value is specified for a  $W(n)$  in the Input Data File, then its initial value prevails.

In addition, some initial values are given "zero-override" priority, which means that  $W(n)$  assumes its nonzero initial value if no value is input, but also if a zero is input. This zero override operates when a zero value would produce meaningless results or cause difficulty in program execution. An example is the plot expansion factor,  $W(82)$ . Section 5.3.2 denotes by square brackets the nonzero initial values that override zero.

To help the user keep track of the unit conversions and initializations, all nonzero  $W(n)$  values, in the units actually used by HARPA, are listed at the beginning of the printout (Appendix A). In the examples given above, if  $W(24)$  were given a value of zero in the Input Data File, no value would be printed for  $W(24)$ . On the other hand, if  $W(82)$  is given a zero value in the Input Data File, a message is printed indicating "INPUT OVERRIDDEN," and the non-zero override value is printed.

### 5.3.2 Explanation of the Input Data Parameters

Because HARPA has evolved from ray-tracing programs for other media, some values of the input parameter index,  $n$ , are not used in HARPA, but may be used in other versions of the program. As far as possible,  $n$  is assigned consistently among the different versions, and blocks of  $n$  are assigned to groups of related parameters.

A list is given next of all the parameters used by HARPA, with a description of their meanings and idiosyncrasies. Those with nonzero initial values need not be entered in the Input Data File, if the value is what you want. If no initial value is indicated, a zero will be assigned if you leave it out of the Input Data File. The default units given in parentheses are those which are assumed if no unit conversions are put into columns 18-24. Also included in the table is the FORTRAN name (where one exists) assigned (in EQUIVALENCE statements) to each variable in the program. Those labeled "not used" can be assigned to additional input parameters, but those labeled "used by other programs" or "used internally" should not be used.

- W(1) EARTH (6370.) -- Radius (kilometers) of the earth. Can be set to a very large value for a "flat-earth" approximation.
- W(2) RAY -- Used by other programs.
- W(3) XMTRH -- Height (kilometers) of the transmitter (source) above sea level. If there is a T in column 24, it is the height above the terrain.
- W(4) TLAT -- North geographic latitude (radians) of the transmitter. Can be entered in kilometers (or degrees) by putting AN KM (or AN DG) beginning in column 18.
- W(5) TLON -- East geographic longitude (radians) of the transmitter. Can be entered in kilometers (or degrees) by putting AN KM (or AN DG) beginning in column 18.
- W(6) OW -- Used internally.
- W(7) FBEG -- Initial acoustic wave frequency (rad/s). Can be entered in Hz (or period in seconds) by putting FQ HZ (or FQ S) beginning in column 18.
- W(8) FEND -- Final frequency (rad/s). Can be entered in Hz (or period in seconds) by putting FQ HZ (or FQ S) beginning in column 18.
- W(9) FSTEP -- Step in frequency (rad/s). Can be entered in Hz (or period in seconds) by putting FQ HZ (or FQ S) beginning in col 18. Set = 0 for no stepping.

- W(10) AZ1 -- Used internally.
- W(11) AZBEG -- Initial azimuth angle (radians east of north) of transmission. Can be entered in degrees by putting AN DG beginning in column 18.
- W(12) AZEND -- Final azimuth angle (radians east of north) of transmission. Can be entered in degrees by putting AN DG beginning in column 18.
- W(13) AZSTEP -- Step in azimuth angle (radians east of north) of transmission. Can be entered in degrees by putting AN DG beginning in column 18. Set = 0 for no stepping.
- W(14) BETA -- Used internally.
- W(15) ELBEG -- Initial elevation angle (radians above horizontal) of transmission. Can be entered in degrees by putting AN DG beginning in column 18.
- W(16) ELEND -- Final elevation angle (radians above horizontal) of transmission. Can be entered in degrees by putting AN DG beginning in column 18.
- W(17) ELSTEP -- Step in elevation angle (radians) of transmission. Can be entered in degrees by putting AN DG beginning in column 18. Set = 0 for no stepping.
- W(18)-W(19) -- Not used.
- W(20) RCVRH -- Height (kilometers) above sea level of the receiver surface when model RHORIZ is used; height of the receiver surface above the terrain when model RTERR is used.
- W(21) ONLY -- Set = 0 to stop frequency increment when ray goes out of bounds (applies only when elevation and azimuth angles are not stepped).
- W(22) HOP -- Maximum number of ray hops (intersections with or closest approaches to the receiver surface); ray calculation stops when reached, printing MAX HOPS. Closest approaches count as two hops.
- W(23) MAXSTP (1000.) -- Maximum number of integration steps per hop; ray calculation stops when reached, printing STEP MAX.
- W(24) PLAT ( $\pi/2$ ) -- Geographic latitude (radians) of the north pole of the computational coordinate system.
- W(25) PLON -- Geographic longitude (radians) of the north pole of the computational coordinate system.
- W(26) HMAX (500.) -- Maximum ray height (kilometers) above sea level; ray calculation stops if exceeded, printing MAX HT.
- W(27) HMIN -- Minimum ray height (kilometers) above sea level; calculation stops if ray goes below this height, printing MIN HT.
- W(28) RGMAX -- Maximum ground range (kilometers at sea level) of the ray from the transmitter; ray calculation stops if exceeded, printing MAX RANG.

- W(29) RAYFNC -- A set of seven binary digits to select execution of HARPA and supplementary programs. To run HARPA, use 100. Setting = 0 is the same as all ones and will run HARPA.
- W(30)-W(32) Used by other programs.
- W(33) EXTINC (999.999) -- Maximum absorption (dB); ray calculation stops if value exceeded, printing EXTINC. Set = 0 for no maximum.
- W(34)-W(40) -- Not used.
- W(41) INTYP (3.): Integration type:  
= 1 for Runge-Kutta integration without error checking;  
= 2 for Adams-Moulton integration without error checking;  
= 3 for Adams-Moulton integration with relative-error checking;  
= 4 for Adams-Moulton integration with absolute-error checking.
- W(42) MAXERR (1.E-4) -- Maximum allowable integration error per step. RKAM routine decreases step size to achieve this error.
- W(43) ERATIO (50.) [50.] -- Ratio of maximum to minimum single-step integration error; RKAM increases step size when error is smaller than W(42) by this factor.
- W(44) STEP1 (1.0) -- Initial integration step size (seconds).
- W(45) STPMAX (100.) -- Maximum integration step size (seconds).
- W(46) STPMIN (1.E-8) -- Minimum integration step size (seconds).
- W(47) FACTR (.5) [0.5] -- Factor multiplying integration step size when decreasing step size.
- W(48)-W(56) Not used.
- W(57) -- Phase-time integration: 0 to not integrate; 1 to integrate; 2 to integrate and print.
- W(58) -- Absorption integration: 0 to not integrate; 1 to integrate; 2 to integrate and print.
- W(59) -- Doppler shift integration: 0 to not integrate; 1 to integrate; 2 to integrate and print.
- W(60) -- Path-length integration: 0 to not integrate; 1 to integrate; 2 to integrate and print.
- W(61)-W(70) -- Assigned to future integration options.
- W(71) SKIP -- [1.E31] Number of integration steps between printed lines. Set = 1 to print every step; = 0 to suppress periodic printing.
- W(72) RAYSET -- Write machine-readable raysets to file PUNCH -- 1 = yes; 0 = no.

W(73) PCNTRW -- Add diagnostic printout lines: 1 = yes; 0 = no.

W(74) PRTSRP -- Produce normal printout every W(71) steps -- 0 = yes; 1 = no.  
Also produces printout at special events.

W(75) HITLET [.15] -- Height (inches on our plotter) of lettering on graphs.  
"FULANN" in description field activates publication-quality lettering on  
graphs when read by WMOD. Any other comment in description field produces  
draft-quality lettering.

W(76) BINRAY -- Write binary raypath description to file TAPE6 -- 1 = yes;  
0 = no.

W(77) PAGLIN (66.) -- Page length (lines) for printout.

W(78)-W(79) -- Not used.

W(80) APOG, PRIGEE -- 0 for normal rayplots; 1 for apogee plots.

W(81) PLT: Rayplot projection:  
1 = vertical plane, polar projection, rectangular expansion;  
2 = horizontal plane, lateral expansion;  
3 = vertical plane, polar plot, radial expansion;  
4 = vertical plane, rectangular plot.  
Make negative to superimpose plot on that from previous sunset.

W(82) PFACTW [1.] -- Vertical or lateral expansion factor for rayplot.

W(83) LLAT -- North latitude (radians) of left edge of plot. To enter in  
degrees (kilometers) put AN DG (AN KM) beginning in column 18.

W(84) LLOE -- East longitude (radians) of left edge of plot. To enter in  
degrees (kilometers) put AN DG (AN KM) beginning in column 18.

W(85) RLAT -- North latitude (radians) of right edge of plot. To enter in  
degrees (kilometers) put AN DG (AN KM) beginning in column 18.

W(86) RLOE -- East longitude (radians) of right edge of plot. To enter in  
degrees (kilometers) put AN DG (AN KM) beginning in column 18.

W(87) TIC -- Distance (radians) between tick marks on horizontal axis of plot.  
To enter in kilometers, put AN KM beginning in column 18.

W(88) HB -- Height (kilometers) of the bottom of the graph above sea level.

W(89) HT -- Height (kilometers) of the top of the graph above sea level.

W(90)-W(95) -- Used by other programs.

W(96) TICV -- Distance (kilometers) between tick marks on vertical axis of  
plot. Notice that the default units are kilometers for the vertical ticks  
and radians for the horizontal ticks.

W(97)-W(99) -- Used by other programs.

W(100) UMODEL -- Check number for background wind model.  
W(101) UFORM -- format code for background wind model.  
W(102) UID -- Data-set ID for background wind model.  
W(103)-W(124) -- Parameters for background wind model.

W(125) DUMODEL -- Check number for perturbation wind model.  
W(126) DUFORM -- Format code for perturbation wind model.  
W(127) DUID -- Data-set perturbation wind model.  
W(128) W(149) -- Parameters for perturbation wind model.

W(150) CMODEL -- Check number for background sound speed model.  
W(151) CFORM -- Format code for background sound speed model.  
W(152) CID -- Data-set ID for background sound speed model.  
W(153) W(174) -- Parameters for background sound speed model.

W(175) DCMODEL -- Check number for perturbation sound speed model.  
W(176) DCFORM -- Format code for perturbation sound speed model.  
W(177) DCID -- Data-set for perturbation sound speed model.  
W(178) W(199) -- Parameters for perturbation sound speed model.

W(200) TMODEL -- Check number for background temperature model.  
W(201) TFORM -- Format code for background temperature model.  
W(202) TID -- Data-set ID for background temperature model.  
W(203) W(224) -- Parameters for background temperature model.

W(225) DTMODEL -- Check number for perturbation temperature model.  
W(226) DTFORM -- Format code for perturbation temperature model.  
W(227) DTID -- Data-set ID for perturbation temperature model.  
W(228) W(249) -- Parameters for perturbation temperature model.

W(250) MMODEL -- Check number for molecular weight model.  
W(251) MFORM -- Format code for molecular weight model.  
W(252) MID -- Data-set ID for molecular weight model.  
W(253) W(274) -- Parameters for molecular weight model.

W(275) RMODEL -- Check number for receiver surface model.  
W(276) RFORM -- Format code for receiver surface model.  
W(277) RID -- Data-set ID for receiver surface model.  
W(278) W(299) -- Parameters for receiver surface model.

W(300) GMODEL -- Check number for background terrain model.  
W(301) GFORM -- Format code for background terrain model.  
W(302) GID -- Data-set ID for background terrain model.  
W(303) W(324) -- Parameters for background terrain model.

W(325) DGMODEL -- Check number for perturbation terrain model.  
W(326) DGFORM -- Format code for perturbation terrain model.  
W(327) DGID -- Data-set ID for perturbation terrain model.  
W(328) W(349) -- Parameters for perturbation terrain model.

W(400) W(500) Parameters for supplementary programs.

W(500) AMODEL -- Check number for viscosity/conductivity model.  
W(501) AFORM -- Format code for viscosity/conductivity model.  
W(502) AID -- Data-set ID for viscosity/conductivity model.  
W(503) W(524) -- Parameters for viscosity/conductivity model.

W(525) DAMODEL -- Check number for perturbation viscosity/conductivity model.  
W(526) DAFORM -- Format code for perturbation viscosity/conductivity model.  
W(527) DAID -- Data-set ID for perturbation viscosity/conductivity model.

W(528) W(549) -- Parameters for perturbation viscosity/conductivity model.

W(550) PMODEL -- Check number for background pressure model.

W(551) PFORM -- Format code for background pressure model.

W(552) PID -- Data-set ID for background pressure model.

W(553) W(574) -- Parameters for background pressure model.

W(575) DPMODEL -- Check number for perturbation pressure model.

W(576) DPFORM -- Format code for perturbation pressure model.

W(577) DPID -- Data-set ID for perturbation pressure model.

W(578) W(599) -- Parameters for perturbation pressure model.

W(600) W(999) -- Assigned to future atmospheric models

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## 5.4 Specifying Tabular Input

In addition to providing values to the W(n) array, the Input Data File lets you enter tabular data to be used by atmospheric model subroutines. In the following discussion, refer to the Input Data File for the sample case (Fig. 5.1) for examples of tabular data.

### 5.4.1 Changing to the Tabular Format

When the sign of the W-array index n is read (in columns 1-3), it is checked for a valid negative value, which signals a change in the format of the data to follow. Any valid negative value selects a corresponding "input common block" that has been dedicated to a particular model subroutine. Table 5.2 shows which values select which common blocks. The line in Figure 5.1 that begins with -1 and has the comment "ENTER DATA SUBSET FOR BACKGROUND WIND MODEL" is an example selecting common block /B1/ to receive data. Because this line must conform to the W-array format, comments must begin after column 24.

Table 5.2--Description of the identifying numbers in the first three columns of the Input Data File

Code number	Prefix for common-block variables*	Description
1-999		Input to elements 1-999 of the W array as described in Table 4.4 and Section 5.3.2
-1	U	Signals start of tabular input to common block /B1/ (wind velocity) (see Table 4.2)
-2	DU	Signals start of tabular input to common block /B2/ (perturbation wind velocity)
-3	C	Signals start of tabular input to common block /B3/ (sound speed)
-4	DC	Signals start of tabular input to common block /B4/ (perturbation sound speed)
-5	T	Signals start of tabular input to common block /B5/ (temperature)
-6	DT	Signals start of tabular input to common block /B6/ (perturbation temperature)
-7	M	Signals start of tabular input to common block /B7/ (molecular weight)
-8	R	Signals start of tabular input to common block /B8/ (receiver surface)
-9	G	Signals start of tabular input to common block /B9/ (terrain)
-10	DG	Signals start of tabular input to common block /B10/ (terrain perturbation)
-17	V	Signals start of tabular input to common block /B17/ (viscosity/conductivity)
-18	DV	Signals start of tabular input to common block /B18/ (viscosity/conductivity perturbation)
-19	PR	Signals start of tabular input to common block /B19/ (pressure)
-20	DP	Signals start of tabular input to common block /B20/ (pressure perturbation)
0		Signals end of tabular input to one of the above common blocks, or if that is not appropriate, end of the input data

\* See Table 4.5.

#### 5.4.2 The Format Line

The line following the negative value of  $n$  begins with an integer that specifies the format of the data to follow. The formats are numbered according to the method shown in Table 5.3.

Format A is alphanumeric and lets you enter descriptive comments on the rest of the line that begins with the format number. That comment is reproduced at the beginning of the program printout. The comment "LOGARITHMIC EASTWARD WIND PROFILE" in Figure 5.1 is an example.

Formats 1, 2, and 3 specify 1, 2, and 3 columns, respectively, of floating-point numbers. If formats 1, 2, or 3 are selected, then columns 4-16 of the format line must contain an end-of-data terminator, such as 999.0 in the sample case. The rest of the format line can contain comments describing the tabular data.

#### 5.4.3 The Units Line

The line following the format line is a line containing unit-conversion specifications for the columnar data to follow. The conversion specifications follow the conventions described in Table 5.1. The 5 characters must be placed in the same 13-character columns as the tabular data to be converted with the extra condition that at least one space must separate adjacent conversion specifications.

#### 5.4.4 The Data Lines

Any number of data lines can follow the format line. They must contain numeric data in the format specified in the format line and must be terminated with the number given in the format line as specifying end-of-data. Data values are read until the terminator is encountered. The data following the "U.S. STANDARD ATMOSPHERE 1962 TEMPERATURE PROFILE" comment in Figure 5.1 is an example of 3-column data entry (format 3) into the common block /B5/, which contains data used by temperature model TTANH5. If the number of data values read in exceeds the maximum allocated in the model subroutine, an error will occur and the program will stop.

Table 5.3--Tabular input data formats available\*

Format number	Data block	Format	Data read	Cycle length	Number of columns	Number of arrays in data block
0	1	I3	Indicates end of data read into the common block	NA	NA	NA
A	1	I3,10A8	Format number,** alphanumeric data that describe the atmospheric model	1	NA	1
1	1	I3,G13.6	Format number,*** terminator data read consecutively into the data block spaced by the cycle length	Equals dimension of arrays in data block	1	Usually 1
	last	G13.6	Terminator indicates end of data for this data block			
2	1 2-	I3,G13.6	Format number,*** terminator data read consecutively into the data block spaced by the cycle length	Equals dimension of arrays in data block	2	Usually 2
	last	2G13.6	Terminator indicates end of data for this data block			
3	1 2-	I3,G13.6	Format number,*** terminator data read consecutively into the data block spaced by the cycle length	Equals dimension of arrays in data block	3	Usually 3
	last	3G13.6	Terminator indicates end of data for this data block			

\* Except for format A, the structure of the data block is a single variable (whose value will be set equal to the number of data values read in to the data block) followed by the data block arrays. This structure must be set up in the subroutines that define the atmospheric model in question.

\*\* Format A implies the data will go into data block 1.

\*\*\* Format numbers 1 through 6 imply the data will go into data block 2. The maximum number of columns is now 6.

#### 5.4.5 The Return Line

After the end-of-data number signifies the end of tabular input, you will usually put a line beginning with a 0 in column 3 to return to the W-array data format.

## PART III: HOW THE PROGRAM WORKS

### 6. The Ray-Tracing Equations

#### 6.1 Hamilton's Equations in Spherical Polar Coordinates

HARPA calculates raypaths by numerically integrating Hamilton's equations. Lighthill (1965, 1978) gives Hamilton's equations in four dimensions (three spatial and one temporal) for Cartesian coordinates. Haselgrove (1954) gives Hamilton's equations in three dimensions for spherical polar coordinates, a more useful coordinate system for geophysical media. Combining the two gives Hamilton's equations in four dimensions in which the three spatial coordinates are earth-centered spherical polar (see Table 6.1 for a definition of the symbols):

$$\frac{dr}{d\tau} = \frac{\partial H}{\partial k_r}, \quad (6.1)$$

$$\frac{d\theta}{d\tau} = \frac{1}{r} \frac{\partial H}{\partial k_\theta}, \quad (6.2)$$

$$\frac{d\phi}{d\tau} = \frac{1}{r \sin\theta} \frac{\partial H}{\partial k_\phi}, \quad (6.3)$$

$$\frac{dt}{d\tau} = - \frac{\partial H}{\partial \omega}, \quad (6.4)$$

$$\frac{dk_r}{d\tau} = - \frac{\partial H}{\partial r} + k_\theta \frac{d\theta}{d\tau} + k_\phi \sin\theta \frac{d\phi}{d\tau}, \quad (6.5)$$

$$\frac{dk_\theta}{d\tau} = \frac{1}{r} \left( - \frac{\partial H}{\partial \theta} - k_\theta \frac{dr}{d\tau} + k_\phi r \cos\theta \frac{d\phi}{d\tau} \right), \quad (6.6)$$

$$\frac{dk_\phi}{d\tau} = \frac{1}{r \sin\theta} \left( - \frac{\partial H}{\partial \phi} - k_\phi \sin\theta \frac{dr}{d\tau} - k_\phi r \cos\theta \frac{d\theta}{d\tau} \right), \quad (6.7)$$

$$\frac{d\omega}{d\tau} = \frac{\partial H}{\partial t}. \quad (6.8)$$

The variables  $r$ ,  $\theta$ ,  $\phi$  are the (Earth-centered) spherical polar coordinates of a point on the raypath;  $k_r$ ,  $k_\theta$ , and  $k_\phi$  are the local Cartesian components of the propagation vector (a vector whose magnitude,

Table 6.1--The more important symbols and their definitions

---

A	In Section 6.1.2, absorption in dB
C	Sound speed
C <sub>ref</sub>	A reference sound speed (= .344 km/s)
f	Wave frequency (in Hz)
Δf	Frequency shift of a wave due to a time-varying medium
H	Hamiltonian
k <sub>r</sub> , k <sub>θ</sub> , k <sub>φ</sub>	Components of the propagation vector in the r, θ, φ directions--a vector normal to the wave front having a magnitude $2\pi/\lambda = \omega/v$
k <sub>disp</sub>	Complex wave number determined by the dispersion relation
M	Mean molecular atmospheric weight (the average is over molecular constituents)
P	Phase path length, phase of the wave divided by the reference wave number ( $2\pi/\lambda_0 = \omega/C_{ref}$ )
P'	Group path length = $C_{ref}t$
p	Atmospheric pressure
R	Gas constant = $8.31436 \times 10^{-3} \text{ kg (kg mole)}^{-1} \text{ km}^2 \text{ s}^{-2} \text{ K}^{-1}$
r, θ, φ	Spherical polar coordinates of a raypath point
s	Geometric raypath length
T	Atmospheric temperature
t	Time of travel of a wave packet (in some cases, used to express the time dependence of the propagation medium)
V	Wind velocity
V <sub>r</sub> , V <sub>θ</sub> , V <sub>φ</sub>	Components of the wind velocity in the r, θ, φ direction
v	Wave phase velocity
γ	= 1.4, the ratio of specific heat at constant pressure to that at constant density
θ	Colatitude in spherical polar coordinates
λ	Wavelength
λ <sub>0</sub> = $(2\pi/\omega)C_{ref}$	Reference wavelength
ρ	Atmospheric density
τ	Independent variable in Hamilton's equations (no physical significance)
φ	Longitude in spherical polar coordinates
Ω	= $\omega - \vec{k} \cdot \vec{V}$ , the intrinsic wave frequency, the wave frequency as seen by an observer moving with the medium
ω = 2πf	Radian wave frequency
Δω = 2πΔf	Radian frequency shift

---

$$k = \sqrt{k_r^2 + k_\theta^2 + k_\phi^2} = 2\pi/\lambda \quad , \quad (6.9)$$

is the wave number, and that points in the wave normal direction) in the r, θ, and φ directions; t is time--in (6.4) it is the propagation time of a wave packet; in (6.8) it expresses the variation with time of a time-varying medium; τ is a parameter whose value depends on the choice of the Hamiltonian H. Section 6.4 explains how the Hamiltonian is defined.

For actual calculation, HARPA uses group path  $P' = C_{ref} t$  (where  $C_{ref}$  is a standard reference speed) as the independent variable because the derivatives with respect to  $P'$  are independent of the choice of Hamiltonian, allowing the program to switch Hamiltonians in the middle of a path. This choice automatically causes the program to take smaller steps in real path length where the calculations are more critical, as when refractive index varies rapidly. These equations are obtained by dividing (6.1) through (6.8) by  $C_{ref}$  times (6.4):

$$\frac{dr}{dP'} = - \frac{1}{C_{ref}} \frac{\partial H / \partial k_r}{\partial H / \partial \omega} , \quad (6.10)$$

$$\frac{d\theta}{dP'} = - \frac{1}{r C_{ref}} \frac{\partial H / \partial k_\theta}{\partial H / \partial \omega} , \quad (6.11)$$

$$\frac{d\phi}{dP'} = - \frac{1}{r C_{ref} \sin\theta} \frac{\partial H / \partial k_\phi}{\partial H / \partial \omega} , \quad (6.12)$$

$$\frac{dk_r}{dP'} = \frac{1}{C_{ref}} \frac{\partial H / \partial r}{\partial H / \partial \omega} + k_\theta \frac{d\theta}{dP'} + k_\phi \sin\theta \frac{d\phi}{dP'} , \quad (6.13)$$

$$\frac{dk_\theta}{dP'} = \frac{1}{r} \left( \frac{1}{C_{ref}} \frac{\partial H / \partial \theta}{\partial H / \partial \omega} - k_\theta \frac{dr}{dP'} + k_\phi r \cos\theta \frac{d\phi}{dP'} \right) , \quad (6.14)$$

$$\frac{dk_\phi}{dP'} = \frac{1}{r \sin\theta} \left( \frac{1}{C_{ref}} \frac{\partial H / \partial \phi}{\partial H / \partial \omega} - k_\phi \sin\theta \frac{dr}{dP'} - k_\theta r \cos\theta \frac{d\theta}{dP'} \right) , \quad (6.15)$$

$$\frac{d(\Delta f)}{dP'} = \frac{1}{2\pi} \frac{d\Delta\omega}{dP'} = \frac{1}{2\pi} \frac{d\omega}{dP'} = - \frac{1}{2\pi} \frac{\partial H / \partial t}{\partial H / \partial \omega} . \quad (6.16)$$

Equation (6.16) for the frequency shift of a wave propagating through a time-varying medium follows directly from Hamilton's equations (6.4) and (6.8). An alternative derivation is given by Bennett (1967). Large frequency shifts should be accumulated along the raypath and the shifted frequency used in calculations at each point on the raypath. Equations (6.1) through (6.8) imply that all eight dependent variables vary along the path, and that at each point on the path the instantaneous value of all parameters (including frequency) is used in further evaluations of the equations. However, the time variation of the atmosphere due to natural causes is so slow that the resulting frequency shifts have negligible effect on the propagation. For this reason, HARPA calculates frequency shift to compare with

frequency-shift measurements, but does not adjust the frequency of the wave used in the propagation calculations.

The first six differential equations, (6.10) through (6.15), are always integrated. By setting W(59), the user can choose whether to have the program integrate (6.16) to calculate the frequency shift.

### 6.1.1 Phase Path

Three other quantities can be calculated by integration along the ray-path. The phase path  $P$  (phase divided by the reference wave number  $2\pi/\lambda_0 = \omega/C_{\text{ref}}$ ) is calculated by integrating

$$\begin{aligned} \frac{dP}{dP'} &= \frac{C_{\text{ref}}}{\omega} \left( k_r \frac{dr}{dP'} + k_\theta r \frac{d\theta}{dP'} + k_\phi r \sin\theta \frac{d\phi}{dP'} \right) \\ &= - \frac{1}{\omega} \frac{k_r \frac{\partial H}{\partial k_r} + k_\theta \frac{\partial H}{\partial k_\theta} + k_\phi \frac{\partial H}{\partial k_\phi}}{\partial H / \partial \omega} \end{aligned} \quad (6.17)$$

### 6.1.2 Absorption

If the absorption per wavelength is small (as it must be for this type of ray tracing to be valid), then an approximate formula can be integrated to give the absorption in decibels:

$$\begin{aligned} \frac{dA}{dP'} &= - \frac{10}{\log_e 10} \frac{\omega}{C_{\text{ref}}} \frac{\text{imag}(k_{\text{disp}}^2)}{k_r^2 + k_\theta^2 + k_\phi^2} \frac{dP}{dP'} \\ &= \frac{10}{\log_e 10} \frac{\text{imag}(k_{\text{disp}}^2)}{k_r^2 + k_\theta^2 + k_\phi^2} \frac{k_r \frac{\partial H}{\partial k_r} + k_\theta \frac{\partial H}{\partial k_\theta} + k_\phi \frac{\partial H}{\partial k_\phi}}{C_{\text{ref}} \partial H / \partial \omega} \end{aligned} \quad (6.18)$$

where  $k_{\text{disp}}$  is the (complex) wave number determined by the dispersion relation. If you want to include the effects of absorption from some independent formula for absorption, then you can add that as a new equation to HAMLTN.

The appropriate equation would be

$$dA/dP' = \omega/C_{\text{ref}} \alpha/k_{\text{real}} dP/dP' \quad (6.19)$$

where  $\alpha$  is an absorption in dB/km, and  $A$  will be the absorption in dB.

### 6.1.3 Path Length

The geometrical path length of the ray can be calculated by integrating

$$\frac{ds}{dP'} = \sqrt{\left(\frac{dr}{dP'}\right)^2 + r^2 \left(\frac{d\theta}{dP'}\right)^2 + r^2 \sin^2 \theta \left(\frac{d\phi}{dP'}\right)^2}$$

$$= \frac{\sqrt{\left(\frac{\partial H}{\partial k_r}\right)^2 + \left(\frac{\partial H}{\partial k_\theta}\right)^2 + \left(\frac{\partial H}{\partial k_\phi}\right)^2}}{c_{ref} |\partial H / \partial \omega|} \quad (6.20)$$

The user can choose to integrate and print frequency shift, phase time, absorption, or path length using Equations (6.16), (6.17), (6.18), or (6.20) by setting the appropriate values of W(59), W(57), W(58), W(60), respectively, in the Input Data File (Figure 2.19).

The user can add differential equations to the program by modifying HAMLTN, the subroutine that evaluates Hamilton's equations.

The Hamiltonian and its derivatives are calculated by one of the versions of dispersion-relation subroutine (with entry point DISPER), which also calculates  $k_{disp}^2$ .

## 6.2 Numerical Integration

Subroutines RKAM and RKAM1 integrate the differential equations numerically using an Adams-Moulton predictor-corrector method with a Runge-Kutta starter. RKAM1 was adapted from a program in the CDC CO-OP library called RKAMSUB, written by G. J. Lastman and dated March 1964. The program executes one integration step by one of four methods the user can specify using W(41). The subroutine is called once for each advance of the independent variable. The flow charts of Figures 6.1 through 6.5 show how the integration routine works.

Usually, RKAM1 is run in mode 3, that is, Adams-Moulton integration with relative-error checking. The user can trade execution time for accuracy by varying the single-step integration error, W(42). RKAM1 will increase or decrease the step length to maintain the specified error. Table 6.2 gives an

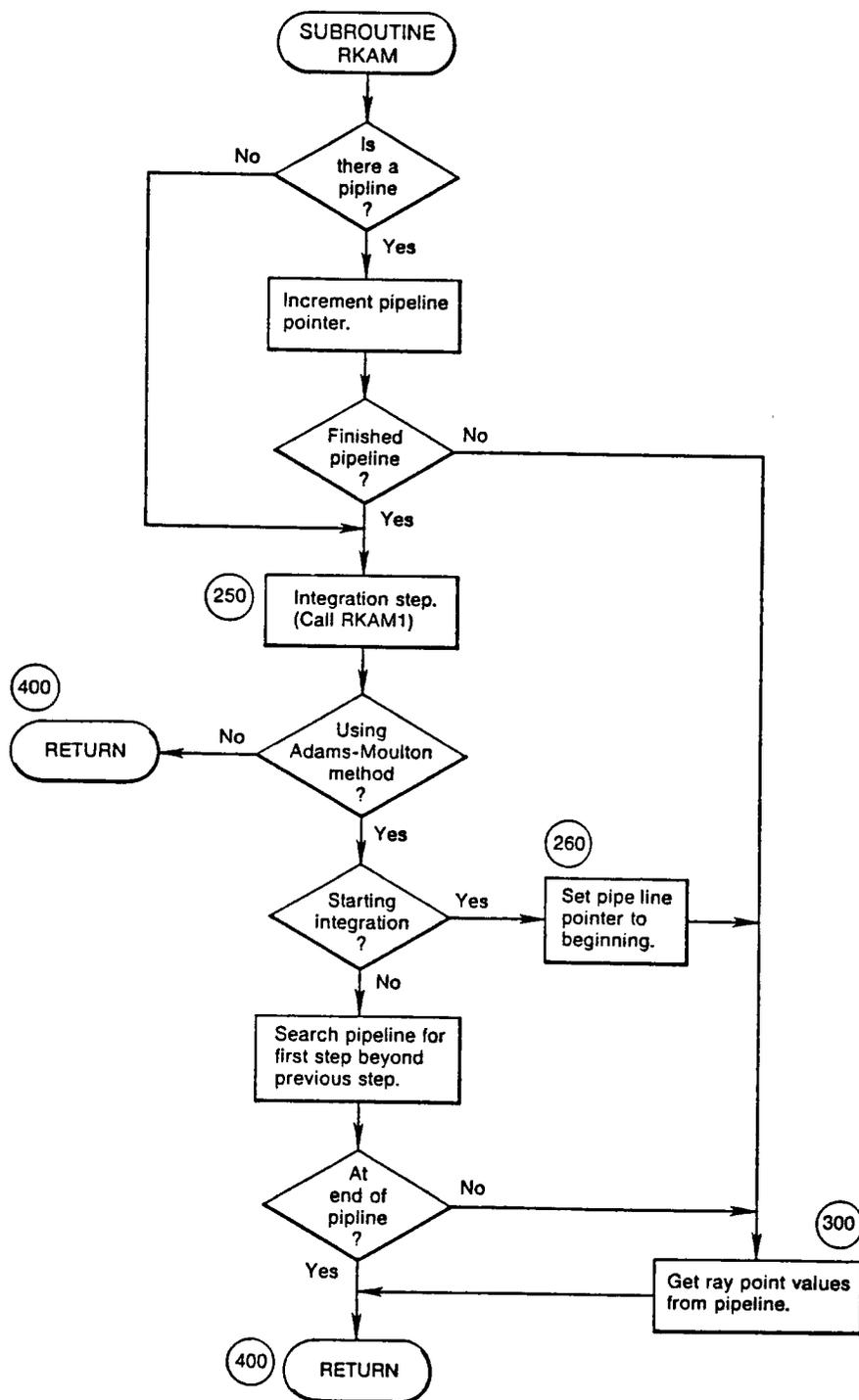


Figure 6.1. Flow chart for subroutine RKAM. The term "pipeline" refers to the sequence of four consecutive integration steps kept by the Adams-Moulton integration method.

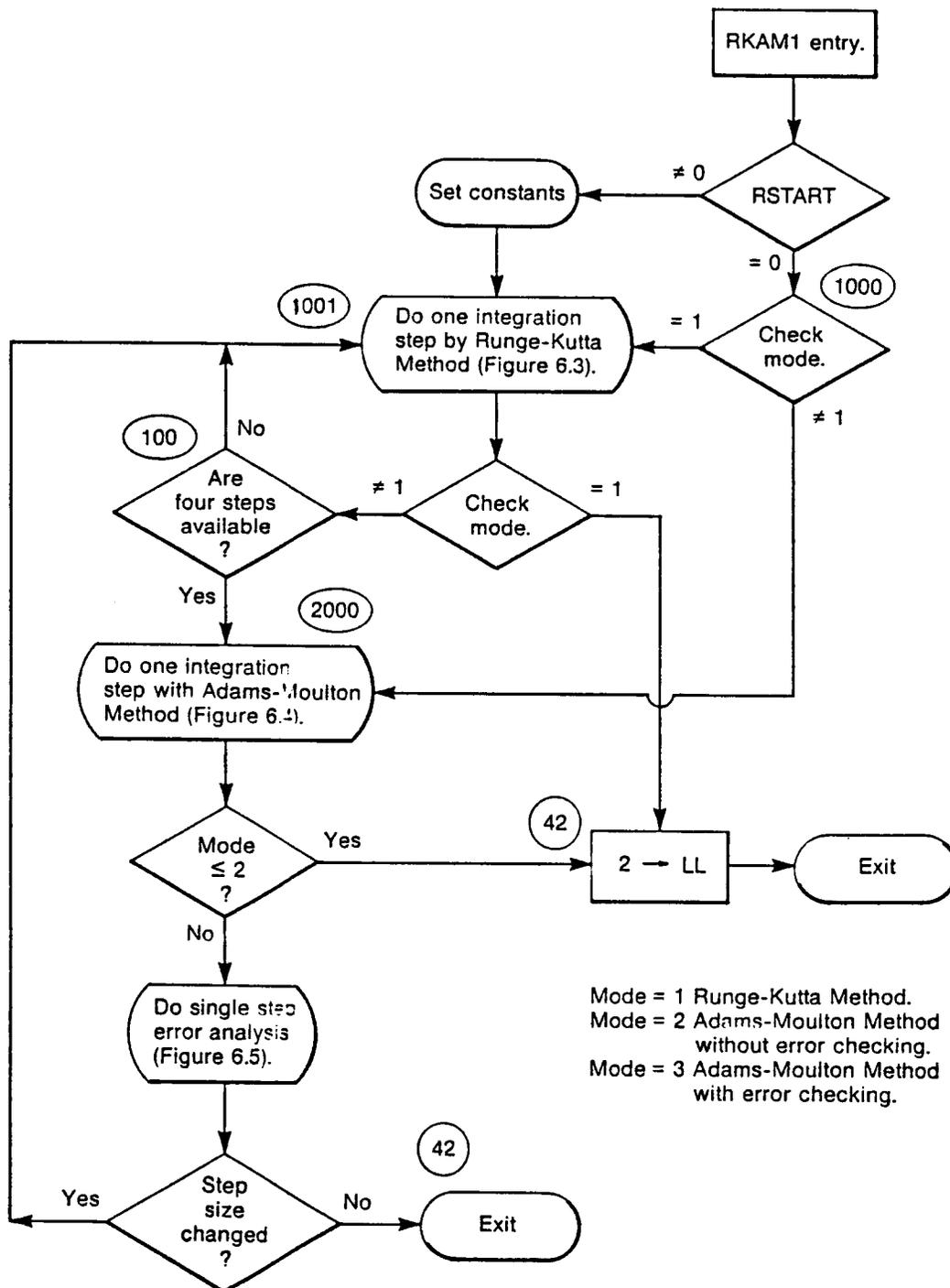


Figure 6.2. Flow chart for subroutine RKAM1.

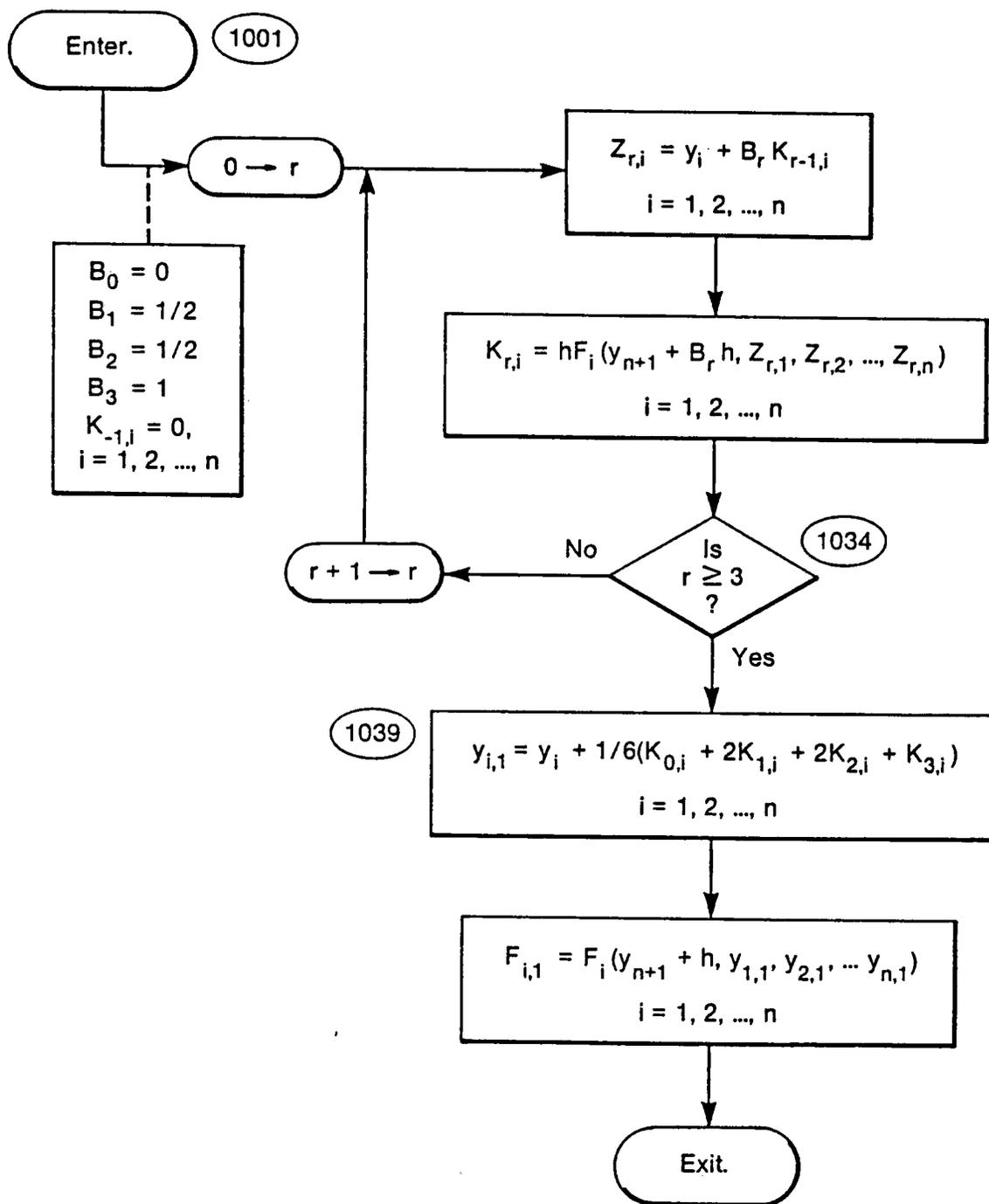


Figure 6.3. Flow chart for the Runge-Kutta procedure. The variables  $y_1, y_2, \dots, y_n$  are the dependent variables,  $n$  is the order of the system, and  $y_{n+1}$  is the independent variable.

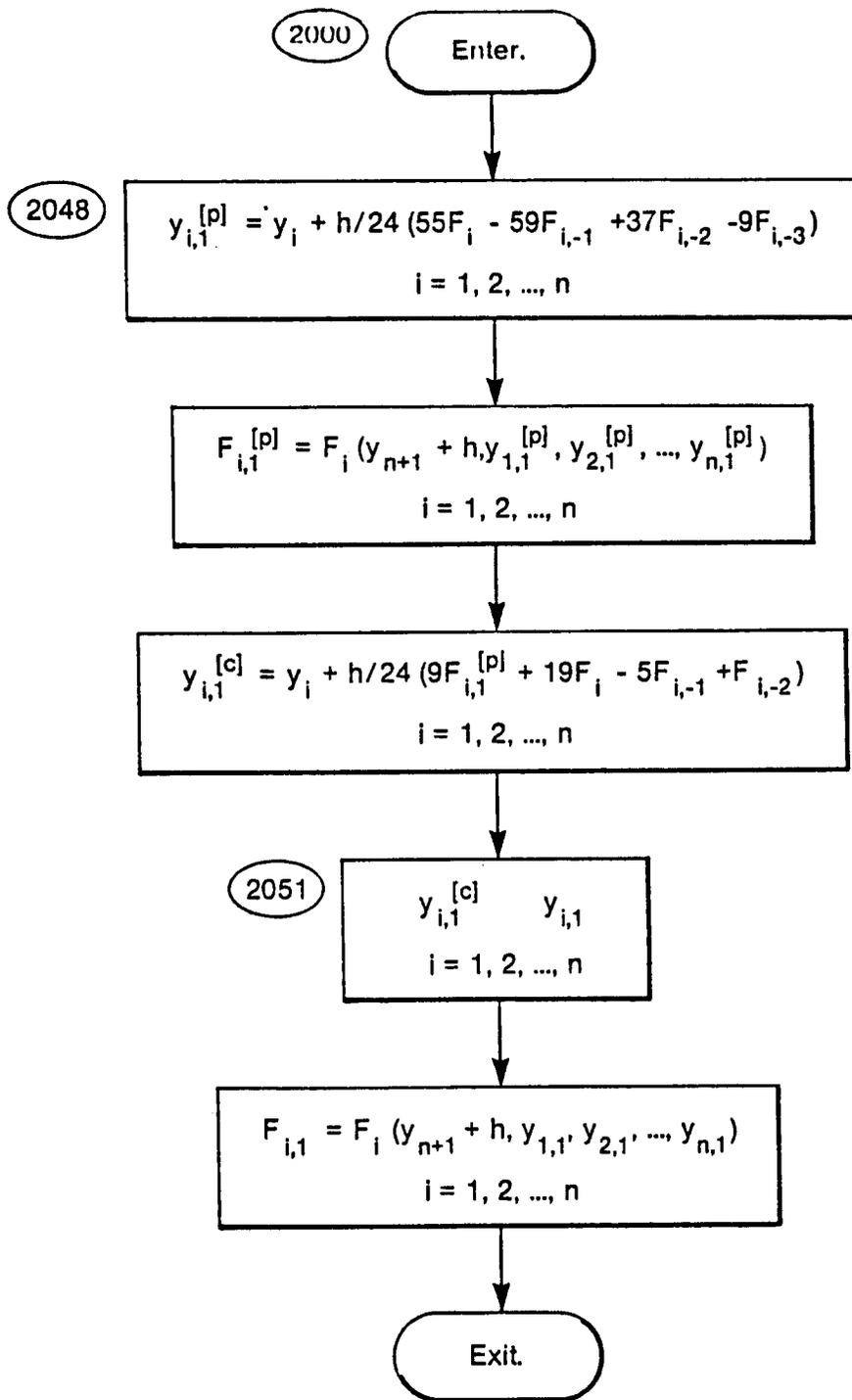


Figure 6.4. Flow chart for the Adams-Moulton integration method. The four starting values needed for this method are supplied by the Runge-Kutta method.

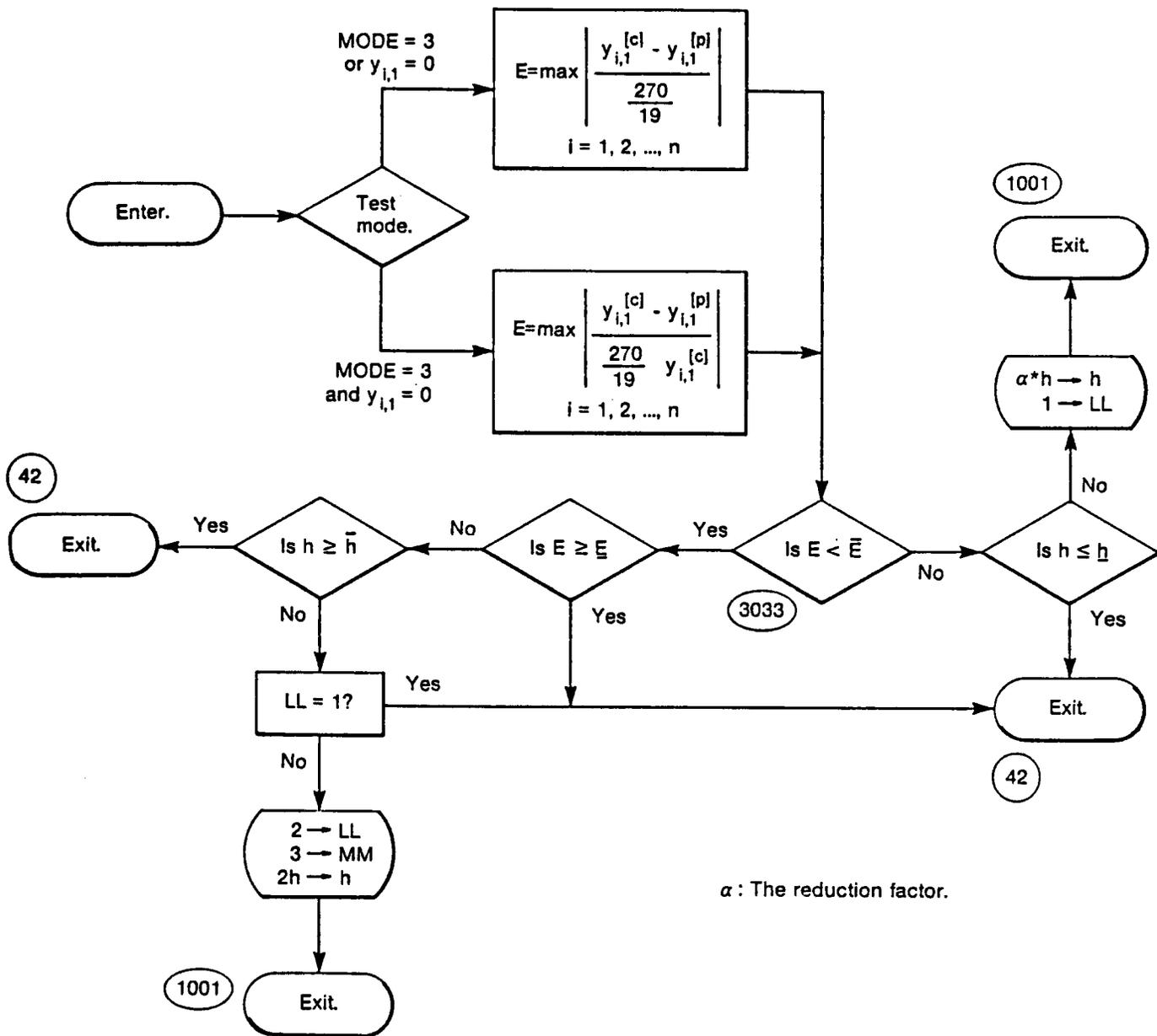


Figure 6.5. Flow chart for the single-step error analysis. The symbol  $E$  represents the maximum single-step error, and  $\bar{E}$ ,  $\underline{E}$ ,  $\bar{h}$ , and  $\underline{h}$  represent the maximum and minimum acceptable single-step error and the maximum and minimum mesh size, respectively.

Table 6.2--Run time vs. accuracy

Maximum integration error, W(42)	Run time (s)	Range error
$10^{-9}$	9.9	$<10^{-7}$
$10^{-8}$	7.1	$<10^{-7}$
$10^{-7}$	4.5	$1 \times 10^{-7}$
$10^{-6}$	3.3	$1 \times 10^{-6}$
$10^{-5}$	2.3	$6 \times 10^{-6}$
$10^{-4}$	1.7	$1.7 \times 10^{-4}$
$10^{-3}$	1.2	$5.7 \times 10^{-3}$

Note: Data obtained using model OT2; elevation angle = 4.46°; range = 1000 km; computer: CYBER 750.

idea of how the tradeoff works for a single ray calculation using the ocean version, HARPO and a model of the ocean sound channel described by Georges et al. (1986).

The user can vary other parameters, W(43) - W(47), that control the way RKAM1 adjusts its step length and controls errors (see Sec. 5.3.2), but the initial values assigned in the sample case have been found to work best for most cases met in practice. If the scale of the model differs greatly from the sample case, the initial step length, W(44), should be adjusted.

### 6.3 The Atmospheric Sound-Speed Model (Subroutine GAMRTDM)

Atmospheric sound-speed models can be specified either directly as  $C(r, \theta, \phi, t)$ , or they can call models of other atmospheric variables such as temperature  $T(r, \theta, \phi, t)$  using a connecting definition of  $C(T)$ . One choice we provide assumes that the atmosphere is a perfect gas with the equation of state

$$p = \frac{\rho RT}{M}, \quad (6.21)$$

where  $p$  is the pressure,  $\rho$  is the density,

$$R = 8.31436 \times 10^{-3} \text{ kg (kg mole)}^{-1} \text{ km}^2 \text{ s}^{-2} \text{ K}^{-1} \quad (6.22)$$

is the universal gas constant, T is the absolute temperature in Kelvins, and

$$M = M(r, \theta, \phi) \quad (6.23)$$

is the mean molecular weight of the atmosphere.

The square of the sound speed is

$$C^2 = \frac{\gamma RT}{M}, \quad (6.24)$$

where

$$\gamma = 1.4 \quad (6.25)$$

is the ratio of the specific heat at constant pressure to the specific heat at constant density. Subroutine GAMRTDM implements Equation (6.24) in HARPA.

The temperature and its gradients are provided as a function of  $t, r, \theta, \phi$  by one of the atmospheric temperature-model subroutines. The molecular weight and its gradients are provided as a function of  $t, r, \theta, \phi$  by the molecular weight model subroutine. The average molecular weight generally decreases with height because the relative constituency of the atmosphere varies with height. The main effect is from the increase in the fraction of mono-atomic molecules with height. Although the height variation of molecular weight varies with season and time of day as the atmosphere expands and contracts, it can be accurately modeled as a function of the atmospheric pressure (Jones and Georges, 1976). The only molecular weight model included in the present models treats it as a constant, however.

The gradients of the square of the sound speed are as follows.

$$\frac{\partial C^2}{\partial t} = C^2 \left( \frac{1}{T} \frac{\partial T}{\partial t} - \frac{1}{M} \frac{\partial M}{\partial t} \right) \quad (6.26)$$

$$\frac{\partial C^2}{\partial r} = C^2 \left( \frac{1}{T} \frac{\partial T}{\partial r} - \frac{1}{M} \frac{\partial M}{\partial r} \right) \quad (6.27)$$

$$\frac{\partial C^2}{\partial \theta} = C^2 \left( \frac{1}{T} \frac{\partial T}{\partial \theta} - \frac{1}{M} \frac{\partial M}{\partial \theta} \right) \quad (6.28)$$

$$\frac{\partial C^2}{\partial \phi} = C^2 \left( \frac{1}{T} \frac{\partial T}{\partial \phi} - \frac{1}{M} \frac{\partial M}{\partial \phi} \right) \quad (6.29)$$

Table 7.11 shows how the output from the sound-speed model subroutine is organized in common block /CC/.

#### 6.4 Acoustic Dispersion Relations

HARPA gains versatility without sacrificing speed by having several versions of some of the subroutines. For example, the four versions of the dispersion relation subroutine allow the user to decide in making up a run module (Section 3.3.2) whether to include or ignore winds and absorption. (If there are no winds (or absorption) in the calculation, it is much cheaper to leave them out of the equations than it is to make the calculations with zero wind, or zero absorption).

The input to the dispersion-relation subroutine is through blank common and common blocks /UU/, /CC/, /TT/, and /MM/. Output is through common block /RIN/. The dispersion-relation subroutine is called through the entry point DISPER. The subroutine names are used only for user identification.

HARPA has four versions of the dispersion-relation subroutine.

- (1) ANWNL - Acoustic waves, No Winds, No Losses
- (2) AWWNL - Acoustic waves, With Winds, No Losses
- (3) ANWWL - Acoustic waves, No Winds, With Losses
- (4) AWWWL - Acoustic Waves, With Winds, With Losses

All of these versions calculate a Hamiltonian and its derivatives and the square of the wave number that satisfies the dispersion relation. All of the above variables and some others are in the common block /RIN/ (described in Table 7.9), which has all of the output from the dispersion-relation subroutines.

##### 6.4.1 ANWNL - Acoustic, No Winds, No Losses

The dispersion relation for pure acoustic waves is

$$k^2 = k_r^2 + k_\theta^2 + k_\phi^2 = \frac{\omega^2}{C^2}, \quad (6.30)$$

where  $C(t,r,\theta,\phi)$  is the speed of sound (provided by one of the sound-speed model subroutines).

At the beginning of the numerical integration, the magnitude of  $\vec{k}$  is automatically set by the program so that the dispersion relation (4.1) is satisfied. During the numerical integration, the components of  $\vec{k}$  are allowed to vary according to Hamilton's equations. Because of integration errors, there will be slight differences between  $k^2$  and

$$k_{\text{disp}}^2 = \frac{\omega^2}{C^2}, \quad (6.31)$$

the value it would have according to the dispersion relation. As a check on the accuracy of the numerical integration and on the consistency of the equations, the quantity

$$\text{ERROR} = \frac{k^2}{k_{\text{disp}}^2} - 1 \quad (6.32)$$

is printed at each step of the raypath calculation. It is possible, however, for ERROR to exceed somewhat the maximum allowable single-step integration error (W42) because  $k$  does not vary monotonically along the raypath. ERROR serves mainly as a check that the integration is proceeding correctly and that there are no errors in computing derivatives in the model subroutines. If ERROR is generally smaller than W(42), then integrated quantities that vary monotonically (like travel time) will be computed with the accuracy given by W(42).

We use the following form of the dispersion relation for the Hamiltonian:

$$H(t,r,\theta,\phi,\omega,k_r,k_\theta,k_\phi) = \omega^2 - (k_r^2 + k_\theta^2 + k_\phi^2) C^2(t,r,\theta,\phi). \quad (6.33)$$

The partial derivatives of the Hamiltonian are

$$\frac{\partial H}{\partial t} = -k^2 \frac{\partial C^2}{\partial t} \quad (6.34)$$

$$\frac{\partial H}{\partial r} = -k^2 \frac{\partial C^2}{\partial r} \quad (6.35)$$

$$\frac{\partial H}{\partial \theta} = -k^2 \frac{\partial C^2}{\partial \theta} \quad (6.36)$$

$$\frac{\partial H}{\partial \phi} = -k^2 \frac{\partial C^2}{\partial \phi} \quad (6.37)$$

$$\frac{\partial H}{\partial \omega} = 2\omega \quad (6.38)$$

$$\frac{\partial H}{\partial k_r} = -2 C^2 k_r \quad (6.39)$$

$$\frac{\partial H}{\partial k_\theta} = -2 C^2 k_\theta \quad (6.40)$$

$$\frac{\partial H}{\partial k_\phi} = -2 C^2 k_\phi \quad (6.41)$$

$$k \cdot \frac{\partial H}{\partial k} = -2 C^2 k^2 \quad (6.42)$$

#### 6.4.2 AWWNL - Acoustic, With Winds, No Losses

The dispersion relation for pure acoustic waves in terms of the sound speed in the presence of winds is

$$\Omega^2 - C^2 k^2 = 0, \quad (6.43)$$

where

$$k^2 = k_r^2 + k_\theta^2 + k_\phi^2 \quad (6.44)$$

and

$$\Omega = \omega - \vec{k} \cdot \vec{V} = \omega - k_r V_r - k_\theta V_\theta - k_\phi V_\phi \quad (6.45)$$

is the intrinsic frequency of the wave (the frequency seen by an observer moving with the wind).  $\vec{V}(t,r,\theta,\phi)$  is the wind velocity (provided by a wind-velocity model subroutine).

At the beginning of the numerical integration, the magnitude of  $k$  is set by the program so that the dispersion relation (6.43) is satisfied. During the numerical integration, the components of  $\vec{k}$  are allowed to vary according to Hamilton's equations. Because of integration errors, there will be slight differences between  $K^2$  and

$$k_{\text{disp}}^2 = \frac{\omega^2}{\left(c + \frac{\vec{k} \cdot \vec{V}}{k}\right)^2} \quad (6.46)$$

the value it would have according to the dispersion relation. Notice that

$$\frac{\vec{k} \cdot \vec{V}}{k} = \frac{k_r V_r + k_\theta V_\theta + k_\phi V_\phi}{\sqrt{k_r^2 + k_\theta^2 + k_\phi^2}} \quad (6.47)$$

is independent of the magnitude of  $\vec{k}$ , as it should be.

As a check on the accuracy of the numerical integration and on the consistency of the equations, the quantity in (6.32) is printed at each step of the raypath calculation.

We use the following form of the dispersion relation for the Hamiltonian:

$$H(t, r, \theta, \phi, \omega, k_r, k_\theta, k_\phi) = \Omega^2(t, r, \theta, \phi, \omega, k_r, k_\theta, k_\phi) - (k_r^2 + k_\theta^2 + k_\phi^2) C^2(t, r, \theta, \phi), \quad (6.48)$$

where the intrinsic frequency  $\Omega$  is given by (6.45)

The partial derivatives of the Hamiltonian are as follows.

$$\frac{\partial H}{\partial t} = 2\Omega \frac{\partial \Omega}{\partial t} - k^2 \frac{\partial C^2}{\partial t} \quad (6.49)$$

$$\frac{\partial H}{\partial r} = 2\Omega \frac{\partial \Omega}{\partial r} - k^2 \frac{\partial C^2}{\partial r} \quad (6.50)$$

$$\frac{\partial H}{\partial \theta} = 2\Omega \frac{\partial \Omega}{\partial \theta} - k^2 \frac{\partial C^2}{\partial \theta} \quad (6.51)$$

$$\frac{\partial H}{\partial \phi} = 2\Omega \frac{\partial \Omega}{\partial \phi} - k^2 \frac{\partial C^2}{\partial \phi} \quad (6.52)$$

$$\frac{\partial H}{\partial \omega} = 2\Omega \quad (6.53)$$

$$\frac{\partial H}{\partial k_r} = -2(\Omega V_r + C^2 k_r) \quad (6.54)$$

$$\frac{\partial H}{\partial k_\theta} = -2(\Omega V_\theta + C^2 k_\theta) \quad (6.55)$$

$$\frac{\partial H}{\partial k_\phi} = -2(\Omega v_\phi + c^2 k_\phi) \quad (6.56)$$

$$\mathbf{k} \cdot \frac{\partial H}{\partial \mathbf{k}} = k_r \frac{\partial H}{\partial k_r} + k_\theta \frac{\partial H}{\partial k_\theta} + k_\phi \frac{\partial H}{\partial k_\phi} = -2(\Omega \mathbf{k} \cdot \mathbf{v} + c^2 k^2) , \quad (6.57)$$

where

$$\frac{\partial \Omega}{\partial t} = -k_r \frac{\partial v_r}{\partial t} - k_\theta \frac{\partial v_\theta}{\partial t} - k_\phi \frac{\partial v_\phi}{\partial t} \quad (6.58)$$

$$\frac{\partial \Omega}{\partial r} = -k_r \frac{\partial v_r}{\partial r} - k_\theta \frac{\partial v_\theta}{\partial r} - k_\phi \frac{\partial v_\phi}{\partial r} \quad (6.59)$$

$$\frac{\partial \Omega}{\partial \theta} = -k_r \frac{\partial v_r}{\partial \theta} - k_\theta \frac{\partial v_\theta}{\partial \theta} - k_\phi \frac{\partial v_\phi}{\partial \theta} \quad (6.60)$$

$$\frac{\partial \Omega}{\partial \phi} = -k_r \frac{\partial v_r}{\partial \phi} - k_\theta \frac{\partial v_\theta}{\partial \phi} - k_\phi \frac{\partial v_\phi}{\partial \phi} . \quad (6.61)$$

#### 6.4.3 ANWWL - Acoustic, No Winds, With Losses and AWWWL - Acoustic, With Winds, With Losses

Propagation losses for acoustic waves in the atmosphere occur when viscosity and thermal conductivity are included in the Navier-Stokes equations that describe fluid dynamics. The acoustic wave dispersion relation that results gives a complex wave number. The imaginary part of that wave number leads to absorption as explained in Section 6.1.2.

If the imaginary part of the wave number is small ( $k_{\text{imag}}^2 \ll k_{\text{real}}^2$ ) (as it must be for ordinary ray tracing such as described here to be valid), then we can neglect the effect of viscosity and thermal conductivity on the real part of the wave number so that the raypaths will be unaffected by viscosity and thermal conductivity.

Within this assumption, we can approximate (the square of) the imaginary part of the acoustic wave number for propagation through a perfect gas as (Gossard and Hooke, 1975, pp. 230-233)

$$k_{\text{imag}}^2 = -\Omega/(\gamma P) [4/3\mu + (\gamma-1)^2 M/(\gamma R) \kappa] k_{\text{real}}^2 , \quad (6.62)$$

where  $\gamma = 1.4$  is the ratio of specific heat at constant pressure to that at constant density,  $P$  is the atmospheric pressure,  $\mu$  is the viscosity,  $M$  is the

atmospheric mean molecular weight,  $R$  is the universal gas constant, and  $\kappa$  is the thermal conductivity.

Whenever you use a dispersion relation with losses (ANWWL or AWWWL), you have to supply models for  $P$ ,  $\mu$ ,  $\kappa$  and  $M$ . We provide one model for  $\mu$  and  $\kappa$  (MUARDC), one for  $P$  (PEXP), and one for  $M$  (MCONST).

## 6.5 Reflecting Rays From Irregular Terrain

This section describes the method HARPA uses to find the intersections of a ray with any terrain surface and to compute the correct reflected ray, even in an anisotropic medium (an atmosphere with winds). A more detailed discussion of terrain-reflection algorithms is given in the report by Jones (1982). Essentially the same methods are used to detect receiver-surface crossings.

### 6.5.1 Detecting Ray Intersections With the Terrain

Detecting that the ray has crossed the terrain surface is straightforward for the simple case shown in Figure 6.6. Figure 6.7 shows a more difficult example in which the ray crosses the terrain surface twice. It is difficult to distinguish such a raypath from the example in Figure 6.8, knowing only the raypath coordinates and ray directions between the integration steps (shown by dots in Figures 6.7 and 6.8). A further difficulty is that iteration of the numerical integration in Figure 6.7 might lead to finding the wrong intersection with the surface of discontinuity, a problem shared by the example in Figure 6.9.

Although infrequent, the difficulties illustrated in Figures 6.7, 6.8 and 6.9 occur often enough that any useful algorithm must be able to handle them. These difficult cases obviously occur more often when large integration steps are used. This section derives algorithms that can handle these difficult cases in addition to the straightforward cases. Figure 6.10 illustrates cases that HARPA's intersection algorithm will not correctly handle unless step length is decreased or the terrain model is made smoother.

HARPA accepts only terrain models whose surface is smooth and whose slope and curvature are continuous. Thus, wedge-shaped surfaces, for example, are

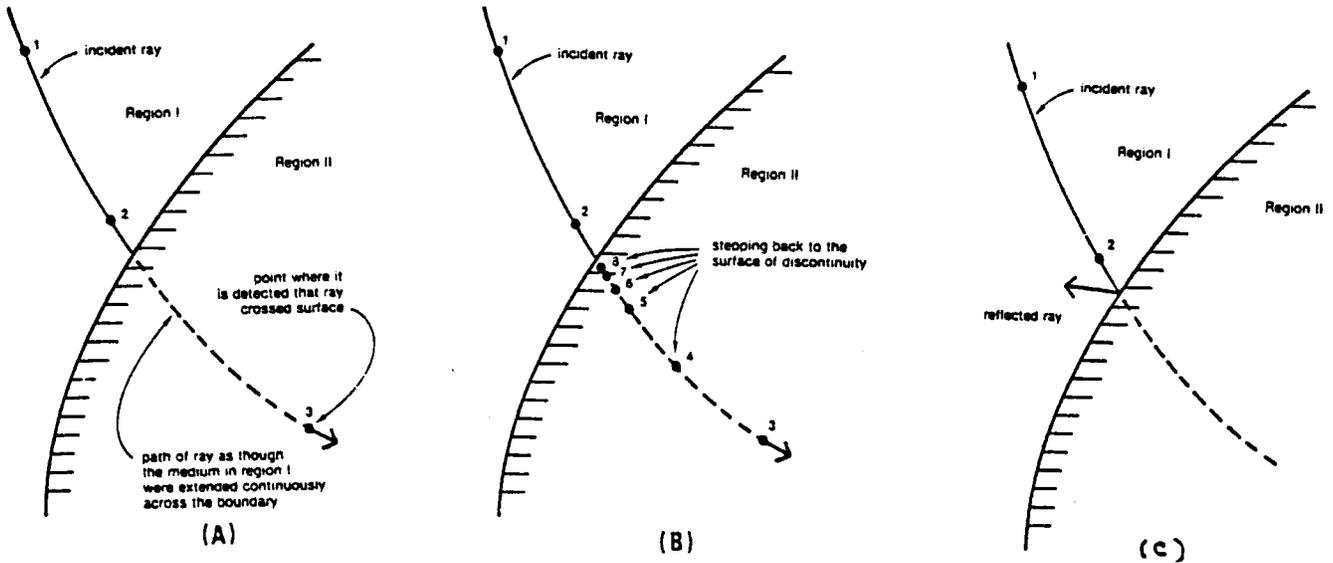


Figure 6.6. Three steps in calculating the intersection and reflection of a ray at a terrain surface: (a) recognition that the ray has crossed the terrain surface (numbers indicate successive positions of the ray after each integration step; the raypath is curved because the atmosphere is inhomogeneous); (b) iteration by numerical integration to find the intersection of the ray with the terrain surface; and (c) computation of the reflected ray ready to start numerical integration in a new direction in the atmosphere. The same algorithm could be used to compute ray refraction at discontinuities of refractive index.

not allowed. Not only are diffraction effects important at such edges, but some of the algorithms developed in this report may not work properly for surfaces with edges. In addition, the algorithms used by HARPA may not always properly handle surfaces that contain caves or tunnels.

At each integration step in the raypath calculation, we assume that the following information is available:

- (1) The position of the ray point ( $r, \theta, \phi$ ) in spherical polar (Earth-centered) coordinates,
- (2) The local Cartesian components ( $k_r, k_\theta, k_\phi$ ) of the wave vector (a vector pointing in the wave-normal direction and normalized so that the magnitude equals the wave number),
- (3) The accumulated group time delay,  $t$ , of the ray, (which is also the independent variable for the numerical integration), and

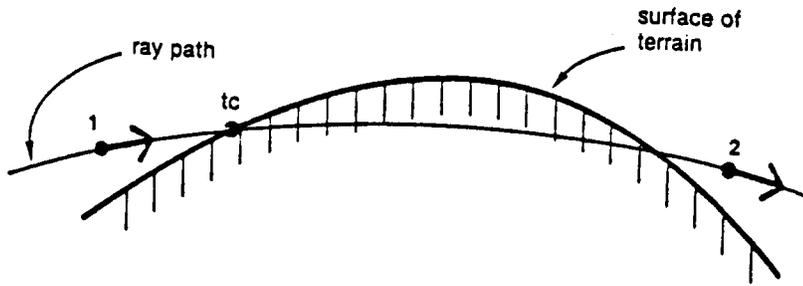


Figure 6.7. A ray crossing a terrain or receiver surface and crossing back again between integration steps. An algorithm that checked only to see if the ray at point 2 was in a different medium than point 1 would miss the intersections.

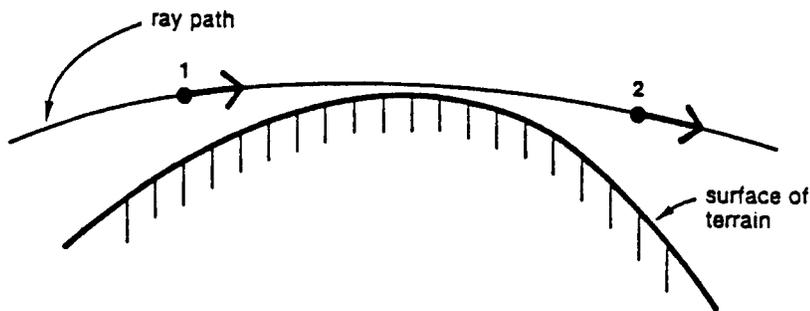


Figure 6.8. A ray that nearly intersects a terrain or receiver surface. A useful intersection algorithm must be able to distinguish this case from the one depicted in figure 6.7.

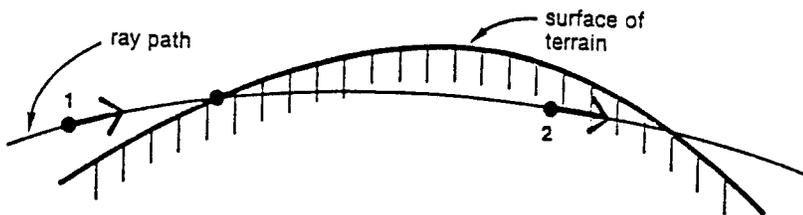


Figure 6.9. A ray crossing a terrain or receiver surface and ending closer to a second intersection. A useful algorithm must step backward and find the first intersection. HARPA will correctly handle the three cases on this page.

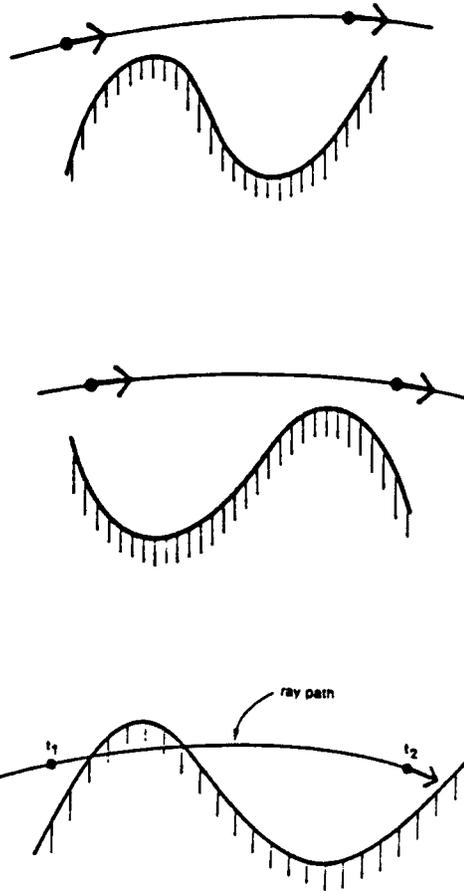


Figure 6.10. Examples of terrain (or receiver-surface) encounters that HARPA's intersection algorithm will not correctly handle. Step length must be decreased, or the terrain model must be smoothed.

(4) The derivatives

$$\dot{r} = dr/dt \tag{6.63}$$

$$\dot{\theta} = d\theta/dt \tag{6.64}$$

$$\dot{\phi} = d\phi/dt \tag{6.65}$$

$$\dot{k}_r = dk_r/dt \tag{6.66}$$

$$\dot{k}_\theta = dk_\theta/dt \tag{6.67}$$

$$\dot{k}_\phi = dk_\phi/dt \tag{6.68}$$

We assume also that the values of any of these variables can be saved from one step to the next for comparison. In particular, we make the following approximations,

$$\ddot{r} \approx (\dot{r}(t_2) - \dot{r}(t_1))/(t_2 - t_1) \quad (6.69)$$

$$\ddot{\theta} \approx (\dot{\theta}(t_2) - \dot{\theta}(t_1))/(t_2 - t_1) \quad (6.70)$$

$$\ddot{\phi} \approx (\dot{\phi}(t_2) - \dot{\phi}(t_1))/(t_2 - t_1) , \quad (6.71)$$

which allow us to estimate the curvature of ray. In using these algorithms, it would probably be useful to incorporate a test of the validity of the above approximations by evaluating both sides of (6.69) - (6.71), but HARPA does not do that.

The simplest method for predicting whether an extension of the raypath from a point will intersect the terrain surface (or the receiver surface) is to extend the ray in a straight line and see if it meets the terrain when the surface is extended as a plane by using the local slope. However, whenever the curvature of the ray and the terrain are small enough for that approximation to be useful, the ray would probably eventually go below the terrain on one of the integration steps, and the prediction from the simplest algorithm would not be needed.

Because we want an algorithm sophisticated enough to estimate the time of nearest intersection (if one occurs) in cases like those in Figures 6.7 or 6.8, we should include at least the local curvature in any approximations. Also, because it would be difficult to deal with a higher order approximation, a quadratic approximation to both the ray and the terrain seems to be the best compromise.

In addition, when searching for an intersection with the terrain (or receiver) surface, the intersection must be in the correct direction. In the case of the terrain, the intersection will always be into the ground. In the case of the receiver surface, the correct direction of crossing will alternate from one crossing to the next, but for each crossing, the direction will be known. For the purposes of the present development, it is useful to define a parameter S that is equal to +1 if the wanted crossing is upward and -1 if the wanted crossing is downward. Thus, the value of S will always be -1 for a terrain crossing.

### 6.5.2 The Surface Model

HARPA expresses an arbitrary model of a terrain or receiver surface in the form

$$f(r, \theta, \phi) = 0 . \quad (6.72)$$

Because  $f$  is zero only on the surface, it always has one sign on one side of the surface and the opposite sign on the other side. Let us call the side of the surface that is underground the inside and the other side the outside. Then we can arbitrarily require that  $f$  be positive outside of the surface and negative inside the surface. We can similarly designate an inside and an outside for the receiver surface and make the same requirement on  $f$ .

Thus, we have

$$f(r, \theta, \phi) > 0 \quad (6.73)$$

outside the surface and

$$f(r, \theta, \phi) < 0 \quad (6.74)$$

inside the surface. The time derivative of  $f$  (which indicates the rate that the ray is moving away from the surface) is

$$\dot{f} = f_r \dot{r} + f_\theta \dot{\theta} + f_\phi \dot{\phi} \quad (6.75)$$

where a subscript indicates a partial derivative with respect to the subscript. The time derivative of (6.75) is

$$\ddot{f} = f_r \ddot{r} + f_\theta \ddot{\theta} + f_\phi \ddot{\phi} + f_{rr} \dot{r}^2 + f_{\theta\theta} \dot{\theta}^2 + f_{\phi\phi} \dot{\phi}^2 + 2f_{r\theta} \dot{r}\dot{\theta} + 2f_{r\phi} \dot{r}\dot{\phi} + 2f_{\theta\phi} \dot{\theta}\dot{\phi}. \quad (6.76)$$

Assuming that (6.76) is nearly constant locally, we have

$$f = f_1 + \dot{f}_1(t - t_1) + \frac{1}{2} \ddot{f}_1(t - t_1)^2 , \quad (6.77)$$

where the subscript 1 refers to the values at the time  $t_1$ . We want to find the value of  $t$  for which the ray intersects the surface, that is, where  $f = 0$ . Let  $t_c$  be the value for which  $f = 0$ . Then

$$0 = f_1 + \dot{f}_1(t_c - t_1) + \frac{1}{2} \ddot{f}_1(t_c - t_1)^2 . \quad (6.78)$$

For simplicity, let us drop the subscript 1 in (6.78), but remember that  $f$  and  $t$  without subscripts refer to the integration step on the raypath where we are trying to estimate the time  $t_c$  where the ray will intersect the surface. Then (6.78) becomes

$$0 = f + \dot{f}(t_c - t) + \frac{1}{2} \ddot{f}(t_c - t)^2 . \quad (6.79)$$

The solution of (6.79), for which the ray is crossing from inside to outside when  $S = +1$  and crossing from outside to inside when  $S = -1$ , is

$$t_c - t = \frac{-\dot{f} + S \sqrt{\dot{f}^2 - 2f \ddot{f}}}{\ddot{f}} . \quad (6.80)$$

Within the approximation made here, the ray will intersect the surface if

$$\dot{f}^2 - 2f \ddot{f} > 0 \quad (6.81)$$

but will make a closest approach to the surface if

$$\dot{f}^2 - 2f \ddot{f} < 0 . \quad (6.82)$$

In the latter case, we can estimate the time  $t_p$  at which  $f$  is a minimum.

$$t_p - t = - \frac{\dot{f}}{\ddot{f}} . \quad (6.83)$$

This is close to the time when the ray makes a closest approach to the surface. If the second derivative in (6.76) is very small, then the formula in (6.80) may be impractical. In that case, the solution

$$t_c - t = \frac{-2f}{\dot{f} + S \sqrt{\dot{f}^2 - 2f \ddot{f}}} \quad (6.84)$$

is more useful. The advantage of (6.84) is that it is uniformly valid as  $\ddot{f}$  approaches zero.

In HARPA, different formulas are used in different circumstances: statement 501 in TRACE uses (6.84) to estimate  $t_c$ . Subroutine BACKUP uses

$$t_c = t - f/\dot{f} \quad (6.85)$$

when it is stepping to an intersection. Subroutine BACKUP uses (6.83) to step to a closest approach. When BACKUP has tried to step to a closest approach and fails after 10 tries, it tries to find an intersection. In that case, it uses (6.80) to give a first estimate for  $t_c$ , then uses (6.85) for iterating. Statement 30 in TRACE uses (6.83) to estimate the time of closest approach. See Section 7.3 for flow charts of these functions.

### 6.5.3 Reflecting the Ray From the Terrain Surface

Once the intersection with the terrain has been found, the ray must be properly reflected. For an isotropic medium, this is straightforward. The algorithm must first project the wave vector into two components parallel to the surface and the component perpendicular to the surface. It then changes sign on the component perpendicular to the surface.

An anisotropic medium (such as an atmosphere with wind) is more difficult. The two components parallel to the surface remain unchanged, as before, but the component perpendicular to the surface must be changed so that the dispersion relation is satisfied. Although this principle is the same for all media, the solution depends on the dispersion relation. At this point, we must specialize to the particular medium of interest, namely, acoustic waves in the presence of winds.

We need to first separate the wave vector  $\vec{k}$  into components perpendicular and parallel to the surface. Let  $\vec{n}$  be a unit vector pointing out of the surface. Then the component of  $\vec{k}$  normal to the surface is

$$k_{\perp} = \vec{k} \cdot \vec{n} \quad (6.86)$$

$$\vec{k}_{\perp} = (\vec{k} \cdot \vec{n}) \vec{n} \quad (6.87)$$

and the part parallel to the surface is

$$\vec{k}_{\parallel} = \vec{k} - (\vec{k} \cdot \vec{n}) \vec{n} . \quad (6.88)$$

The dispersion relation for acoustic waves in the presence of winds is

$$-\Omega^2 + c^2 k^2 = 0 , \quad (6.89)$$

where  $\Omega = \omega - \vec{k} \cdot \vec{v}$  (6.90)

is the intrinsic frequency,  $\omega$  is the wave frequency, and  $\vec{v}$  is the wind velocity.

With the help of (6.90), we can separate (6.89) as follows:

$$-(\omega - \vec{k}_\perp \cdot \vec{v} - \vec{k}_\parallel \cdot \vec{v})^2 + c^2 k_\perp^2 + c^2 k_\parallel^2 = 0 . \quad (6.91)$$

We want to solve (6.91) for  $k_\perp$ , assuming  $\vec{k}_\parallel$  to be known. We can rewrite (6.89) as

$$(c^2 - v_\perp^2) k_\perp^2 + 2 \Omega_\parallel v_\perp k_\perp - \Omega_\parallel^2 + c^2 k_\parallel^2 = 0 , \quad (6.92)$$

where

$$\Omega_\parallel = \omega - \vec{k}_\parallel \cdot \vec{v} \quad (6.93)$$

and

$$\vec{v}_\perp = (\vec{v} \cdot \vec{n}) \vec{n} , \quad v_\perp = \vec{v} \cdot \vec{n} \quad (6.94)$$

is the component of wind normal to the surface. The quadratic formula gives the solution to (6.92) as

$$k_\perp = \frac{-\Omega_\parallel v_\perp \pm c \sqrt{\Omega_\parallel^2 - k_\parallel^2 (c^2 - v_\perp^2)}}{c^2 - v_\perp^2} . \quad (6.95)$$

One solution of (6.95) should be the normal component of  $\vec{k}$  for the incident wave, the other the normal component of  $\vec{k}$  for the reflected wave. To convert from the incident wave to the reflected wave, it is necessary simply to change the sign of

$$k_\perp + \frac{\Omega_\parallel v_\perp}{c^2 - v_\perp^2} . \quad (6.96)$$

To do this, we can use (6.87) and (6.88) to write

$$\vec{k} = \vec{k} - (\vec{k} \cdot \vec{n}) \vec{n} + (\vec{k} \cdot \vec{n}) \vec{n} . \quad (6.97)$$

This is equivalent to

$$\vec{k} = \vec{k} - (\vec{k} \cdot \vec{n})\vec{n} - \frac{\Omega_{\parallel} v_{\perp}}{c^2 - v_{\perp}^2} \vec{n} + (\vec{k} \cdot \vec{n})\vec{n} + \frac{\Omega_{\parallel} v_{\perp} \vec{n}}{c^2 - v_{\perp}^2} . \quad (6.98)$$

Let us assume that (6.98) applies to the incident wave, that is,

$$\vec{k}_{inc} = \vec{k}_{inc} - (\vec{k}_{inc} \cdot \vec{n})\vec{n} - \frac{\Omega_{\parallel} v_{\perp}}{c^2 - v_{\perp}^2} \vec{n} + (\vec{k}_{inc} \cdot \vec{n})\vec{n} + \frac{\Omega_{\parallel} v_{\perp} \vec{n}}{c^2 - v_{\perp}^2} , \quad (6.99)$$

where the subscript inc signifies the incident wave. To get the wave vector for the reflected wave, we need only reverse the sign of the last two terms in (6.99), that is,

$$\vec{k}_{ref} = \vec{k}_{inc} - 2(\vec{k}_{inc} \cdot \vec{n})\vec{n} - 2 \frac{\Omega_{\parallel} v_{\perp} \vec{n}}{c^2 - v_{\perp}^2} , \quad (6.100)$$

where the subscript ref signifies the reflected wave.

To be more explicit, we can write (6.100) in terms of components. We assume an earth-centered spherical polar-coordinate system  $(r, \theta, \phi)$ . We then consider Cartesian components of  $\vec{k}$ ,  $(k_r, k_{\theta}, k_{\phi})$  in the  $r, \theta,$  and  $\phi$  directions. We also consider components of  $n$ ,  $(n_r, n_{\theta}, n_{\phi})$  in the  $r, \theta,$  and  $\phi$  directions. Then (6.100) is equivalent to

$$k_{r \text{ ref}} = k_{r \text{ inc}} - 2(\vec{k}_{inc} \cdot \vec{n})n_r - \frac{2\Omega_{\parallel} v_{\perp} n_r}{c^2 - v_{\perp}^2} \quad (6.101a)$$

$$k_{\theta \text{ ref}} = k_{\theta \text{ inc}} - 2(\vec{k}_{inc} \cdot \vec{n})n_{\theta} - \frac{2\Omega_{\parallel} v_{\perp}}{c^2 - v_{\perp}^2} n_{\theta} \quad (6.101b)$$

$$k_{\phi \text{ ref}} = k_{\phi \text{ inc}} - 2(\vec{k}_{inc} \cdot \vec{n})n_{\phi} - \frac{2\Omega_{\parallel} v_{\perp}}{c^2 - v_{\perp}^2} n_{\phi} . \quad (6.101c)$$

One might wonder whether it is realistic to allow a component of the wind normal (or even parallel) to the surface of the terrain. Rather than debate this point here, we simply point out that HARPA does not check wind models to see if they satisfy continuity or physical boundary conditions (in fact, many of our models don't). This is the responsibility of those who design wind models, if such conditions are important in their applications. The last term

in (6.101) guarantees that the dispersion relation will be satisfied for the reflected wave, even if the wind does not vanish at the surface.

#### 6.5.4 Unit-Normal Directions From the Surface

The previous section requires unit normal directions to the surface. Because  $f$  is a constant along the surface, the gradient of  $f$  is in the same direction as the unit normal. That is

$$\vec{\nabla}f = f_r \hat{i}_r + \frac{f_\theta}{r} \hat{i}_\theta + \frac{f_\phi}{r \sin \theta} \hat{i}_\phi \propto \vec{n} . \quad (6.102)$$

Taking the ratio of components gives

$$n_\theta = \frac{f_\theta}{r f_r} n_r \quad (6.103)$$

and

$$n_\phi = \frac{f_\phi}{f_r r \sin \theta} n_r . \quad (6.104)$$

The solution of (6.103), and (6.104), while requiring  $n_r^2 + n_\theta^2 + n_\phi^2 = 1$ , is

$$n_r = \frac{f_r}{\sqrt{f_r^2 + \frac{f_\theta^2}{r^2} + \frac{f_\phi^2}{r^2 \sin^2 \theta}}} , \quad (6.105)$$

$$n_\theta = \frac{f_\theta}{r \sqrt{f_r^2 + \frac{f_\theta^2}{r^2} + \frac{f_\phi^2}{r^2 \sin^2 \theta}}} , \quad (6.106)$$

$$n_\phi = \frac{f_\phi}{r \sin \theta \sqrt{f_r^2 + \frac{f_\theta^2}{r^2} + \frac{f_\phi^2}{r^2 \sin^2 \theta}}} . \quad (6.107)$$

## 6.6 Coordinate Systems

HARPA uses two different earth-centered spherical polar-coordinate systems, one geographic and one computational, because it is easier to express some models in a different coordinate system. Input data for the coordinates of the transmitter, W(4) and W(5), and input data for the coordinates of the north pole of the computational coordinate system, W(24) and W(25), are entered in geographic coordinates. Putting W(25) equal to  $0^\circ$  and W(24) equal to  $90^\circ$  would superimpose the two north poles and equate the two coordinate systems.

When the two coordinate systems do not coincide, the atmospheric models calculate wind, sound speed, temperature, and molecular weight in terms of the computational coordinate system. Dudziak (1961) describes the transformations between these coordinate systems.



## 7. Structure of the Program

This chapter explains how the parts of HARPA work together, including a brief description of each program subroutine and detailed flow charts of the central ray-tracing parts. Also included are hierarchical or organization diagrams that show the calling sequences of the principal ray-tracing operations and details of the common-block structure and usage.

### 7.1 Description of the Subroutines

Following is a list of all the programs, subroutines, and functions that constitute HARPA, that is, the functions inside the dashed lines of Figure 1.1. They are listed in the order they appear in Files 3, 4, and 5 of the distribution tape and in the source-code listings of Appendix D. The routines are divided into a RAY-TRACING "CORE," the set of programs that is always required to do ray tracing, DISPERSION-RELATION ROUTINES, from which you must select one, and ATMOSPHERIC MODEL SUBROUTINES, from which you select the routines that correspond to the atmospheric models you want to use. A more detailed description of the distribution-tape structure is given in Sec. 3.3.1.

#### 7.1.1 Ray-Tracing Core

PROGRAM RAYTRC -- The main program; sets the initial conditions for each ray and calls TRACE.

SUBROUTINE DFSYS -- Contains system-dependent functions such as date, time (user must modify).

SUBROUTINE DFCNST -- Defines machine-dependent constants (user must modify).

SUBROUTINE READW1 -- Reads variable-length tabular data from input data table.

SUBROUTINE GTUNIT -- Interprets units line in tabular input data.

SUBROUTINE SREAD1 -- Handles unassigned labeled-common blocks.

FUNCTION READW -- Reads input data table into W array, converting units.

SUBROUTINE CLEAR -- Sets n elements of an array to zero.

FUNCTION ND2B -- Converts decimal digits to positionally equivalent binary numbers when reading W(29).

FUNCTION UCON -- Provides keyword units conversion for input data.

SUBROUTINE TRACE -- Calculates a raypath for the requested number of hops.

FUNCTION PCROSS -- Tests whether ray crosses a surface.

SUBROUTINE RCROSS -- Estimates point where ray crosses a surface.

SUBROUTINE HAMLTN -- Calculates Hamilton's equations for ray tracing and other quantities to be integrated.

SUBROUTINE RKAM -- Keeps track of integration steps performed by RKAM1 and makes them available to calling subroutines.

SUBROUTINE RKAM1 -- Numerically integrates Hamilton's equations.

SUBROUTINE BACKUP -- Moves the ray point to the last intersection with receiver or terrain surface.

FUNCTION REFLECT -- Computes normal and parallel components of K vector at ground reflections.

SUBROUTINE FIT -- Computes 3 types of parabolic fit to raypath relative to terrain.

FUNCTION GET -- Gets the value of the terrain function and its derivatives; calls the terrain model subroutine if necessary.

FUNCTION GET1 -- Second version of GET to avoid self-calls.

FUNCTION ITEST -- Passes integer values through for variables typed real.

SUBROUTINE CONBLK -- Data-initialization and file-opening service routine.

FUNCTION WCHANGE -- Determines equivalence of two W arrays for producing raysets.

FUNCTION RENORM -- Normalizes a vector to a specified magnitude.

SUBROUTINE SET2 -- Sets n components of vector to a specified single value.

SUBROUTINE PRINTR -- Prints details of the raypath calculation at specified intervals and produces computer-readable output (raysets).

SUBROUTINE ATMOSHD -- Includes page headings in printout.

SUBROUTINE PUTDES -- Prints model information on printout header.

FUNCTION NUMSTG -- Converts a numeric value to a string.

SUBROUTINE SFILL -- Fills a string with n specified characters.

FUNCTION STRIM -- Determines position of last nonblank character of a string.

FUNCTION RERR -- Computes for subroutine PRINTR the largest relative integration error.

SUBROUTINE RERROR -- Reports error conditions and stops program.

SUBROUTINE STOPIT -- Prints error condition and stops program.

SUBROUTINE PUTKST -- Multiple ENTRY points to produce line-printer output while accounting for line count, new page, etc.

SUBROUTINE OPNREP -- Increases portability among FORTRAN 77 systems for opening files with replacement.

SUBROUTINE OVERRD -- Tests for "zero-override" condition in input data (Sec. 5.3.1).

SUBROUTINE SFILTR -- Filters extraneous characters from plot annotations.

FUNCTION ALCOSH -- Compute  $\log[\cosh(x)]$  and use large-argument approx.

SUBROUTINE GAUSEL -- Calculates coefficients of functions to fit points in TTABLE.

[PLOTTING ROUTINES]

SUBROUTINE RAYPLT -- Main plotting program; initializes, reads input, plots projections of rays on a vertical or horizontal plane.

SUBROUTINE PLOT -- XY plotting routine, called by RAYPLT.

SUBROUTINE LABPLT -- Labels rayplots.

[TICK/ANNOTATION ROUTINES]

SUBROUTINE PLTHLB -- Plots horizontal ticks and annotation for rayplot.

SUBROUTINE PLTANH -- Generic horizontal tick annotation.

SUBROUTINE SETXY -- Plot initialization; sets projection parameters.

SUBROUTINE TIKLINE -- Draws straight line with ticks at intervals.

SUBROUTINE PLTANOT -- Puts general annotations on plots.

SUBROUTINE DRAWTKS -- Draws plot boundary, ticks, and labels for horizontal ray projection.

SUBROUTINE PLTLB -- Puts vertical tick annotations on rayplots.

SUBROUTINE ARCTIC -- Draws curved range axis for rayplot.

BLOCK DATA PLOTBL -- Initializes plot range variables.

## [GRAPHICS WRITE ROUTINES]

SUBROUTINE DDINIT -- Initializes plotting process (writes header line to TAPE5).

SUBROUTINE DDBP -- Sets a vector origin (writes IX,IY to TAPE5).

SUBROUTINE DDVC -- Plots a vector (writes IX,IY for vector end point to TAPE5).

SUBROUTINE DDTEXT -- Writes an array (character string) to TAPE 5 in tabular text mode.

SUBROUTINE DDTAB -- Sends instruction to TAPE5 that initializes tabular (text) plotting.

SUBROUTINE DDFR -- Sends instruction to TAPE5 to advance a microfilm frame.

SUBROUTINE DDEND -- Empties plot buffer and releases plotting command file to microfilm plot queue.

SUBROUTINE DASH -- Sets dashed-line mode; that is, all plotted curves will be dashed instead of solid after a call to subroutine DASH.

SUBROUTINE RESET('DASH') -- Sets solid-line mode; that is, all plotted curves will be solid lines after this call.

SUBROUTINE HEIGHT -- If you do not have the DISSPLA\* plotting package, load SUBROUTINE SMPANN instead of SUBROUTINE FULANN, and you can ignore this routine.

SUBROUTINE MX1ALF -- If you do not have the DISSPLA\* plotting package, load SUBROUTINE SMPANN instad of SUBROUTINE FULANN, and you can ignore this routine.

SUBROUTINE MX2ALF -- If you do not have the DISSPLA\* plotting package, load SUBROUTINE SMPANN instead of SUBROUTINE FULANN, and you can ignore this routine.

SUBROUTINE SCMPLEX -- If you do not have the DISSPLA\* plotting package, load SUBROUTINE SMPANN instead of SUBROUTINE FULANN, and you can ignore this routine.

### 7.1.2 Dispersion Relation Routines

SUBROUTINE ANWNL -- Acoustic wave, no winds, no losses.

SUBROUTINE AWWNL -- Acoustic wave, with wind, no losses.

SUBROUTINE ANWWL -- Acoustic wave, no wind, with losses.

SUBROUTINE AWWWL -- Acoustic wave, with wind, with losses.

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\* DISSPLA is the proprietary product of ISSCO, Inc.

### 7.1.3 Atmospheric Model Subroutines

SUBROUTINE WLINEAR -- Constant upward or northward background wind; linear eastward wind profile.

SUBROUTINE WTIDE -- Eastward and northward background wind profiles that are sinusoidal in height and time and are in time quadrature.

SUBROUTINE ULOGZ2 -- Logarithmic atmospheric boundary-layer profile; eastward background wind only.

SUBROUTINE VVORTX3 -- Vertical vortex wind perturbation with viscous core and Gaussian height profile.

SUBROUTINE WGAUSS2 -- Eastward perturbation wind that decays in three dimensions (jet).

SUBROUTINE NPWIND -- Do-nothing wind perturbation model.

SUBROUTINE GAMRTDM -- Sound-speed model:  $C^2 = \gamma RT/M$ .

SUBROUTINE CSTANH -- Background sound-speed profile with linear segments joined smoothly.

SUBROUTINE NPSPEED -- Do-nothing sound-speed-perturbation model.

SUBROUTINE CBLOB2 -- Sound-speed perturbation with Gaussian decay in three dimensions.

SUBROUTINE TLINEAR -- Background linear temperature profile.

SUBROUTINE TTANH5 -- Background height profile of temperature with linear segments joined smoothly.

SUBROUTINE TTABLE -- Background tabular temperature profiles with cubic interpolation between points.

SUBROUTINE NTEMP -- Do-nothing background temperature model.

SUBROUTINE TBLOB2 -- Temperature perturbation with Gaussian decay in three dimensions.

SUBROUTINE NPTEMP -- Do-nothing temperature perturbation model.

SUBROUTINE MCONST -- Constant molecular weight model.

#### [TERRAIN MODELS]

SUBROUTINE GHORIZ -- Terrain model at fixed height above sea level.

SUBROUTINE GLORENZ -- Lorentzian-ridge terrain model.

SUBROUTINE GTANH -- 2-D terrain model with a series of linear segments joined smoothly.

[ABSORPTION MODELS]

SUBROUTINE NPERR -- Do-nothing terrain-perturbation model.

SUBROUTINE MUARDC -- ARDC background absorption formula.

SUBROUTINE NPABSR -- Do-nothing absorption-perturbation model.

SUBROUTINE PEXP -- Exponential background pressure profile.

SUBROUTINE NPPRES -- Do-nothing pressure-perturbation model.

[RECEIVER-SURFACE MODELS]

SUBROUTINE RHORIZ -- Horizontal receiver-surface model.

SUBROUTINE RTERR -- Receiver-surface model at fixed height above terrain.

SUBROUTINE RVERT -- Vertical (conical) receiver surface at a fixed radius from a specified origin.

[ANNOTATION MODELS]

SUBROUTINE SMPANN -- Initializes plot in draft mode (must be used if you don't have DISSPLA).

SUBROUTINE FULANN -- Initializes plot in publication-quality mode (requires DISSPLA).

## 7.2 HARPA Organization Diagrams

This section contains hierarchical diagrams, Figures 7.1 through 7.4, that show how the principal subroutines are interrelated by calling sequences. These diagrams are not flow charts; they show how control passes among the program modules. Not all subroutines are shown, only the major ones that perform the ray-tracing function.

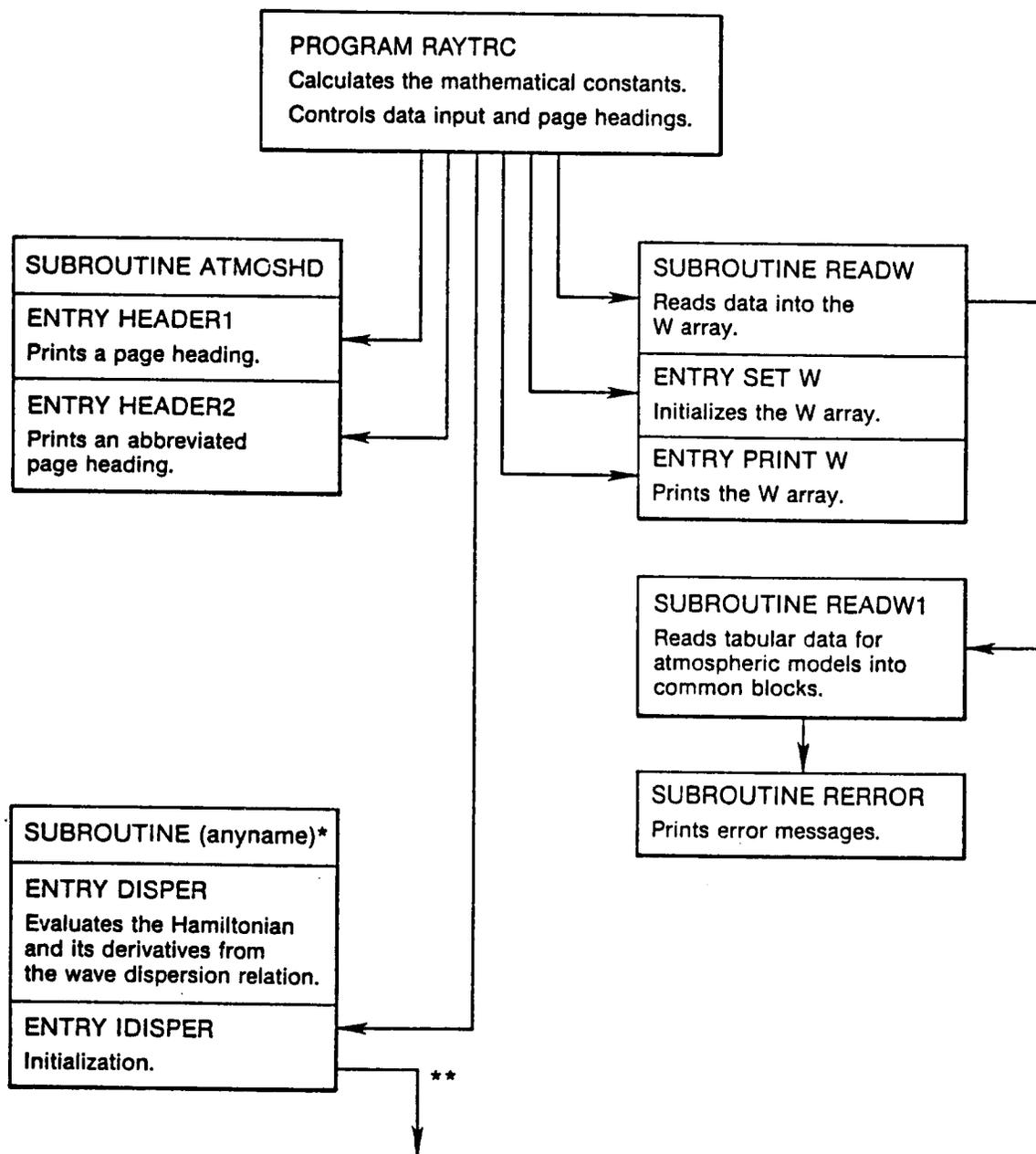


Figure 7.1. Block diagram (not a flow chart) of the ray-tracing program showing the relation (hierarchy, what calls what) of the main program to other subroutines during the initialization stage (immediately after new input data are read in).

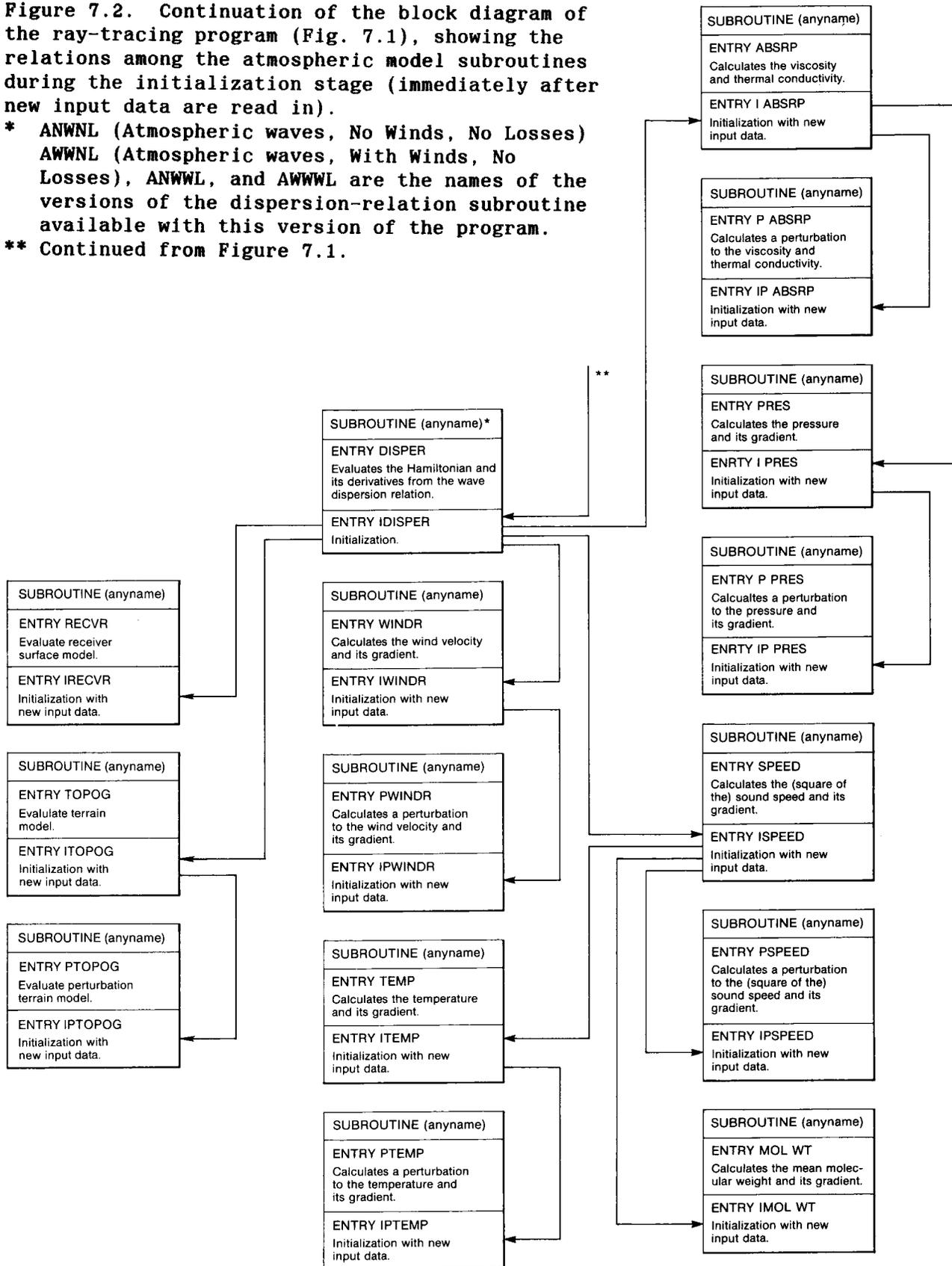
\* ANWNL (Acoustic, No Winds, No Losses), AWWNL, With Winds, No Losses), ANWWL, and AWWWL are the names of the versions of the dispersion-relation subroutine available.

\*\* Figure 7.2 shows the continuation of this block diagram.

Figure 7.2. Continuation of the block diagram of the ray-tracing program (Fig. 7.1), showing the relations among the atmospheric model subroutines during the initialization stage (immediately after new input data are read in).

\* ANWNL (Atmospheric waves, No Winds, No Losses)  
 AWWNL (Atmospheric waves, With Winds, No Losses), ANWWL, and AWWWL are the names of the versions of the dispersion-relation subroutine available with this version of the program.

\*\* Continued from Figure 7.1.



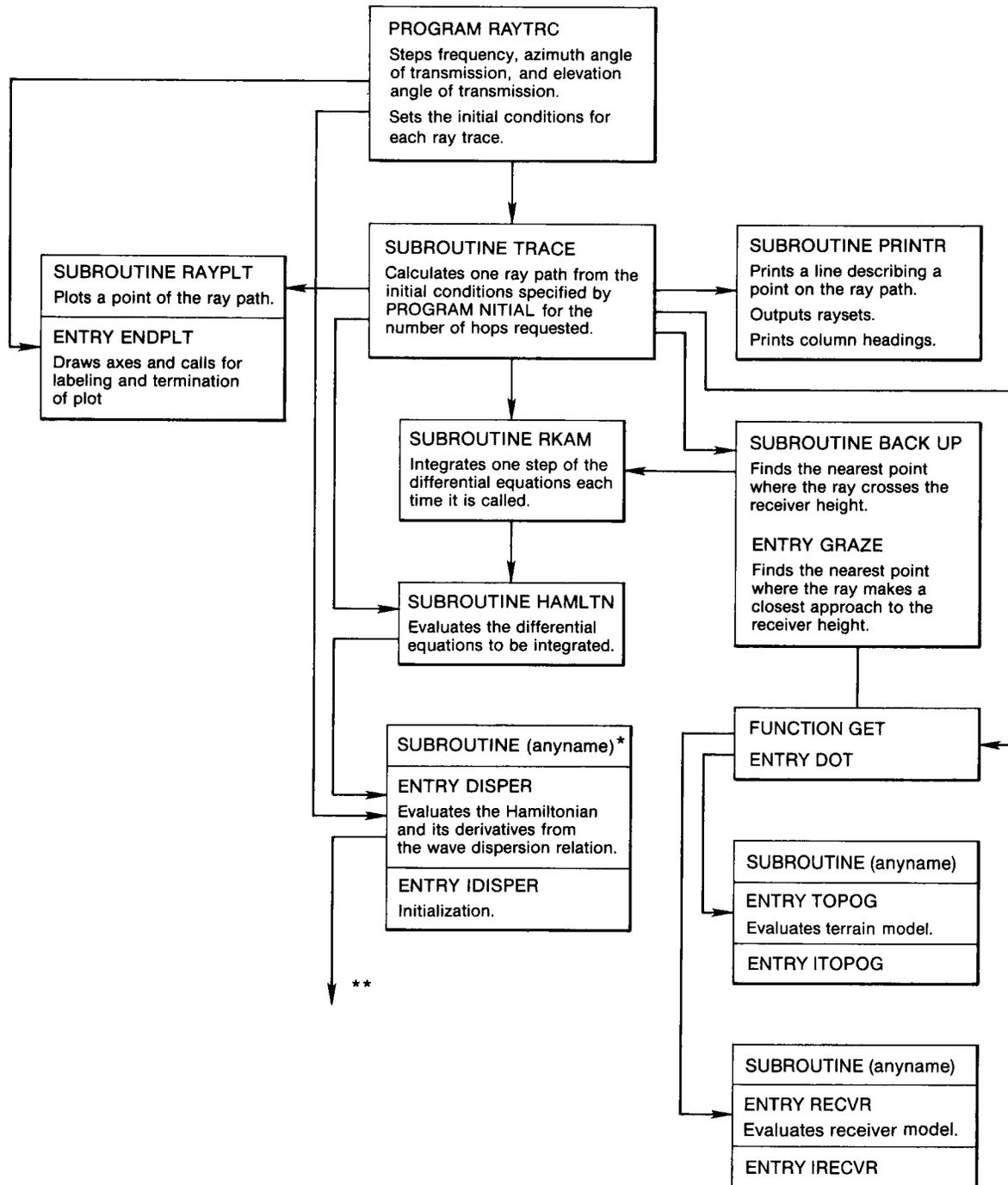


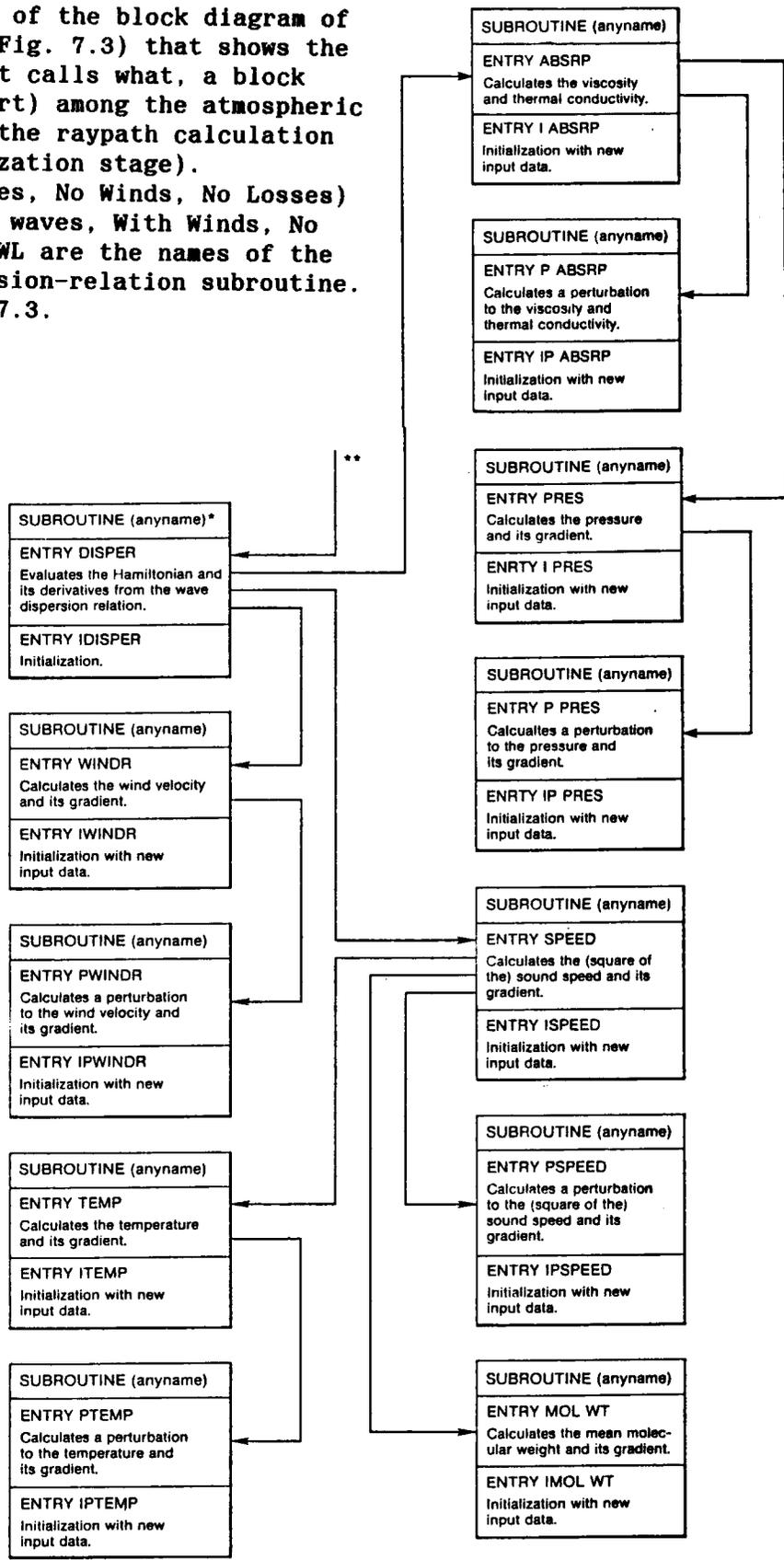
Figure 7.3. Block diagram (not a flow chart) of the ray-tracing program showing the relations (hierarchy, what calls what) among the main program and the subroutines during the raypath calculation stage (after the initialization stage).

\* ANWWL (Acoustic, No Winds, No Losses) and AWWNL (Acoustic, With Winds, No Losses), AWWNL and ANWWL are the names of the versions of the dispersion-relation subroutine.

\*\* Figure 7.4 shows the continuation of the block diagram that shows the relations among the atmospheric model subroutines.

Figure 7.4. Continuation of the block diagram of the ray-tracing program (Fig. 7.3) that shows the relations (hierarchy, what calls what, a block diagram is not a flow chart) among the atmospheric model subroutines during the raypath calculation stage (after the initialization stage).

\* ANWNL (Atmospheric waves, No Winds, No Losses) and AWWNL (Atmospheric waves, With Winds, No Losses), AWWWL and ANWWL are the names of the versions of the dispersion-relation subroutine.  
 \*\* Continued from Figure 7.3.



### 7.3 Flow Charts for Program RAYTRC and Subroutines TRACE and BACKUP

These three routines contain the central logic of the raypath calculations and so are described in detail in flow-chart form.

This ray-tracing program consists of various subroutines that perform specific tasks in calculating raypaths. The division of labor makes it easier to modify the program to solve specific problems. Often it may be necessary to change only one or two subroutines to convert the program to a different use.

The main program (RAYTRC) sets up the initial conditions (transmitter location, wave frequency, and direction of transmission) for each ray trace. In setting up the initial conditions for each ray trace, the main program (RAYTRC) steps frequency, azimuth angle of transmission, and elevation angle of transmission (see Figs. 7.5 and 7.6). Then subroutine TRACE calculates one raypath for the requested number of crossings of the specified receiver height. Subroutine TRACE is the heart of the ray-tracing program. It is the most complicated subroutine included, but also the most important to understand. The flow charts in Figures 7.6 and 7.7 explain how TRACE works.

Subroutine RKAM integrates the differential equations numerically using an Adams-Moulton predictor-corrector method with a Runge-Kutta starter. Subroutine HAMLTN evaluates the differential equations to be integrated. Subroutine DISPER calculates the Hamiltonian and its derivatives, the wave number from the dispersion relation, and the wave polarization. (Four versions of subroutine DISPER are included.) Subroutines WIND, SPEED, TEMP, MOLWT, RECUR, TOPOG, ABSRP, and PRES calculate the atmospheric wind speed, sound speed, temperature, mean molecular weight, receiver surface, terrain, viscosity/thermal conductivity, and pressure. Several versions of these eight subroutines are included, and it is easy to add more. Subroutine BACKUP finds an intersection of the ray with the receiver surface or with the terrain. The flow charts in Figures 7.8 through 7.10 and Section 6.5 explain how BACKUP works.

Subroutine PRINTR prints information describing the raypath and outputs the results in computer-readable form (raysets). Subroutine RAYPLT plots the raypath. The block diagrams in Figures 7.1 through 7.4 show the relationships among these (and other) subroutines.

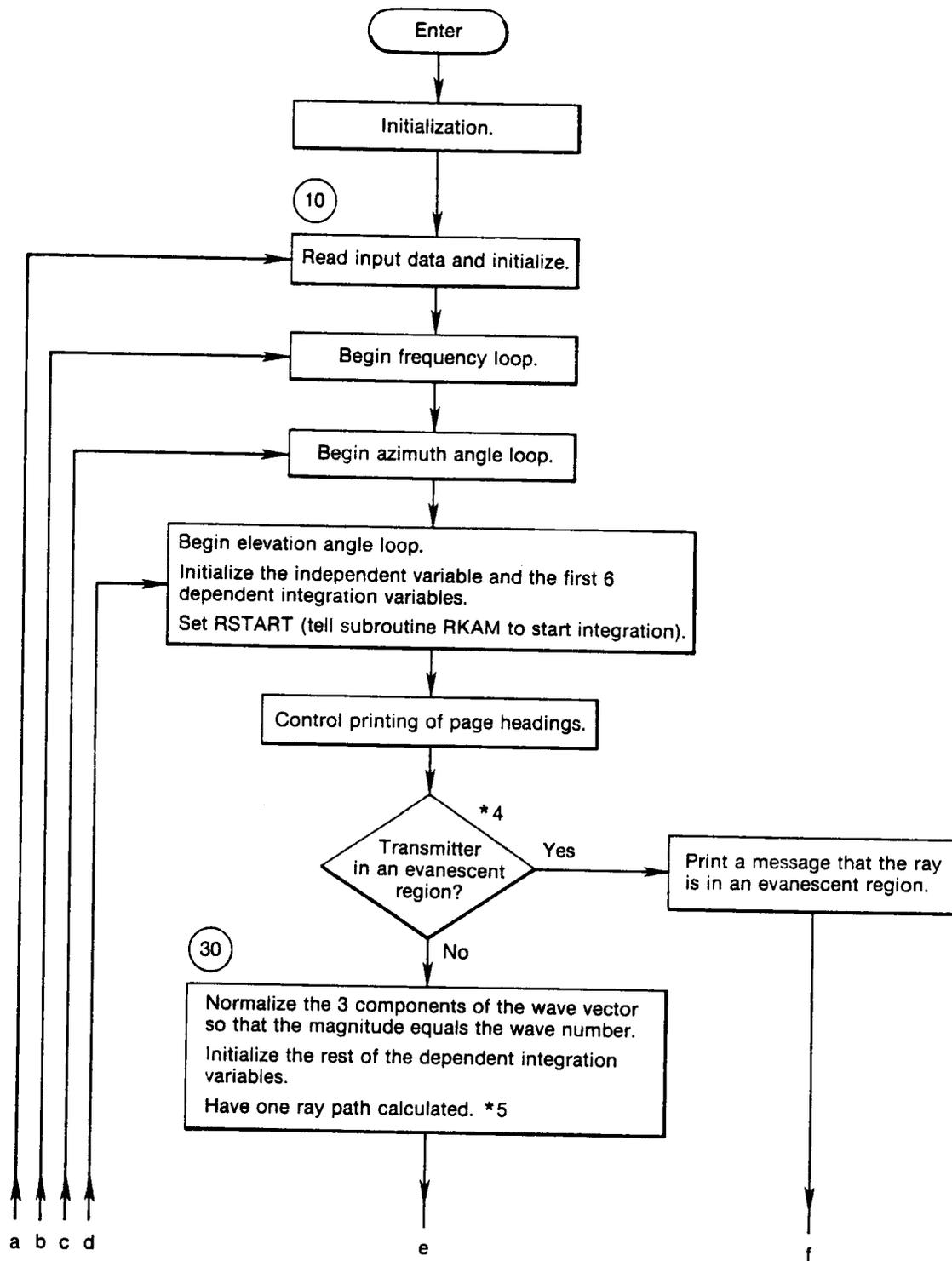


Figure 7.5. Flow chart for program RAYTRC. Circled block numbers correspond to program statement numbers.

\*4 There are no evanescent regions for pure acoustic waves (with no cutoff frequency).

\*5 Subroutine TRACE calculates one raypath.

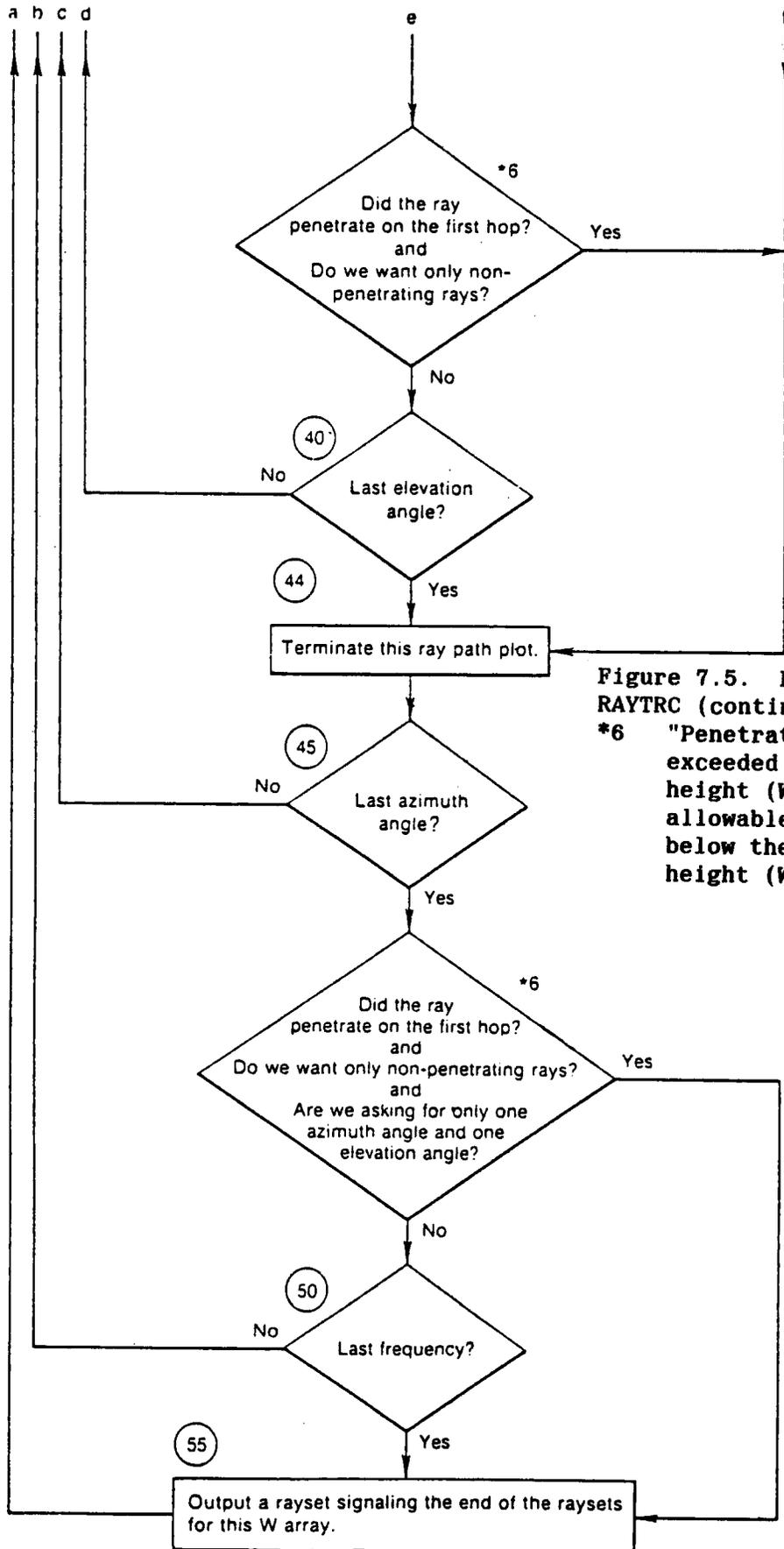
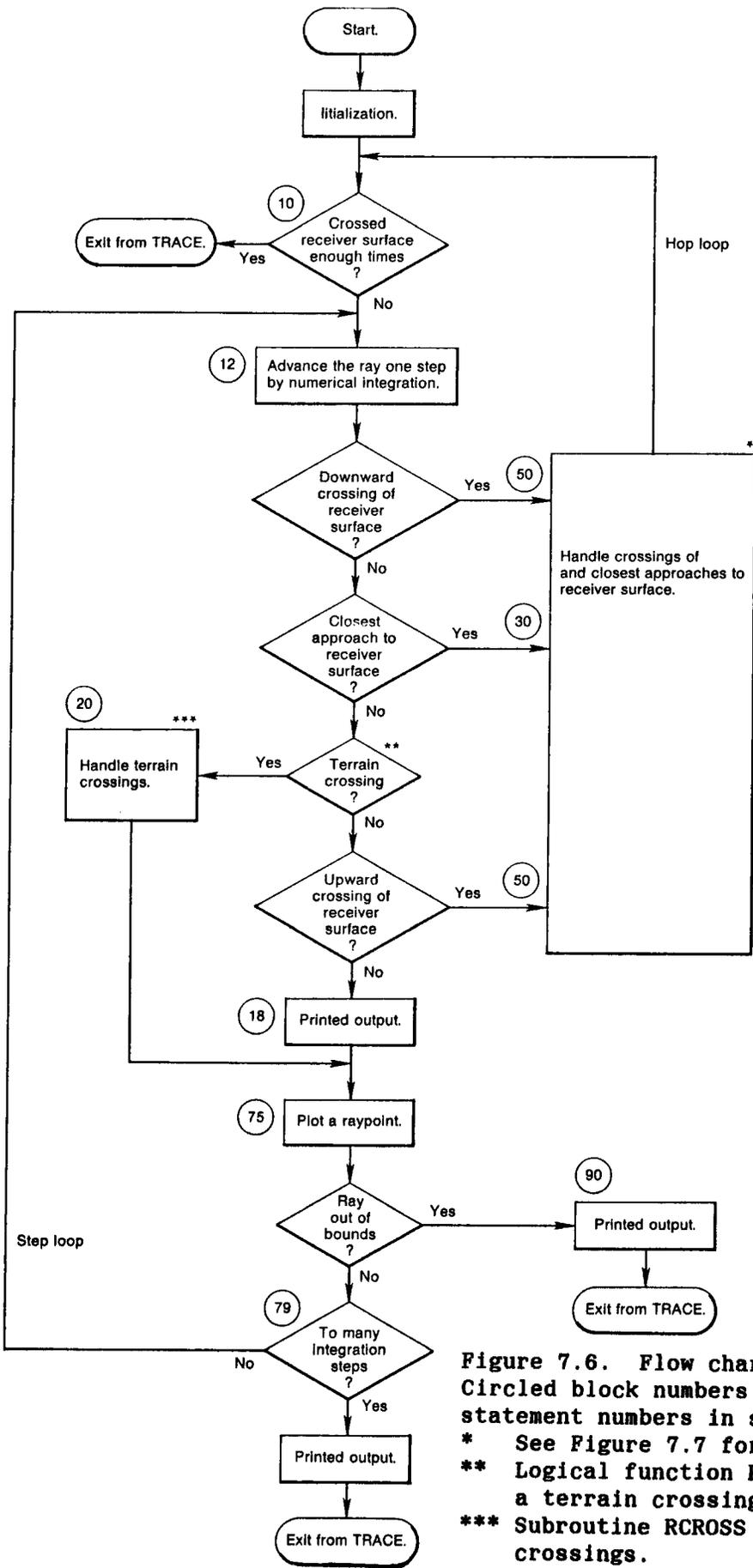


Figure 7.5. Flow chart for program RAYTRC (continued).

\*6 "Penetrate" means the ray exceeded the maximum allowable height (W26) or the maximum allowable range (W28) or went below the minimum allowable height (W27).



**Figure 7.6. Flow chart for subroutine TRACE.**  
 Circled block numbers correspond to program statement numbers in subroutine TRACE.  
 \* See Figure 7.7 for details.  
 \*\* Logical function PCROSS estimates whether a terrain crossing has occurred.  
 \*\*\* Subroutine RCROSS handles terrain crossings.

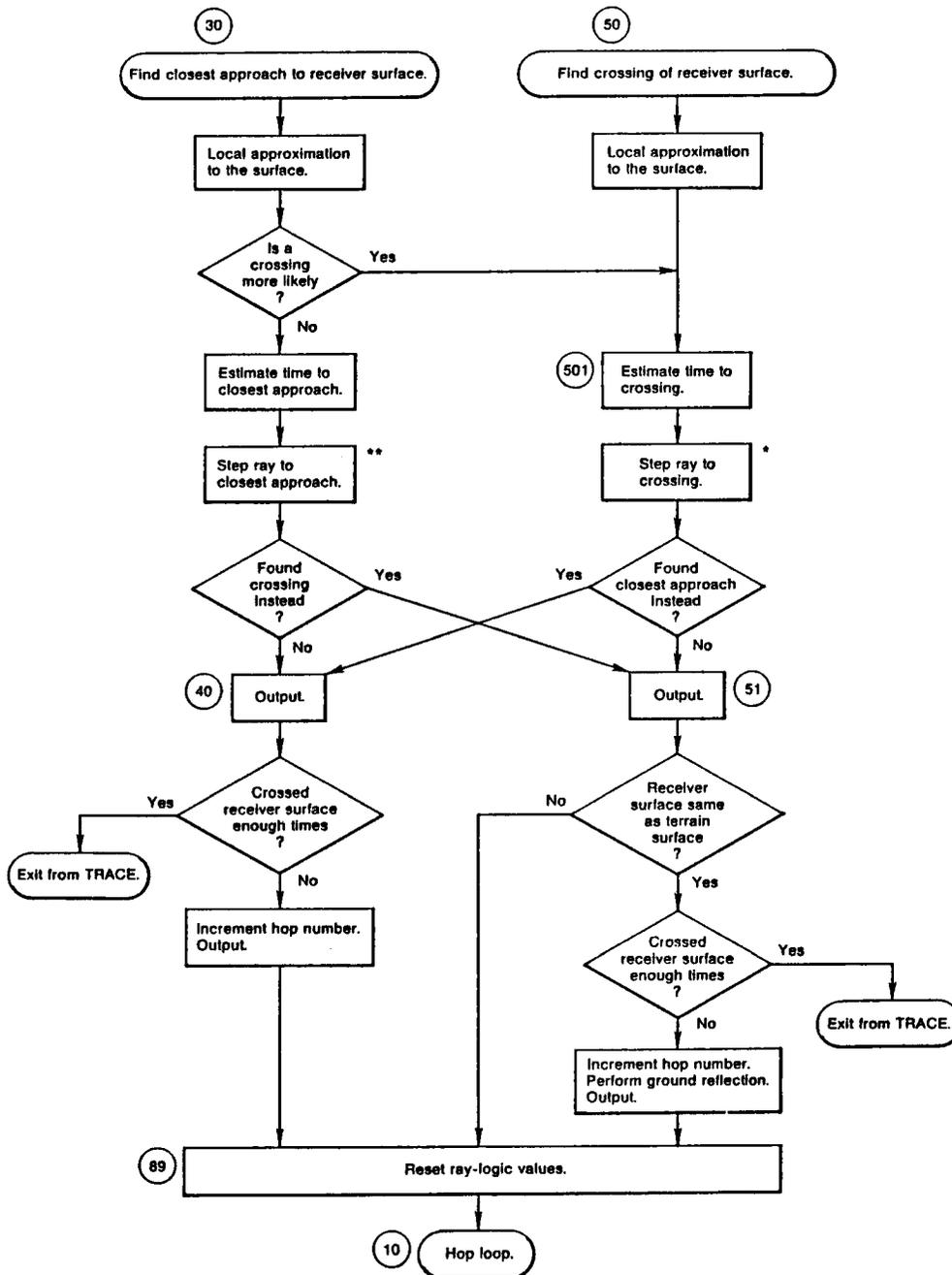


Figure 7.7. Flow chart showing some details of finding crossings of and closest approaches to receiver surface. Circled block numbers correspond to program statement numbers in subroutine TRACE.

\* See Figure 7.8 for details (subroutine BACKUP).

\*\* See Figure 7.8 for details (entry point GRAZE in subroutine BACKUP).

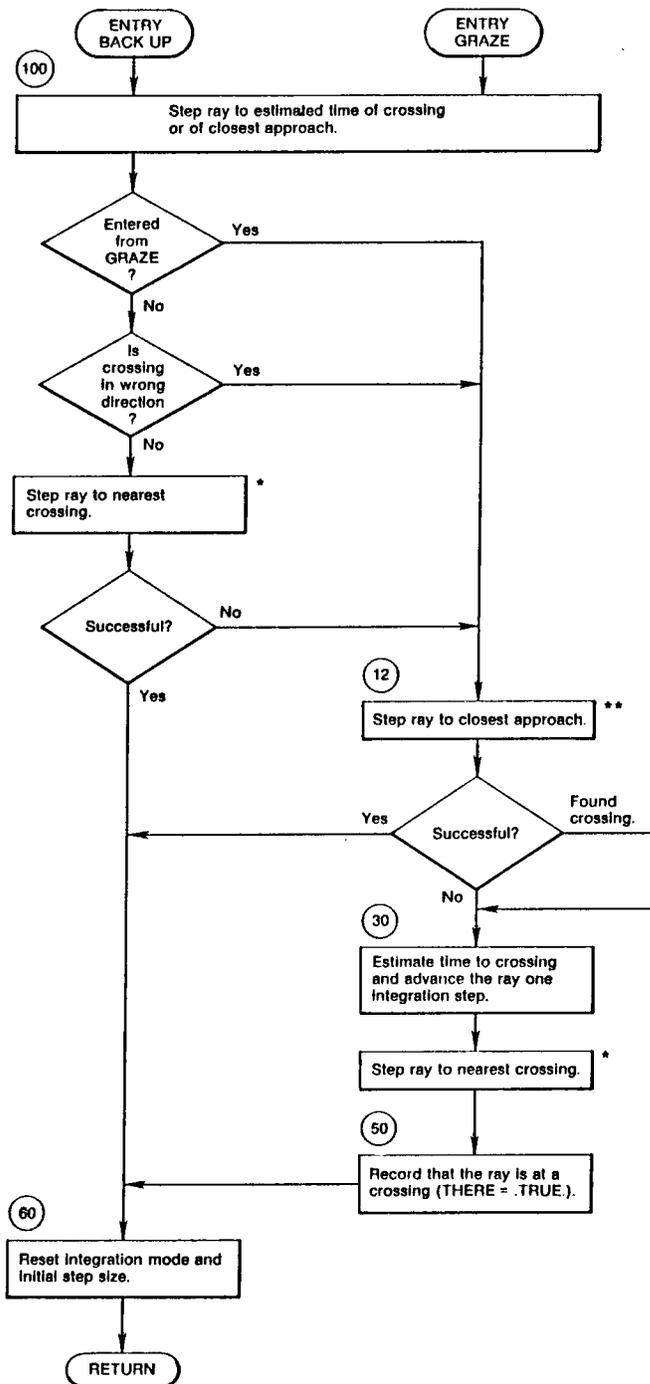


Figure 7.8. Flow chart for subroutine BACKUP. Circled block numbers correspond to program statement numbers. Entry BACKUP steps the ray to a crossing with a specified height. Entry GRAZE steps the ray to a point of closest approach to the specified height. The calling routine (subroutine TRACE) specifies the height with which the ray is to intersect, the direction of crossing (up or down), and estimates the time of crossing (group time delay). Asterisks identify supplementary procedures.

\* See Figure 7.9 for details of the algorithm that steps the ray by numerical integration to the nearest crossing of a specified height.

\*\* See Figure 7.10 for details of the algorithm that steps the ray by numerical integration to a closest approach to a specified height.

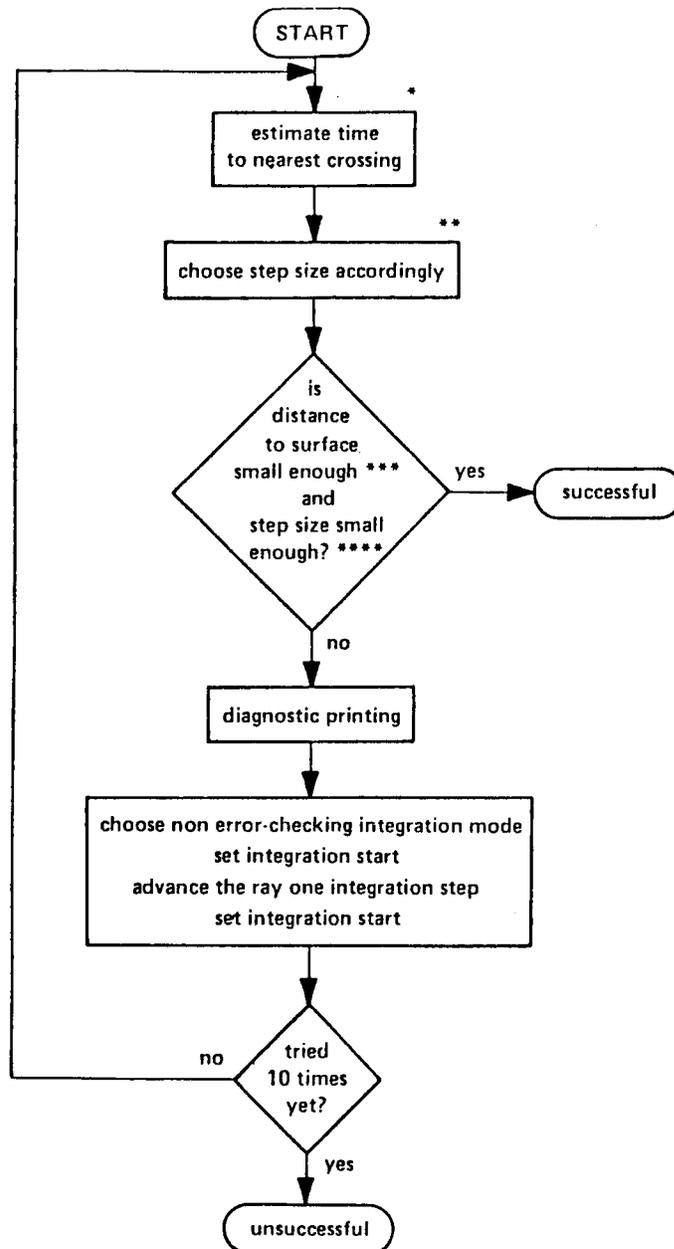


Figure 7.9. Flow chart for the algorithm that steps the ray by numerical integration to a crossing of a specified height. Circled block numbers correspond to program statement numbers.

\* See Equation (6.85) to estimate the time of the nearest crossing of the specified height.

\*\* The step size should be no larger than that being used by the numerical integration routine to maintain accuracy in the error-checking mode.

\*\*\*  $0.5 \times 10^{-4}$  km.

\*\*\*\* Small enough to ensure the required accuracy and smaller than the smallest allowable step size.

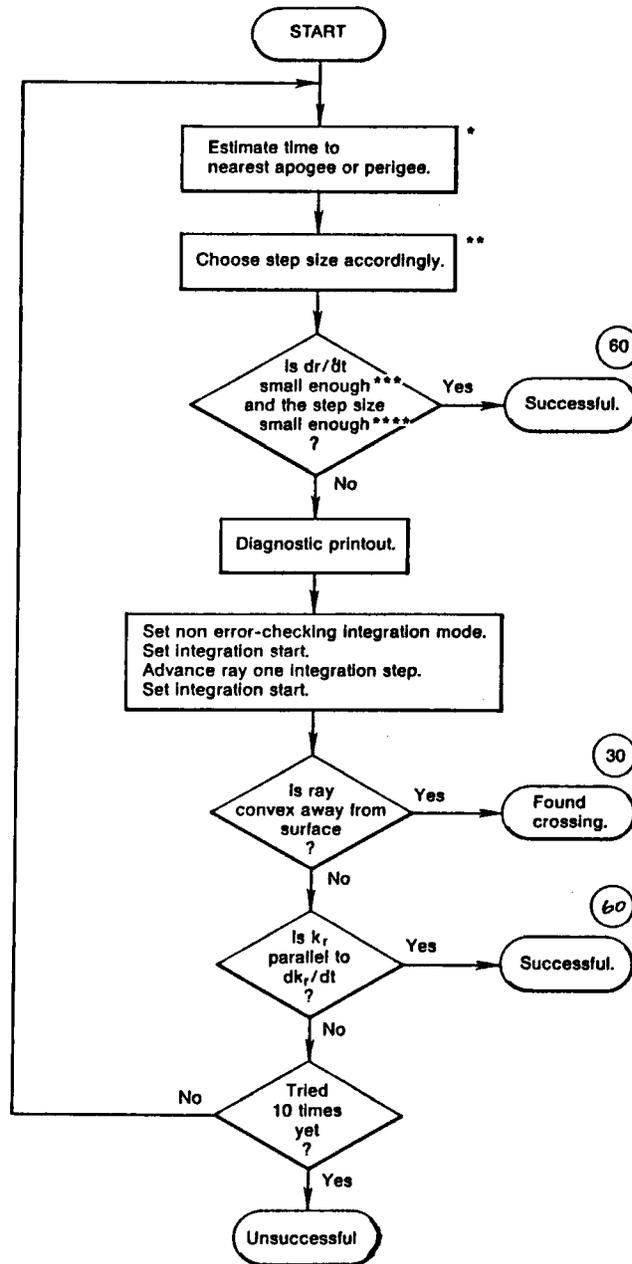


Figure 7.10. Flow chart for the algorithm that steps the ray by numerical integration to a point of closest approach to a specified height. Circled block numbers correspond to program statement numbers.

- \* See Equation (6.91) to estimate the time of the nearest crossing of the specified height.
- \*\* The step size should be no larger than that being used by the numerical integration routine to maintain accuracy in the error-checking mode.
- \*\*\*  $10^{-8}$  km/km.
- \*\*\*\* Small enough to ensure the required accuracy and smaller than the smallest allowable step size.

The listings of most of the subroutines have comments that should help in understanding how they work. In addition, Tables 7.1 through 7.40 define the variables in the common blocks.

Table 7.1--Definitions of the parameters in blank common

Position in common	Variable name	Definition
1-20	R	The dependent variables in the differential equations being integrated--the definitions of the first six are fixed, but the others may be varied by the program user
1	R(1) or R	$r$
2	R(2) or TH	$\theta$
3	R(3) or PH	$\phi$
4	R(4) or KR	$k_r$
5	R(5) or KTH	$k_\theta$
6	R(6) or KPH	$k_\phi$
7-12	R(7)-R(12) or RKVARS(1)- RKVARS(6)	Those variables the user has chosen to integrate, taken in the following order: P -phase path in kilometers A -absorption in decibels $\Delta f$ -Doppler shift in hertz s -geometrical path length in kilometers
13-20	R(13)-R(20)	Reserved for future expansion
21	TPULSE	Group path length in kilometers (the independent variable in the differential equations)
22	CSTEP	Step length in group path
23-42	DRDT	The derivatives of the dependent variables with respect to the independent variable TPULSE

R and TPULSE are initialized in program RAYTRC and changed in subroutines TRACE, RKAM, and BACK UP.

CSTEP is calculated in subroutine RKAM.

DRDT is calculated in subroutine HAMLTN and used in subroutine RKAM.

## 7.4 Common-Block Structure and Usage

We use common blocks instead of calling sequences to pass information between subroutines and functions because it is faster. This section describes how those common blocks are organized and which blocks link which program modules, and defines the variables in each block.

Table 7.1 defines the variables in blank common. These are mostly the dependent variables in the numerical integration and their derivatives. Nearly all of the subprograms use this common block.

Table 7.2 describes the common block /MCONST/, which contains mathematical constants. Table 7.3 describes the common block /PCONST/, which contains physical constants.

Many common blocks are used to communicate among the various routines in the program. Table 7.4 lists those common blocks and shows which routines use those common blocks. Blank common, common blocks /MCONST/, /PCONST/, /WW/, and the common blocks listed in Tables 4.2 and 4.3 are not included in Table 7.4. Table 7.5 lists the variable names in these common blocks that are used for input and output by each routine. Tables 7.6 through 7.32 list all of the variables in these common blocks and give the meanings of those variables.

Table 7.17 describes common block /RIN/, which contains parameters output by all of the versions of the dispersion relation subroutines (all of which have the entry point name DISPER). Tables 7.33 through 7.40 describe the common blocks /UU/, /CC/, /TT/, /MM/, /RR/, /GG/, /AA/, and /PP/, which contain the parameters output by the various atmospheric models.

Table 7.2--Definitions of the parameters in common block /MCONST/\*

Position in common	Variable name	Definition
1	PI	$\pi$
2	PIT2	$2\pi$
3	PID2	$\pi/2$
4	DEGS	$180.0/\pi$
5	RAD	$\pi/180.0$
6	ALN10	$\log_e 10$

\* These parameters are set in program RAYTRC.

Table 7.3--Definitions of the parameters in common block /PCONST/

Position in common	Variable name	Definition
1	CREF	A reference sound speed (0.344 km/s), the reference sound speed in air at 20°C, <u>Handbook of Chemistry and Physics</u> (1954, page 2312), used to convert group delay time in seconds to an equivalent group path length in kilometers, and to convert a phase time in seconds to an equivalent phase-path length in kilometers
2	RGAS	The gas constant, = $8.31436 \times 10^{-3}$ kg (kg mole) <sup>-1</sup> km <sup>2</sup> s <sup>-2</sup> K <sup>-1</sup> (this value of the gas constant gives a sound speed in km/s)
3	GAMMA	$\gamma$ , the ratio of specific heat at constant pressure to that at constant density, = 1.4



**Table 7.5--Input and output variables to routines in common blocks other than blank common and labeled common blocks /MCONST/, /PCONST/, and /WW/ and other than the common blocks listed in Tables 4.2 and 4.3**

Routine	<u>Input parameters</u>		<u>Output parameters</u>	
	common block	parameter name	common block	parameter name
RAYTRC	/FLG/	IHOP	/HDRC/	DAT
	/RIN/	KAY2	/HDRC/	INITID
	/FLG/	LINES	/FLG/	LINES
	/RK/	NEQS	/FLG/	NEWWP
	/ERR/	NERG	/FLG/	NEWWR
	/ERR/	NERP	/FILEC/	NPLTDP
	/ERR/	NERR	/FLGP/	NSET
	/ERR/	NERT	/HDR/	SEC
	/RAYDEV/	NRYIND	/HDRC/	TOD
	/RIN/	OMEGMAX	/RK/	RSTART
	/RIN/	OMEGMIN		
	/FLG/	PENET		
	/RIN/	SGN		
DFCNST			/CRMACH/	RMACH
READW1	/RAYDEV/	NDEVTMP		
	/RAYDEV/	NRYIND		
READW	/B1/→/B20/		/B1/→/B20/	
	/FLG/	LINES		
	/RAYDEV/	NDEVTMP		
	/RAYDEV/	NFRMAT		
	/RAYDEV/	NRYIND		
	/FLGP/	NSET		
UCON	/UONC/	CNVC	/UONV/	CNVV
	/UONV/	CNVV		
	/UONC/	PCV		
TRACE	/TRAC/	D2Z	/TRAC/	DROLD
	/TRAC/	GROUND	/RK/	E1MAX
	/CRKTIME/	IRKTIME	/RK/	E1MIN
	/TRAC/	RAD	/RK/	E2MAX
	/TRAC/	RAD1	/RK/	E2MIN
	/TRAC/	THERE	/RK/	FACT
	/TRAC/	ZDOT	/TRLOCAL/	FDOT
	/TRLOCAL/	RSIGN	/TRLOCAL/	GDOLD
	/TRLOCAL/	HOME	/TRLOCAL/	GDOT
	/TRLOCAL/	FDOT	/TRLOCAL/	GOLD
			/TRAC/	GROUND
			/TRAC/	HOME
			/FLG/	HPUNCH
			/FLG/	IHOP

Table 7.5--(continued)

Routine	<u>Input parameters</u>		<u>Output parameters</u>	
	common block	parameter name	common block	parameter name
TRACE (continued)			/CRKTIME/ /RK/ /TRAC/ /FLG/ /FLG/ /TRAC/ /TRLOCAL/ /RK/ /RK/ /TRAC/ /TRAC/	IRKTIME MODE NEWRAY NEWTRC PENET ROLD RSIGN RSTART STEP THERE TOLD
PCROSS	/TRAC/ /TRAC/	OSMT SMT		
RCROSS	/TRAC/ /TRAC/	RAD1 ZDOT	/TRLOCAL/ /TRLOCAL/ /FLG/ /TRLOCAL/ /RK/	FDOT HOME HPUNCH RSIGN RSTART
HAMLTN	/RIN/			
RKAM	/RKAMS/ /RK/ /RKAMS/ /CRKTIME/ /RKAMS/ /RK/ /RK/ /RK/ /RK/ /RK/ /RKAMS/ /RKAMS/	ALPHA E1MAX FV IRKTIME MM MODE NEQS RSTART STEP XV YU	/RK/ /CRKTIME/ /RKAMS/ /RK/ /RK/ /RKAMS/	E1MAX IRKTIME MM MODE NEQS XV
RKAM1	/RK/ /RK/ /RK/ /RK/ /RK/ /RK/ /RK/ /RK/ /RK/ /RK/ /RK/	E1MAX E1MIN E2MAX E2MIN FACT MODE NN RSTART SPACE	/RKAMS/ /RKAMS/ /RK/ /RK/ /RKAMS/ /RKAMS/ /RK/ /RK/ /RKAMS/ /RKAMS/	ALPHA EPM E1MIN FACT FV MM RSTART XV YU

Table 7.5--(continued)

Routine	Input parameters		Output parameters	
	common block	parameter name	common block	parameter name
BACKUP	/TRAC/	DROLD	/RK/	MODE
	/TRAC/	D2Z	/RK/	RSTART
	/RK/	E1MAX	/RK/	STEP
	/RK/	E2MIN	/TRAC/	THERE
	/RK/	FACT	/TRAC/	TOLD
	/RK/	MODE	/TRAC/	ZDOT
	/TRAC/	RAD1		
REFLECT	/FNDER/	NPZPH		
	/FNDER/	NPZR		
	/FNDER/	NPZTH		
FIT	/TRAC/	DROLD	/TRAC/	D2Z
	/FNDER/	NPZPH	/TRAC/	OSMT
	/FNDER/	NPZPHPH	/TRAC/	RAD
	/FNDER/	NPZR	/TRAC/	RAD1
	/FNDER/	NPZRPH	/TRAC/	SMT
	/FNDER/	NPZRR	/TRAC/	ZDOT
	/FNDER/	NPZRTH		
	/FNDER/	NPZTH		
	/FNDER/	NPZTHPH		
	/FNDER/	NPZTHTH		
	/FNDER/	NZ		
	/TRAC/	TOLD		
	GET	/CRKTIME/	IRKTIME	/FNDER/
/CRKTIME/		RKTIME	/FNDER/	NPZPHPH
/CRMACH/		RMACH	/FNDER/	NPZR
			/FNDER/	NPZRPH
			/FNDER/	NPZRR
			/FNDER/	NPZRTH
			/FNDER/	NPZTH
			/FNDER/	NPZTHPH
			/FNDER/	NPZTHTH
			/FNDER/	NSELECT
		/FNDER/	NTIME	
		/FNDER/	NZ	
		/CGET/	ZERO	
GET1	/CRKTIME/	IRKTIME	/CGET/	ZERO
	/CRKTIME/	RKTIME		
	/CRMACH/	RMACH		
CONBLK	/RAYDEV/	NRYIND	/UONC/	CNVC
			/UONV/	CNVV
			/CRKTIME/	IRKTIME
			/RIN/	KVECT

Table 7.5--(continued)

Routine	Input parameters		Output parameters	
	common block	parameter name	common block	parameter name
CONBLK (continued)			/RIN/	LPOLAR
			/RAYCON/	MCONP
			/RAYDEV/	NDEVTMP
			/RAYDEV/	NFRMAT
			/RAYDEV/	NRYIND
			/RIN/	OMEGMAX
			/RIN/	OMEGMIN
			/UONC/	PCV
			/RIN/	POLAR
			/RIN/	RAYNAME
			/HDRC/	DAT
			/HDRC/	INITID
			/PROCFL/	LIST
			/PROCFL/	PITBL
			/PROCFL/	PNTBL
			/HDR/	SEC
			/HDRC/	TOD
PRINTR	/FLG/	HPUNCH	/FLG/	LINES
	/FLG/	IHOP	/ERR/	NERG
	/RIN/	KAY2	/ERR/	NERP
	/FLG/	LINES	/ERR/	NERR
	/RK/	NEQS	/ERR/	NERT
	/FLG/	NTYP	/FLG/	NEWWP
	/RIN/	POLAR		
	/RIN/	TYPE		
ATMOSHD	/HDRC/	DAT	/FLG/	LINES
	/RINPL/	DISPM	/FLG/	NTYP
	/FLG/	LINES		
	/RIN/	MODRIN		
	/FLGP/	NSET		
	/RIN/	RAYNAME		
	/HDRC/	TOD		
PUTKST	/FLG/	LINES	/FLG/	LINES
RAYPLT	/FLG/	NEWTRC	/PLT/	ALPHA
	/FLG/	NEWWR	/PLT/	APLT
	/FILEC/	NPLTDP	/FLG/	NEWTRC
			/FLG/	NEWWR
			/PLT/	PRESET
			/PLT/	RMAX
			/PLT/	RMIN
			/PLT/	XL
			/PLT/	XR
			/PLT/	YB
			/PLT/	YT

Table 7.5--(continued)

Routine	Input parameters		Output parameters	
	common block	parameter name	common block	parameter name
PLOT	/PLT/	ALPHA	/DD/	IX
	/PLT/	APLT	/DD/	IY
	/PLT/	RESET	/PLT/	RESET
	/PLT/	RMAX		
	/PLT/	RMIN		
	/PLT/	XMAXO		
	/PLT/	XMINO		
	/PLT/	YMAXO		
LABPLT	/HDRC/	DAT	/DD/	IOR
	/RIN/	MODRIN	/DD/	IS
			/DD/	IT
			/DD/	IX
PLTANH	/RAYCON/	MCONP	/DD/	IOR
	/LABCLT/	PROJCT	/DD/	IX
	/LABCLT/	RMAX	/DD/	IY
	/LABCLT/	RMIN		
	/LABCLT/	THMAX		
SETXY			/LABCLT/	PROJCT
			/LABCLT/	RMAX
			/LABCLT/	RMIN
			/LABCLT/	THMAX
			/LABCLT/	THMIN
PLOTANOT	/ANNCTC/	ANOTES	/DD/	IOR
	/ANNCTC/	HNOTES	/DD/	IX
	/DD/	IX	/DD/	IY
	/DD/	IY		
	/ANNCTL/	LENA		
	/ANNCTL/	LENHA		
	/LABCLT/	THMAX		
	/LABCLT/	THMIN		
PLTLB	/DD/	IX	/DD/	IOR
	/DD/	IY	/DD/	IX
	/LABCLT/	PROJCT		
	/LABCLT/	RMAX		
	/LABCLT/	RMIN		

Table 7.5--(continued)

Routine	Input parameters		Output parameters	
	common block	parameter name	common block	parameter name
PLOTBL			/KNKN/ /DDLIM/	
DDBP	/DD/ /DD/ /KNKN/ /DDLIM/ /DDLIM/ /DDLIM/ /DDLIM/	IX IY KNBP MNIX MNIY MXIX MXIY	/KNKN/ /DDLIM/ /DDLIM/ /DDLIM/ /DDLIM/	KNBP MNIX MNIY MXIX MXIY
DDVC	/DD/ /DD/ /KNKN/ /DDLIM/ /DDLIM/ /DDLIM/ /DDLIM/	IX IY KNVC MNIX MNIY MXIX MXIY	/KNKN/ /DDLIM/ /DDLIM/ /DDLIM/ /DDLIM/	KNVC MNIX MNIY MXIX MXIY
DDTEXT	/DD/ /DD/ /DD/ /KNKN/	IOR IX IY KNDT	/KNKN/	KNDT

Table 7.6--Definitions of the parameters in common block /HDR/

Position in common	Variable name	Definition
1	SEC	Total elapsed computer calculation time at end of calculating previous raypath

**Table 7.7--Definitions of the parameters in common block /UONC/**

<b>Position in common</b>	<b>Variable name</b>	<b>Definition</b>
1-4	PCV	List of valid unit types for units conversion: blank (no conversion), AN (angle), LN (length), FQ (frequency)
5-20	CNVC	An array of lists of valid physical units for each unit type for units conversion: blank (no conversion), M (meters), KM (kilometers), DG (degrees), etc

**Table 7.8--Definitions of the parameters in common block /UONV/**

<b>Position in common</b>	<b>Variable name</b>	<b>Definition</b>
1-16	CNVV	An array of units conversion factors corresponding to the array CNVC in common block /UONC/

Table 7.9--Definitions of the parameters in common block /RKAMS/

Position in common	Variable name	Definition
1-5	XV	Values of independent variable for 5 integration steps
6-85	FV	Values of the derivatives of the 20 dependent variables for 4 integration steps
86-285	YU	Values of the 20 dependent variables for 5 integration steps (in double precision)
286	EPM	The amount by which the independent variable changed during the previous call to SUBROUTINE RKAM1
287	ALPHA	Value of the independent variable at the beginning of the latest integration step
288	MM	Relative integration step number (varies from 1 to 4)

Table 7.10--Definitions of the parameters in common block /CGET/

Position in common	Variable name	Definition
1	ZERO	A great circle distance at sea level corresponding to a central earth angle that is twice the smallest floating point variable that can be stored in one single precision word in the computer being used

Table 7.11--Definitions of the parameters in common block /CRMACH/

Position in common	Variable name	Definition
1	RMACH(1)	Smallest positive magnitude = $B^{(EMIN-1)}$
2	RMACH(2)	Largest magnitude = $B^{EMAX}*(1-B^{(-T)})$
3	RMACH(3)	Smallest relative spacing = $B^{(-T)}$
4	RMACH(4)	Largest relative spacing = $B^{(1-T)}$
5	RMACH(5)	$\text{Log}_{10} B = \text{Log}_{10} 2$

Notes: 1. B = the number base used by the computer (= 2 for most computers)  
 2. T = the number of bits in the mantissa of a floating point number  
 3. EMIN = the most negative allowable exponent  
 4. EMAX = the largest allowable positive exponent

Table 7.12--Definitions of the parameters in common block /CRKTIME/

Position in common	Variable name	Definition
1	IRKTIME	The number of times that SUBROUTINE RKAM has been called (used to compare FTIME or GTIME with to know whether F or G need to be updated)
1	RKTIME	Floating point name of IRKTIME

Table 7.13--Definitions of the parameters in common block /TRLOCAL/

Position in common	Variable name	Definition
1	RSIGN	+1 if next receiver-surface crossing is going up; -1 if going down
2	HOME	.TRUE. if ray is going away from receiver surface; .FALSE. otherwise
3	FDOT	Rate of change of distance of ray above the receiver surface
4	GDOT	Rate of change of distance of ray above the terrain
5	GOLD	Value of G at previous integration step (= distance of ray above terrain)
6	GDOLD	Value of GDOT at previous integration step

Table 7.14--Definitions of the parameters in common block /RK/\*

Position in common	Variable name	Definition
1	N	The number of equations being integrated
2	STEP	The initial step in group path in kilometers
3	MODE	Defines type of integration used (same as W41), see Section 5.3.2
4	E1MAX	Maximum allowable single step error (same as W42)
5	E1MIN	Minimum allowable single step error (= W42/W43)
6	E2MAX	Maximum step length (same as W45)
7	E2MIN	Minimum step length (same as W46)
8	FACT	Factor to use to decrease step length (same as W47)
9	RSTART	Nonzero to initialize numerical integration, zero to continue integration

\* These parameters are calculated in subroutine READW (some are temporarily reset in subroutine BACKUP) and are used in subroutine RKAM.

Table 7.15--Definitions of the parameters in common block /TRAC/\*

Position in common	Variable name	Definition
1	GROUND	.TRUE. if the ray is on the surface of the Earth
2	PERIGE	.TRUE. if the ray has just made a perigee
3	THERE	.TRUE. if the ray is at the receiver height
4	MINDIS	.TRUE. if the ray has just made a closest approach to the receiver height
5	NEWRAY	Not used in this version of the program
6	SMT	An estimation of the vertical distance to an apogee or perigee of the ray
7	OSMT	Value of SMT at previous integration step
8-27	ROLD	Value of R(1) (=r in r,θ,φ earth- centered spherical polar coordinate system) at previous integration step
28-47	DROLD	Value of dr/dt at previous integra- tion step
48	TOLD	Value of t (= independent variable for numerical integration) at previous integration step
49	ZDOT	dZ/dt (= dF/dt or dG/dt, depending on the situation)
50	D2Z	d <sup>2</sup> Z/dt <sup>2</sup> (= d <sup>2</sup> F/dt <sup>2</sup> or d <sup>2</sup> G/dt <sup>2</sup> , depending on the situation)
51	RAD	(dZ/dt) <sup>2</sup> - 2 Z d <sup>2</sup> Z/dt <sup>2</sup>
52	RAD1	√RAD

\* These parameters are used for communication between subroutines TRACE and BACKUP.

Table 7.16--Definitions of the parameters in common block /FINDER/

Position in common	Variable name	Definition	Value
1	NZ	Relative position of F in common block /RR/ (or G in common block /GG/)	1
2	NPZR	Relative position of PFR in common block /RR/ (or PGR in common block /GG/)	2
3	NPZRR	Relative position of PFRR in common block /RR/ (or PGRR in common block /GG/)	3
4	NPZRTH	Relative position of PFRTH in common block /RR/ (or PGRTH in common block /GG/)	4
5	NPZRPH	Relative position of PFRPH in common block /RR/ (or PGRPH in common block /GG/)	5
6	NPZTH	Relative position of PFTH in common block /RR/ (or PGTH in common block /GG/)	6
7	NPZPH	Relative position of PFPH in common block /RR/ (or PGPH in common block /GG/)	7
8	NPZTHTH	Relative position of PFTHTH in common block /RR/ (or PGTHTH in common block /GG/)	8
9	NPZPHPH	Relative position of PFPHPH in common block /RR/ (or PGPHPH in common block /GG/)	9
10	NPZTHPH	Relative position of PFTHPH in common block /RR/ (or PGTHPH in common block /GG/)	10
11	NSELECT	Relative position of FSELECT in common block /RR/ (or GSELECT in common block /GG/)	11
12	NTIME	Relative position of FTIME in common block /RR/ (or GTIME in common block /GG/)	12

Table 7.17--Definition of the parameters in common block /RIN/\*

Position in common	Variable name	Definition
1-8	MODRIN	Description of version of DISPER in BCD
9-14	RAYNAME	Hollerith names of the characteristic rays in a birefringent medium (= blank for this version of the program)
15-17	TYPE	= Hollerith 1 or 3 if this version of DISPER includes wind, = Hollerith 2 or 3 if this version of DISPER includes losses
18	SPACE	TRUE, if the ray is in a homogeneous non-dissipative medium (Unconditionally set to FALSE in this version of the program)
19	OMEGMIN	Minimum frequency for nonevanescant propagation (= 0 for this version of the program)
20	OMEGMAX	Maximum frequency for nonevanescant propagation (not applicable for this version of the program, set to 0)
21,22	KAY2	$k^2$ , square of the complex wave number
23,24	H	Hamiltonian (complex)
25,26	PHPT	$\partial H/\partial t$ (complex)
27,28	PHPR	$\partial H/\partial r$ (complex)
29,30	PHPTH	$\partial H/\partial \theta$ (complex)
31,32	PHPPH	$\partial H/\partial \phi$ (complex)
33,34	PHPOM	$\partial H/\partial \omega$ (complex)
35,36	PHPKR	$\partial H/\partial k_r$ (complex)
37,38	PHPKTH	$\partial H/\partial k_\theta$ (complex)
39,40	PHPKPH	$\partial H/\partial k_\phi$ (complex)
41,42	KPHPK	$\vec{k} \cdot \partial H/\partial \vec{k}$ (complex) = $k_r \partial H/\partial k_r + k_\theta \partial H/\partial k_\theta + k_\phi \partial H/\partial k_\phi$
43,44	POLAR	Characteristic transverse polarization of the wave (complex) (= 0 for this version of the program)
45,46	LPOLAR	Characteristic longitudinal polarization of the wave (complex) (= 1 for this version of the program)
47	SGN	= +1 or -1; used for ray tracing in complex space

\* These parameters are calculated in subroutine DISPER and used in subroutine HAMLTN.

Note: In some subroutines, the real and imaginary parts of the complex variables have separate names.

Table 7.18--Definitions of the parameters in common block /ERR/

Position in common	Variable name	Definition
1	NERG	Index number for the dependent variable for the integration that gives G
2	NERR	Index number for the dependent variable for the integration that gives $\partial G/\partial r$
3	NERT	Index number for the dependent variable for the integration that gives $\partial G/\partial \theta$
4	NERP	Index number for the dependent variable for the integration that gives $\partial G/\partial \phi$

Table 7.19--Definitions of the parameters in common block /RAYDEV/

Position in common	Variable name	Definition
1	NRYIND	Device unit number for input data
2	NDEVTMP	Device unit number for temporary output and input
3	NFRMAT	Device unit number for secondary input file (not used by ray tracing program)
4		Device unit number for graphics output
5		Device unit number for binary raypath coordinate output

**Table 7.20--Definitions of the parameters in common block /FLGP/**

<b>Position in common</b>	<b>Variable name</b>	<b>Definition</b>
1	NSET	Runset number

**Table 7.21--Definitions of the parameters in common block /RINPL/**

<b>Position in common</b>	<b>Variable name</b>	<b>Definition</b>
1	DISPM	Character string identifier for the dispersion relation model

Table 7.22--Definitions of the parameters in common block /FLG/\*

Position in COMMON	Variable	Definition
1	NTYP	Wave polarization indicator (not used in this version of program)
2	NEWWR	Set equal to .TRUE. to tell sub- routine RAYPLT there is a new W array
3	NEWWP	Set equal to .TRUE. to tell sub- routine PRINTR there is a new W array
4	PENET	Set equal to .TRUE. if the ray left the allowed region of the atmosphere
5	LINES	Number of lines printed on the cur- rent page
6	IHOP	Hop number (at the beginning of each ray, subroutine TRACE sets this parameter to zero so that subroutine RAYPLT will begin a new line in plotting the raypath, and subroutine PRINTR will print column headings and punch a transmitter rayset)
7	HPUNCH	The height to be output on the ray- sets

\* The parameters are used to communicate between various subroutines.

Table 7.23--Definitions of the parameters in common block /RINPL/

Position in common	Variable name	Definition
1	DISPM	Character string identifier for the dispersion relation model

Table 7.24--Definitions of the parameters in common block /FILEC/

Position in common	Variable name	Definition
1	NPLTDP	Set equal to the device unit number for binary raypath coordinate output (variable in position 5 of common block /RAYDEV/) if binary raypath coordinate output has been requested, set to zero otherwise

Table 7.25--Definitions of the parameters in common block /PLT/\*

Position in common	Variable name	Definition
1	XMINO,XL	The x-coordinate of the left side of the plotting area in kilometers
2	XMAXO,XR	The x-coordinate of the right side of the plotting area in kilometers
3	XMINO,YB	The y-coordinate of the bottom of the plotting area in kilometers
4	XMAXO,YT	The y-coordinate of the top of the plotting area in kilometers
5	RESET	Set equal to one whenever the plotting area is changed

\* These parameters are used for communication between subroutine RAYPLT and subroutine PLOT.

Table 7.26--Definitions of the parameters in common block /RAYCON/

Position in COMMON	Variable name	Definition
1	MCONP	Set to zero for the raytracing program to indicate that the abscissa in raypath plots is a central-earth angle in radians, set non-zero for the contouring program to indicate that the abscissa in contour plots is a great-circle distance in kilometers

Table 7.27--Definitions of the parameters in common block /ANNCTC/

Position in COMMON	Variable name	Definition
1-8	ANOTES	Character strings to label the ordinate of raypath plots
9-20	HNOTES	Character strings to label the abscissa of raypath plots

Table 7.28--Definitions of the parameters in common block /ANNCTL/

Position in COMMON	Variable name	Definition
1-4	LENA	Lengths of the character strings that label the ordinate of raypath plots
5-7	LENHA	Lengths of the character strings that label the abscissa of raypath plots

Table 7.29--Definitions of the parameters in common block /LABCLT/

Position in common	Variable name	Definition
1	PROJCT	Number that indicates which type of projection is being used for raypath plots
2	THMIN	$\theta_{\min}$ , minimum value of the abscissa of a raypath plot
3	THMAX	$\theta_{\max}$ , maximum value of the abscissa of a raypath plot
4	RMIN	$r_{\min}$ , minimum value of the ordinate of a raypath plot
5	RMAX	$r_{\max}$ , maximum value of the ordinate of a raypath plot

Table 7.30--Definitions of the parameters in common block /DD/

Position in common	Variable name	Definition
1	IN	Intensity IN = 0 specifies normal intensity IN = 1 specifies high intensity
2	IOR	Orientation IOR = 0 specifies upright orientation IOR = 1 specifies rotated orientation (90° counterclockwise)
3	IT	Italics (Font) IT = 0 specifies non-italic (Roman) symbols IT = 1 specifies italic symbols
4	IS	Symbol size IS = 0 specifies miniature size IS = 1 specifies small size IS = 2 specifies medium size IS = 3 specifies large size
5	IC	Symbol case IC = 0 specifies uppercase IC = 1 specifies lowercase
6	ICC	Character code, 0-63 (R1 format) ICC and IC together specify the symbol plotted
7	IX	X-coordinate, 0-1023
8	IY	Y-coordinate, 0-1023

Table 7.31--Definitions of the parameters in common block /KNKN/

Position in common	Variable name	Definition
1	KNBP	Number of times SUBROUTINE DDBP was called
2	KNVC	Number of times SUBROUTINE DDVC was called
3	KNDT	Number of times SUBROUTINE DDTEXT was called

Table 7.32--Definitions of the parameters in common block /DDLIM/

Position in common	Variable name	Definition
1	MXIX	Maximum value of IX
2	MXIY	Maximum value of IY
3	MNIX	Minimum value of IX
4	MNIY	Minimum value of IY

Table 7.33--Definitions of the parameters in common block /UU/

Position in common	Variable name	Definition
1-4	MODU	Wind-velocity model and parameter identification
1	MODU(1)	Name of wind-velocity subroutine
2	MODU(2)	Wind-velocity parameter identification number
3	MODU(3)	Name of wind-velocity perturbation subroutine
4	MODU(4)	Wind-velocity perturbation parameter identification number
5	V	$ V $ , wind speed in km/s
6	PVT	$\partial V /\partial t$
7	PVR	$\partial V /\partial r$
8	PVTH	$\partial V /\partial \theta$
9	PVPH	$\partial V /\partial \phi$
10	VR	$V_r$ , upward component of wind velocity
11	PVRT	$\partial V_r/\partial t$
12	PVRR	$\partial V_r/\partial r$
13	PVRRTH	$\partial V_r/\partial \theta$
14	PVRPH	$\partial V_r/\partial \phi$
15	VTH	$V_\theta$ , southward component of wind velocity
16	PVTHT	$\partial V_\theta/\partial t$
17	PVTHR	$\partial V_\theta/\partial r$
18	PVTHTH	$\partial V_\theta/\partial \theta$
19	PVTHPH	$\partial V_\theta/\partial \phi$
20	VPH	$V_\phi$ , eastward component of wind velocity
21	PVPHT	$\partial V_\phi/\partial t$
22	PVPHR	$\partial V_\phi/\partial r$
23	PVPHTH	$\partial V_\phi/\partial \theta$
24	PVPHPH	$\partial V_\phi/\partial \phi$

Table 7.34--Definitions of the parameters in common block /CC/

Position in	Variable	Definition	common	name
1-4	MODC	Sound-speed model and parameter identification		
1	MODC(1)	Name of sound-speed subroutine		
2	MODC(2)	Sound-speed parameter identification number		
3	MODC(3)	Name of sound-speed perturbation subroutine		
4	MODC(4)	Sound-speed perturbation parameter identification number		
5	CS	$c^2$ , square of sound speed in $\text{km}^2/\text{s}^2$		
6	PCST	$\partial c^2 / \partial t$		
7	PCSR	$\partial c^2 / \partial r$		
8	PCSTH	$\partial c^2 / \partial \theta$		
9	PCSPH	$\partial c^2 / \partial \phi$		

Table 7.35--Definitions of the parameters in common block /TT/

Position in common	Variable name	Definition
1-4	MODT	Temperature model and parameter identification
1	MODT(1)	Name of temperature subroutine
2	MODT(2)	Temperature parameter identifica- tion number
3	MODT(3)	Name of temperature-perturbation subroutine
4	MODT(4)	Temperature-perturbation-parameter identification number
5	T	T, temperature in kelvins
6	PTT	$\partial T / \partial t$
7	PTR	$\partial T / \partial r$
8	PTTH	$\partial T / \partial \theta$
9	PTPH	$\partial T / \partial \phi$

Table 7.36--Definitions of the parameters in common block /MM/

Position in common	Variable name	Definition
1-4	MODM	Molecular weight model and parameter identification
	MODM(1)	Name of molecular weight subroutine
2	MODM(2)	Parameter identification number for molecular weight model
3	MODM(3)	Unused now
4	MODM(4)	Unused now
5	M	M, mean molecular weight
6	PMT	$\partial M / \partial t$
7	PMR	$\partial M / \partial r$
8	PMTH	$\partial M / \partial \theta$
9	PMPH	$\partial M / \partial \phi$

Table 7.37--Definitions of the parameters in common block /RR/

Position in common	Variable name	Definition
1-4	MODREC	Receiver-surface model and parameter identification
1	MODREC(1)	Name of receiver-surface subroutine
2	MODREC(2)	Parameter identification number for receiver-surface model
3	MODREC(3)	Unused now
4	MODREC(4)	Unused now
5	F	$f(r, \theta, \phi)$ defined in (6.72)-(6.74)
6	PFR	$\partial f / \partial r$
7	PFRR	$\partial^2 f / \partial r^2$
8	PFRTH	$\partial^2 f / \partial r \partial \theta$
9	PFRPH	$\partial^2 f / \partial r \partial \phi$
10	PFTH	$\partial f / \partial \theta$
11	PFPH	$\partial f / \partial \phi$
12	PFTHTH	$\partial^2 f / \partial \theta^2$
13	PFPHPH	$\partial^2 f / \partial \phi^2$
14	PFTHPH	$\partial^2 f / \partial \theta \partial \phi$
15	FSELECT	= "RECEIVER"
16	FTIME	An integer that is initialized to equal -1 at the beginning of each raypath calculation and is incremented by 1 at each integration step so that it is possible to determine whether the variables in this common block are current

Table 7.38--Definitions of the parameters in common block /GG/

Position in common	Variable name	Definition
1-4	MODG	Terrain model and parameter identification
1	MODG(1)	Name of terrain subroutine
2	MODG(2)	Terrain-parameter identification number
3	MODG(3)	Name of terrain-perturbation subroutine
4	MODG(4)	Terrain-perturbation parameter identification number
5	G	$g(r, \theta, \phi)$ defined in the same way as $f(r, \theta, \phi)$ in (6.72)-(6.74)
6	PGR	$\partial g / \partial r$
7	PGRR	$\partial^2 g / \partial r^2$
8	PGRTH	$\partial^2 g / \partial r \partial \theta$
9	PGRKPH	$\partial^2 g / \partial r \partial \phi$
10	PGTH	$\partial g / \partial \theta$
11	PGPH	$\partial g / \partial \theta$
12	PGTHTH	$\partial^2 g / \partial \theta^2$
13	PGPHPH	$\partial^2 g / \partial \phi^2$
14	PGTHPH	$\partial^2 g / \partial \theta \partial \phi$
15	GSELECT	= "TERRAIN"
16	GTIME	An integer that is initialized to equal -1 at the beginning of each raypath calculation and is incremented by 1 at each integration step so that it is possible to determine whether the variables in this common block are current

Table 7.39--Definitions of the parameters in common block /AA/

Position in common	Variable name	Definition
1-4	MODA	Viscosity/thermal conductivity model and parameter identification
1	MODA(1)	Name of viscosity/thermal conductivity subroutine
2	MODA(2)	Viscosity/thermal conductivity parameter identification number
3	MODA(3)	Name of viscosity/thermal conductivity perturbation subroutine
4	MODA(4)	Viscosity/thermal conductivity perturbation parameter identification number
5	MU	$\mu$ , viscosity
6	MUPT	$\partial\mu/\partial t$
7	MUPR	$\partial\mu/\partial r$
8	MUPTH	$\partial\mu/\partial\theta$
9	MUPPH	$\partial\mu/\partial\phi$
10	KAPPA	$\kappa$ , thermal conductivity
11	KAPPT	$\partial\kappa/\partial t$
12	KAPPR	$\partial\kappa/\partial r$
13	KAPPTH	$\partial\kappa/\partial\theta$
14	KAPPPH	$\partial\kappa/\partial\phi$

Table 7.40--Definitions of the parameters in common block /PP/

Position in common	Variable name	Definition
1-4	MODP	Pressure model and parameter identification
1	MODP(1)	Name of pressure subroutine
2	MODP(2)	Pressure-parameter identifica- tion number
3	MODP(3)	Name of pressure-perturbation subroutine
4	MODP(4)	Pressure-perturbation parameter identification number
5	P	P, pressure
6	PPT	$\partial p / \partial t$
7	PPR	$\partial p / \partial r$
8	PPTH	$\partial p / \partial \theta$
9	PPPH	$\partial p / \partial \phi$

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## APPENDIX A: PRINTOUT AND RAYSET LISTING FOR THE SAMPLE CASE

This appendix contains an abbreviated printout and rayset listing for the sample case. To save space, we have listed the printout for an elevation-angle increment of  $20^\circ$  instead of  $5^\circ$ , the increment used to produce the ray plots and raysets. Users should compare their sample-case output with this printout to be sure they are identical. The meanings of the printed quantities are explained in Sections 2.5.1 and 2.5.2, and the meanings of rayset quantities are listed in Figures 2.9 and 2.10.

\*\*\*\*\* H A R P A \*\*\*\*\*  
 HAMILTONIAN ACOUSTIC RAY-TRACING PROGRAM FOR THE ATMOSPHERE

BY  
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RUN SET NUMBER 1  
 ATMOSPHERIC MODEL ID — S03  
 ATMOSPHERIC MODEL DESCRIPTION — SAMPLE CASE FOR HARPA DOCUMENTATION REV. 2-10-86

MODEL TYPE	SUBROUTINE NAME	DATA SET ID	DESCRIPTION
DISPERSION RELATION	AWWL	3.00	ACOUSTIC WAVE *** WITH WIND ***** WITH LOSSES
BACKGROUND WIND VELOCITY	ULOGZ2	.00	LOGARITHMIC EASTWARD WIND PROFILE. U*=.5 M/S. Z0=1 KM
WIND VELOCITY PERTURBATION	NPWIND	.00	NO WIND PERTURBATION
BACKGROUND SOUND SPEED	GAMRTDM	.00	SOUND SPEED IN TERMS OF TEMPERATURE MODEL
BACKGROUND SOUND SPEED PERTURBATION	CBLOB2	2.00	50% INCREASE IN SQ. SOUND SPEED AT 125KM HT, 335KM N, 125KM E
BACKGROUND TEMPERATURE	TTANH5	1.00	U.S. STANDARD ATMOSPHERE 1962 TEMPERATURE PROFILE
TEMPERATURE PERTURBATION	TBLOB2	2.00	50% CYLINDRICAL INCREASE IN TEMPERATURE AT 105KM N., 105 KM W
MOLECULAR WEIGHT	MCONST	29.00	MOLECULAR WEIGHT = 29
BACKGROUND TERRAIN	GLORENZ	2.00	RIDGE 2-KM HIGH, 30-KM WIDE ALONG EQUATOR
TERRAIN PERTURBATION	NPERR	.00	NO TERRAIN PERTURBATION
BACKGROUND VISCOSITY/ THERMAL CONDUCTIVITY	MJURDC	1.00	ARDC VISCOSITY AND THERMAL CONDUCTIVITY MODEL
VISCOSITY/THERMAL CONDUCTIVITY PERTURBATION	NPABSR	.00	NO VISCOSITY/CONDUCTIVITY PERTURBATION
BACKGROUND PRESSURE	PEXP	1.00	EXPONENTIAL PRESSURE MODEL, SCALE HEIGHT = 8.5 KM
PRESSURE PERTURBATION	NPRES	.00	NO PRESSURE PERTURBATION
RECEIVER SURFACE	RTERR	.00	RECEIVER SURFACE 5 KM ABOVE TERRAIN

INPUT DATA FILE FOR RUN SET NUMBER 1

S03-1 SAMPLE CASE FOR HARPA DOCUMENTATION REV. 2-10-86  
 1 6370. EARTH RADIUS, KM (6370.)  
 3 13. TRANSMITTER HEIGHT, KM (T=ABOVE TERRAIN)  
 4 200. N. TRANSMITTER LATITUDE, KM  
 5 0. E. TRANSMITTER LONGITUDE, KM  
 7 .05 INITIAL FREQUENCY, HZ  
 11 45. INITIAL AZIMUTH ANGLE, DEG  
 15 -20. INITIAL ELEVATION ANGLE, DEG  
 16 140. FINAL ELEVATION ANGLE, DEG  
 17 20. STEP IN ELEVATION ANGLE, DEG  
 20 5. RECEIVER HEIGHT, KM  
 22 3. MAXIMUM NUMBER OF HOPS (1.0)  
 23 1000. MAXIMUM NUMBER OF STEPS PER HOP (1000.)  
 26 500. MAXIMUM RAY HEIGHT, KM (500.)  
 27 -1. MINIMUM RAY HEIGHT, KM  
 28 1000. MAXIMUM RANGE, KM  
 29 0000100. DO: EIGRAY/RNG-TIM/RNG-ELV/NEW-PROJ/RAYTRC/CONT/PROF  
 33 999.999 MAXIMUM ABSORPTION, DB (999.999)  
 42 1.0E-6 SINGLE-STEP INTEGRATION ERROR (1.0E-4)  
 44 .1 INITIAL INTEGRATION STEP SIZE, KM (1.0)  
 57 2. PHASE PATH (0=NO; 1=INTEGRATE; 2=INTEGRATE/PRINT)  
 58 2. ABSORPTION (0=NO; 1=INTEGRATE; 2=INTEGRATE/PRINT)  
 60 2. PATH LENGTH (0=NO; 1=INTEGRATE; 2=INTEGRATE/PRINT)  
 71 50. NUMBER OF INTEGRATION STEPS PER PRINT [1.E31]  
 72 1. OUTPUT RAYSETS (1=YES; 0=NO)  
 73 0. DIAGNOSTIC PRINTOUT (1=YES; 0=NO)  
 74 0. PRINT RAY STEPS (0=YES; 1=NO)  
 75 .15 FULANN LETTER HEIGHT [0.15 IN]  
 76 0. BINARY RAY OUTPUT (1=YES; 0=NO)  
 77 57. LINES PER PAGE IN PRINTOUT (57.)  
 81 1. RAYPLOT PROJECTION (1=VERT; 2=HORIZ) PLANE  
 82 1. PLOT-EXPANSION FACTOR [1.0]  
 83 -100. N. LATITUDE OF LEFT PLOT EDGE, KM  
 84 -300. E. LONGITUDE OF LEFT PLOT EDGE, KM  
 85 500. N. LATITUDE OF RIGHT PLOT EDGE, KM  
 86 300. E. LONGITUDE OF RIGHT PLOT EDGE, KM  
 87 100. AN KM DISTANCE BETWEEN TIC MARKS, KM  
 88 0. HEIGHT ABOVE SEA LEVEL OF BOTTOM OF GRAPH, KM  
 89 300. HEIGHT ABOVE SEA LEVEL OF TOP OF GRAPH, KM  
 96 100. DISTANCE BETWEEN VERTICAL TIC MARKS, KM  
 100 6. ULOG22 WIND MODEL CHECK NUMBER  
 102 3. BACKGROUND WIND DATA SET ID  
 103 5. REFERENCE WIND SPEED, M/S  
 104 .35 VON KARMAN'S CONSTANT  
 105 1. ROUGHNESS HEIGHT, KM  
 150 1. GAMRTDM SOUND SPEED MODEL CHECK NUMBER  
 175 2. CBLOB2 MODEL CHECK NUMBER  
 177 2. SOUND SPEED PERTURBATION DATA SET ID  
 178 .5 FRACTIONAL INCREASE OF SQUARED SOUND SPEED  
 179 125. HEIGHT OF MAXIMUM INCREASE, KM

180	335.	AN KM	N. LATITUDE OF MAXIMUM INCREASE, KM
181	125.	AN KM	E. LONGITUDE OF MAXIMUM INCREASE, KM
182	25.		GAUSSIAN WIDTH IN HEIGHT OF INCREASE, KM
183	50.	AN KM	N-S WIDTH OF THE INCREASE, KM
184	25.	AN KM	E-W WIDTH OF THE INCREASE, KM
200	7.		TTANH5 TEMPERATURE MODEL CHECK NUMBER
202	1.		BACKGROUND TEMPERATURE DATA SET ID
225	2.		TBLOB2 MODEL CHECK NUMBER
227	2.		TEMPERATURE PERTURBATION DATA SET ID
228	-5		FRACTIONAL TEMPERATURE INCREASE
229	0.		HEIGHT OF MAXIMUM INCREASE, KM
230	105.	AN KM	N. LATITUDE OF MAXIMUM INCREASE, KM
231	-105.	AN KM	E. LONGITUDE OF MAXIMUM INCREASE, KM
232	0.		GAUSSIAN WIDTH IN HEIGHT OF INCREASE, KM
233	50.	AN KM	N-S WIDTH OF THE INCREASE, KM
234	25.	AN KM	E-W WIDTH OF THE INCREASE, KM
250	1.		MCONST MOLECULAR WEIGHT MODEL CHECK NUMBER
252	29.		MOLECULAR WEIGHT DATA SET ID
253	29.		MOLECULAR WEIGHT
275	2.		RTERR RECEIVER MODEL CHECK NUMBER
300	4.		GLORENZ TERRAIN MODEL CHECK NUMBER
302	2.		TERRAIN MODEL DATA SET ID
303	2.		HEIGHT OF THE RIDGE, KM
304	0.		N. LATITUDE OF THE RIDGE CENTER
305	30.	AN KM	HALF-WIDTH OF THE RIDGE, KM
325	0.		NPTERR NO TERRAIN PERTURBATION
500	1.		MUARDC VISC/COND MODEL CHECK NUMBER
502	1.		VISC/COND MODEL DATA SET ID
503	1.458E-06		VISCOSITY COEFFICIENT BETA
504	110.4		SUTHERLAND'S CONSTANT, KELVINS
505	1.91		PRANDTL NUMBER
525	0.		NPABS NO VISC/COND PERTURBATION
550	1.		PEXP PRESSURE MODEL CHECK NUMBER
552	1.		BACKGROUND PRESSURE MODEL DATA SET ID
553	101328.		PRESSURE AT SEA LEVEL, N/SQ.M.
554	8.5		PRESSURE SCALE HEIGHT, KM
575	0.		NPPRES NO PRESSURE PERTURBATION
-1			DATA SUBSET FOR BACKGROUND WIND MODEL
A			LOGARITHMIC EASTWARD WIND PROFILE, U*=.5 M/S, Z0=1 KM
0			RETURN TO W ARRAY DATA SET
-2			DATA SUBSET FOR WIND PERTURBATION MODEL
A			NO WIND PERTURBATION
0			RETURN TO W ARRAY DATA SET
-3			DATA SUBSET FOR BACKGROUND SOUND-SPEED MODEL
A			SOUND SPEED IN TERMS OF TEMPERATURE MODEL
0			RETURN TO W ARRAY DATA SET
-4			DATA SUBSET FOR SOUND-SPEED PERTURBATION MODEL
A			50% INCREASE IN SQ. SOUND SPEED AT 125KM HT, 335KM N, 125KM E
0			RETURN TO W ARRAY DATA SET
-5			DATA SUBSET FOR TEMPERATURE MODEL
A			U.S. STANDARD ATMOSPHERE 1962 TEMPERATURE PROFILE
3	999.0		TEMPERATURE PROFILE FOR 1962 STD ATMOSPHERE
0.	288.000		0.
15.0000	190.500		10.0000
52.0000	320.000		7.50000

95.0000	191.000	10.0000
165.0000	1451.000	50.0000
300.0000	1586.000	0.
999.0000		

0 RETURN TO W ARRAY DATA SET  
 0 DATA SUBSET FOR TEMPERATURE PERTURBATION MODEL  
 -6 A 50% CYLINDRICAL INCREASE IN TEMPERATURE AT 105KM N., 105 KM W  
 0 RETURN TO W ARRAY DATA SET  
 0 DATA SUBSET FOR MOLECULAR WEIGHT MODEL  
 -7 A MOLECULAR WEIGHT = 29  
 0 RETURN TO W ARRAY DATA SET  
 0 DATA SUBSET FOR RECEIVER SURFACE MODEL  
 -8 A RECEIVER SURFACE 5 KM ABOVE TERRAIN  
 0 RETURN TO W ARRAY DATA SET  
 0 DATA SUBSET FOR TERRAIN MODEL  
 -9 A RIDGE 2-KM HIGH, 30-KM WIDE ALONG EQUATOR  
 0 RETURN TO W ARRAY DATA SET  
 0 DATA SUBSET FOR TERRAIN PERTURBATION MODEL  
 -10 A NO TERRAIN PERTURBATION  
 0 RETURN TO W ARRAY DATA SET  
 0 DATA SUBSET FOR VISC/COND MODEL  
 -17 A ARDC VISCOSITY AND THERMAL CONDUCTIVITY MODEL  
 0 RETURN TO W ARRAY DATA SET  
 -18 A NO VISCOSITY/CONDUCTIVITY PERTURBATION  
 0 DATA SUBSET FOR VISC/COND PERTURBATION MODEL  
 0 RETURN TO W ARRAY DATA SET  
 -19 A EXPONENTIAL PRESSURE MODEL, SCALE HEIGHT = 8.5 KM  
 0 DATA SUBSET FOR BACKGROUND PRESSURE MODEL  
 0 RETURN TO W ARRAY DATA SET  
 -20 A NO PRESSURE PERTURBATION  
 0 DATA SUBSET FOR PRESSURE PERTURBATION MODEL  
 0 RETURN TO W ARRAY DATA SET  
 0 \*\*\*\*\* END OF RUN SET NUMBER 1 \*\*\*\*\*

INITIAL VALUES FOR THE W ARRAY  
ONLY NONZERO VALUES PRINTED -- ALL ANGLES IN RADIANs

N	W(N)	N	W(N)
1	.6370000000000000E+04	175	.2000000000000000E+01
3	.130440097799511E+02	177	.2000000000000000E+01
4	.313971742543171E-01	178	.5000000000000000E+00
7	.314159265358979E+00	179	.1250000000000000E+03
11	.785398163397446E+00	180	.525902668759810E-01
15	-.349065850398864E+00	181	.196232339089482E-01
16	.244346095279205E+01	182	.2500000000000000E+02
17	.349065850398864E+00	183	.784929356357927E-02
20	.5000000000000000E+01	184	.392464678178964E-02
22	.3000000000000000E+01	200	.7000000000000000E+01
23	.1000000000000000E+04	202	.1000000000000000E+01
24	.157079632679490E+01	225	.2000000000000000E+01
26	.5000000000000000E+01	227	.2000000000000000E+01
27	-.1000000000000000E+01	228	.5000000000000000E+00
28	.1000000000000000E+04	230	.164835164835164E-01
29	.1000000000000000E+03	231	-.164835164835164E-01
33	.9999990000000000E+03	233	.784929356357927E-02
41	.3000000000000000E+01	234	.392464678178964E-02
42	.999999999999997E-06	250	.1000000000000000E+01
43	.5000000000000000E+02	252	.2900000000000000E+02
44	.1000000000000000E+00	253	.2900000000000000E+02
45	.1000000000000000E+03	275	.2000000000000000E+01
46	.1000000000000000E-07	300	.4000000000000000E+01
47	.5000000000000000E+00	302	.2000000000000000E+01
57	.2000000000000000E+01	303	.2000000000000000E+01
58	.2000000000000000E+01	305	.470957613814754E-02
60	.2000000000000000E+01	500	.1000000000000000E+01
71	.5000000000000000E+02	502	.1000000000000000E+01
72	.1000000000000000E+01	503	.1458000000000000E-05
75	.5700000000000000E+00	504	.1104000000000000E+03
81	.1000000000000000E+01	505	.1910000000000000E+01
82	.1000000000000000E+01	550	.1000000000000000E+01
83	.1000000000000000E+01	552	.1000000000000000E+01
84	-.156985871271585E-01	553	.1013280000000000E+06
85	-.470957613814755E-01	554	.8500000000000000E+01
86	.784929356357926E-01		
87	.470957613814755E-01		
89	.156985871271585E-01		
96	.1000000000000000E+03		
100	.6000000000000000E+01		
102	.3000000000000000E+01		
103	.5000000000000000E-02		
104	.3500000000000000E+00		
105	.1000000000000000E+01		
150	.1000000000000000E+01		

AZIMUTH ANGLE OF TRANSMISSION = 45.000000 DEG TRANSMITTER LATITUDE = 1.798926 DEG FREQUENCY = .050000 HZ  
 ELEVATION ANGLE OF TRANSMISSION = -20.000000 DEG TRANSMITTER LONGITUDE = .000000 DEG SINGLE STEP ERROR = 1.000000E-06

ERROR	EVENT	ELEVATION ABOVE TERRAIN		RANGE	AZIMUTH DEVIATION		ELEVATION ANGLE		PULSE TIME SEC	PHASE TIME SEC	ABSORPTION DB	PATH LENGTH KM
		SEA LEVEL KM	ABOVE TERRAIN KM		XMTR DEG	LOCAL DEG	XMTR DEG	LOCAL DEG				
-.7E-13	XMTR	13.0440	13.0000	.0000	-3.840	-3.838	-15.304	-12.169	.0000	.0000	.0000	.0000
.2E-06	RCVR	5.0367	5.0000	29.4887	-2.735	-2.735	-13.252	10.682	91.9612	91.9612	.0000	30.6167
.2E-06	GRND REF	.0313	.0000	56.3108	-2.343	-2.340	-5.874	12.148	172.2877	172.2877	.0000	57.9288
.8E-07	RCVR	5.0270	5.0000	83.1414	-3.794	-3.792	4.603	5.546	252.6076	252.6076	.0000	85.2361
-.1E-06		30.1362	30.1186	179.8168	-3.954	-3.953	4.264	-4.61	553.4076	553.4076	.0000	185.6886
-.1E-06	APOGEE	30.8025	30.7860	196.4513	-3.954	-3.953	4.264	-4.61	601.4076	601.4076	.0000	202.4308
-.1E-06	WAVE REV	30.8025	30.7860	196.4513	-4.435	-4.436	-1.671	-18.721	601.4076	601.4076	.0000	202.4308
.1E-06	RCVR	11.0830	11.0709	283.7756	-4.374	-4.375	-2.877	-12.129	870.2076	870.2076	.0000	292.7749
.3E-06	RCVR	5.0112	5.0000	307.3288	-4.374	-4.375	-2.877	-12.129	943.0763	943.0763	.0000	317.1400
.3E-06	MAX HOPS	5.0112	5.0000	307.3288	-4.374	-4.375	-2.877	-12.129	943.0763	943.0763	.0000	317.1400

THIS RAY CALCULATION TOOK 2.430 SEC

ELEVATION ANGLE OF TRANSMISSION	ELEVATION ABOVE TERRAIN	RANGE	AZIMUTH DEVIATION		ELEVATION ANGLE		PULSE TIME SEC	PHASE TIME SEC	ABSORPTION DB	PATH LENGTH KM		
			XMTR DEG	LOCAL DEG	XMTR DEG	LOCAL DEG						
-.7E-14	XMTR	13.0440	13.0000	.0000	.0000	.0000	.0000	.0000	.0000	.0000		
.1E-07	APOGEE	19.8306	19.8069	114.8628	-4.945	-4.945	2.856	-3.376	352.1000	352.1000	.0000	115.4148
.1E-07	WAVE REV	19.8306	19.8069	114.8628	-4.945	-4.945	2.856	-3.376	352.1000	352.1000	.0000	115.4148
.1E-07		19.1628	19.1412	135.8244	-4.991	-4.991	1.962	-3.544	416.1000	416.1000	.0000	136.4540
.4E-07	MIN DIST	13.0453	13.0303	225.0470	-4.938	-4.939	-1.012	-0.003	689.9096	689.9096	.0000	226.1364
.4E-07	MIN DIST	13.0453	13.0303	225.0470	-4.938	-4.939	-1.012	-0.003	689.9096	689.9096	.0000	226.1364
.3E-07	WAVE REV	13.0683	13.0535	229.2405	-4.930	-4.932	-1.025	.687	702.7096	702.7096	.0000	230.3388
.5E-07	APOGEE	19.8297	19.8195	339.8931	-4.937	-4.942	-3.888	-3.372	1041.9096	1041.9096	.0000	341.5344
.5E-07	WAVE REV	19.8297	19.8195	339.8931	-4.937	-4.942	-3.888	-3.372	1041.9096	1041.9096	.0000	341.5344
.1E-06		17.9660	17.9568	377.5546	-4.964	-4.970	-9.53	-5.329	1157.1096	1157.1096	.0000	379.3655
.7E-07	MIN DIST	13.0423	13.0348	450.1421	-4.932	-4.941	-2.025	-0.001	1379.8701	1379.8701	.0000	452.3210
.7E-07	MAX HOPS	13.0423	13.0348	450.1421	-4.932	-4.941	-2.025	-0.001	1379.8701	1379.8701	.0000	452.3210

THIS RAY CALCULATION TOOK .903 SEC

ELEVATION ANGLE OF TRANSMISSION	ELEVATION ABOVE TERRAIN	RANGE	AZIMUTH DEVIATION		ELEVATION ANGLE		PULSE TIME SEC	PHASE TIME SEC	ABSORPTION DB	PATH LENGTH KM		
			XMTR DEG	LOCAL DEG	XMTR DEG	LOCAL DEG						
-.7E-14	XMTR	13.0440	13.0000	.0000	.0000	.0000	.0000	.0000	.0000	.0000		
-.4E-06	APOGEE	30.8011	30.7734	83.6250	-5.591	-5.592	11.572	-3.90	256.1000	256.0999	.0000	86.3124
-.4E-06	WAVE REV	30.8011	30.7734	83.6250	-5.591	-5.592	11.572	-3.90	256.1000	256.0999	.0000	86.3124
-.4E-06		30.2160	30.1900	96.9373	-5.605	-5.605	9.576	-5.195	294.5000	294.4999	.0000	99.7046
.1E-06	RCVR	5.0170	5.0000	194.6869	-5.322	-5.324	-3.233	-12.129	598.2812	598.2810	.0000	201.1925
.2E-06	GRND REF	.0152	.0000	221.5510	-4.860	-4.863	-4.358	10.662	678.8281	678.8280	.0000	228.5831
.1E-06	RCVR	5.0137	5.0000	248.4283	-4.646	-4.651	1.271	5.571	759.3772	759.3771	.0000	255.9751
.3E-08		30.1249	30.1149	345.1581	-4.694	-4.699	1.172	-4.37	1060.1772	1060.1771	.0000	356.4343
.2E-08	APOGEE	30.7976	30.7881	361.7989	-4.694	-4.699	1.172	-4.37	1108.1772	1108.1771	.0000	373.1773
.2E-08	WAVE REV	30.7976	30.7881	361.7989	-4.694	-4.699	1.172	-4.37	1108.1772	1108.1771	.0000	373.1773
.3E-06		11.0982	11.0907	449.1534	-4.851	-4.860	-2.268	-18.731	1376.9772	1376.9772	.0000	463.5327
.5E-06	RCVR	5.0070	5.0000	472.7741	-4.790	-4.799	-3.098	-12.126	1450.0603	1450.0603	.0000	487.9710
.5E-06	MAX HOPS	5.0070	5.0000	472.7741	-4.790	-4.799	-3.098	-12.126	1450.0603	1450.0603	.0000	487.9710

THIS RAY CALCULATION TOOK 1.968 SEC

AZIMUTH ANGLE OF TRANSMISSION = 45.000000 DEG TRANSMITTER LATITUDE = 1.798926 DEG FREQUENCY = .050000 HZ  
 ELEVATION ANGLE OF TRANSMISSION = 40.000000 DEG TRANSMITTER LONGITUDE = .000000 DEG SINGLE STEP ERROR = 1.000000E-06

ERROR	EVENT	ELEVATION ABOVE		RANGE	AZIMUTH DEVIATION		ELEVATION ANGLE		PULSE TIME SEC	PHASE TIME SEC	ABSORPTION DB	PATH LENGTH KM
		SEA LEVEL KM	TERRAIN KM		XMTR DEG	LOCAL DEG	XMTR DEG	LOCAL DEG				
-.7E-14	XMTR	13.0440	13.0000	.0000	-6.654	-6.654	32.014	28.195	.0000	.0000	.0000	.0000
.6E-07		43.9246	43.8912	48.7564	-7.168	-7.222	28.443	39.168	169.7000	169.7000	.0000	58.0370
-.6E-06		88.4749	88.4526	134.7274	-7.340	-5.047	26.407	-1.194	438.5000	438.4999	.0001	155.8842
-.7E-06	APOGEE	104.2225	104.2036	175.8021	-7.530	-5.047	26.407	-1.194	555.3000	555.2998	.0016	201.2805
-.7E-06	WAVE REV	104.2225	104.2036	175.8021	-7.530	-5.047	26.407	-1.194	555.3000	555.2998	.0016	201.2805
-.8E-06		101.0975	101.0797	192.8408	-8.907	-3.080	23.481	-21.450	596.9000	596.8998	.0024	218.9577
-.6E-06		62.3998	62.3857	263.9313	-9.527	-4.128	9.343	-26.431	827.3000	827.2997	.0031	301.0331
-.1E-06		15.0673	15.0566	359.8298	-9.536	-4.137	-2.911	-35.775	1124.9000	1124.8997	.0031	409.0699
.5E-06	RCVR	5.0103	5.0000	374.1414	-9.488	-4.092	-3.670	34.996	1178.0787	1178.0784	.0031	426.5820
.4E-06	GRND REF	.0101	.0000	381.4687	-9.442	-4.046	-2.930	35.772	1204.2519	1204.2517	.0031	435.4618
.4E-06	RCVR	5.0099	5.0000	388.7966	-9.681	-4.287	2.238	23.933	1230.4249	1230.4249	.0031	444.3416
.2E-05		48.1493	48.1410	462.4781	-10.088	-4.698	5.685	35.429	1478.4251	1478.4251	.0034	530.3500
.7E-06		93.4113	93.4046	554.2751	-10.201	-4.812	6.050	-1.123	1763.2256	1763.2256	.0050	633.9752
.5E-06	APOGEE	104.7397	104.7335	592.3256	-10.256	-4.812	6.050	-1.123	1867.2251	1867.2256	.0050	674.8220
.5E-06	WAVE REV	104.7397	104.7335	592.3256	-10.256	-4.812	6.050	-1.123	1867.2251	1867.2256	.0050	674.8220
.4E-06		98.6801	98.6742	618.2918	-10.509	-5.125	5.031	-27.897	1934.4251	1934.4256	.0063	702.0891
.2E-05		57.6827	57.6776	694.9466	-10.575	-5.196	-3.849	-37.480	2180.8251	2180.8256	.0068	790.0545
-.2E-06		8.8419	8.8375	788.1424	-10.564	-5.185	-4.148	-35.793	2478.4251	2478.4263	.0068	896.3113
.2E-05	RCVR	5.0043	5.0000	793.7415	-10.564	-5.185	-4.148	-35.793	2498.7527	2498.7538	.0068	903.1062
.2E-05	MAX HOPS	5.0043	5.0000	793.7415	-10.564	-5.185	-4.148	-35.793	2498.7527	2498.7538	.0068	903.1062

THIS RAY CALCULATION TOOK 2.999 SEC

ELEVATION ANGLE OF TRANSMISSION =	60.0000 DEG	ELEVATION ANGLE	RANGE	AZIMUTH DEVIATION	PULSE TIME SEC	PHASE TIME SEC	ABSORPTION DB	PATH LENGTH KM
-.7E-14	XMTR	13.0440	13.0000	.0000	.0000	.0000	.0000	.0000
-.2E-06		46.3009	46.2626	25.0438	124.9000	124.9000	.0000	41.7284
-.4E-08		89.3597	89.3273	60.1377	284.9000	284.8999	.0001	97.5354
-.5E-06		132.3433	132.3186	116.6785	444.9000	444.8998	.0357	170.6495
-.4E-06	APOGEE	144.8719	144.8545	199.2131	572.1000	572.0997	.5014	256.4120
-.4E-06	WAVE REV	144.8719	144.8545	199.2131	572.1000	572.0997	.5014	256.4120
-.4E-06		144.7473	144.7304	205.5626	581.7000	581.6997	.5557	262.9118
-.9E-05		98.5307	98.5184	308.1052	792.9000	792.8996	.9118	380.9940
.4E-06		42.8401	42.8290	352.0479	997.7000	997.7001	.9121	452.4670
.3E-05	RCVR	5.0104	5.0000	378.8921	1138.5475	1138.5483	.9121	498.9910
.9E-06	GRND REF	.0103	.0000	382.0800	1156.1759	1156.1768	.9121	504.9226
.1E-05	RCVR	5.0102	5.0000	385.2681	1173.8043	1173.8052	.9121	510.8543
.5E-05		55.5496	55.5403	422.6504	1359.4043	1359.4055	.9121	573.9536
-.2E-05		111.6528	111.6443	468.6814	1564.2043	1564.2058	.9138	647.1544
-.2E-05	APOGEE	144.7403	144.7336	567.1420	1743.4043	1743.4054	1.3398	755.3699
-.2E-05	WAVE REV	144.7403	144.7336	567.1420	1743.4043	1743.4054	1.3398	755.3699
-.2E-05		129.1384	129.1325	632.9859	1852.2043	1852.2051	1.6910	824.9860
.2E-05		71.4679	71.4625	692.1644	2060.2043	2060.2046	1.7111	909.4548
.6E-06		10.1142	10.1093	739.1827	2284.2043	2284.2055	1.7111	987.0659
.4E-05	RCVR	5.0049	5.0000	742.5637	2302.9500	2302.9512	1.7111	993.1950
.4E-05	MAX HOPS	5.0049	5.0000	742.5637	2302.9500	2302.9512	1.7111	993.1950

AZIMUTH ANGLE OF TRANSMISSION = 45.00000 DEG TRANSMITTER LATITUDE = 1.798926 DEG  
 ELEVATION ANGLE OF TRANSMISSION = 80.00000 DEG TRANSMITTER LONGITUDE = .000000 DEG  
 FREQUENCY = .050000 HZ  
 SINGLE STEP ERROR = 1.000000E-06

ERROR	EVENT	ABOVE SEA LEVEL KM	ELEVATION ABOVE TERRAIN KM	RANGE KM	AZIMUTH XMITR DEG	LOCAL DEG	ELEVATION ANGLE DEG	XMITR DEG	LOCAL DEG	PULSE TIME SEC	PHASE TIME SEC	ABSORPTION DB	PATH LENGTH KM
.0E+00	XMITR	13.0440	13.0000	.0000	-20.387	-20.387	80.000	73.094	79.301	.0000	.0000	.0000	.0000
-.7E-07		35.1397	35.0968	6.6778	-20.997	-20.997	79.301	71.681	79.854	73.7000	73.7000	.0000	23.0919
-.9E-06		77.2842	77.2436	21.0030	-21.928	-21.928	79.854	71.049	76.820	203.3000	203.2999	.0000	67.6482
-.1E-05		108.2005	108.1614	32.1000	-19.107	-19.107	76.820	69.768	69.185	302.5000	302.4998	.0000	100.5561
-.1E-05		147.3742	147.3380	48.3230	-15.606	-15.606	69.185	67.609	64.942	382.5000	382.4998	.1114	143.1468
-.1E-05		198.2845	198.2527	73.8397	-14.390	-14.390	64.942	66.634	64.191	462.5000	462.4997	48.2402	200.5408
-.1E-05	EXTING	224.5590	224.5294	88.0081	-151.291	-151.291	64.191	77.457	65.030	500.9000	500.8997	1076.3153	230.6701

ELEVATION ANGLE OF TRANSMISSION = 100.0000 DEG

-.7E-14	XMITR	13.0440	13.0000	.0000	44.760	44.760	80.000	82.899	80.016	.0000	.0000	.0000	.964 SEC
-.2E-12	MAX LONG	13.3109	13.2669	.0332	-124.524	-124.524	80.016	82.768	79.618	.9000	.9000	.0000	.2690
-.8E-07		32.0143	31.9693	2.3953	-122.131	-122.131	79.618	82.213	79.622	63.7000	63.7000	.0000	19.1228
-.5E-06		70.8034	70.7559	7.8116	-114.124	-114.124	79.622	82.014	78.188	182.1000	182.1000	.0000	58.2976
-.1E-05	MAX LONG	103.9528	103.9032	12.5474	-115.247	-115.247	78.188	81.950	76.537	290.9000	290.8999	.0005	91.8275
-.1E-05		110.6394	110.5893	13.5646	-127.481	-127.481	76.537	81.266	70.665	308.5000	308.4998	.0012	98.5992
-.1E-05		140.9497	140.8962	19.2197	-144.932	-144.932	70.665	79.006	66.040	370.9000	370.8998	.0511	129.6767
-.1E-05		190.9721	190.9095	33.5431	-151.291	-151.291	66.040	77.457	65.030	450.9000	450.8997	20.1684	182.4295
-.1E-05	EXTING	224.9996	224.9286	45.5105	-154.193	-154.193	65.030	77.457	65.030	500.5000	500.4996	1126.0582	218.9079

ELEVATION ANGLE OF TRANSMISSION = 120.0000 DEG

-.7E-14	XMITR	13.0440	13.0000	.0000	14.765	14.765	60.000	63.861	56.548	.0000	.0000	.0000	.977 SEC
-.1E-06		46.1915	46.1409	16.1398	-162.825	-162.825	56.548	64.177	62.055	123.3000	123.3000	.0000	36.9103
-.4E-06		90.1163	90.0541	36.7256	-163.537	-163.537	62.055	62.382	41.494	283.3000	283.2999	.0001	85.5976
-.6E-06		119.2382	119.1634	54.4176	-169.420	-169.420	41.494	44.937	3.174	382.5000	382.4999	.0047	120.1510
-.2E-06	APOGEE	152.4306	152.2250	135.0070	-169.378	-169.378	3.174	42.894	-.188	548.9000	548.9000	.9310	211.3774
-.2E-06	WAVE REV	152.7178	152.4727	145.0531	-164.096	-164.096	-.188	42.894	-.188	564.9000	564.9000	1.1915	221.6716
-.1E-05		111.3236	109.6405	243.7566	-159.847	-159.847	42.894	20.668	-48.079	564.9000	564.9000	2.3500	335.7976
-.6E-05	MAX LONG	93.6766	92.4536	253.9614	-162.436	-162.436	-48.079	16.333	-61.003	766.5000	766.5000	2.3514	356.7367
-.2E-05	MAX LONG	79.4894	78.5126	259.9170	-161.359	-161.359	-61.003	13.070	-61.003	827.3000	827.2999	2.3515	372.5074
-.8E-05		54.7302	54.1010	272.6007	-159.875	-159.875	13.070	-2.826	-57.476	971.3000	971.3000	2.3516	400.8575
-.6E-07	RCVR	5.3003	5.0000	299.0948	-158.813	-158.813	-57.476	-3.774	54.094	1153.6795	1153.6806	2.3516	457.5233
-.7E-06	GRND REF	2.797	.0000	302.3604	-158.847	-158.847	54.094	-2.831	56.842	1171.9866	1171.9878	2.3516	463.5177
-.5E-06	RCVR	5.2607	5.0000	305.6826	-158.498	-158.498	56.842	5.884	55.667	1190.2861	1190.2873	2.3516	469.5109
-.7E-05		56.6194	56.4724	334.2104	-157.769	-157.769	55.667	9.444	60.760	1380.6861	1380.6876	2.3516	528.8274
-.2E-05	MAX LONG	81.0713	80.9539	347.1532	-156.847	-156.847	60.760	13.507	45.584	1470.2861	1470.2882	2.3516	556.9184
-.4E-05	MAX LONG	94.3487	94.2425	353.1353	-156.085	-156.085	45.584	13.507	45.584	1521.4861	1521.4881	2.3518	571.7558
-.3E-05		112.9029	112.8138	365.1172	-156.085	-156.085	4.301	14.257	-.783	1585.4879	1585.4879	2.3536	594.2539
-.3E-05	APOGEE	147.4966	147.4612	453.9279	-155.833	-155.833	4.301	14.257	-.783	1771.0861	1771.0874	2.9599	694.3670
-.3E-05	WAVE REV	147.4966	147.4612	453.9279	-155.833	-155.833	4.554	10.956	-24.695	1873.4861	1873.4872	3.4692	753.3817
-.2E-05		134.5112	134.4879	509.7279	-155.031	-155.031	20.668	4.297	-60.571	2068.6861	2068.6867	3.5120	813.9165
-.9E-06	MAX LONG	93.3241	93.3063	551.2271	-154.973	-154.973	5.416	3.933	-59.875	2081.4861	2081.4866	3.5121	828.7383
-.3E-05	MAX LONG	80.0572	80.0402	557.3032	-154.227	-154.227	6.163	-2.667	-59.566	2315.0861	2315.0875	3.5121	832.5357
-.9E-06		76.6838	76.6669	558.9313	-154.193	-154.193	6.198	-3.461	-56.730	2345.7311	2345.7326	3.5121	905.9410
-.1E-05		13.1140	13.1003	594.5164	-154.193	-154.193	6.198	-3.461	-56.730	2345.7311	2345.7326	3.5121	915.2955
-.2E-05	RCVR	5.0134	5.0000	599.1689	-154.193	-154.193	6.198	-3.461	-56.730	2345.7311	2345.7326	3.5121	915.2955
-.2E-05	MAX HOPS	5.0134	5.0000	599.1689	-154.193	-154.193	6.198	-3.461	-56.730	2345.7311	2345.7326	3.5121	915.2955

THIS RAY CALCULATION TOOK .977 SEC

AZIMUTH ANGLE OF TRANSMISSION = 45.000000 DEG TRANSMITTER LATITUDE = 1.798926 DEG FREQUENCY = .050000 HZ  
ELEVATION ANGLE OF TRANSMISSION = 140.000000 DEG TRANSMITTER LONGITUDE = .000000 DEG SINGLE STEP ERROR = 1.000000E-06

ERROR	EVENT	ELEVATION ABOVE TERRAIN		RANGE		AZIMUTH DEVIATION		ELEVATION ANGLE		PULSE TIME SEC	PHASE TIME SEC	ABSORPTION DB	PATH LENGTH KM
		KM	ABOVE SEA LEVEL KM	KM	DEG	XMTR DEG	LOCAL DEG	XMTR DEG	LOCAL DEG				
-.7E-14	XMTR	13.0440	13.0000	30.7729	-170.963	9.037	42.927	42.927	34.744	.0000	.0000	.0000	.0000
-.2E-06		41.9304	41.8733	68.5015	-170.511	9.475	40.560	40.560	40.574	147.3000	147.3000	.0000	42.3367
-.2E-06		72.7148	72.6319	99.5121	-169.250	10.185	42.160	42.160	27.018	307.2999	307.2999	.0000	91.3556
-.5E-06		105.4267	105.3047	123.0044	-169.527	7.625	37.922	37.922	-.231	467.3000	467.2999	.0010	137.0069
-.2E-06	APOGEE	111.7581	111.5888	123.0044	-169.527	7.625	37.922	37.922	-.231	534.5000	534.4999	.0048	162.0291
-.2E-06	WAVE REV	111.7581	111.5888	123.0044	-169.527	7.625	37.922	37.922	-.231	534.5000	534.4999	.0048	162.0291
-.7E-06		99.0190	98.7170	154.3398	-168.405	-1.721	28.212	28.212	-39.256	627.3000	627.2999	.0091	197.3682
.4E-05		50.6802	49.2224	203.6148	-161.833	-10.394	9.505	9.505	-32.617	854.5000	854.5001	.0095	270.1590
.2E-05	RCVR	5.8098	5.0000	255.5846	-157.368	-6.592	-2.768	-2.768	-36.018	1083.9370	1083.9370	.0095	341.4045
.2E-05	GRND REF	.6338	.0000	263.3761	-157.096	-6.666	-3.879	-3.879	27.499	1112.8739	1112.8748	.0095	350.8503
.1E-05	RCVR	5.5009	5.0000	271.3368	-156.827	-6.406	-2.810	-2.810	33.954	1141.7055	1141.7065	.0095	360.2767
.1E-05		51.4803	51.3472	329.9398	-153.800	-3.387	5.126	5.126	29.986	1388.1055	1388.1074	.0095	436.8222
.2E-05	MAX LONG	77.5366	77.4586	365.2769	-152.219	-1.808	8.298	8.298	40.528	1528.9055	1528.9074	.0096	482.1444
.5E-06	MAX LONG	96.7313	96.6704	384.5933	-151.260	-.849	10.441	10.441	38.317	1624.9055	1624.9075	.0098	510.2986
.2E-07		100.4016	100.3440	389.2695	-151.074	-.663	10.786	10.786	32.940	1644.1055	1644.1075	.0100	516.4371
.2E-06	APOGEE	109.2373	109.1943	417.3020	-150.307	.103	10.980	10.980	-.377	1727.3055	1727.3075	.0129	547.2455
.2E-06	WAVE REV	109.2373	109.1943	417.3020	-150.307	.103	10.980	10.980	-.377	1727.3055	1727.3075	.0129	547.2455
.8E-06		98.8690	98.8362	446.8125	-149.588	.822	8.767	8.767	-35.440	1816.9055	1816.9075	.0158	580.0213
.4E-06	MAX LONG	95.7525	95.7208	450.5518	-149.468	.942	8.285	8.285	-39.400	1832.9055	1832.9075	.0159	585.0253
.9E-06	MAX LONG	76.5533	76.5264	470.0849	-148.799	1.612	5.524	5.524	-40.094	1928.9055	1928.9075	.0161	613.1416
.1E-05		52.8328	52.8115	502.7766	-148.075	2.336	2.238	2.238	-30.029	2056.9055	2056.9078	.0162	654.3369
.1E-05	RCVR	5.0143	5.0000	565.8781	-147.184	3.229	-3.356	-3.356	-33.478	2313.8622	2313.8650	.0162	734.3758
.1E-05	MAX HOPS	5.0143	5.0000	565.8781	-147.184	3.229	-3.356	-3.356	-33.478	2313.8622	2313.8650	.0162	734.3758

THIS RAY CALCULATION TOOK 2.778 SEC

\*\*\*\*\* H A R P A \*\*\*\*\*  
 HAMILTONIAN ACOUSTIC RAY-TRACING PROGRAM FOR THE ATMOSPHERE

BY  
 R. M. JONES, J. P. RILEY AND T. M. GEORGES  
 WAVE PROPAGATION LABORATORY  
 NATIONAL OCEANIC AND ATMOSPHERIC ADMINISTRATION  
 BOULDER, COLORADO 80303

RUN SET NUMBER 2

ATMOSPHERIC MODEL ID — S03

ATMOSPHERIC MODEL DESCRIPTION — SAMPLE CASE FOR HARPA DOCUMENTATION REV. 2-10-86

MODEL TYPE	SUBROUTINE NAME	DATA SET ID	DESCRIPTION
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DISPERSION RELATION	AWWWL	3.00	ACOUSTIC WAVE *** WITH WIND ***** WITH LOSSES
BACKGROUND WIND VELOCITY	ULOGZ2	.00	LOGARITHMIC EASTWARD WIND PROFILE, U=.5 M/S, Z0=1 KM
WIND VELOCITY PERTURBATION	NPWIND	.00	NO WIND PERTURBATION
BACKGROUND SOUND SPEED	GAMRTDM	2.00	SOUND SPEED IN TERMS OF TEMPERATURE MODEL
SOUND SPEED PERTURBATION	CBLOB2	1.00	50% INCREASE IN SQ. SOUND SPEED AT 125KM HT, 335KM N, 125KM E
BACKGROUND TEMPERATURE	TTANH5	2.00	U.S. STANDARD ATMOSPHERE 1962 TEMPERATURE PROFILE
TEMPERATURE PERTURBATION	TBLOB2	2.00	50% CYLINDRICAL INCREASE IN TEMPERATURE AT 105KM N., 105 KM W
MOLECULAR WEIGHT	MCONST	29.00	MOLECULAR WEIGHT = 29
BACKGROUND TERRAIN	GLORENZ	2.00	RIDGE 2-KM HIGH, 30-KM WIDE ALONG EQUATOR
TERRAIN PERTURBATION	NPERR	.00	NO TERRAIN PERTURBATION
BACKGROUND VISCOSITY/ THERMAL CONDUCTIVITY	MUARDC	1.00	ARDC VISCOSITY AND THERMAL CONDUCTIVITY MODEL
CONDUCTIVITY/THERMAL CONDUCTIVITY PERTURBATION	NPABSR	.00	NO VISCOSITY/CONDUCTIVITY PERTURBATION
BACKGROUND PRESSURE	PEXP	1.00	EXPONENTIAL PRESSURE MODEL, SCALE HEIGHT = 8.5 KM
PRESSURE PERTURBATION	NPPRES	.00	NO PRESSURE PERTURBATION
RECEIVER SURFACE	RTERR	.00	RECEIVER SURFACE 5 KM ABOVE TERRAIN

INPUT DATA FILE FOR RUN SET NUMBER 2

S03-2 SAMPLE CASE FOR HARPA DOCUMENTATION REV. 2-10-86  
 71 0. NUMBER OF INTEGRATION STEPS PER PRINT  
 72 0. OUTPUT RAYSETS (1=YES; 0=NO)  
 73 1. DIAGNOSTIC PRINTOUT (1=YES; 0=NO)  
 81 2. RAYPLOT PROJECTION (1=VERT; 2=HORIZ) PLANE  
 82 3. PLOT-EXPANSION FACTOR  
 0 \*\*\*\*\* END OF RUN SET NUMBER 2 \*\*\*\*\*

INITIAL VALUES FOR THE W ARRAY  
ONLY NONZERO VALUES PRINTED — ALL ANGLES IN RADIAN

N	W(N)	N	W(N)
1	.6370000000000000E+04	175	.2000000000000000E+01
3	.1304400977995111E+02	177	.2000000000000000E+01
4	.313971742543171E-01	178	.5000000000000000E+00
7	.314159265358979E+00	179	.1250000000000000E+03
11	.7853981633397446E+00	180	.525902668759810E-01
15	-.349065850398864E+00	181	.196232339089482E-01
16	.244346095279205E+01	182	.2500000000000000E+02
17	.349065850398864E+00	183	.784929356357927E-02
20	.5000000000000000E+01	184	.392464678178964E-02
22	.3000000000000000E+01	200	.7000000000000000E+01
23	.1000000000000000E+04	202	.1000000000000000E+01
24	.157079632679490E+01	225	.2000000000000000E+01
26	.5000000000000000E+03	227	.2000000000000000E+01
27	-.1000000000000000E+01	228	.5000000000000000E+00
28	.1000000000000000E+04	230	.164835164835164E-01
29	.1000000000000000E+03	231	-.164835164835164E-01
33	.9999990000000000E+03	233	.784929356357927E-02
41	.3000000000000000E+01	234	.392464678178964E-02
42	.999999999999999E-06	250	.1000000000000000E+01
43	.5000000000000000E+02	252	.2900000000000000E+02
44	.1000000000000000E+00	253	.2900000000000000E+02
45	.1000000000000000E+03	275	.2000000000000000E+01
46	.1000000000000000E-07	300	.4000000000000000E+01
47	.5000000000000000E+00	302	.2000000000000000E+01
57	.2000000000000000E+01	303	.2000000000000000E+01
58	.2000000000000000E+01	305	.470957613814754E-02
60	.2000000000000000E+01	500	.1000000000000000E+01
71	.999999999999999E+30	502	.1000000000000000E+01
73	.1000000000000000E+01	503	.1458000000000000E-05
75	.1500000000000000E+00	504	.1104000000000000E+03
77	.5700000000000000E+02	505	.1910000000000000E+01
81	.2000000000000000E+01	550	.1000000000000000E+01
82	.3000000000000000E+01	552	.1000000000000000E+01
83	-.156985871271585E-01	553	.1013280000000000E+06
84	-.470957613814755E-01	554	.8500000000000000E+01
85	.784929356357926E-01		
86	.470957613814755E-01		
87	.156985871271585E-01		
89	.3000000000000000E+03		
96	.1000000000000000E+03		
100	.6000000000000000E+01		
102	.3000000000000000E+01		
103	.5000000000000000E-02		
104	.3500000000000000E+00		
105	.1000000000000000E+01		
150	.1000000000000000E+01		

INPUT OVERRIDDEN

AZIMUTH ANGLE OF TRANSMISSION = 45.000000 DEG TRANSMITTER LATITUDE = 1.798926 DEG FREQUENCY = .050000 HZ  
 ELEVATION ANGLE OF TRANSMISSION = -20.000000 DEG TRANSMITTER LONGITUDE = .000000 DEG SINGLE STEP ERROR = 1.000000E-06

ERROR	EVENT	ELEVATION ABOVE		RANGE	AZIMUTH DEVIATION		ELEVATION ANGLE		PULSE TIME SEC	PHASE TIME SEC	ABSORPTION DB	PATH LENGTH KM
		SEA LEVEL KM	TERRAIN KM		XMTR DEG	LOCAL DEG	XMTR DEG	LOCAL DEG				
-.1E-13	XMTR	13.0440	13.0000	.0000	-3.791	-3.790	-15.146	-11.856	.0000	.0000	.0000	.0000
.2E-06	BACK UP0	4.7586	4.7222	30.8625	-3.840	-3.838	-15.304	-12.169	96.1000	96.1000	.0000	32.0196
.2E-06	BACK UP1	5.0367	5.0000	29.4888	-3.840	-3.838	-15.304	-12.169	91.9614	91.9614	.0000	30.6168
.2E-06	RCVR	5.0367	5.0000	29.4887	-2.616	-2.612	-13.171	-10.714	91.9612	91.9612	.0000	30.6167
.2E-06	BACK UP0	-	-	58.7368	-2.735	-2.731	-13.252	-10.703	179.5613	179.5613	.0000	60.3988
.2E-06	BACK UP1	.0313	.0000	56.3108	-2.735	-2.735	-13.252	-10.682	172.2877	172.2877	.0000	57.9268
.2E-06	GRND REF	.0313	.0000	56.3108	-2.344	-2.340	-5.842	12.186	172.2877	172.2877	.0000	57.9268
.8E-07	BACK UP0	5.0597	5.0326	83.3006	-2.343	-2.340	-5.874	12.148	253.0877	253.0877	.0000	85.3987
.8E-07	BACK UP1	5.0270	5.0000	83.1414	-2.343	-2.340	-5.874	12.148	252.6076	252.6076	.0000	85.3987
.8E-07	RCVR	5.0270	5.0000	83.1414	-2.343	-2.340	-5.874	12.148	252.6076	252.6076	.0000	85.3987
-.1E-06	APOGEE	30.8025	30.7860	196.4513	-3.954	-3.953	4.264	-4.61	601.4076	601.4076	.0000	202.4308
-.1E-06	WAVE REV	30.8025	30.7860	196.4513	-3.954	-3.953	4.264	-4.61	601.4076	601.4076	.0000	202.4308
.3E-06	BACK UP0	4.7476	4.7365	308.6340	-4.374	-4.368	-2.925	-11.832	947.0076	947.0076	.0000	318.4730
.3E-06	BACK UP1	5.0112	5.0000	307.3289	-4.374	-4.375	-2.877	-12.129	943.0763	943.0763	.0000	317.1400
.3E-06	RCVR	5.0112	5.0000	307.3288	-4.374	-4.375	-2.877	-12.129	943.0763	943.0763	.0000	317.1400
.3E-06	MAX HOPS	5.0112	5.0000	307.3288	-4.374	-4.375	-2.877	-12.129	943.0763	943.0763	.0000	317.1400

THIS RAY CALCULATION TOOK 2.009 SEC

ELEVATION ANGLE OF TRANSMISSION =	ABOVE SEA LEVEL KM	TERRAIN KM	RANGE KM	XMTR DEG	LOCAL DEG	XMTR DEG	LOCAL DEG	THIS RAY CALCULATION TOOK
-.7E-14	13.0440	13.0000	.0000	-4.945	-4.945	2.856	-3.76	.0000
.1E-07	19.8306	19.8069	114.8628	-4.945	-4.945	2.856	-3.76	.0000
.1E-07	19.8306	19.8069	114.8628	-4.945	-4.945	2.856	-3.76	.0000
.4E-07	13.0538	13.0389	227.5993	-4.933	-4.935	-1.021	.417	.0000
.4E-07	13.0453	13.0303	225.0474	-4.938	-4.939	-1.012	-.003	.0000
.4E-07	13.0453	13.0303	225.0470	-4.938	-4.939	-1.012	-.003	.0000
.4E-07	13.0453	13.0303	225.0470	-4.938	-4.939	-1.012	-.003	.0000
.4E-07	13.0453	13.0303	225.0470	-4.938	-4.939	-1.012	-.003	.0000
.3E-07	13.0683	13.0535	229.2495	-4.930	-4.932	-1.025	.687	.0000
.5E-07	19.8297	19.8195	339.8931	-4.937	-4.942	-.368	-.372	.0000
.5E-07	19.8297	19.8195	339.8931	-4.937	-4.942	-.368	-.372	.0000
.7E-07	13.0505	13.0431	452.6454	-4.930	-4.939	-2.035	.411	.0000
.7E-07	13.0423	13.0348	450.1425	-4.932	-4.941	-2.025	-.001	.0000
.7E-07	13.0423	13.0348	450.1421	-4.932	-4.941	-2.025	-.001	.0000
.7E-07	13.0423	13.0348	450.1421	-4.932	-4.941	-2.025	-.001	.0000
.7E-07	13.0423	13.0348	450.1421	-4.932	-4.941	-2.025	-.001	.0000

THIS RAY CALCULATION TOOK .908 SEC

AZIMUTH ANGLE OF TRANSMISSION = 45.000000 DEG TRANSMITTER LATITUDE = 1.798926 DEG FREQUENCY = .050000 HZ  
 ELEVATION ANGLE OF TRANSMISSION = 20.000000 DEG TRANSMITTER LONGITUDE = .000000 DEG SINGLE STEP ERROR = 1.000000E-06

ERROR	EVENT	ELEVATION		AZIMUTH		ELEVATION		PULSE TIME SEC	PHASE TIME SEC	ABSORPTION DB	PATH LENGTH KM
		ABOVE SEA LEVEL KM	ABOVE TERRAIN KM	XMTR DEG	LOCAL DEG	XMTR DEG	LOCAL DEG				
-.7E-14	XMTR	13.0440	13.0000			11.572	20.000	.0000	.0000	.0000	.0000
-.4E-06	APOGEE	30.8011	30.7734	-5.591	-5.592	11.572	-3.390	256.1000	256.0999	.0000	86.3124
-.4E-06	WAVE REV	30.8011	30.7734	-5.591	-5.592	11.572	-3.390	256.1000	256.0999	.0000	86.3124
.1E-06	BACK UP0	4.7875	4.7706	-5.307	-5.309	-3.291	-11.809	601.7000	601.6998	.0000	202.3515
.1E-06	BACK UP1	5.0170	5.0000	-5.322	-5.324	-3.233	-12.129	598.2812	598.2811	.0000	201.1925
.1E-06	RCVR	5.0170	5.0000	-5.322	-5.324	-3.233	-12.129	598.2812	598.2811	.0000	201.1925
.2E-06	BACK UP0	- .4426	- .4577	-4.806	-4.807	-4.450	-10.681	686.0810	686.0810	.0000	231.0486
.2E-06	BACK UP1	.0152	.0000	-4.860	-4.862	-4.358	-10.669	678.8280	678.8280	.0000	228.5831
.2E-06	GRND REF	.0152	.0000	-4.860	-4.863	-4.358	-10.662	678.8281	678.8280	.0000	228.5831
.1E-06	BACK UP0	5.0043	5.0306	-4.497	-4.499	-2.958	12.156	759.8281	759.8280	.0000	256.1279
.1E-06	BACK UP1	5.0137	5.0000	-4.498	-4.500	-2.966	12.121	759.3772	759.3771	.0000	255.9751
.1E-06	RCVR	5.0137	5.0000	-4.498	-4.500	-2.966	12.121	759.3772	759.3771	.0000	255.9751
.2E-08	APOGEE	30.7976	30.7881	-4.694	-4.699	1.172	-4.37	1108.1772	1108.1771	.0000	373.1773
.2E-08	WAVE REV	30.7976	30.7881	-4.694	-4.699	1.172	-4.37	1108.1772	1108.1771	.0000	373.1773
.5E-06	BACK UP0	4.7578	4.7507	-4.784	-4.794	-3.131	-11.845	1453.7772	1453.7772	.0000	489.2314
.5E-06	BACK UP1	5.0070	5.0000	-4.790	-4.799	-3.098	-12.126	1450.0604	1450.0604	.0000	487.9710
.5E-06	RCVR	5.0070	5.0000	-4.790	-4.799	-3.098	-12.126	1450.0603	1450.0603	.0000	487.9710
.5E-06	MAX HOPS	5.0070	5.0000	-4.790	-4.799	-3.098	-12.126	1450.0603	1450.0603	.0000	487.9710

THIS RAY CALCULATION TOOK 1.995 SEC

ELEVATION ANGLE OF TRANSMISSION	DEG	ELEVATION		AZIMUTH		PULSE TIME SEC	PHASE TIME SEC	ABSORPTION DB	PATH LENGTH KM		
		ABOVE SEA LEVEL KM	ABOVE TERRAIN KM	XMTR DEG	LOCAL DEG						
-.7E-14	XMTR	13.0440	13.0000			.0000	.0000	.0000	.0000		
-.7E-06	APOGEE	104.2225	104.2036	-7.340	-5.047	26.407	-1.194	555.3000	555.2998	.0016	201.2805
-.7E-06	WAVE REV	104.2225	104.2036	-7.340	-5.047	26.407	-1.194	555.3000	555.2998	.0016	201.2805
.5E-06	BACK UP0	4.7800	4.7697	-9.535	-4.136	-2.946	-35.687	1179.3000	1179.2997	.0031	426.9943
.5E-06	BACK UP1	5.0103	5.0000	-9.536	-4.137	-2.911	-35.775	1178.0786	1178.0784	.0031	426.5820
.5E-06	RCVR	5.0103	5.0000	-9.536	-4.137	-2.911	-35.775	1178.0787	1178.0784	.0031	426.5820
.4E-06	BACK UP0	-1.0136	-1.0236	-9.471	-4.073	-3.822	-34.925	1209.4787	1209.4784	.0031	437.2394
.4E-06	BACK UP1	.0101	.0000	-9.488	-4.089	-3.670	-34.999	1204.2520	1204.2517	.0031	435.4618
.4E-06	GRND REF	.0101	.0000	-9.488	-4.092	-3.670	-34.996	1204.2519	1204.2517	.0031	435.4618
.4E-06	BACK UP0	5.1658	5.1559	-9.442	-4.046	-2.908	35.833	1231.2519	1231.2517	.0031	444.6205
.4E-06	BACK UP1	5.0099	5.0000	-9.442	-4.046	-2.930	35.772	1230.4251	1230.4249	.0031	444.3416
.4E-06	RCVR	5.0099	5.0000	-9.442	-4.046	-2.930	35.772	1230.4251	1230.4249	.0031	444.3416
.5E-06	APOGEE	104.7397	104.7335	-10.201	-4.812	6.050	-1.123	1867.2256	1867.2256	.0050	674.8220
.5E-06	WAVE REV	104.7397	104.7335	-10.201	-4.812	6.050	-1.123	1867.2251	1867.2251	.0050	674.8220
.2E-05	BACK UP0	4.6132	4.6089	-10.562	-5.183	-4.179	-35.647	2500.8251	2500.8263	.0068	903.8062
.2E-05	BACK UP1	5.0043	5.0000	-10.564	-5.185	-4.148	-35.793	2498.7527	2498.7538	.0068	903.1062
.2E-05	RCVR	5.0043	5.0000	-10.564	-5.185	-4.148	-35.793	2498.7527	2498.7538	.0068	903.1062
.2E-05	MAX HOPS	5.0043	5.0000	-10.564	-5.185	-4.148	-35.793	2498.7527	2498.7538	.0068	903.1062

THIS RAY CALCULATION TOOK 2.989 SEC

AZIMUTH ANGLE OF TRANSMISSION = 45.000000 DEG TRANSMITTER LATITUDE = 1.798926 DEG FREQUENCY = .050000 HZ  
ELEVATION ANGLE OF TRANSMISSION = 60.000000 DEG TRANSMITTER LONGITUDE = .000000 DEG SINGLE STEP ERROR = 1.000000E-06

ERROR	EVENT	ELEVATION ABOVE TERRAIN		RANGE	AZIMUTH DEVIATION		ELEVATION ANGLE		PULSE TIME	PHASE TIME	ABSORPTION	PATH LENGTH
		SEA LEVEL	ABOVE		XMTR	LOCAL	XMTR	LOCAL				
-.7E-14	XMTR	13.0440	13.0000	.0000	-7.589	-1.829	32.272	60.000	.0000	.0000	.0000	.0000
-.4E-06	APOGEE	144.8719	144.8545	199.2131	-7.589	-1.829	32.272	-.221	572.0997	572.0997	.5014	256.4120
-.4E-06	WAVE REV	144.8719	144.8545	199.2131	-7.589	-1.829	32.272	-.221	572.0997	572.0997	.5014	256.4120
-.3E-05	BACK UP0	4.5785	4.5681	379.1757	-10.259	-3.574	-2.982	-59.317	1140.1009	1140.1009	.9121	499.5078
-.3E-05	BACK UP1	5.0104	5.0000	378.8921	-10.259	-3.574	-2.917	-59.417	1138.5475	1138.5475	.9121	498.9910
-.3E-05	RCVR	5.0104	5.0000	378.8921	-10.259	-3.574	-2.917	-59.417	1138.5475	1138.5475	.9121	498.9910
-.9E-06	BACK UP0	-1.0303	-1.0406	382.7092	-10.243	-3.558	-3.825	-58.392	1159.7475	1159.7475	.9121	506.1395
-.9E-06	BACK UP1	.0103	.0000	382.0800	-10.249	-3.565	-3.669	-58.549	1156.1759	1156.1759	.9121	504.9226
-.9E-06	GRND REF	.0103	.0000	382.0800	-10.249	-3.572	-3.669	-58.546	1156.1759	1156.1759	.9121	504.9226
-.1E-05	BACK UP0	5.2243	5.2141	385.4089	-10.241	-3.563	-2.894	-59.464	1174.5759	1174.5759	.9121	511.1106
-.1E-05	BACK UP1	5.0102	5.0000	385.2681	-10.240	-3.563	-2.925	-59.414	1173.8043	1173.8043	.9121	510.8543
-.1E-05	RCVR	5.0102	5.0000	385.2681	-10.240	-3.563	-2.925	-59.414	1173.8043	1173.8043	.9121	510.8543
-.2E-05	APOGEE	144.7403	144.7336	567.1420	-11.193	-4.522	10.360	-1.201	1743.4054	1743.4054	1.3398	755.3699
-.2E-05	WAVE REV	144.7403	144.7336	567.1420	-11.193	-4.522	10.360	-1.201	1743.4054	1743.4054	1.3398	755.3699
-.4E-05	BACK UP0	4.8787	4.8738	742.6466	-11.689	-5.024	-3.968	-59.394	2303.4055	2303.4055	1.7111	993.3461
-.4E-05	BACK UP1	5.0049	5.0000	742.5637	-11.689	-5.024	-3.958	-59.423	2302.9512	2302.9512	1.7111	993.1950
-.4E-05	RCVR	5.0049	5.0000	742.5637	-11.689	-5.024	-3.958	-59.423	2302.9512	2302.9512	1.7111	993.1950
-.4E-05	MAX HOPS	5.0049	5.0000	742.5637	-11.689	-5.024	-3.958	-59.423	2302.9512	2302.9512	1.7111	993.1950

ELEVATION ANGLE OF TRANSMISSION = 80.0000 DEG THIS RAY CALCULATION TOOK 3.260 SEC  
 .0E+00 XMTR 13.0440 13.0000 .0000 .0000 .0000 .0000  
 -.1E-05 EXTINC 224.5590 224.5294 88.0081 -14.390 -14.394 66.634 80.000 80.000 500.9000 500.8997 1076.3153 230.6701

ELEVATION ANGLE OF TRANSMISSION = 100.0000 DEG THIS RAY CALCULATION TOOK .944 SEC  
 -.7E-14 XMTR 13.0440 13.0000 .0000 .0000 .0000 .0000  
 -.2E-12 MAX LONG 13.3109 13.2669 .0332 -135.240 44.760 82.899 80.016 .0000 .0000 .0000 .0000  
 -.1E-05 MAX LONG 110.6394 110.5893 13.5646 -115.247 64.752 81.950 76.537 308.5000 308.4998 .0012 98.5992  
 -.1E-05 EXTINC 224.9996 224.9286 45.5105 -151.291 28.707 77.457 65.030 500.5000 500.4996 1126.0582 218.9079

THIS RAY CALCULATION TOOK .967 SEC

AZIMUTH ANGLE OF TRANSMISSION = 45.000000 DEG TRANSMITTER LATITUDE = 1.798926 DEG FREQUENCY = .050000 HZ  
 ELEVATION ANGLE OF TRANSMISSION = 120.000000 DEG TRANSMITTER LONGITUDE = .000000 DEG SINGLE STEP ERROR = 1.000000E-06

ERROR	EVENT	ELEVATION ABOVE TERRAIN		RANGE	AZIMUTH DEVIATION		ELEVATION ANGLE		PULSE TIME SEC	PHASE TIME SEC	ABSORPTION DB	PATH LENGTH KM
		KM	KM		XMTR DEG	LOCAL DEG	XMTR DEG	LOCAL DEG				
-.7E-14	XMTR	13.0440	13.0000	.0000			60.000		.0000			.0000
.2E-06	APOGEE	152.7178	152.4727	145.0531	-169.378	2.943	42.894	-1.188	564.9000	564.9000	1.1915	221.6716
.2E-06	WAVE REV	152.7178	152.4727	145.0531	-169.378	2.943	42.894	-1.188	564.9000	564.9000	1.1915	221.6716
.6E-06	MAX LONG	93.6766	92.4536	253.9614	-163.165	-2.285	16.333	-61.003	827.3000	827.2999	2.3514	356.7367
-.2E-05	MAX LONG	79.4894	78.5126	259.9170	-162.436	-1.561	13.070	-61.038	881.6939	881.6939	2.3515	372.5074
-.6E-07	BACK UP0	5.2948	4.9945	299.0982	-159.875	.978	-2.827	-57.473	1153.7000	1153.7012	2.3516	457.5298
-.6E-07	BACK UP1	5.3003	5.0000	299.0948	-159.875	.978	-2.826	-57.476	1153.6795	1153.6806	2.3516	457.5233
-.6E-07	RCVR	5.3003	5.0000	299.0948	-159.875	.978	-2.826	-57.476	1153.6795	1153.6806	2.3516	457.5233
-.7E-06	BACK UP0	-.5223	-.7987	302.9344	-159.849	.997	-3.924	-54.285	1174.8795	1174.8806	2.3516	464.5041
-.7E-06	BACK UP1	.2797	.0000	302.3604	-159.847	1.001	-3.774	-54.763	1171.9866	1171.9878	2.3516	463.5177
-.7E-06	GRND REF	.2797	.0000	302.3604	-159.847	1.001	-3.774	-54.763	1171.9866	1171.9878	2.3516	463.5177
-.5E-06	BACK UP0	5.6107	5.3512	305.8975	-159.809	.553	-2.765	-57.003	1191.5866	1191.5878	2.3516	469.9225
-.5E-06	BACK UP1	5.2607	5.0000	305.6826	-159.813	.585	-2.831	-56.842	1190.2861	1190.2873	2.3516	469.5109
-.5E-06	RCVR	5.2607	5.0000	305.6826	-159.813	.585	-2.831	-56.842	1190.2861	1190.2873	2.3516	469.5109
-.2E-05	MAX LONG	81.0713	80.9539	347.1532	-157.769	2.617	9.444	60.760	1470.2861	1470.2882	2.3518	556.9184
-.4E-06	MAX LONG	94.3487	94.2425	353.1353	-157.340	3.046	11.220	60.149	1521.4861	1521.4881	2.3518	571.7558
-.3E-05	APOGEE	147.4966	147.4612	453.9279	-156.085	4.301	14.257	-78.3	1771.0861	1771.0874	2.9599	694.3670
-.3E-05	WAVE REV	147.4966	147.4612	453.9279	-156.085	4.301	14.257	-78.3	1771.0861	1771.0874	2.9599	694.3670
-.9E-06	MAX LONG	93.3241	93.3063	551.2271	-155.276	5.113	5.734	-60.529	2017.4861	2017.4867	3.5120	813.9165
-.3E-05	MAX LONG	80.0572	80.0402	557.3032	-155.031	5.358	4.297	-60.571	2068.6861	2068.6867	3.5121	828.7383
-.2E-05	BACK UP0	4.6476	4.6343	599.3981	-154.193	6.198	-3.461	-56.556	2347.0861	2347.0875	3.5121	915.2955
-.2E-05	BACK UP1	5.0134	5.0000	599.1689	-154.193	6.198	-3.461	-56.556	2345.7311	2345.7326	3.5121	915.2955
-.2E-05	RCVR	5.0134	5.0000	599.1689	-154.193	6.198	-3.461	-56.556	2345.7311	2345.7326	3.5121	915.2955
-.2E-05	MAX HOPS	5.0134	5.0000	599.1689	-154.193	6.198	-3.461	-56.730	2345.7311	2345.7326	3.5121	915.2955

THIS RAY CALCULATION TOOK 3.174 SEC													
ELEVATION ANGLE OF TRANSMISSION = 140.0000 DEG	ERROR	EVENT	ELEVATION ABOVE TERRAIN		RANGE	AZIMUTH DEVIATION		ELEVATION ANGLE		PULSE TIME SEC	PHASE TIME SEC	ABSORPTION DB	PATH LENGTH KM
			KM	KM		XMTR DEG	LOCAL DEG	XMTR DEG	LOCAL DEG				
-.7E-14	XMTR	13.0440	13.0000	.0000			40.000		.0000			.0000	
-.2E-06	APOGEE	111.7581	111.5888	123.0044	-169.527	7.625	37.922	-2.31	534.5000	534.4999	.0048	162.0291	
-.2E-06	WAVE REV	111.7581	111.5888	123.0044	-169.527	7.625	37.922	-2.31	534.5000	534.4999	.0048	162.0291	
.2E-05	BACK UP0	5.6287	4.8252	255.8244	-157.357	-6.582	-2.808	-35.841	1084.9000	1084.9009	.0095	341.7092	
.2E-05	BACK UP1	5.8098	5.0000	255.5846	-157.368	-6.592	-2.768	-36.018	1083.9362	1083.9370	.0095	341.4045	
.2E-05	RCVR	5.8098	5.0000	255.5846	-157.368	-6.592	-2.768	-36.018	1083.9361	1083.9370	.0095	341.4045	
.2E-05	BACK UP0	.6338	.0000	263.3761	-157.096	-6.316	-3.984	-28.922	1115.9361	1115.9371	.0095	351.8883	
.2E-05	BACK UP1	.6338	.0000	263.3761	-157.096	-6.316	-3.984	-28.922	1115.9361	1115.9371	.0095	351.8883	
.2E-05	GRND REF	6.1439	5.6559	272.2417	-156.788	-6.666	-3.879	-27.499	1112.8739	1112.8748	.0095	350.8503	
.1E-05	BACK UP0	5.5670	5.0674	271.4310	-156.623	-6.368	-2.674	-34.607	1145.2739	1145.2749	.0095	350.8503	
.1E-05	BACK UP1	5.5009	5.0000	271.3369	-156.827	-6.406	-2.796	-34.602	1142.0749	1142.0749	.0095	360.3933	
.1E-05	RCVR	5.5009	5.0000	271.3368	-156.827	-6.406	-2.810	-33.954	1141.7057	1141.7067	.0095	360.2768	
.2E-05	MAX LONG	77.5366	77.4586	365.2769	-152.219	-6.406	-2.810	-33.954	1141.7055	1141.7065	.0095	360.2768	
.5E-06	MAX LONG	96.7313	96.6704	384.5933	-151.260	-1.103	8.298	40.528	1528.9055	1528.9074	.0095	482.1444	
.2E-06	APOGEE	109.2373	109.1943	417.3020	-150.307	.163	10.980	-37.7	1727.3055	1727.3075	.0129	510.2986	
.2E-06	WAVE REV	109.2373	109.1943	417.3020	-150.307	.163	10.980	-37.7	1727.3055	1727.3075	.0129	510.2986	
.4E-06	MAX LONG	95.7525	95.7208	450.5518	-149.468	1.942	8.285	-39.400	1832.9055	1832.9075	.0129	547.2455	
.9E-06	MAX LONG	76.5533	76.5264	470.0849	-148.799	1.612	5.524	-40.094	1928.9055	1928.9075	.0161	585.0253	
.1E-05	BACK UP0	4.6166	4.6024	566.4724	-147.183	3.230	-3.398	-33.043	2316.1955	2316.1983	.0162	735.0914	
.1E-05	BACK UP1	5.0143	5.0000	565.8781	-147.184	3.229	-3.356	-33.478	2313.8622	2313.8650	.0162	734.3758	
.1E-05	RCVR	5.0143	5.0000	565.8781	-147.184	3.229	-3.356	-33.478	2313.8622	2313.8650	.0162	734.3758	
.1E-05	MAX HOPS	5.0143	5.0000	565.8781	-147.184	3.229	-3.356	-33.478	2313.8622	2313.8650	.0162	734.3758	

THIS RAY CALCULATION TOOK 2.725 SEC

S03-1 SAMPLE CASE FOR HARPA DOCUMENTATION REV. 2-10-86  
 ULOGZ2 3.0 NPWIND .0 GAMRTDM .0 CBLOB2 2.0  
 TTANH5 1.0 TBLOB2 2.0 MCONST 29.0 NO MODL .0  
 PEXP 1.0 NPPRES .0 MUARDC 1.0 NPABSR .0  
 GLORENZ 2.0 NPTErr .0 RTErr .0 NO MODL .0

LOGARITHMIC EASTWARD WIND PROFILE, U\*=.5 M/S, Z0=1 KM

NO WIND PERTURBATION

SOUND SPEED IN TERMS OF TEMPERATURE MODEL

50% INCREASE IN SQ. SOUND SPEED AT 125KM HT, 335KM N, 125KM E

U.S. STANDARD ATMOSPHERE 1962 TEMPERATURE PROFILE

50% CYLINDRICAL INCREASE IN TEMPERATURE AT 105KM N., 105 KM W

MOLECULAR WEIGHT = 29

RIDGE 2-KM HIGH, 30-KM WIDE ALONG EQUATOR

S033	130440	1799	0	50000	3142	4500000	-2000000	0	0	0	3T
	50367	294887	-3840	-3838-12169	9196124	9196123	0	0	0	0	1R
	313	563108	-2735	-2735 10693	17228767	17228768	0	0	0	0	2G
	50270	831414	-2343	-2340 12148	25260761	25260764	0	0	0	0	2R
	50112	3073288	-4374	-4375-12129	94307633	94307634	0	0	0	0	3R
S033	130440	1799	0	50000	3142	4500000	-1500000	0	0	0	3T
	59174	560059	-3651	-3649 -11	16962526	16962525	0	0	0	0	1M
	59174	560059	-3651	-3649 -11	16962526	16962525	0	0	0	0	2M
	59185	3248490	-4500	-4501 -2	99099938	99099939	0	0	0	0	3M
S033	130440	1799	0	50000	3142	4500000	-1000000	0	0	0	3T
	95112	406604	-4161	-4160 -12	12374135	12374135	0	0	0	0	1M
	95112	406604	-4161	-4160 -12	12374135	12374135	0	0	0	0	2M
	95115	2807459	-4767	-4769 -3	85924969	85924971	0	0	0	0	3M
S033	130440	1799	0	50000	3142	4500000	-500000	0	0	0	3T
	119700	256779	-4424	-4424 -14	7831383	7831383	0	0	0	0	1M
	119700	256779	-4424	-4424 -14	7831383	7831383	0	0	0	0	2M
	119705	2542307	-4873	-4875 -3	77890316	77890317	0	0	0	0	3M
S033	130440	1799	0	50000	3142	4500000	0	0	0	0	3T
	130453	2250470	-4938	-4939 -3	68990961	68990962	0	0	0	0	1M
	130453	2250470	-4938	-4939 -3	68990961	68990962	0	0	0	0	2M
	130423	4501421	-4932	-4941 -1	137987009	137987013	0	0	0	0	3M
S033	130440	1799	0	50000	3142	4500000	500000	0	0	0	3T
	119724	2027348	-4988	-4989 -4	62186567	62186568	0	0	0	0	1M
	119724	2027348	-4988	-4989 -4	62186567	62186568	0	0	0	0	2M
	119693	4312567	-4949	-4957 -1	132228323	132228325	0	0	0	0	3M
S033	130440	1799	0	50000	3142	4500000	1000000	0	0	0	3T
	95149	1993238	-5015	-5017 -4	61147865	61147865	0	0	0	0	1M
	95149	1993238	-5015	-5017 -4	61147865	61147865	0	0	0	0	2M
	95110	4393846	-4931	-4939 -1	134683577	134683579	0	0	0	0	3M
S033	130440	1799	0	50000	3142	4500000	1500000	0	0	0	3T
	59270	2127216	-4948	-4950 -4	65140567	65140562	0	0	0	0	1M
	59270	2127216	-4948	-4950 -4	65140567	65140562	0	0	0	0	2M
	59192	4814803	-4791	-4801 -1	147243522	147243515	0	0	0	0	3M
S033	130440	1799	0	50000	3142	4500000	2000000	0	0	0	3T
	50170	1946869	-5322	-5324-12129	59828119	59828103	0	0	0	0	1R
	152	2215510	-4860	-4863 10665	67882811	67882797	0	0	0	0	2G
	50137	2484283	-4498	-4500 12121	75937724	75937711	0	0	0	0	2R
	50070	4727741	-4790	-4799-12126	145006034	145006027	0	0	0	0	3R
S033	130440	1799	0	50000	3142	4500000	2500000	0	0	0	3T
	50164	2044020	-5581	-5584-19279	62541213	62541173	0	0	0	0	1R
	154	2198518	-5299	-5304 18131	67332802	67332761	0	0	0	0	2G
	50145	2353069	-5054	-5059 19271	72124354	72124310	0	0	0	0	2R

50073	4608314	-5232	-5245-19276	141475510	141475369	0	0	0	0	3R
S033	130440	1799	0	50000	3142	4500000	3000000	0	0	3T
50145	2387553	-5803	-5808-25431	71841724	71841676	0	0	0	0	1R
139	2499430	-5617	-5624 24351	75461318	75461270	0	0	0	0	2G
50133	2611336	-5446	-5453 25425	79080884	79080835	0	0	0	0	2R
50065	5163074	-5562	-5579-25432	156441221	156441073	0	0	0	0	3R
S033	130440	1799	0	50000	3142	4500000	3500000	0	0	3T
50063	5513279	-7508	-5984-29065	162974268	162974290	2	0	0	0	1R
61	5608414	-7434	-5912 28128	166149079	166149107	2	0	0	0	2G
50060	5703560	-7363	-5841 29063	169323893	169323927	2	0	0	0	2R
615060	10006822	-7658	-6166-14096	295883893	295883991	5	0	0	0	3F
S033	130440	1799	0	50000	3142	4500000	4000000	0	0	3T
50103	3741414	-9536	-4137-35775	117807866	117807837	3	0	0	0	1R
101	3814687	-9488	-4092 34998	120425195	120425167	3	0	0	0	2G
50099	3887966	-9442	-4046 35772	123042513	123042487	3	0	0	0	2R
50043	7937415-10564	-5185-35793	249875267	249875381	7	0	0	0	0	3R
S033	130440	1799	0	50000	3142	4500000	4500000	0	0	3T
50125	3091011	-9743	-3791-44213	102900551	102900586	6	0	0	0	1R
123	3145487	-9709	-3762 43355	105086946	105086986	6	0	0	0	2G
50121	3199967	-9676	-3729 44209	107273331	107273377	6	0	0	0	2R
50058	6455868-11160	-5225-44221	215828181	215828361	16	0	0	0	0	3R
S033	130440	1799	0	50000	3142	4500000	5000000	0	0	3T
50135	2885700-10288	-2785-49919	98659438	98659471	15	0	0	0	0	1R
133	2930535-10275	-2780 49061	100647939	100647981	15	0	0	0	0	2G
50131	2975374-10263	-2768 49914	102636428	102636484	15	0	0	0	0	2R
50065	6062118-12249	-4762-49923	207558128	207558752	40	0	0	0	0	3R
S033	130440	1799	0	50000	3142	4500000	5500000	0	0	3T
50133	3020692-11403	-647-53317	101084059	101084117	56	0	0	0	0	1R
131	3060560-11420	-673 52507	102978779	102978846	56	0	0	0	0	2G
50130	3100432-11437	-689 53313	104873491	104873569	56	0	0	0	0	2R
50067	6218924-14191	-3448-53321	210124746	210125585	115	0	0	0	0	3R
S033	130440	1799	0	50000	3142	4500000	6000000	0	0	3T
50104	3788921-10259	-3574-59417	113854747	113854834	912	0	0	0	0	1R
103	3820800-10249	-3572 58548	115617591	115617680	912	0	0	0	0	2G
50102	3852681-10240	-3563 59414	117380431	117380523	912	0	0	0	0	2R
50049	7425637-11689	-5024-59423	230295002	230295121	1711	0	0	0	0	3R
S033	130440	1799	0	50000	3142	4500000	6500000	0	0	3T
50057	5821218	-6448	-6098-64257	142399710	142400008183625	0	0	0	0	1R
56	5847356	-6435	-6089 63372	144082823	144083135183625	0	0	0	0	2G
50056	5873495	-6422	-6077 64256	145765935	145766261183625	0	0	0	0	2R
1684896	10011309	-6189	-5873-18166	234725935	234726873365871	0	0	0	0	3F
S033	130440	1799	0	50000	3142	4500000	7000000	0	0	3T
2195558	1936549	-7763	-7799 30028	59050000	59049975999999	0	0	0	0	1E
S033	130440	1799	0	50000	3142	4500000	7500000	0	0	3T
2225112	1285167-10383-10389	49233	52810000	52809965999999	0	0	0	0	0	1E
S033	130440	1799	0	50000	3142	4500000	8000000	0	0	3T
2245590	880081-14390-14394	64191	50090000	50089965999999	0	0	0	0	0	1E
S033	130440	1799	0	50000	3142	4500000	8500000	0	0	3T
2247730	555666-22417-22421	77477	48650000	48649969999999	0	0	0	0	0	1E
S033	130440	1799	0	50000	3142	4500000	9000000	0	0	3T
2251046	297077-44996-12280	90000	48250000	48249969999999	0	0	0	0	0	1E
S033	130440	1799	0	50000	3142	4500000	9500000	0	0	3T
2248568	228757247892	67890 77673	48650000	48649969999999	0	0	0	0	0	1E
S033	130440	1799	0	50000	3142	4500000	10000000	0	0	3T
2249996	455105208709	28707 65030	50050000	50049964999999	0	0	0	0	0	1E

S033	130440	1799	0	50000	3142	4500000	10500000	0	0	0	3T
	2233740	789299196959	16939	51415	52490000	52489964999999		0	0	0	1E
S033	130440	1799	0	50000	3142	4500000	11000000	0	0	0	3T
	2208428	1259606191906	8518	36751	57130000	57129972999999		0	0	0	1E
S033	130440	1799	0	50000	3142	4500000	11500000	0	0	0	3T
	2124423	2422518195818	-4466	9647	71370000	71370035999999		0	0	0	1E
S033	130440	1799	0	50000	3142	4500000	12000000	0	0	0	3T
	53003	2990948200125	978-57476	115367948	115368064	2352		0	0	0	1R
	2797	3023604200153	553 54429	117198663	117198779	2352		0	0	0	2G
	52607	3056826200187	580 56842	119028614	119028727	2352		0	0	0	2R
	50134	5991689205807	6198-56730	234573114	234573255	3512		0	0	0	3R
S033	130440	1799	0	50000	3142	4500000	12500000	0	0	0	3T
	60949	2479241201442	-6590-49243	105715988	105716092	185		0	0	0	1R
	9420	2525083201621	-7410 43874	107849212	107849323	185		0	0	0	2G
	58035	2573712201820	-7226 45970	109976807	109976925	185		0	0	0	2R
	50205	5082746211925	2861-45468	216607576	216608152	214		0	0	0	3R
S033	130440	1799	0	50000	3142	4500000	13000000	0	0	0	3T
	67320	2291697202541-11202-46567	101774969	101775077	44			0	0	0	1R
	15155	2342259202856-11710 40332	104050187	104050302	44			0	0	0	2G
	62782	2396807203195-11392 41940	106320535	106320655	44			0	0	0	2R
	50204	5018625215998 1379-41034	214865783	214866002	58			0	0	0	3R
S033	130440	1799	0	50000	3142	4500000	13500000	0	0	0	3T
	66041	2326700202456 -9909-42477	102595360	102595461	18			0	0	0	1R
	13438	2386724202782-10342 35491	105091010	105091118	18			0	0	0	2G
	60892	2450630203127-10017 38011	107580043	107580156	18			0	0	0	2R
	50180	5222047215158 1990-37119	219900993	219901351	26			0	0	0	3R
S033	130440	1799	0	50000	3142	4500000	14000000	0	0	0	3T
	58098	2555846202632 -6592-36018	108393614	108393701	10			0	0	0	1R
	6338	2633761202904 -6666 28584	111287389	111287482	10			0	0	0	2G
	55009	2713368203173 -6406 33954	114170553	114170650	10			0	0	0	2R
	50143	5658781212816 3229-33478	231386220	231386499	16			0	0	0	3R

## APPENDIX B: BLANK INPUT-PARAMETER FORMS

This appendix provides blank Input Parameter Forms for all of the atmospheric models (including terrain and receiver-surface models) that we have developed for HARPA. The forms describe each model mathematically and list the variable input parameters you have to specify. We recommend reproducing these forms and filling them out when setting up atmospheric models for HARPA. The filled-out forms should then be saved as a record of the models you have defined.

The FORTRAN source codes for the corresponding model subroutines are listed in Appendix D under the model name. No forms are given for the do-nothing versions NTEMP, NPTEMP, NPSPEED, NPTERR, NPPRES, and NPWIND. The forms are arranged as follows:

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FORM TO SPECIFY INPUT DATA FOR A  
THREE-DIMENSIONAL RAYPATH CALCULATION

Atmospheric ID (3 characters) \_\_\_\_\_ Name \_\_\_\_\_  
Date \_\_\_\_\_

Title (77 characters) \_\_\_\_\_

Transmitter: Height \_\_\_\_\_ km, nm, ft (W3)  
 \_\_\_\_\_ above terrain  
 \_\_\_\_\_ above sea level  
 Latitude \_\_\_\_\_ rad, deg, km (W4)  
 Longitude \_\_\_\_\_ rad, deg, km (W5)  
 Frequency, initial \_\_\_\_\_ rad/s, Hz, s (W7)  
                   final \_\_\_\_\_ (W8)  
                   step \_\_\_\_\_ (W9)  
 Azimuth angle, initial \_\_\_\_\_ rad, deg clockwise of north (W11)  
                           final \_\_\_\_\_ (W12)  
                           step \_\_\_\_\_ (W13)  
 Elevation angle, initial \_\_\_\_\_ rad, deg (W15)  
                           final \_\_\_\_\_ (W16)  
                           step \_\_\_\_\_ (W17)

Receiver: Height \_\_\_\_\_ km, nm, ft (W20)  
 \_\_\_\_\_ above sea level (rcvr model RHORIZ)  
 \_\_\_\_\_ above terrain (rcvr model RTERR)  
 Distance from origin \_\_\_\_\_ rad, deg, km (W30) (rcvr model RVERT)  
 Latitude of origin \_\_\_\_\_ rad, deg, km (W31) (rcvr model RVERT)  
 Longitude of origin \_\_\_\_\_ rad, deg, km (W32) (rcvr model RVERT)

Stop frequency stepping \_\_\_\_\_ (W21 = 1.)  
 when ray goes out of bounds  
 Maximum height \_\_\_\_\_ km (W26)  
 Minimum height \_\_\_\_\_ km (W27)  
 Maximum range \_\_\_\_\_ km (W28)  
 Maximum number of hops \_\_\_\_\_ (W22)  
 Maximum number of steps per hop \_\_\_\_\_ (W23)  
 Maximum allowable error per step \_\_\_\_\_ (W42)

Additional calculations: \_\_\_\_\_ = 1. to integrate  
   \_\_\_\_\_ = 2. to integrate and print  
 Phase path \_\_\_\_\_ (W57)  
 Absorption \_\_\_\_\_ (W58)  
 Doppler shift \_\_\_\_\_ (W59)  
 Path length \_\_\_\_\_ (W60)

Printout: \_\_\_\_\_ Every \_\_\_\_\_ steps of the ray trace (W71)

Computer readable output (raysets): \_\_\_\_\_ (W72 = 1.)  
 Diagnostic printing: \_\_\_\_\_ (W73 = 1.)  
 Suppress all printout \_\_\_\_\_ (W74 = 1.)

FORM TO SPECIFY INPUT PARAMETERS FOR PLOTTING A  
PROJECTION OF THE RAYPATH

Model ID: \_\_\_\_\_

Plot directly during raypath calculations \_\_\_\_\_, or  
plot from precomputed raypaths \_\_\_\_\_  
in disk file \_\_\_\_\_

Normal or apogee plots: Normal \_\_\_\_\_ (W80=0.0)  
Plot apogees only \_\_\_\_\_ (W80=1.0)

Projection:

Vertical plane, polar plot, rectangular expansion \_\_\_\_\_ (W81=1.0)  
Horizontal plane, lateral expansion \_\_\_\_\_ (W81=2.0)  
Vertical plane, polar plot, radial expansion \_\_\_\_\_ (W81=3.0)  
Vertical plane, rectangular plot \_\_\_\_\_ (W81=4.0)

Superimpose these raypath plots on the graph of the previous sunset:

Yes \_\_\_\_\_ (W81 negative.)  
No \_\_\_\_\_ (W81 positive.)

Vertical or lateral expansion factor \_\_\_\_\_ (W82)

Coordinates of the left edge of the graph:

Latitude = \_\_\_\_\_ (rad, deg, km) north (W83)  
Longitude = \_\_\_\_\_ (rad, deg, km) east (W84)

Coordinates of the right edge of the graph:

Latitude = \_\_\_\_\_ (rad, deg, km) north (W85)  
Longitude = \_\_\_\_\_ (rad, deg, km) east (W86)

Distance between horizontal tick marks = \_\_\_\_\_ rad, deg, km (W87)

Height above sea level of bottom of graph = \_\_\_\_\_ km (W88)

Height above sea level of top of graph = \_\_\_\_\_ km (W89)

Distance between vertical tick marks = \_\_\_\_\_ km (W96)

FORM TO SPECIFY AN ATMOSPHERIC MODEL  
(including terrain model)

Name \_\_\_\_\_

Date \_\_\_\_\_

Atmospheric ID (3 characters) \_\_\_\_\_

Coordinates of the north pole of the computational coordinate system:

North geographic latitude: \_\_\_\_\_ rad, km, deg (W24)

East geographic longitude: \_\_\_\_\_ rad, km, deg (W25)

Models:

	Subroutine Name	Data set ID
Dispersion relation	_____	
Wind velocity	_____	(W102)
Wind-velocity perturbation	_____	(W127)
Sound speed	_____	(W152)
Sound-speed perturbation	_____	(W177)
Temperature	_____	(W202)
Temperature perturbation	_____	(W227)
Molecular weight	_____	(W252)
Terrain	_____	(W302)
Terrain perturbation	_____	(W327)
Viscosity/conductivity	_____	(W502)
Viscosity/conductivity perturbation	_____	(W527)
Pressure	_____	(W552)
Pressure perturbation	_____	(W557)
Receiver surface*	_____	
Plot-annotation model*	_____	

\*The receiver-surface model and plot-annotation model are not considered part of the atmospheric ID

FORM TO SPECIFY INPUT DATA FOR  
WIND-VELOCITY MODEL WLINEAR

This subroutine specifies constant radial (upward), zonal (eastward) and meridional (southward) winds, allowing a linear height gradient of the zonal component.

$$U_{\theta} = U_{\theta 0}$$

$$U_{\phi} = U_{\phi 0} + \frac{du_{\phi}}{dz} z$$

$$u_r = U_{r0}$$

$z = r - r_e$ , where  $r_e$  is the Earth radius, and  $r$  is the radial coordinate of ray point.

Specify--

the model check for WLINEAR = 1.0 (W100)

the input data-format code = \_\_\_\_\_ (W101)

an input data-set identification number = \_\_\_\_\_ (W102)

an 80-character description of the wind-velocity profile:

---

the constant upward wind,  $U_{r0} =$  \_\_\_\_\_ km/s, m/s (W103)

the constant southward wind,  $U_{\theta 0} =$  \_\_\_\_\_ km/s, m/s (W104)

the ground value of the eastward wind,  $U_{\phi 0} =$  \_\_\_\_\_ km/s, m/s (W105)

the height gradient of  $u_{\phi}$ ,  $du_{\phi}/dz =$  \_\_\_\_\_ km/s/km, m/s/km (W106)

(This subroutine can be used with its input parameters zero when no wind field is desired.)

OTHER MODELS REQUIRED: Any wind-perturbation model. Use NPWIND if no perturbation is desired.

FORM TO SPECIFY INPUT DATA FOR  
WIND-VELOCITY MODEL WTIDE

This subroutine represents the wind field of the atmospheric tides by zonal and meridional height profiles that are sinusoidal and in phase quadrature. The profiles progress downward with time, giving a corkscrew effect:

$$u_{\theta} = U_{\theta 0} \sin \left\{ 2\pi \left( \frac{z}{\lambda_z} + \frac{t}{\tau} \right) \right\}$$

$$u_{\phi} = U_{\phi 0} \cos \left\{ 2\pi \left( \frac{z}{\lambda_z} + \frac{t}{\tau} \right) \right\}$$

$z = r - r_e$ , where  $r_e$  is the Earth radius, and  $r$  is the radial coordinate of the ray point.

Specify--

the model check for WTIDE = 5.0 (W100)

the input data-format code = \_\_\_\_\_ (W101)

an input data-set identification number = \_\_\_\_\_ (W102)

an 80-character description of the model, including description of parameter values:

---

the amplitude of the meridional component,  $U_{\theta 0} =$  \_\_\_\_\_ km/s, m/s (W104)

the amplitude of the zonal component,  $U_{\phi 0} =$  \_\_\_\_\_ km/s, m/s (W103)

the vertical wavelength,  $\lambda_z =$  \_\_\_\_\_ km (W105)

the time in wave periods,  $t/\tau =$  \_\_\_\_\_ (W106)

the wave period,  $\tau =$  \_\_\_\_\_ sec (W107)

(The Earth's poles should be avoided in ray calculations because discontinuities appear there.)

OTHER MODELS REQUIRED: Any wind-perturbation model. Use NPWIND if no perturbation is desired.

FORM TO SPECIFY INPUT DATA  
FOR WIND-VELOCITY MODEL ULOGZ2

A logarithmic wind profile of the atmospheric boundary layer neglecting Coriolis forces. The eastward wind is given by

$$u_{\phi} = \frac{u_*}{k} \ln \frac{z}{z_0} \quad \text{for} \quad z > z_0 e$$

$$u_{\phi} = \frac{u_*}{k} \frac{z}{z_0 e} \quad \text{for} \quad z \leq z_0 e ,$$

where  $z = G(r, \theta, \phi)$  is determined by the terrain model and is the height above or some kind of distance from the terrain, depending on the terrain model, and  $r$  is the radial coordinate of the ray point.

Specify--

- the model check for ULOGZ2 = 6.0 (W100)
- the input data-format code = \_\_\_\_\_ (W101)
- an input data-set identification number = \_\_\_\_\_ (W102)
- an 80-character description of the wind velocity profile:

- 
- the reference wind speed,  $u_* =$  \_\_\_\_\_ km/s, m/s (W103)
- von Kármán's constant,  $k =$  \_\_\_\_\_ (W104) (.35 recommended)
- the roughness height,  $z_0 =$  \_\_\_\_\_ km (W105)

OTHER MODELS REQUIRED: Any wind-perturbation model. Use NPWIND if no perturbation is desired.

$(\overline{uw} = -u_*^2$  is the surface stress at the ground.)

FORM TO SPECIFY INPUT DATA FOR  
WIND-VELOCITY MODEL VVORTX3

This subroutine models a vortex with a viscous core and a Gaussian intensity profile in the vertical. The axis of the vortex is vertical and may be positioned above any geographic latitude and longitude. The vortex rotates anticlockwise looking down. The core (inside  $r_0$ ) is essentially a solid-rotating fluid, while outside  $r_0$ ,  $|u|$  falls off as the inverse radius.

$$u_\theta = - \frac{1.397 R_e U_0 r_0}{r^2} (1 - e^{-1.26 r^2/r_0^2}) (\phi - \phi_0) e^{-\left[\frac{h - h_{\max}}{w_H}\right]^2}$$

$$u_\phi = \frac{1.397 R_e U_0 r_0}{r^2} (1 - e^{-1.26 r^2/r_0^2}) (\theta - \theta_0) e^{-\left[\frac{h - h_{\max}}{w_H}\right]^2}$$

where  $\theta_0 = \pi/2 - \lambda_0$  and  $r$  is the radial distance from the vortex center. The numerical constants normalize the function so that  $|U| = U_0$  at  $r = r_0$ .  $R_e$  is the radius of the Earth,  $\theta$  is the colatitude,  $\phi$  is the longitude, and  $h$  is the height above sea level.

Specify--

the model check for VVORTX3 = 9.0 (W100)

the input data-format code = \_\_\_\_\_ (W101)

an input data-set identification number = \_\_\_\_\_ (W102)

an 80-character description of the model, including description of parameter values:

the maximum tangential wind,  $U_0 =$  \_\_\_\_\_ km/s, m/s (W103)

the radius of the vortex core (to  $u = U_0$ ),  $r_0 =$  \_\_\_\_\_ km (W104)

the latitude of the vortex center,  $\lambda_0 =$  \_\_\_\_\_ rad, deg, km N (W105)

the longitude of the vortex center,  $\phi_0 =$  \_\_\_\_\_ rad, deg, km E (W106)

the Gaussian width in height of the vortex,  $w_H =$  \_\_\_\_\_ km, m (W107)

the height of the vortex,  $h_{\max} =$  \_\_\_\_\_ km, m (W108)

OTHER MODELS REQUIRED: Any wind-perturbation model. Use NPWIND if no perturbation is desired.

FORM TO SPECIFY INPUT DATA FOR  
WIND-VELOCITY MODEL WGAUSS2

This subroutine specifies a zonal (eastward) wind field whose intensity decays in a Gaussian manner in all three space dimensions.

$$u_{\phi} = U_{\phi 0} \exp\left\{-\left(\frac{z-z_0}{W_z}\right)^2 - \left(\frac{\theta-\theta_0}{W_{\theta}}\right)^2 - \left(\frac{\phi-\phi_0}{W_{\phi}}\right)^2\right\}$$

$z = r - r_e$ , where  $r_e$  is the Earth radius,  $\theta_0 = \pi/2 - \lambda_0$ , and  $r$  is the radial coordinate of the ray point.  $\theta$  is the colatitude.  $\phi$  is the longitude.

Notice that this wind field does not satisfy continuity if  $W_{\phi} \neq 0$ .

Specify--

the model check for WGAUSS2 = 8.0 (W100)

the input data-format code = \_\_\_\_\_ (W101)

an input data-set identification number = \_\_\_\_\_ (W102)

an 80-character description of the model, including description of parameter values:

the maximum value of  $u_{\phi}$ ,  $U_{\phi 0} =$  \_\_\_\_\_ km/s, m/s (W103)

the height where  $u_{\phi}$  maximizes,  $z_0 =$  \_\_\_\_\_ km (W107)

the Gaussian width in height of  $u_{\phi}$ ,  $W_z =$  \_\_\_\_\_ km (W104)\*

the latitude where  $u_{\phi}$  maximizes,  $\lambda_0 =$  \_\_\_\_\_ rad, deg, km N (W108)

the meridional width of  $u_{\phi}$ ,  $W_{\theta} =$  \_\_\_\_\_ rad, deg, km (W105)\*

the longitude where  $u_{\phi}$  maximizes,  $\phi_0 =$  \_\_\_\_\_ rad, deg, km E (W109)

the zonal width of  $u_{\phi}$ ,  $W_{\phi} =$  \_\_\_\_\_ rad, deg, km (W106)\*

OTHER MODELS REQUIRED: Any wind-perturbation model. Use NPWIND if no perturbation is desired.

\*Setting  $W_z$ ,  $W_{\theta}$  or  $W_{\phi} = 0$  results in no space variation in that direction.

FORM TO SPECIFY  
SOUND-SPEED MODEL GAMRTDM

This model specifies sound speed in terms of a background temperature model using

$$c^2 = \frac{\gamma RT}{M} ,$$

where  $\gamma = 1.4$ , R is the universal gas constant, T is the absolute temperature in Kelvins, and  $M(r,\theta,\phi)$  is a model of the mean molecular weight of the atmosphere. See Sec. 6.3 for further description of this model.

Specify --

The model check for GAMRTDM = 1.0 (W150)

OTHER MODELS REQUIRED: Any background temperature model; any molecular weight model.



FORM TO SPECIFY INPUT DATA FOR SOUND-SPEED  
PERTURBATION MODEL CBLOB2

An increase (or decrease) in sound speed in a localized region that decays in a Gaussian manner in all three spatial directions.

$$c^2(r, \theta, \phi) = c_0^2(r, \theta, \phi) \left( 1 + \Delta \exp \left\{ - \left( \frac{z-z_0}{W_z} \right)^2 - \left( \frac{\theta-\theta_0}{W_\theta} \right)^2 - \left( \frac{\phi-\phi_0}{W_\phi} \right)^2 \right\} \right)$$

$c_0^2(r, \theta, \phi)$  is the square of the sound speed specified by a sound-speed model.  $(r, \theta, \phi)$  are the coordinates of the ray point in an Earth-centered spherical polar-coordinate system.  $\theta_0 = \pi/2 - \lambda_0$  and  $z = r - r_e$ , where  $r_e$  is the Earth radius.

Specify--

the model check for subroutine CBLOB2 = 2.0 (W175)

the input data-format code = \_\_\_\_\_ (W176)

an input data-set identification number = \_\_\_\_\_ (W177)

an 80-character description for the sound-speed perturbation model, including description of parameter values:

---

the strength of the fractional increase (or decrease),  $\Delta$  = \_\_\_\_\_ (W178)

the height of maximum effect,  $z_0$  = \_\_\_\_\_ km (W179)

the latitude of maximum effect,  $\lambda_0$  = \_\_\_\_\_ rad, deg, km N (W180)

the longitude of maximum effect,  $\phi_0$  = \_\_\_\_\_ rad, deg, km E (W181)

the Gaussian width in height of the effect,  $W_z$  = \_\_\_\_\_ km (W182)\*

the meridional width of the effect,  $W_\theta$  = \_\_\_\_\_ rad, deg, km (W183)\*

the zonal width of the effect,  $W_\phi$  = \_\_\_\_\_ rad, deg, km (W184)\*

OTHER MODELS REQUIRED: none.

---

\* Setting  $W_z$ ,  $W_\theta$ , or  $W_\phi$  = zero results in no space variation in that direction.

FORM TO SPECIFY INPUT DATA FOR  
ATMOSPHERIC TEMPERATURE MODEL TLINEAR

This subroutine specifies an atmospheric temperature that increases linearly with height.

$$T = T_0 + \left(\frac{dT}{dz}\right) z$$

$z = r - r_e$ , where  $r_e$  is the Earth radius and  $r$  is the radial coordinate of the ray point.

Specify--

the model check for TLINEAR = 1.0 (W200)

the input data-format code = \_\_\_\_\_ (W201)

an input data-set identification number = \_\_\_\_\_ (W202)

an 80-character description of the model, including description of parameter values:

---

the ground temperature,  $T_0$  = \_\_\_\_\_ °K (W203)

the temperature gradient,  $dT/dz$  = \_\_\_\_\_ °K/km (W204)

(set = 0 for isothermal atmosphere)

OTHER MODELS REQUIRED: Any temperature-perturbation model. Use NPTEMP if no perturbations are desired.

FORM TO SPECIFY INPUT DATA FOR  
TEMPERATURE MODEL TTANH5

This model represents the temperature profile by a sequence of linear segments that are smoothly joined by hyperbolic functions:

$$T = T_0 + \frac{c_1}{2} (z-z_0) + \sum_{i=1}^n \delta_i \left( \frac{c_{i+1} - c_i}{2} \right) \ln \left\{ \frac{\cosh \left( \frac{z-z_i}{\delta_i} \right)}{\cosh \left( \frac{z_i-z_0}{\delta_i} \right)} \right\} + \frac{c_{n+1}}{2} (z-z_0)$$

$$\frac{dT}{dz} = c_1 + \sum_{i=1}^n \left( \frac{c_{i+1} - c_i}{2} \right) \left\{ \tanh \left( \frac{z-z_i}{\delta_i} \right) + 1 \right\}$$

$$c_i = (T_i - T_{i-1}) / (z_i - z_{i-1})$$

$z = r - r_e$ , where  $r_e$  is the Earth radius, and  $r$  is the radial coordinate of the ray point. Thus,  $\delta_i$  is the half-thickness of a region centered at approximately  $z_i$  km, in which  $dT/dz$  changes from  $c_i$  to  $c_{i+1}$ . Start by drawing a profile using linear segments and get  $T_i$  and  $z_i$  from the corners. Then select  $\delta_i$  to round the corners. The final profile will not go through  $(T_i, z_i)$ .

Specify--

the model check for TTANH5 = 7.0 (W200)  
the input data-format code = \_\_\_\_\_ (W201)  
an input data-set identification number = \_\_\_\_\_ (W202)  
an 80-character description of the model with parameters:

---

and the profile values:

the number of points in the profile -2 = n = \_\_\_\_\_

the profile:    i                     $z_i$                      $T_i$                      $\delta_i$   
    (km,m)                    (°K)                    (km,m)

**OTHER MODELS REQUIRED:** Any temperature-perturbation model. Use NPTEMP if no perturbations are desired. FUNCTION ALCOSH.

FORM TO SPECIFY INPUT DATA FOR  
ATMOSPHERIC TEMPERATURE MODEL TTABLE

This model represents the temperature profile by a sequence of cubic segments such that the temperature gradient is continuous through each profile point. This is not a cubic spline; the coefficients of the cubic fit in each segment depend on only the four nearest profile points.

The coefficients of the cubic are calculated as follows: each set of three successive points in the profile is first fit with a quadratic. The slope of that quadratic at the middle profile point is then assigned to that profile point. This procedure assigns a slope to every profile point except the first and last. A slope of zero is assigned to the first and last point. Between each pair of profile points the coefficients of the cubic are chosen so that the curve goes through the two points and matches the assigned slope at the two points. Those four conditions determine the four coefficients. Both the temperature and its gradient are continuous throughout the profile, even at the profile points.

Specify--

the model check number for TTABLE = 6.0 (W200)

the input data-format code = 2.0 (W201)

an input data-set identification number = \_\_\_\_\_ (W202)

an 80-character description of the profile:

---

and the profile values:

the number of points in the profile, n = \_\_\_\_\_

the profile:                      height (km)                      Temperature (K)

**OTHER MODELS REQUIRED:** Subroutine GAUSEL and any temperature-perturbation model. Use NPTEMP if no perturbations are desired.

FORM TO SPECIFY INPUT DATA FOR  
ATMOSPHERIC TEMPERATURE-PERTURBATION MODEL TBLOB2

An increase (or decrease) in temperature in a localized region that decays in a Gaussian manner in all three spatial directions.

$$T(r, \theta, \phi) = T_0(r, \theta, \phi) \left\{ 1 + \Delta \exp \left[ - \left( \frac{z - z_0}{W_z} \right)^2 - \left( \frac{\theta - \theta_0}{W_\theta} \right)^2 - \left( \frac{\phi - \phi_0}{W_\phi} \right)^2 \right] \right\}$$

$T_0(r, \theta, \phi)$  is the temperature specified by a temperature model.  $(r, \theta, \phi)$  are the coordinates of the ray point in an Earth-centered spherical polar coordinate system.  $\theta_0 = \pi/2 - \lambda_0$  and  $z = r - r_e$ , where  $r_e$  is the Earth radius. Specify--

the model check for subroutine TBLOB2 = 2.0 (W225)

the input data-format code = \_\_\_\_\_ (W226)

an input data-set identification number = \_\_\_\_\_ (W227)

an 80-character description for the temperature-perturbation model, including description of parameter values:

---

the strength of the increase (or decrease),  $\Delta$  = \_\_\_\_\_ (W228)

the height of maximum effect,  $z_0$  = \_\_\_\_\_ km (W229)

the latitude of maximum effect,  $\lambda_0$  = \_\_\_\_\_ rad, deg, km N (W230)

the longitude of maximum effect,  $\phi_0$  = \_\_\_\_\_ rad, deg, km E (W231)

the Gaussian width in height of the effect,  $W_z$  = \_\_\_\_\_ km (W232)\*

the meridional width of the effect,  $W_\theta$  = \_\_\_\_\_ rad, deg, km (W233)\*

the zonal width of the effect,  $W_\phi$  = \_\_\_\_\_ rad, deg, km (W234)\*

OTHER MODELS REQUIRED: none.

---

\* Setting  $W_z$ ,  $W_\theta$ , or  $W_\phi$  = zero results in no space variation in that direction.

FORM TO SPECIFY INPUT DATA FOR  
ATMOSPHERIC MOLECULAR-WEIGHT MODEL MCONST

A constant molecular weight (independent of height, longitude, latitude,  
and time)

Specify--

the model check for MCONST = 1.0 (W250)

the input data-format code = \_\_\_\_\_ (W251)

an input data-set identification number = \_\_\_\_\_ (W252)

an 80-character description of the molecular weight:

---

the value of the constant molecular weight, M = \_\_\_\_\_ (W253)

OTHER MODELS REQUIRED: none.

FORM TO SPECIFY INPUT DATA FOR  
VISCOSITY/CONDUCTIVITY MODEL MUARDC

This subroutine calculates the atmospheric molecular viscosity using the ARDC formula for viscosity and calculates atmospheric thermal conductivity from the value of viscosity using a Prandtl number specified by the user. This model is used only to calculate acoustic absorption when either AWWWL or ANWWL is used.

The ARDC formula for viscosity is (U.S. Standard Atmosphere, 1976, p. 19, NOAA, NASA, USAF, U.S. Government Printing Office, Washington, D.C., October 1976)

$$\mu = \beta T^{3/2}/(S+T) ,$$

where T is the atmospheric temperature in Kelvins.

The atmospheric thermal conductivity using the Prandtl approximation (e.g., Francis Weston Sears, Thermodynamics, Addison-Wesley, 1956, pp. 267-9) is

$$\kappa = \gamma R\mu/((\gamma-1)M Pr) ,$$

where  $\gamma$  is the ratio specific heats = 1.4,  
R is the universal gas constant,  
and M is the mean atmospheric molecular weight.

Specify --

the model check for subroutine MUARDC = 1.0 (W500)

the input data-format code = \_\_\_\_\_ (W501)

an input data-set identification number = \_\_\_\_\_ (W502)

an 80-character description for the absorption model, including description of parameter values:

---

the viscosity constant,  $\beta =$  \_\_\_\_\_  $\text{kg s}^{-1} \text{m}^{-1} \text{K}^{-1/2}$  (W503)  
( $1.458 \times 10^{-6} \text{ kg s}^{-1} \text{m}^{-1} \text{K}^{-1/2}$  suggested)

Sutherland's constant, S = \_\_\_\_\_ Kelvins (W504)  
(110.4 Kelvins suggested)

Prandtl number, Pr = \_\_\_\_\_ (W505) (0.733 suggested)

OTHER MODELS REQUIRED: Any atmospheric temperature model and any atmospheric molecular weight model.

FORM TO SPECIFY INPUT DATA FOR  
PRESSURE MODEL PEXP

This model is used only to calculate absorption when either AWWWL or ANWWL is used. The pressure is given by

$$P = P_0 \exp(-z/H),$$

where  $z$  is the height above sea level.

Specify --

the model check for subroutine PEXP = 1.0 (W550)

the input data-format code =            (W551)

an input data-set identification number =            (W552)

an 80-character description for the pressure model, including description of parameter values:

---

the pressure at sea level,  $P_0 =$             Newtons/m<sup>2</sup> (W553)

( $1.01328 \times 10^5$  Newtons/m<sup>2</sup> suggested)

the pressure scale height,  $H =$             km, m (W554)

OTHER MODELS REQUIRED: Any pressure-perturbation model. Use NPPRES if no perturbation is desired.

FORM TO SPECIFY INPUT DATA FOR  
TERRAIN MODEL GHORIZ

A constant-height terrain model, i.e., a sphere concentric with the Earth.

$$g(r, \theta, \phi) = h - z_0 ,$$

where  $h = r - r_e$  ,

$$\frac{\partial g}{\partial r} = 1 , \quad \frac{\partial g}{\partial \theta} = 0 , \quad \frac{\partial g}{\partial \phi} = 0 ,$$

$$\frac{\partial^2 g}{\partial r^2} = \frac{\partial^2 g}{\partial r \partial \theta} = \frac{\partial^2 g}{\partial \theta \partial r} = \frac{\partial^2 g}{\partial r \partial \phi} = \frac{\partial^2 g}{\partial \phi \partial r} = \frac{\partial^2 g}{\partial \theta^2} = \frac{\partial^2 g}{\partial \theta \partial \phi} = \frac{\partial^2 g}{\partial \phi \partial \theta} = \frac{\partial^2 g}{\partial \phi^2} = 0 ,$$

and  $r_e$  is the radius of the Earth.

Specify --

The model check number for GHORIZ = 1.0 (W300)

The input data-format code number = \_\_\_\_\_ (W301)

The input data-set identification number = \_\_\_\_\_ (W302)

an 80-character description of the model including parameters:

---

The constant terrain height,  $z_0$  = \_\_\_\_\_ km, (W303)

**OTHER MODELS REQUIRED:** Any terrain-perturbation model. Use NPERR if no perturbation is desired.

FORM TO SPECIFY INPUT DATA FOR  
TERRAIN MODEL GLORENZ

An east-west Lorentzian-shaped ridge.

$$g(r, \theta, \phi) = h - z,$$

where  $h = r - r_e$ ,

$$z = z_0 / (1 + ((\theta - \theta_0) / \Delta\theta)^2) + z_B,$$

$$\theta_0 = \pi/2 - \lambda_0,$$

and  $r_e$  is the radius of the Earth.

Specify--

the model check number for GLORENZ = 4.0 (W300)

the input data-format code number = \_\_\_\_\_ (W301)

the input data-set identification number = \_\_\_\_\_ (W302)

an 80-character description of the model including parameters:

---

the height of the ridge,  $z_0$  = \_\_\_\_\_ km, m (W303)

the latitude of the ridge center,  $\lambda_0$  = \_\_\_\_\_ rad, deg, km (W304)

the half-width of the ridge,  $\Delta\theta$  = \_\_\_\_\_ rad, deg, km (W305)

base of the ridge (negative if below sea level)  $z_B$  = \_\_\_\_\_ m, km (W306)

OTHER MODELS REQUIRED: Any terrain-perturbation model. Use NPERR if no perturbation is desired.



FORM TO SPECIFY INPUT DATA  
FOR RECEIVER-SURFACE MODEL RHORIZ

A receiver-surface model that is a horizontal surface (i.e., a sphere concentric with the Earth).

$$f(r, \theta, \phi) = h - z_R ,$$

where

$$h = r - r_e$$

and

$r_e$  is the Earth radius

$$\frac{\partial f}{\partial t} = \frac{\partial f}{\partial \theta} = \frac{\partial f}{\partial \phi} = 0$$

$$\frac{\partial f}{\partial r} = 1.0 .$$

Specify--

the model check number for subroutine RHORIZ = 1.0 (W275)

the input data-format code number = \_\_\_\_\_ (W276)

an 80-character description of the model including parameters:

---

the receiver surface height,  $z_R$  = \_\_\_\_\_ km (W20)

OTHER MODELS REQUIRED: none.

FORM TO SPECIFY INPUT DATA  
FOR RECEIVER-SURFACE MODEL RTERR

A receiver-surface model in which the receiver surface is a fixed height above the terrain surface.

$$f(r, \theta, \phi) = g(r, \theta, \phi) + z_R$$

$$\frac{\partial f}{\partial r} = \frac{\partial g}{\partial r}, \quad \frac{\partial f}{\partial \theta} = \frac{\partial g}{\partial \theta}, \quad \frac{\partial f}{\partial \phi} = \frac{\partial g}{\partial \phi},$$

where  $g(r, \theta, \phi)$  and its derivatives are specified in common block /GG/ by the terrain model.

Specify--

the model check number for subroutine RTERR = 2.0 (W275)

the input data-format code number = \_\_\_\_\_ (W276)

an 80-character description of the model including parameters:

---

the height of the receiver surface above the terrain,  $z_R =$  \_\_\_\_\_ km (W20)

OTHER MODELS REQUIRED: Any terrain model.

FORM TO SPECIFY INPUT DATA FOR  
RECEIVER-SURFACE MODEL RVERT

A receiver surface that is a vertical (conical) surface a constant distance from a given origin on the Earth's surface

$$f(r, \theta, \phi) = \sin \lambda_0 \cos \theta + \cos \lambda_0 \sin \theta \cos(\phi - \phi_0) - \cos \alpha_0$$

$$\frac{\partial f}{\partial t} = \frac{\partial f}{\partial r} = 0$$

$$\frac{\partial f}{\partial \theta} = -\sin \lambda_0 \sin \theta + \cos \lambda_0 \cos \theta \cos(\phi - \phi_0)$$

$$\frac{\partial f}{\partial \phi} = -\cos \lambda_0 \sin \theta \sin(\phi - \phi_0) .$$

Specify--

the model check number for subroutine RVERT = 3.0 ~~2.0~~ (W275)

the input data-format code number = \_\_\_\_\_ (W276)

an 80-character description of the model including parameters:

the distance of the surface from the origin,

$\alpha_0 =$  \_\_\_\_\_ rad, deg, km (278)

the latitude of the origin,  $\lambda_0 =$  \_\_\_\_\_ rad, deg, km N (W279)

the longitude of the origin,  $\phi_0 =$  \_\_\_\_\_ rad, deg, km E (W280)

OTHER MODELS REQUIRED: none.

## APPENDIX C: CDC 250 PLOT PACKAGE AND DISSPLA INTERFACE

This appendix describes the plotting commands used by DD PLOT, our local microfilm plotting system, and also an interface called DDSPLA to the DISSPLA\* plot package in common use. Figure C1 shows the steps necessary to obtain graphical output from HARPA, if you have DISSPLA. If you do not have DISSPLA and want graphical output on your own plotting system, you will have to insert the equivalent instructions used by your system into a skeleton plotting routine DDALT. This information was taken with permission from "User's Guide to Cathode-Ray Plotter Subroutines" by L. David Lewis, ESSA Technical Memorandum ERL TM-ORSS5, January 1970. The routines used in this version of HARPA assume DISSPLA version 9.0 and are listed in Appendix D.

The CDC-250 Microfilm Recorder, under control of the NOAA Boulder CDC-CYBER 750 computer, plots data on the face of a high-resolution cathode ray tube, which is photographed onto standard size, perforated, 35-mm film.

The plotting area, called a frame, is a square. Plotting positions are described in rectangular coordinates. Coordinate values are integers in the range 0 - 1023; (0,0) is the "lower left-hand corner."

Plotting specifications are transmitted to the DD PLOT routines via the following COMMON.

```
COMMON/DD/IN,IOR,IT,IS,IC,ICC,IX,IY
```

The usage of each of the eight variables is listed below, followed by an explanation of the subroutine calls.

IN	Intensity. IN=0 specifies normal intensity. IN=1 specifies high intensity.
IOR	Orientation IOR=0 specifies upright orientation. IOR=1 specifies rotated orientation (90° counter-clockwise).

---

\*DISSPLA is the proprietary product of ISSCO, Inc.

IT           Italics (Font).  
 IT=0 specifies non-italic (Roman) symbols.  
 IT=1 specifies italic symbols.

IS           Symbol size.  
 IS=0 specifies miniature size.  
 IS=1 specifies small size.  
 IS=2 specifies medium size.  
 IS=3 specifies large size.

IC           Symbol case.  
 IC=0 specifies uppercase.  
 IC=1 specifies lowercase.

ICC          Character code, 0-63 (R1 format).  
 ICC and IC together specify the symbol plotted.

IX           X-coordinate, 0-1023.

IY           Y-coordinate, 0-1023.

CALL DDINIT (N, ID) is required to initialize the plotting process.

ID is a string of characters to identify the person getting the plot and giving the telephone extension and the place to deliver the microfilm plot.

N is the number of characters in the string "ID."

CALL DDBP       defines a vector origin in position IX, IY.

CALL DDVC       plots a vector (straight line), with intensity IN, from the vector origin defined by the previous DDBP or DDVC call, to the vector end position at IX, IY. A single call to DDBP followed by successive calls to DDVC (with changing IX and IY) plots connected vectors.

CALL DDTAB      initializes tabular plotting.

CALL DDTEXT (N, NT) plots a given array in a tabular mode after initiating tabular plotting by using DDTAB, as described above. NT is an array of length N, containing "text" for tabular plotting. Text consists of character codes, packed eight per word (A8 Format). Text characters are plotted as tabular symbols until the command character ≠ (octal code 14, card code 4,8, or the alphabetic shift counterpart of the = on the keypunch) occurs. The command character is not plotted. DDTEXT interprets the next character as a command; after the command is processed, tabular plotting resumes until ≠ is again encountered. ≠ means end of text: DDTEXT returns to the calling routine.

CALL DDFR       causes a frame advance operation. Plotting on the current frame is completed, and the film advances to the next frame.

CALL DDEND                empties the plot buffer and releases the plotting command file to the microfilm plot queue.

#### DISSPLA CALLS

HARPA calls the following DISSPLA routines directly, rather than through the DDPLOT package. Therefore, if you want to do plotting with a plotting package other than DISSPLA, you will have to convert the following DISSPLA calls to corresponding calls in your plotting package.

CALL DASH                sets dashed-line mode. That is, all plotted curves will be dashed instead of solid.

CALL RESET('DASH') sets solid-line mode. That is, all plotted curves will be solid lines after this call.

HARPA calls a routine named SETANN. SETANN is an entry point in SUBROUTINE FULANN and also in SUBROUTINE SMPANN. When running HARPA, you must make a choice whether to load FULANN or SMPANN. If you do not have the DISSPLA plotting package, then load SMPANN because it makes no special character-generating calls to DISSPLA routines. If you do have the DISSPLA plotting package, then load FULANN. SUBROUTINE FULANN calls the following DISSPLA subroutines directly. If you have the DISSPLA plotting package, then the manual will explain the meaning of these routines. If you do not have the DISSPLA plotting package, then load SMPANN, and ignore these routines.

HEIGHT

MX1ALF

MX2ALF

SCMPLX

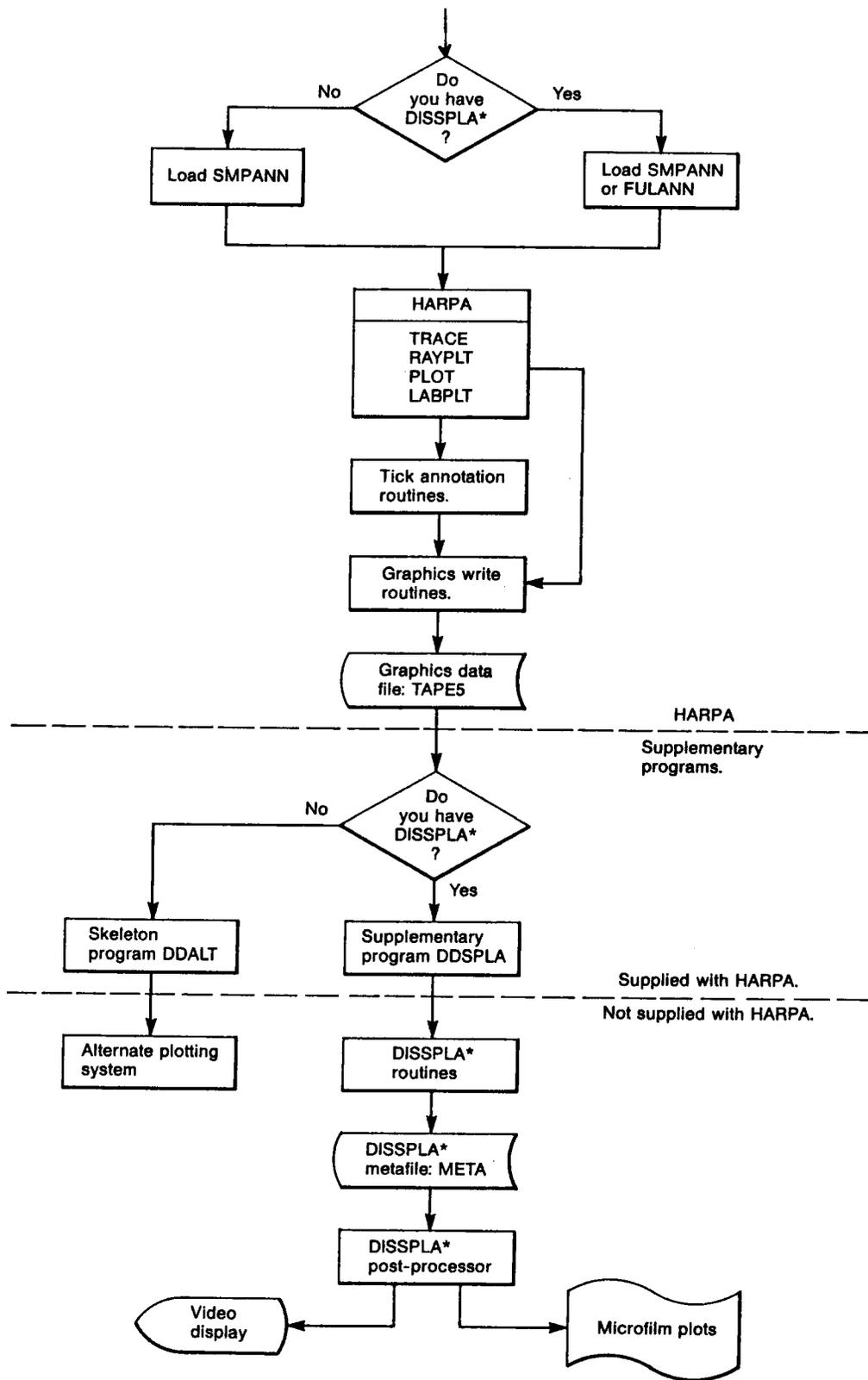


Figure C1. An organization chart that shows how graphical output is produced by a series of programs, some of which are a part of HARPA, and others of which are either supplied along with HARPA or are commercial packages.

## APPENDIX D: FORTRAN SOURCE CODE LISTING

This appendix contains the FORTRAN source-code listing for HARPA, including all of its subroutines and atmospheric models. Their order is the same as the order of the programs in Files 3 through 7 of the distribution tape and the list in Section 7.1. Table D1 lists the routines in alphabetical order, the page where the source code can be found, and the approximate size of each module in bytes.

Where DATA statements are used to initialize variables contained in labeled-common blocks, the sequence number (col. 73-80) contains the code "BL." To adhere strictly to the FORTRAN 77 standard, these statements must be put into separate BLOCK DATA modules. Most FORTRAN environments permit our syntax, however.

```
*****  
WARNING: THIS LISTING IS PROVIDED FOR INFORMATION PURPOSES ONLY. THOSE WHO  
WANT TO USE THE PROGRAM MUST OBTAIN THE SOURCE CODE ON MAGNETIC TAPE FROM THE  
AUTHORS (SEE SECTION 3.1). COPYING THE CODE LISTED HERE WILL NOT PRODUCE A  
USABLE PROGRAM.  
*****
```

Table D1--Alphabetical list of source-code modules

Module Name	Source Bytes	Page	Module Name	Source Bytes	Page
ALCOSH	384	295	NUMSTG	512	291
ANWNL	4736	321	OPNREP	896	294
ANWWL	5376	326	OVERRD	1024	294
ARCTIC	1792	316	PCROSS	768	257
ATMOSHD	8192	286	PEXP	3712	385
AWWNL	5120	323	PLOT	3200	302
AWWWL	5760	329	PLOTBL	128	317
BACKUP	3968	264	PLTANH	2816	309
CBLOB2	4480	354	PLTANOT	2432	311
CLEAR	256	250	PLTHLB	128	309
CONBLK	7424	273	PLTLB	1792	314
CSTANH	4992	349	PRINTR	14720	278
DASH	128	319	PUTDES	512	291
DDALT	6016	405	PUTKST	2176	293
DDBP	512	317	RAYPLT	8320	297
DDEND	256	319	RAYTRC	8576	229
DDFR	128	319	RCROSS	2688	257
DDINIT	256	317	READW	8960	243
DDSPLA	15488	399	READW1	6656	237
DDTAB	128	318	REFLECT	2944	266
DDTEXT	384	318	RENORM	512	278
DDVC	512	318	RERR	512	292
DFCNST	1536	234	RERROR	256	293
DFSYS	1152	233	RESET	128	319
DRAWTKS	1280	313	RHORIZ	3584	390
FIT	2432	268	RKAM	1408	260
FULANN	1792	397	RKAM1	3072	262
GAMRTDM	3968	347	RTERR	3584	391
GAUSEL	2688	295	RVERT	8832	394
GET	3456	271	SCMPLX	128	320
GET1	2944	269	SET2	128	278
GHORIZ	3328	373	SETXY	384	307
GLORENZ	4480	375	SFILL	512	292
GTANH	5376	378	SFILTR	128	295
GTUNIT	128	240	SMPANN	1536	396
HAMLTN	2944	258	SREAD1	512	242
HEIGHT	128	320	STOPIT	256	293
ITEST	256	271	STRIM	512	292
LABPLT	6400	305	TBLOB2	4480	367
MCONST	3456	371	TIKLINE	640	311
MUARDC	4096	381	TLINEAR	3840	356
MX1ALF	128	320	TRACE	9344	252
MX2ALF	128	320	TTABLE	6016	361
ND2B	384	250	TTANH5	5120	359
NPABSR	3200	384	UCON	2432	250
NPPRES	3072	388	ULOGZ2	4480	337
NPSPEED	3072	352	VVORTX3	4992	340
NPTEMP	3072	369	WCHANGE	512	277
NPTErr	384	381	WGAUSS2	4480	343
NPWIND	3456	345	WLINEAR	4096	333
NTEMP	3328	365	WTIDE	4352	335

## RAY-TRACING CORE (Tape File 3)

	PROGRAM RAYTRC	RAYTRC 2
C	MAIN PROGRAM FOR THE RAY TRACING PACKAGE.	RAYTRC 3
C	SETS THE INITIAL CONDITIONS FOR EACH RAY AND CALLS TRACE	RAYTRC 4
C		RAYTRC 5
C	COMMON DECK "RAYDEV" INSERTED HERE	CRAYDEV2
C	DEVICE ASSIGNED TO RAYTRC INPUT FILE	CRAYDEV4
C	COMMON/RAYDEV/NRYIND,NDEVTMP,NFRMAT,NDEVGRP,NDEVBIN	CRAYDEV5
	LOGICAL WCHANGE,FIRST	RAYTRC 7
	REAL WS(400)	RAYTRC 8
C	COMMON DECK "FILEC" INSERTED HERE	CFILEC 2
	COMMON /FILEC/NPLTDP	CFILEC 4
C	COMMON DECK "CERR" INSERTED HERE	CERR 2
	COMMON/ERR/NERG,NERR,NERT,NERP	CERR 3
C	COMMON DECK "GG" INSERTED HERE	CGG 2
	REAL MODG	CGG 4
	COMMON/GG/MODG(4)	CGG 5
	COMMON/GG/G,PGR,PGRR,PGRTH,PGRPH	CGG 6
	COMMON/GG/PGTH,PGPH,PGTHTH,PGPHPH,PGTHPH,GSELECT,GTIME	CGG 7
C	COMMON DECK "HDR" INSERTED HERE	CHDR 2
	CHARACTER*10 INITID*80,DAT,TOD	CHDR 4
	COMMON/HDR/SEC	CHDR 5
	COMMON/HDR/INITID,DAT,TOD	CHDR 6
C	COMMON DECK "CONST" INSERTED HERE	CCONST 2
	COMMON/PCONST/CREG,RGAS,GAMMA	CCONST 4
	COMMON/MCONST/PI,PIT2,PID2,DEGS,RAD,ALN10	CCONST 5
C	COMMON DECK "FLAG" INSERTED HERE	CFLAG 2
	LOGICAL NEWWR,NEWWP,NEWTRC,PENET	CFLAG 4
	COMMON /FLG/ NTYP,NEWWR,NEWWP,NEWTRC,PENET,LINES,IHOP,HPUNCH	CFLAG 5
	COMMON/FLGP/NSET	CFLAG 6
C	COMMON DECK "RINPLEX" INSERTED HERE	CRINPLE2
	REAL KAY2,KAY2I	CRINPLE4
	COMPLEX PNP,POLAR,LPOLAR	CRINPLE5
	LOGICAL SPACE	CRINPLE6
	CHARACTER DISPM*6	CRINPLE7
	COMMON/RINPL/DISPM	CRINPLE8
	COMMON /RIN/ MODRIN(8),RAYNAME(2,3),TYPE(3),SPACE	CRINPLE9
	COMMON/RIN/OMEGMIN,OMEGMAX,KAY2,KAY2I	CRINPL10
	COMMON/RIN/PNP(10),POLAR,LPOLAR,SGN	CRINPL11
C	COMMON DECK "RK" INSERTED HERE	CRK 2
C	DEFINE SIZE REQUIRED FOR RAY STATE SAVE ARRAY	CRK 4
	PARAMETER (LRKAMS=87+2*100,NXRKMS=12+LRKAMS,MXEQPT=21)	CRK 5
	PARAMETER (NRKSAV=NXRKMS+MXEQPT-1)	CRK 6
	COMMON /RK/ NEQS,STEP,MODE,E1MAX,E1MIN,E2MAX,E2MIN,FACT,RSTART	CRK 7
C	COMMON DECK "RKAM" INSERTED HERE	RKAMCOM2
	REAL KR,KTH,KPH	RKAMCOM4
	COMMON//R,TH,PH,KR,KTH,KPH,RKVAR(14),TPULSE,CSTEP,DRDT(20)	RKAMCOM5
C	COMMON DECK "WWR" INSERTED HERE	CWWR 2
	PARAMETER (NWARSZ=1000)	CWW1 3
	COMMON/WW/ID(10),MAXW,W(NWARSZ)	CWW1 4
	REAL MAXSTP,MAXERR,INTYP,LLAT,LLON	CWW2 2
	EQUIVALENCE (EARTH,W(1)),(RAY,W(2)),(XMTRH,W(3)),(TLAT,W(4)),	CWW2 3
	1 (TLON,W(5)),(OW,W(6)),(FBEG,W(7)),(FEND,W(8)),(FSTEP,W(9)),	CWW2 4
	2 (AZ1,W(10)),(AZBEG,W(11)),(AZEND,W(12)),(AZSTEP,W(13)),	CWW2 5
	3 (BETA,W(14)),(ELBEG,W(15)),(ELEND,W(16)),(ELSTEP,W(17)),	CWW2 6
	8 (RCVRH,W(20)),	CWW2 7

4	(ONLY,W(21)),(HOP,W(22)),(MAXSTP,W(23)),(PLAT,W(24)),(PLON,W(25))	CWW2	8
5	(HMAX,W(26)),(RAYFNC,W(29)),(EXTINC,W(33)),	CWW2	9
6	(HMIN,W(27)),(RGMAX,W(28)),	CWW2	10
8	(INTYP,W(41)),(MAXERR,W(42)),(ERATIO,W(43)),	CWW2	11
6	(STEP1,W(44)),(STPMAX,W(45)),(STPMIN,W(46)),(FACTR,W(47)),	CWW2	12
7	(SKIP,W(71)),(RAYSET,W(72)),(PRTSRP,W(74)),(HITLET,W(75))	CWW2	13
9	,(BINRAY,W(76)),(PAGLN,W(77)),(PLT,W(81)),(PFACTR,W(82)),	CWW2	14
1	(LLAT,W(83)),(LLON,W(84)),(RLAT,W(85)),(RLON,W(86))	CWW2	15
2	,(TIC,W(87)),(HB,W(88)),(HT,W(89)),(TICV,W(96))	CWW2	16
C	CHARACTER TMP80*80	RAYTRC19	
C	DATA FIRST/.TRUE./	RAYTRC20	
C	INITIALIZE FILES , SET CONTANTS AND MAKE SYSTEM CALLS	RAYTRC21	
C	CALL STDINI	RAYTRC22	
C	INITIALIZE LINE COUNTS FOR CURRENT AND LAST HEADER	RAYTRC23	
C	LINES=0	RAYTRC24	
C	LHDRPG=0	RAYTRC25	
C	REWIND NRYIND	RAYTRC26	
C	INITIALIZE RAYSET FILE	RAYTRC27	
5	READ(NRYIND,'(A)',END=8) TMP80	RAYTRC28	
	WRITE(9,'(A)') TMP80	RAYTRC29	
	GO TO 5	RAYTRC30	
C	WRITE(9,'(A)') '****SOFT EOF*****'	RAYTRC31	
8	REWIND NRYIND	RAYTRC32	
C	READ IN USERS NAME AND TELEPHONE EXTENSION FOR IDENTIFYING	RAYTRC33	
C	MICROFILM PLOTS.	RAYTRC34	
C	REPOSITION DINP AFTER IDENTIFIER	RAYTRC35	
C	READ(NRYIND,'(A)',END=6000) TMP80	RAYTRC36	
C	C***** READ W ARRAY AND PRINT NON-ZERO VALUES	RAYTRC37	
	IRUN=0	RAYTRC38	
	NSET=0	RAYTRC39	
C	CALL READW	RAYTRC40	
10	NSET=NSET+1	RAYTRC41	
	ICODE=ND2B(INT(RAYFNC))	RAYTRC42	
C	PROCESS RAYPATH CALCULATIONS ONLY IF W(29) IS BEING USED	RAYTRC43	
	IF((RAYFNC.NE.0.).AND.(AND(ICODE,4).EQ.0)) GO TO 10	RAYTRC44	
C	C***** LET ROUTINES PRINTR AND RAYPLT KNOW THERE IS A NEW W ARRAY	RAYTRC45	
	NEWWP=.TRUE.	RAYTRC46	
	NEWWR=.TRUE.	RAYTRC47	
	IRUN=IRUN+1	RAYTRC48	
C	SET BINARY RAY FILE UNIT TO ZERO IF NO OUTPUT WANTED	RAYTRC49	
C	NPLTDP=0	RAYTRC50	
	IF(BINRAY.NE.0.0) NPLTDP=NDEVBIN	RAYTRC51	
C	C***** INITIALIZE THE MODELS VIA 'DISPER'	RAYTRC52	
	CALL IDISPER	RAYTRC53	
		RAYTRC54	
		RAYTRC55	
		RAYTRC56	
		RAYTRC57	
		RAYTRC58	
		RAYTRC59	
		RAYTRC60	
		RAYTRC61	
		RAYTRC62	
		RAYTRC63	
		RAYTRC64	

C	IF(FIRST.AND.PLT.NE.0.) CALL DDINIT(8,INITID)	RAYTRC65
	IF(PLT.NE.0.) FIRST=.FALSE.	RAYTRC66
C		RAYTRC67
C	PREVENT RERUNNING SAME MODEL CASES	RAYTRC68
	IF(IRUN.EQ.1) GO TO 12	RAYTRC69
	IF(.NOT.WCHANGE(WS(1),W(1))) GO TO 10	RAYTRC70
	PRINT *, 'PROCESSING FOR RUNSET #', NSET	RAYTRC71
C		RAYTRC72
12	CALL RMOVE(WS,W,400)	RAYTRC73
C		RAYTRC74
	OW=0.	RAYTRC75
	BETA=0.	RAYTRC76
	AZ1=0.	RAYTRC77
C		RAYTRC78
	CALL HEADER1	RAYTRC79
C		RAYTRC80
C	C***** PRINT OUT THE CONTENTS OF THE 'W' ARRAY	RAYTRC81
C	C***** DETERMINE TRANSMITTER LOCATION IN COMPUTATIONAL COORDINATE	RAYTRC82
C	C***** SYSTEM (GEOMAGNETIC COORDINATES IF DIPOLE FIELD IS USED)	RAYTRC83
	SP=SIN (PLAT)	RAYTRC84
	CP=SIN (PID2-PLAT)	RAYTRC85
	SDPH=SIN (TLON-PLON)	RAYTRC86
	CDPH=SIN (PID2-(TLON-PLON))	RAYTRC87
	SL=SIN (TLAT)	RAYTRC88
	CL=SIN (PID2-TLAT)	RAYTRC89
	ALPHA=ATAN2 (-SDPH*CP, -CDPH*CP*SL+SP*CL)	RAYTRC90
	TH0=ACOS (CDPH*CP*CL+SP*SL)	RAYTRC91
	PH0=ATAN2 (SDPH*CL, CDPH*SP*CL-CP*SL)	RAYTRC92
C		RAYTRC93
	R=EARTH	RAYTRC94
	TH=TH0	RAYTRC95
	PH=PH0	RAYTRC96
	CALL TOPOG	RAYTRC97
C		RAYTRC98
C	OBTAIN ABSOLUTE HEIGHT OF THE TRANSMITTER.	RAYTRC99
C	IF IT WAS SPECIFIED AS RELATIVE TO THE TERRAIN, THEN REMOVE	RAYTR100
C	THE FLAG VALUE 10**40 WHICH WAS ADDED AT INPUT.	RAYTR101
C		RAYTR102
	TMP=XMTRH	RAYTR103
	IF(XMTRH .EQ. 1.E-40) XMTRH=0.0	RAYTR104
	IF( ABS(XMTRH) .GE. 1.E20 ) XMTRH=XMTRH*1.E-40	RAYTR105
	IF(TMP.NE.XMTRH) XMTRH=XMTRH-G/PGR	RAYTR106
C		RAYTR107
C	CHECK THAT TRANSMITTER IS ABOVE TERRAIN.	RAYTR108
C		RAYTR109
	IF(-G/PGR .LE. XMTRH) GO TO 655	RAYTR110
C		RAYTR111
	PRINT 640, IRUN	RAYTR112
	WRITE(3,640) IRUN	RAYTR113
640	FORMAT('0***** TRANSMITTER BELOW TERRAIN. RUN ',I3	RAYTR114
	1 , ' TERMINATED.'/'SEE W-ARRAY PRINTOUT. INPUT CONTINUES.'//)	RAYTR115
	CALL SETOVR	RAYTR116
	CALL PRINTW	RAYTR117
	GO TO 10	RAYTR118
		RAYTR119

C		RAYTR120
655	CALL SETOVR	RAYTR121
	CALL PRINTW	RAYTR122
	CALL IPRINTR	RAYTR123
C*****	INITIALIZE PRINT CONTROL PARAMTERS	RAYTR124
	LINSPP=PAGLN	RAYTR125
	LNPHPG=LINSPP/2	RAYTR126
	IF(LNPHPG.LT.40) LNPHPG=LINSPP	RAYTR127
C		RAYTR128
C*****	LOOP ON FREQUENCY, AZIMUTH ANGLE, AND ELEVATION ANGLE	RAYTR129
	NFREQ=1	RAYTR130
	IF (FSTEP.NE.0.) NFREQ=(FEND-FBEG)/FSTEP+1.5	RAYTR131
	NAZ=1	RAYTR132
	IF (AZSTEP.NE.0.) NAZ=(AZEND-AZBEG)/AZSTEP+1.5	RAYTR133
	NBETA=1	RAYTR134
	IF (ELSTEP.NE.0.) NBETA=(ELEND-ELBEG)/ELSTEP+1.5	RAYTR135
	DO 50 NF=1,NFREQ	RAYTR136
	OW=FBEG+(NF-1)*FSTEP	RAYTR137
	DO 45 J=1,NAZ	RAYTR138
	AZ1=AZBEG+(J-1)*AZSTEP	RAYTR139
	AZA=AZ1*DEGS	RAYTR140
	GAMMA1=PI-AZ1+ALPHA	RAYTR141
	SGAMMA=SIN (GAMMA1)	RAYTR142
	CGAMMA=SIN (PID2-GAMMA1)	RAYTR143
	DO 40 I=1,NBETA	RAYTR144
	BETA=ELBEG+(I-1)*ELSTEP	RAYTR145
	EL=BETA*DEGS	RAYTR146
	CBETA=SIN (PID2-BETA)	RAYTR147
	R=EARTHTR+XMTRH	RAYTR148
	TH=THO	RAYTR149
	PH=PHO	RAYTR150
	KR=SIN (BETA)	RAYTR151
	KTH=CBETA*CGAMMA	RAYTR152
	KPH=CBETA*SGAMMA	RAYTR153
	TPULSE=0.	RAYTR154
	RSTART=1.	RAYTR155
C*****	THE FOLLOWING LINE NEEDED FOR RAY TRACING IN COMPLEX SPACE	RAYTR156
	SGN=1.0	RAYTR157
C*****	CALL MODELS	RAYTR158
	CALL DISPER	RAYTR159
C		RAYTR160
	LINPG=LINES-LHDRPG	RAYTR161
	IF(I.EQ.1 .OR. LINPG.GE.LINSPP-20) THEN	RAYTR162
C		RAYTR163
C	PUT OUT SUBHEADERS FROM MEDIA AND PRINTR ROUTINES	RAYTR164
	CALL HEADER2	RAYTR165
	CALL PRNHD1(' ')	RAYTR166
C		RAYTR167
C	COMPUTE LINE COUNT OF THIS HEADER	RAYTR168
	LHDRPG=LINES/LINSPP*LINSPP	RAYTR169
	ELSEIF(LINPG.GE.LNPHPG-10 .AND. LINPG.LE.LNPHPG) THEN	RAYTR170
C	PUT OUT PAGE FEED WITH SUBHEADER IF AT HALF PAGE	RAYTR171
	CALL PRNHD2('1')	RAYTR172
	ELSE	RAYTR173
C	PUT OUT SUBHEADER	RAYTR174

	CALL PRNHD2(' ')	RAYTR175
	ENDIF	RAYTR176
C	IF (KAY2.GT.0.) GO TO 30	RAYTR177
	WRITE(3,2900) OMEGMIN,OMEGMAX	RAYTR178
2900	FORMAT (58H0TRANSMITTER IN EVANESCENT REGION, TRANSMISSION IMPOSSIBLE/20HOMINIMUM FREQUENCY =,E17.10,20H MAXIMUM FREQUENCY =,E17.10)	RAYTR179
	GO TO 44	RAYTR180
30	CALL RENORM(KR,KAY2,3)	RAYTR181
	CALL CLEAR(RKVAR,NEQS-6)	RAYTR182
	CALL TOPOG	RAYTR183
	IF (NERG.GT.0) RKVAR(NERG)=G	RAYTR184
	IF (NERR.GT.0) RKVAR(NERR)=PGR	RAYTR185
	IF (NERT.GT.0) RKVAR(NERT)=PGTH	RAYTR186
	IF (NERP.GT.0) RKVAR(NERP)=PGPH	RAYTR187
C		RAYTR188
C	CALCULATE ONE RAY PATH	RAYTR189
	CALL TRACE	RAYTR190
	OSEC=SEC	RAYTR191
	CALL SYSSEC(SEC)	RAYTR192
	DIFF=SEC-OSEC	RAYTR193
C		RAYTR194
C	ADD TO LINES COUNT FOR ELAPSED TIME REPORT	RAYTR195
	LINES=LINES+2	RAYTR196
	WRITE(3,3500) DIFF	RAYTR197
3500	FORMAT (/T93,'THIS RAY CALCULATION TOOK ',F8.3,' SEC')	RAYTR198
C		RAYTR199
	IF (PENET.AND.ONLY.NE.0..AND.IHOP.EQ.1) GO TO 44	RAYTR200
40	CONTINUE	RAYTR201
44	IF (PLT.GT.0.AND.(NAZ.LE.1.OR.NBETA.GT.1)) CALL ENDPLT	RAYTR202
45	CONTINUE	RAYTR203
	IF (PLT.GT.0.AND.NAZ.GT.1.AND.NBETA.LE.1) CALL ENDPLT	RAYTR204
	IF (PENET.AND.ONLY.NE.0..AND.IHOP.EQ.1.AND.NAZ.EQ.1.AND.NBETA.EQ.1)	RAYTR205
1	GO TO 55	RAYTR206
50	CONTINUE	RAYTR207
55	IF (RAYSET.NE.0.) WRITE(9,5000)	RAYTR208
5000	FORMAT (78X,1H-)	RAYTR209
	GO TO 10	RAYTR210
6000	PRINT *,'DINP EMPTY OR NOT FOUND'	RAYTR211
	STOP	RAYTR212
	END	RAYTR213
		RAYTR214
		RAYTR215

	SUBROUTINE DFSYS	DFSYS 2
	CHARACTER DAT*(*),DATX*10	DFSYS 3
	CHARACTER TIM*(*),TIMX*10	DFSYS 4
C		DFSYS 5
C	ALL ROUTINES WHICH RELY ON SYSTEM BASED FUNCTIONS, SUCH AS TIME	DFSYS 6
C	OF DAY OR MAY BENEFIT FROM SYSTEM AVAILABLE ROUTINES FOR BETTER	DFSYS 7
C	PERFORMANCE, SUCH AS 'RMOVE' HAVE BEEN COLLECTED IN THIS ROUTINE.	DFSYS 8
C		DFSYS 9
	ENTRY RMOVE(X,Y,N)	DFSYS 10

C	MOVE 'N' COMPONENTS OF ARRAY 'Y' TO ARRAY 'X'.	DFSYS 11
C	THIS LOGIC WILL HANDLE OVERLAP CASES ONLY FOR X(M)=X(M+N1)	DFSYS 12
C	WITH N1>0, M=1,N.	DFSYS 13
C	REAL X(N),Y(N)	DFSYS 14
C		DFSYS 15
C	IF(N.LE.0) RETURN	DFSYS 16
C	USE CYBER BUILT-IN ROUTINE	DFSYS 17
C	CALL MOVLEV(Y,X,N)	DFSYS 18
C		DFSYS 19
C	THE EQUIVALENT FORTRAN CODING FOR THIS ROUTINE ARE THE FOLLOWING	DFSYS 20
C	TWO LINES.	DFSYS 21
C	DO 10 I=1,N	DFSYS 22
10	X(I)=Y(I)	DFSYS 23
C		DFSYS 24
C	RETURN	DFSYS 25
C	ENTRY SYSSEC(SECS)	DFSYS 26
C		DFSYS 27
C	OBTAIN CURENT TIME OF DAY IN SECONDS FROM SYSTEM ROUTINE	DFSYS 28
C	SECS=0	DFSYS 29
C	SYSTEM CALL NEEDED FOR THE CYBER NOS OP SYS	DFSYS 30
C	CALL SECOND(SECS)	DFSYS 31
C	SYSTEM CALL NEEDED FOR CRAY COMPUTER UNDER CTSS	DFSYS 32
C	CALL TIMEUSED(ICPU,IO,ISYS,MEM)	DFSYS 33
C	SECS=ICPU/1.E6	DFSYS 34
C	RETURN	DFSYS 35
C		DFSYS 36
C	ENTRY SYSTIM(TIM)	DFSYS 37
C		DFSYS 38
C	OBTAIN CURENT TIME OF DAY AS A CHARACTER STRING FROM SYSTEM ROUTI	DFSYS 39
C	TIM='TIME'	DFSYS 40
C	SYSTEM CALL NEEDED FOR THE CYBER NOS OP SYS	DFSYS 41
C	CALL TIME(TIM)	DFSYS 42
C	SYSTEM CALL NEEDED FOR THE CRAY CTSS OP SYS	DFSYS 43
C	CALL TIMEDATE(TIM,DATX,MACH)	DFSYS 44
C	RETURN	DFSYS 45
C		DFSYS 46
C	ENTRY SYSDAT(DAT)	DFSYS 47
C		DFSYS 48
C	OBTAIN CURENT DATE AS A CHARACTER STRING FROM SYSTEM ROUTINE	DFSYS 49
C	DAT='DATE'	DFSYS 50
C	SYSTEM CALL NEEDED FOR THE CYBER NOS OP SYS	DFSYS 51
C	CALL DATE(DAT)	DFSYS 52
C	SYSTEM CALL NEEDED FOR THE CRAY CTSS OP SYS	DFSYS 53
C	CALL TIMEDATE(TIMX,DAT,MACH)	DFSYS 54
C	RETURN	DFSYS 55
C	ENTRY MORTEM	DFSYS 56
C	STOP 'POST MORTEM'	DFSYS 57
C	END	DFSYS 58
C		
C	SUBROUTINE DFCNST	DFCNST 3
C		DFCNST 6

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C      THIS MODULE PROVIDES CONSTANTS WHICH ARE EXPLICITLY DEPENDENT      DFCNST 7
C      ON MACHINE ARCHITECTURE AND SHOULD BE EXAMINED WHEN MAKING ANY    DFCNST 8
C      MIGRATION OF THE RAY TRACING ROUTINES.                            DFCNST 9
C                                                                           DFCNST10
C      COMMON DECK "RMACH" INSERTED HERE                                  CRMACH 2
C      COMMON/CRMACH/RMACH(5)                                           CRMACH 4
C                                                                           DFCNST12
C      SINGLE PRECISION MACHINE CONSTANTS                                DFCNST13
C      (SEE DIGITAL SIGNAL PROCESSING, IEEE PRESS 1979 P S-7)          DFCNST14
C                                                                           DFCNST15
C      THE CONSTANTS ARE DERIVED FROM THE FOLLOWING                      DFCNST16
C      FORM FOR FLOATING POINT NUMBERS:                                  DFCNST17
C                                                                           DFCNST18
C      SIGN (B**E)* ( (X(1)/B) + ... + (X(T)/B**T) )                   DFCNST19
C      FOR MOST MACHINES THE BASE B=2.                                    DFCNST20
C      FOR THE CYBER 60-BIT MACHINES                                     DFCNST21
C      T=48, EMIN=-974 AND EMAX=1070.                                    DFCNST22
C      FOR THE PDP-11 AND VAX-11 MACHINES                               DFCNST23
C      T=24, EMIN=-127 AND EMAX=127                                     DFCNST24
C                                                                           DFCNST25
C      RMACH(1)  SMALLEST POSITIVE MAGNITUDE = B**(EMIN-1)              DFCNST26
C      RMACH(2)  LARGEST MAGNITUDE          = B**EMAX*(1-B**(-T))       DFCNST27
C      RMACH(3)  SMALLEST RELATIVE SPACING = B**(-T)                   DFCNST28
C      RMACH(4)  LARGEST RELATIVE SPACING   = B**(1-T)                  DFCNST29
C      RMACH(5)  LOG10(B=2)                = LOG10(B=2)                 DFCNST30
C                                                                           DFCNST31
C      CONSTANTS HERE ARE FOR CDC 6000/7000/CYBER SERIES COMPUTERS      DFCNST32
C      PLEASE SUBSTITUTE FOR OTHER MACHINES                              DFCNST33
C                                                                           DFCNST34
C                                                                           DFCNST35
C      INTEGER SMALL(2)                                                 DFCNST36
C      INTEGER LARGE(2)                                                 DFCNST37
C      INTEGER RIGHT(2)                                                 DFCNST38
C      INTEGER DIVER(2)                                                 DFCNST39
C      INTEGER LOG10(2)                                                 DFCNST40
C                                                                           DFCNST41
C      EQUIVALENCE (RMACH(1),SMALL(1))                                   DFCNST42
C      EQUIVALENCE (RMACH(2),LARGE(1))                                   DFCNST43
C      EQUIVALENCE (RMACH(3),RIGHT(1))                                   DFCNST44
C      EQUIVALENCE (RMACH(4),DIVER(1))                                   DFCNST45
C      EQUIVALENCE (RMACH(5),LOG10(1))                                   DFCNST46
C                                                                           DFCNST47
C      MACHINE CONSTANTS FOR CYBER 170/180 COMPUTERS                    DFCNST48
C                                                                           DFCNST49
C      DATA RMACH(1) / O"00014000000000000000" /                      DFCNST50
C      DATA RMACH(2) / O"37767777777777777777" /                      DFCNST51
C      DATA RMACH(3) / O"16404000000000000000" /                      DFCNST52
C      DATA RMACH(4) / O"16414000000000000000" /                      DFCNST53
C      DATA RMACH(5) / O"17164642023241175720" /                      DFCNST54
C                                                                           DFCNST55
C      C***REFERENCES  FOX, P.A., HALL, A.D., SCHRYER, N.L, *FRAMEWORK FOR DFCNST56
C      A PORTABLE LIBRARY*, ACM TRANSACTIONS ON MATHE-                DFCNST57
C      MATICAL SOFTWARE, VOL. 4, NO. 2, JUNE 1978,                    DFCNST58
C      PP. 177-188.                                                    DFCNST59
C      C***ROUTINES CALLED  XERROR                                       DFCNST60

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SUBROUTINE READW1(AB,NWOK,MSET,MX,NTBL,ITBL,FRMTBL,GP)
C HANDLES INPUT OF TABULAR DATA REQUIRED BY SOME MODELS. READW1 2
C COMMON DECK "RAYDEV" INSERTED HERE READW1 3
C DEVICE ASSIGNED TO RAYTRC INPUT FILE CRAYDEV2
COMMON/RAYDEV/NRYIND,NDEVTMP,NFRMAT,NDEVGRP,NDEVBIN CRAYDEV4
C COMMON DECK "CUCON" INSERTED HERE CRAYDEV5
COMMON/UCONV/CNVV(4,4) CUCON 2
CHARACTER PCV*3,CNVC*2 CUCON 4
COMMON/UCONC/PCV(4),CNVC(4,4) CUCON 5
C COMMON DECK "CONST" INSERTED HERE CUCON 6
COMMON/PCONST/CREF,RGAS,GAMMA CCONST 2
COMMON/MCONST/PI,PIT2,PID2,DEGS,RAD,ALN10 CCONST 4
C COMMON DECK "WWR" INSERTED HERE CCONST 5
PARAMETER (NWARSZ=1000) CWWR 2
COMMON/WW/ID(10),MAXW,W(NWARSZ) CWW1 3
REAL MAXSTP,MAXERR,INTYP,LLAT,LLON CWW1 4
EQUIVALENCE (EARTH,W(1)),(RAY,W(2)),(XMTRH,W(3)),(TLAT,W(4)), CWW2 2
1 (TLON,W(5)),(OW,W(6)),(FBEG,W(7)),(FEND,W(8)),(FSTEP,W(9)), CWW2 3
2 (AZ1,W(10)),(AZBEG,W(11)),(AZEND,W(12)),(AZSTEP,W(13)), CWW2 4
3 (BETA,W(14)),(ELBEG,W(15)),(ELEND,W(16)),(ELSTEP,W(17)), CWW2 5
8 (RCVRH,W(20)), CWW2 6
4 (ONLY,W(21)),(HOP,W(22)),(MAXSTP,W(23)),(PLAT,W(24)),(PLON,W(25)) CWW2 7
5,(HMAX,W(26)),(RAYFNC,W(29)),(EXTINC,W(33)), CWW2 8
6 (HMIN,W(27)),(RGMX,W(28)), CWW2 9
8 (INTYP,W(41)),(MAXERR,W(42)),(ERATIO,W(43)), CWW2 10
6 (STEP1,W(44)),(STPMAX,W(45)),(STPMIN,W(46)),(FACTR,W(47)), CWW2 11
7 (SKIP,W(71)),(RAYSET,W(72)),(PRTSRP,W(74)),(HITLET,W(75)) CWW2 12
9 ,(BINRAY,W(76)),(PAGLN,W(77)),(PLT,W(81)),(PFACTR,W(82)), CWW2 13
1 (LLAT,W(83)),(LLON,W(84)),(RLAT,W(85)),(RLON,W(86)) CWW2 14
2,(TIC,W(87)),(HB,W(88)),(HT,W(89)),(TICV,W(96)) CWW2 15
LOGICAL NWOK,AB CWW2 16
C READW1 8
CHARACTER LINE*80,ALPHA*3,FBUF*3 READW1 9
PARAMETER (NVAR=6,ALPHA=' A',NACDE=-1,NFIELD=13) READW110
INTEGER IPV(NVAR),NTBL(10),ITBL(10),FRMTBL(10) READW111
CHARACTER*8 PU(NVAR) READW112
REAL GP(*),V(NVAR),CONV(NVAR) READW113
C READW114
C READW115
C THE DATA STRUCTURE EXPECTED BY THIS PROGRAM FOR A DATA BLOCK IS READW116
C SPECIFIED FOR A GIVEN MODEL BY THE THREE ARRAYS NTBL,ITBL,FRMTBL. READW117
C THE TYPE OF DATA EXPECTED FOR A GIVEN FORMAT GROUP IS TAKEN FROM READW118
C ARRAY FRMTBL. IT MUST HAVE AN ENTRY FOR A GIVEN TYPE OF FORMAT READW119
C WHICH IS EITHER ZERO, IF THAT FORMAT IS NOT ALLOWED OR AN ENTRY READW120
C WHOSE VALUE IS EQUAL TO THAT FORMAT TYPE. CURRENTLY ONLY TWO READW121
C FORMAT TYPES ARE ALLOWED, 1 FOR ALPHA AND 2 FOR NUMERIC. READW122
C TO ALLOW MORE FLEXIBILITY IN THE INPUT FILE THE NUMERIC FORMAT READW123
C TYPE IN TURN ALLOWS FOR 3 DIFFERENT DATA FORMATS, SEE BELOW. READW124
C READW125
C OFFSETS INTO THE GENERAL ARRAY 'GP' FOR EACH FORMAT ARE GIVEN READW126
C IN THE ARRAY 'NTBL'. THE SPACING BETWEEN DATA VALUES IN EACH LINE READW127
C READ IS GIVEN IN ARRAY 'ITBL'. THIS SCHEME DOES NOT ALLOW FOR X,Y READW128
C ,Z CYCLES BUT RATHER SEPARATE ARRAYS OF X VALUES, THEN Y VALUES, READW129

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C	AND THEN Z VALUES(ETC. UP TO 'NVAR' VARIABLES).	READW130
C		READW131
	NWOK=.TRUE.	READW132
C		READW133
C	INITIALIZE ANY ALPHANUMERIC ARRAYS TO BLANKS	READW134
	IF(FRMTBL(1).EQ.1) CALL SET2(GP(NTBL(1)),1H ,NTBL(2)-NTBL(1))	READW135
C		READW136
C	BEGIN MULTI-FORMAT LOOP	READW137
5	READ(NRYIND, '(A,A)', END=200) FBUF,LINE	READW138
	IF(NDEVTMP.GT.0) WRITE(NDEVTMP, '(A,A)') FBUF,LINE	READW139
	IF(FBUF.EQ.ALPHA) THEN	READW140
	NFRM=NACDE	READW141
	ELSE	READW142
	READ(FBUF,10) NFRM	READW143
	ENDIF	READW144
10	FORMAT(BZ,I3,A)	READW145
	IF(NFRM .EQ. 0) RETURN	READW146
C		READW147
C	FORMAT #1 IS ASSIGNED TO ALPHANUMERIC INPUT AND LARGER NUMBERS	READW148
C	FOR NUMERIC INPUT.	READW149
C		READW150
C	CHECK NOW FOR NUMERICAL FORMATS.	READW151
C	THESE ARE PROVIDED FOR EASE OF INPUT OF TABULATED DATA	READW152
C	AND ARE PARTLY 'TRANSPARENT' TO THE MODEL INVOLVED. I.E.	READW153
C	THE USER HAS THE OPTION OF SPECIFYING THE NUMBER OF DATA COLUMNS.	READW154
C	INPUT FORMAT NUMBER SPECIFIES THE NUMBER OF COLUMNS OF INPUT DATA	READW155
C	I.E. FOR VALUE 1 A SINGLE DATA COLUMN IS EXPECTED, FOR A VALUE	READW156
C	2 TWO DATA COLUMNS ARE EXPECTED, ETC.	READW157
C		READW158
C	DETERMINE FORMAT NUMBER	READW159
	IF(NFRM.EQ.NACDE) THEN	READW160
	IT=1	READW161
C	ALPHANUMERIC FORMATS MUST BE FIRST IN LIST	READW162
C	SINCE NO OFFSET SPECIFIER IS ALLOWED IN A FULL ALPHA LINE	READW163
	IF(FRMTBL(1).EQ.1) GO TO 100	READW164
	ELSE	READW165
	READ(LINE, '(I2)') IT	READW166
	IT=MAX0(IT,2)	READW167
	IF(IT.LE.MX) GO TO 100	READW168
	ENDIF	READW169
C		READW170
15	AB=.TRUE.	READW171
	PRINT 20, MSET,NFRM,MX	READW172
20	FORMAT(' FOR SET',I5,' FORMAT NUMBER',I5,' EXCEEDS LIMIT OF',I5)	READW173
C	ERROR IN INPUT DATA , STOP HERE	READW174
	STOP	READW175
C		READW176
C	THE 'NTBL' TABLE PROVIDES A LIST OF OFFSETS TO VARIABLE GROUPS IN	READW177
C	MODEL ARRAYS, 'ITBL' GIVES ELEMENT SEPARATION TO ALLOW FOR 2-	READW178
C	DIMENSIONAL ARRAYS AND 'FRMTBL' SPECIFIES THE INPUT FORMAT.	READW179
C		READW180
100	N1=NTBL(IT)	READW181
	N3=ITBL(IT)	READW182
	N2=NTBL(IT+1)-N3	READW183
C		READW184

	IF(NFRM.NE.NACDE) GO TO 110	READW185
C		READW186
	READ(LINE,1010)((GP(I+J-1),I=N1,N2,N3),J=1,N3)	READW187
1010	FORMAT(10A8)	READW188
	GO TO 5	READW189
C		READW190
110	IF(NFRM.LT.1 .OR. NFRM.GT.NVAR) GO TO 200	READW191
C	HANDLE NUMERIC FORMATS	READW192
C		READW193
C	N1 IS STARTING ELEMENT WHICH WILL BE AFTER THE DATA COUNT	READW194
C	VALUE(NEED NELS*N3+1 TOTAL ELEMENTS)	READW195
	N1=N1+1	READW196
	N=0	READW197
C		READW198
C	# ELEMENTS IS EQUAL TO FORMAT NUMBER	READW199
	NELS=NFRM	READW100
C	READ UNITS CONVERSION SPECIFICATION LINE	READW101
	READ(LINE,1018) (PU(I),I=1,3)	READW102
	IF(PU(2).NE.' ') READ(LINE,2024) DELIM	READW103
	IF(PU(2).EQ.' ') READ(LINE,1020) DELIM,(PU(I),I=1,NELS)	READW104
C		READW105
C	ALLOW FOR BLANK CONVERSION LINE PRODUCED BY EIGENRAY ROUTINE	READW106
	IF(DELIM.EQ.0) READ(LINE,2024) DELIM	READW107
C		READW108
C	READ NEXT LINE AND EXTRACT UNIT CONVERSION SPECS IF PRESENT	READW109
C	IN FLOATING FORMAT	READW110
	READ(NRYIND,'(A)') LINE	READW111
	CALL GTUNIT(LINE,PU,NFIELD,NELS, NCARY)	READW112
C	CARRY COUNT IS ZERO IF LINE CONTAINED UNITS SPECIFIERS	READW113
	IF(NCARY.EQ.0.AND.NDEVTMP.GT.0) WRITE(NDEVTMP,'(A)') LINE	READW114
C		READW115
1018	FORMAT(10(A,5X))	READW116
1020	FORMAT(BZ,3X,G10.3,8X,10A)	READW117
2024	FORMAT(T43,G10.3)	READW118
1025	FORMAT(BZ,10G13.6)	READW119
C		READW120
C	LOOK UP CONVERSION CONSTANTS	READW121
	DO 2030 I=1,NELS	READW122
2030	CALL UCON(IPV(I),PU(I),CONV(I))	READW123
C		READW124
C	DELIMITOR TESTING REQUIRES THE INNER LOOP BE EXECUTED	READW125
C	AT LEAST ONCE	READW126
	NX=MAX0(1,N3)	READW127
	N2=MAX0(N2,N1)	READW128
C	BEGIN SINGLE DATA FORMAT LOOP	READW129
	DO 150 J=0,10000	READW130
	IF(NELS.GT.1) THEN	READW131
	IF(NCARY.EQ.0) READ(NRYIND,'(A)') LINE	READW132
	NCARY=0	READW133
	IF(NDEVTMP.GT.0) WRITE(NDEVTMP,'(A)') LINE	READW134
	READ(LINE,1025) (V(I),I=1,NELS)	READW135
	ENDIF	READW136
	K=0	READW137
	DO 145 I=N1+J,N2+J,NX	READW138
	K=K+1	READW139

	IF(NELS.EQ.1) THEN	READW140
	IF(NCARY.EQ.0) READ(NRYIND,'(A)',END=10000) LINE	READW141
	NCARY=0	READW142
	IF(NDEVTMP.GT.0) WRITE(NDEVTMP,'(A)') LINE	READW143
C	FOR SINGLE COLUMN CASE READ NOW	READW144
	READ(LINE,1020) V(K)	READW145
	ENDIF	READW146
	IF(V(K) .EQ. DELIM) GO TO 160	READW147
C		READW148
C	APPLY ANY SCALING CONVERSIONS	READW149
	V(K)=V(K)*CONV(K)	READW150
	IF(J.LT.N3) GP(I)=V(K)	READW151
145	N=N+1	READW152
150	CONTINUE	READW153
C		READW154
10000	IF(V(1).NE.DELIM) CALL ERROR('READW1','NO DELIM',FLOAT(MSET))	READW155
C		READW156
C	SAVE NUMBER OF VALUES AND ELEMENTS(AS FRACTIONAL PART)	READW157
160	IF(N1.GT.1) GP(N1-1)=N+NELS/10.	READW158
C		READW159
C	CONTINUE MULTI-FORMAT LOOP	READW160
	GO TO 5	READW161
C		READW162
200	CALL ERROR('READW1','BAD FORMAT',FLOAT(MSET))	READW163
C		READW164
	END	READW165

	SUBROUTINE GTUNIT(LINE,PU,NFIELD,NVAR, LN)	READW166
C	GTUNIT IS USED TO EXTRACT UNIT CONVERSION SPECIFIERS FROM TABULAR	READW167
C	DATA INPUT.	READW168
C	CONVERSION SPECIFICATIONS ARE TAKEN FROM 'LINE' INPUT STRING.	READW169
C	A FLOATING FORMAT FALLING WITHIN SUCCESSIVE FIELDS OF	READW170
C	LENGTH 'NFIELD' IS PROVIDED FOR.	READW171
C	OUTPUT IS TO UNIT SPECIFIER ARRAY 'PU' FOR A MAXIMUM OF 'NVAR'	READW172
C	FIELDS. FOR A SUCCESS/FAIL RETURN VALUE, 'LN' GIVES THE NUMBER	READW173
C	OF NON-BLANK CHARACTERS USEFUL FOR UNIT DECODING, ZERO IMPLIES	READW174
C	NO USEFUL UNIT INFORMATION WAS FOUND.	READW175
C		READW176
	PARAMETER (MAXLN=130)	READW177
	CHARACTER*(*) LINE,PU(NVAR),TMP*(MAXLN),TMP1*(MAXLN)	READW178
	INTEGER STRIM	READW179
C		READW180
	LN=STRIM(LINE)	READW181
	IF(LN.LT.1) THEN	READW182
	DO 5 I=1,NVAR	READW183
5	PU(I)=' '	READW184
	RETURN	READW185
	ENDIF	READW186
C		READW187
	TMP=' '	READW188
	CALL SFILTR(LINE,TMP,' 0123456789+-E')	READW189

	IF (STRIM(TMP).LT.1) RETURN	READW190
C	SIGNIFY WE CONSUMED THIS LINE	READW191
	LN=0	READW192
C		READW193
	TMP1=LINE	READW194
C	PLACE INTER-SPECIFIER DELIMITORS	READW195
	DO 10 I=NFIELD,NFIELD*NVAR,NFIELD	READW196
	IF (TMP1(I:I).NE.' ') THEN	READW197
	IF (TMP1(I+1:I+1).NE.' ') THEN	READW198
C	IF NO ROOM FOR A BLANK, ITS AN ERROR	READW199
	CALL RERROR('GTUNIT','FORMAT ER1',FLOAT(I))	READW200
	ELSE	READW201
	TMP1(I+1:I+1)='#'	READW202
	ENDIF	READW203
	ELSE	READW204
	TMP1(I:I)='#'	READW205
	ENDIF	READW206
10	CONTINUE	READW207
C		READW208
	NOW SQUEEZE OUT THE BLANKS	READW209
C	CALL SFILTR(TMP1,TMP,'')	READW210
C	HOPEFULLY SOMETHING LEFT	READW211
C		READW212
	NL=STRIM(TMP)	READW213
	ILIN=1	READW214
	DO 20 I=1,NVAR	READW215
C	CHECK FOR EMPTY CONVERSIONS	READW216
	IF (TMP(ILIN:ILIN).EQ.'#') THEN	READW217
	ILIN=ILIN+1	READW218
	PU(I)=' '	READW219
	GO TO 20	READW220
	ENDIF	READW221
C	GET NEXT UNIT TYPE	READW222
	PU(I)(1:2)=TMP(ILIN:ILIN+1)	READW223
C	GET NEXT PHYSICAL UNIT(BLANKS HAVE BEEN REMOVED)	READW224
C	SHORT PHRASE IF A BLANK WAS REMOVED	READW225
	IF (TMP(ILIN+3:ILIN+3).NE.'#') THEN	READW226
	IF (TMP(ILIN+4:ILIN+4).NE.'#') THEN	READW227
C	IF INCORRECT GROUPING OF LETTERS, ITS AN ERROR	READW228
	CALL RERROR('GTUNIT','FORMAT ER2',FLOAT(ILIN))	READW229
	ELSE	READW230
C	ADD TWO LETTER UNIT	READW231
	PU(I)(3:5)=' '//TMP(ILIN+2:ILIN+3)	READW232
	ILIN=ILIN+5	READW233
	ENDIF	READW234
	ELSE	READW235
C	ADD ONE LETTER UNIT	READW236
	PU(I)(3:5)=' '//TMP(ILIN+2:ILIN+2)	READW237
	ILIN=ILIN+4	READW238
	ENDIF	READW239
20	CONTINUE	READW240
C		READW241
	SHOULD HAVE USED UP ALL THE TEXT BY NOW	READW242
C	IF (ILIN.LE.NL) CALL RERROR('GTUNIT','FORMAT ER3',FLOAT(ILIN))	READW243
	END	READW244

	SUBROUTINE SREAD1(AB,NWOK,NW)	SREAD1 9
C	THIS IS THE FALLTHROUGH FEATURE FOR READW WHEN ENCOUNTERING	SREAD110
C	A NON STANDARD LABELED COMMON BLOCK. SREAD1 WILL ADD TABULAR	SREAD111
C	DATA TO THE DEFAULT GP ARRAY PGP AND INCLUDE INDEX OFFSET	SREAD112
C	VALUES TO A LOOKUP ARRAY 'LIST'.	SREAD113
C	COMMON DECK "CPROCFL" INSERTED HERE	CPROCFL2
C	INTEGER PMX,PNTBL,PITBL,PFRMTBL,IDSP(10)	CPROCFL4
C	PARAMETER DECK "PGROUPS"	PGROUPS2
	PARAMETER (NCHPG1=11,NWPV=250,NSPGP=NCHPG1+2*NWPV+1)	PGROUPS3
	PARAMETER (MNGRP=9,MXGRP=69,MXLIST=MXGRP-MNGRP+2)	PGROUPS4
	COMMON/PROCFL/LIST(MXLIST)	CPROCFL6
	COMMON/PROCFL/PMX,PNTBL(10),PITBL(10),PFRMTBL(10),PGP(NSPGP)	CPROCFL7
	EQUIVALENCE (PGP,IDSP)	CPROCFL8
C		SREAD115
C	CHARACTER ITOC*7	SREAD116
		SREAD117
	DATA LIST/MXLIST*0/	SAD1BL 2
	DATA PMX/2/	SAD1BL 3
	DATA PNTBL/1,NCHPG1,NSPGP,7*0/	SAD1BL 4
	DATA PITBL/1,NWPV,8*0/	SAD1BL 5
	DATA PFRMTBL/1,2,8*0/	SAD1BL 6
C		SREAD120
	NWA=IABS(NW)-(MNGRP-2)	SREAD121
	IF(NWA.LT.2 .OR. NWA.GT.MXLIST) CALL STOPIT	SREAD122
	1 ( 'SREAD1 NW='//ITOC(NW)//','LIST(1)='//ITOC(LIST(1)) )	SREAD123
C		SREAD124
	CALL READW1(AB,NWOK,NW,PMX,PNTBL,PITBL,PFRMTBL,PGP)	SREAD125
C		SREAD126
C	UPDATE THE LIST, LIST(1)=MAXIMUM USED ELEMENT	SREAD127
	LIST(1)=MAX0(LIST(1),NWA)	SREAD128
	LIST(NWA)=PNTBL(1)	SREAD129
C		SREAD130
C	GET NEXT NUMERICAL INDEX FROM THE POINTER ARRAY	SREAD131
	NLN=PNTBL(2)	SREAD132
C		SREAD133
C	NUMBER OF VALUES IS INTEGRAL PART OF FIRST ELEMENT	SREAD134
	NPTS=PGP(NLN)	SREAD135
C	NUMBER OF ROWS IS KEPT AS FRACTIONAL PART	SREAD136
	NELS=(PGP(NLN)-NPTS)*10.+5	SREAD137
	N2=NPTS/NELS	SREAD138
	NMX=PITBL(2)	SREAD139
C	MAKE ADJUSTMENTS TO LENGTHS AND OFFSETS	SREAD140
	PITBL(2)=NMX-N2-(NCHPG1-1)	SREAD141
	NUP=NPTS+NCHPG1	SREAD142
	PNTBL(1)=PNTBL(1)+NUP	SREAD143
	PNTBL(2)=PNTBL(2)+NUP	SREAD144
	NLN=NLN+1	SREAD145
C		SREAD146
C	LOOP TO MOVE NELS-1 ROWS OF PGP(NMX,NELS) TO PGP(N2,NELS)	SREAD147
C	THUS MAKING PGP A CONTIGUOUS ARRAY	SREAD148

	NTO=NLN+N2	SREAD149
	NFRM=NLN+NMX	SREAD150
	DO 100 I=2,NELS	SREAD151
	IF(NTO.GT.0 .AND. NFRM+N2-1.LE.NSPGP)	SREAD152
1	CALL RMOVE(PGP(NTO),PGP(NFRM),N2)	SREAD153
	NTO=NTO+N2	SREAD154
100	NFRM=NFRM+NMX	SREAD155
	END	SREAD156

	FUNCTION READW(XX)	READW 2
C	READS W ARRAY MAKING ANY NECESSARY CONVERSION OF UNITS.	READW 3
C	VARIABLE LENGTH 'TABULAR' DATA IS READ BY SUBROUTINE 'READW1'	READW 4
C	WHICH IS CALLED FOR NEGATIVE W-ARRAY INDICES.	READW 5
C		READW 6
C	COMMON DECK "CONST" INSERTED HERE	CCONST 2
	COMMON/PCONST/CREG,RGAS,GAMMA	CCONST 4
	COMMON/MCONST/PI,PIT2,PID2,DEGS,RAD,ALN10	CCONST 5
C	COMMON DECK "WWR" INSERTED HERE	CWWR 2
	PARAMETER (NWARSZ=1000)	CWW1 3
	COMMON/WW/ID(10),MAXW,W(NWARSZ)	CWW1 4
	REAL MAXSTP,MAXERR,INTYP,LLAT,LLON	CWW2 2
	EQUIVALENCE (EARTH, W(1)), (RAY, W(2)), (XMTRH, W(3)), (TLAT, W(4)),	CWW2 3
1	(TLON, W(5)), (OW, W(6)), (FBEG, W(7)), (FEND, W(8)), (FSTEP, W(9)),	CWW2 4
2	(AZ1, W(10)), (AZBEG, W(11)), (AZEND, W(12)), (AZSTEP, W(13)),	CWW2 5
3	(BETA, W(14)), (ELBEG, W(15)), (ELEND, W(16)), (ELSTEP, W(17)),	CWW2 6
8	(RCVRH, W(20)),	CWW2 7
4	(ONLY, W(21)), (HOP, W(22)), (MAXSTP, W(23)), (PLAT, W(24)), (PLON, W(25))	CWW2 8
5,	(HMAX, W(26)), (RAYFNC, W(29)), (EXTINC, W(33)),	CWW2 9
6	(HMIN, W(27)), (RGMX, W(28)),	CWW2 10
8	(INTYP, W(41)), (MAXERR, W(42)), (ERATIO, W(43)),	CWW2 11
6	(STEP1, W(44)), (STPMAX, W(45)), (STPMIN, W(46)), (FACTR, W(47)),	CWW2 12
7	(SKIP, W(71)), (RAYSET, W(72)), (PRTSRP, W(74)), (HITLET, W(75))	CWW2 13
9	, (BINRAY, W(76)), (PAGLN, W(77)), (PLT, W(81)), (PFACTR, W(82)),	CWW2 14
1	(LLAT, W(83)), (LLON, W(84)), (RLAT, W(85)), (RLON, W(86))	CWW2 15
2,	(TIC, W(87)), (HB, W(88)), (HT, W(89)), (TICV, W(96))	CWW2 16
C	COMMON DECK "B1" INSERTED HERE	CB1 2
	INTEGER UMX, UNTBL, UITBL, UFRMTBL, IDSU(10)	CB1 4
	COMMON/B1/UMX, UNTBL(10), UITBL(10), UFRMTBL(10), UGP(10)	CB1 5
	EQUIVALENCE (UGP, IDSU)	CB1 6
C	COMMON DECK "B2" INSERTED HERE	CB2 2
	INTEGER DUMX, DUNTBL, DUITBL, DUFRMTB, IDSDU(10)	CB2 4
	COMMON/B2/DUMX, DUNTBL(10), DUITBL(10), DUFRMTB(10), DUGP(10)	CB2 5
	EQUIVALENCE (DUGP, IDSDU)	CB2 6
C	COMMON DECK "B3" INSERTED HERE	CB3 2
	INTEGER CMX, CNTBL, CITBL, CFRMTBL, IDSC(10)	CB3 4
	COMMON/B3/CMX, CNTBL(10), CITBL(10), CFRMTBL(10), CGP(512)	CB3 5
	EQUIVALENCE (CGP, IDSC), (ANC, CGP(11))	CB3 6
C	COMMON DECK "B4" INSERTED HERE	CB4 2
	INTEGER DCMX, DCNTBL, DCITBL, DCFRMTB, IDSDC(10)	CB4 4
	COMMON/B4/DCMX, DCNTBL(10), DCITBL(10), DCFRMTB(10), DCGP(10)	CB4 5
	EQUIVALENCE (DCGP, IDSDC)	CB4 6

C	COMMON DECK "B5" INSERTED HERE	CB5	2
	INTEGER TMX,TNTBL,TITBL,TFRMTBL,IDST(10)	CB5	4
	COMMON/B5/TMX,TNTBL(10),TITBL(10),TFRMTBL(10),TGP(262)	CB5	5
	EQUIVALENCE (TGP,IDST),(ANT,TGP(11))	CB5	6
C	COMMON DECK "B6" INSERTED HERE	CB6	2
	INTEGER DTMX,DTNTBL,DTITBL,DTFRMTB,IDSDT(10)	CB6	4
	COMMON/B6/DTMX,DTNTBL(10),DTITBL(10),DTFRMTB(10),DTGP(10)	CB6	5
	EQUIVALENCE (DTGP,IDSDT)	CB6	6
C	COMMON DECK "B7" INSERTED HERE	CB7	2
	INTEGER MMX,MNTBL,MITBL,MFRMTBL,IDSM(10)	CB7	4
	REAL MGP	CB7	5
	COMMON/B7/MMX,MNTBL(10),MITBL(10),MFRMTBL(10),MGP(10)	CB7	6
	EQUIVALENCE (MGP,IDSM)	CB7	7
C	COMMON DECK "B9" INSERTED HERE	CB8	2
	INTEGER GMX,GNTBL,GITBL,GFRMTBL,IDSG(10)	CB8	4
	COMMON/B9/GMX,GNTBL(10),GITBL(10),GFRMTBL(10),GGP(113)	CB8	5
	EQUIVALENCE (GGP,IDSG),(ANG,GGP(11))	CB8	6
C		READW	17
C	COMMON DECK "B10" INSERTED HERE	CB9	2
	INTEGER DGMX,DGNTBL,DGITBL,DGFRMTB,IDS DG(10)	CB9	4
	COMMON/B10/DGMX,DGNTBL(10),DGITBL(10),DGFRMTB(10),DGGP(10)	CB9	5
	EQUIVALENCE (DGGP,IDS DG)	CB9	6
C		READW	19
C	COMMON DECK "B8" INSERTED HERE	CB10	2
	INTEGER RMX,RNTBL,RITBL,RFRMTBL,IDSR(10)	CB10	4
	COMMON/B8/RMX,RNTBL(10),RITBL(10),RFRMTBL(10),RGP(10)	CB10	5
	EQUIVALENCE (RGP,IDSR)	CB10	6
C		READW	21
C	COMMON DECK "CB17" INSERTED HERE	CB17	2
	INTEGER VMX,VNTBL,VITBL,VFRMTBL,IDSV(10)	CB17	4
	COMMON/B17/VMX,VNTBL(10),VITBL(10),VFRMTBL(10),VGP(53)	CB17	5
	EQUIVALENCE (VGP,IDS V),(ANV,VGP(11))	CB17	6
C	COMMON DECK "CB18" INSERTED HERE	CB18	2
	INTEGER DVMX,DVNTBL,DVITBL,DVFRMTB,IDS DV(10)	CB18	4
	COMMON/B18/DVMX,DVNTBL(10),DVITBL(10),DVFRMTB(10),DVGP(11)	CB18	5
	EQUIVALENCE (DVGP,IDS DV),(ANDV,DVGP(11))	CB18	6
C	COMMON DECK "CB19" INSERTED HERE	CB19	2
	INTEGER PRMX,PRNTBL,PRITBL,PRFRMTB,IDS PR(10)	CB19	4
	COMMON/B19/PRMX,PRNTBL(10),PRITBL(10),PRFRMTB(10),PRGP(11)	CB19	5
	EQUIVALENCE (PRGP,IDS PR),(ANP,PRGP(11))	CB19	6
C	COMMON DECK "CB20" INSERTED HERE	CB20	2
	INTEGER DPMX,DPNTBL,DPITBL,DPFRMTB,IDS DP(10)	CB20	4
	COMMON/B20/DPMX,DPNTBL(10),DPITBL(10),DPFRMTB(10),DPGP(11)	CB20	5
	EQUIVALENCE (DPGP,IDS DP),(ANDP,DPGP(11))	CB20	6
C		READW	26
	PARAMETER (MXCMTS=83,BIGVAL=1.E30)	READW	27
	CHARACTER*38 WFRMT,WNOTES(2)	READW	28
	CHARACTER*80 LINEX,NUMSTG	READW	29
	CHARACTER*100 STMP1,STMP2	READW	30
	INTEGER STRIM,WCOMTS(MXCMTS)	READW	31
	CHARACTER*1 DEG,KM,NM,FEET,CYCLE,PER,MSKMS	READW	32
C	COMMON DECK "RAYDEV" INSERTED HERE	CRAYDEV2	
C	DEVICE ASSIGNED TO RAYTRC INPUT FILE	CRAYDEV4	
	COMMON/RAYDEV/NRYIND,NDEVTMP,NFRMAT,NDEVGRP,NDEVBIN	CRAYDEV5	
	LOGICAL NWOK,AB,UCON	READW	34

C		READW 35
C	COMMON DECK "FLAG" INSERTED HERE	CFLAG 2
	LOGICAL NEWWR,NEWWP,NEWTRC,PENET	CFLAG 4
	COMMON /FLG/ NTYP,NEWWR,NEWWP,NEWTRC,PENET,LINES,IHOP,HPUNCH	CFLAG 5
	COMMON/FLGP/NSET	CFLAG 6
C	CHARACTER PC*1	READW 37
C		READW 38
	INTEGER XMX,XNTBL(10),XITBL(10),XFRMTBL(10)	READW 39
	REAL XGP(11)	READW 40
C		READW 41
	DATA XMX/2/	READW 42
	DATA XNTBL/1,11,12,7*0/	READW 43
	DATA XITBL/1,9*0/	READW 44
	DATA XFRMTBL/1,2,8*0/	READW 45
C		READW 46
	DATA WCOMTS,WNOTES/MXCMTS*1, ' ',' INPUT OVERRIDDEN'/	READW 47
C		READW 48
	AB=.FALSE.	READW 49
	READW=0.0	READW 50
C		READW 51
	IF(NDEVTMP.GT.0) REWIND NDEVTMP	READW 52
C		READW 53
	READ(NRYIND,1000,END=3) ID	READW 54
1000	FORMAT (BZ,10A8)	READW 55
	IF(NDEVTMP.GT.0) WRITE(NDEVTMP,1000) ID	READW 56
	GO TO 4	READW 57
C		READW 58
3	READW=1.0	READW 59
	IF(NFRMAT.LT.0) RETURN	READW 60
C		READW 61
	PRINT 1040	READW 62
	WRITE(3,1040)	READW 63
1040	FORMAT(' END OF INPUT DATA')	READW 64
	CALL ENDPLT	READW 65
33	IF(PLT.NE.0.0) CALL DDEND	READW 66
	STOP	READW 67
C		READW 68
4	READ(NRYIND,'(A)',END=10001) STMP1	READW 69
C		READW 70
	READ(STMP1,1100) NW,WWW,LINEX	READW 71
1100	FORMAT (BZ,I3,E14.7,A)	READW 72
	IF(NDEVTMP.GT.0.AND.(NFRMAT.NE.-2.OR.NW.LT.0))	READW 73
1	WRITE(NDEVTMP,'(A)') STMP1	READW 74
10001	IF (NW.EQ.0) GO TO 10	READW 75
	IF(NW.GT.MAXW) GO TO 3400	READW 76
C		READW 77
	IF (NW.LE.MAXW .AND. NW.GT.0) GO TO 5	READW 78
C	TABULAR INPUT DATA	READW 79
	NWOK=.FALSE.	READW 80
C	'OPEN' THE TEMP FILE	READW 81
1150	FORMAT(I3,T18,A)	READW 82
	NWP=-NW	READW 83
	IF(NFRMAT.EQ.-2) THEN	READW 84
C	USE DUMMY ARRAYS TO ABSORB TABULAR DATA	READW 85
		READW 86

	CALL READW1(AB,NWOK,NW,XXM,XNTBL,XITBL,XFRMTBL,XGP)	READW 87
	ELSEIF(NWP.EQ.1) THEN	READW 88
	CALL READW1(AB,NWOK,NW,UMX,UNTBL,UITBL,UFRMTBL,UGP)	READW 89
	ELSEIF(NWP.EQ.2) THEN	READW 90
	CALL READW1(AB,NWOK,NW,DUMX,DUNTBL,DUITBL,DUFRMTB,DUGP)	READW 91
	ELSEIF(NWP.EQ.3) THEN	READW 92
	CALL READW1(AB,NWOK,NW,CMX,CNTBL,CITBL,CFRMTBL,CGP)	READW 93
	ELSEIF(NWP.EQ.4) THEN	READW 94
	CALL READW1(AB,NWOK,NW,DCMX,DCNTBL,DCITBL,DCFRMTB,DCGP)	READW 95
	ELSEIF(NWP.EQ.5) THEN	READW 96
	CALL READW1(AB,NWOK,NW,TMX,TNTBL,TITBL,TFRMTBL,TGP)	READW 97
	ELSEIF(NWP.EQ.6) THEN	READW 98
	CALL READW1(AB,NWOK,NW,DTMX,DTNTBL,DTITBL,DTFRMTB,DTGP)	READW 99
	ELSEIF(NWP.EQ.7) THEN	READW100
	CALL READW1(AB,NWOK,NW,MMX,MNTBL,MITBL,MFRMTBL,MGP)	READW101
	ELSEIF(NWP.EQ.8) THEN	READW102
	CALL READW1(AB,NWOK,NW,RMX,RNTBL,RITBL,RFRMTBL,RGP)	READW103
	ELSEIF(NWP.EQ.9) THEN	READW104
	CALL READW1(AB,NWOK,NW,GMX,GNTBL,GITBL,GFRMTBL,GGP)	READW105
	ELSEIF(NWP.EQ.10) THEN	READW106
	CALL READW1(AB,NWOK,NW,DGMX,DGNTBL,DGITBL,DGFRMTB,DGGP)	READW107
	ELSEIF(NWP.EQ.17) THEN	READW108
	CALL READW1(AB,NWOK,NW,VMX,VNTBL,VITBL,VFRMTBL,VGP)	READW109
	ELSEIF(NWP.EQ.18) THEN	READW110
	CALL READW1(AB,NWOK,NW,DVMX,DVNTBL,DVITBL,DVFRMTB,DVGP)	READW111
	ELSEIF(NWP.EQ.19) THEN	READW112
	CALL READW1(AB,NWOK,NW,PRMX,PRNTBL,PRITBL,PRFRMTB,PRGP)	READW113
	ELSEIF(NWP.EQ.20) THEN	READW114
	CALL READW1(AB,NWOK,NW,DPMX,DPNTBL,DPITBL,DPFRMTB,DPGP)	READW115
	ELSE	READW116
	CALL SREAD1(AB,NWOK,NW)	READW117
	ENDIF	READW118
	IF(NWOK) GO TO 4	READW119
C		READW120
3400	WRITE(3,4000) NW,MAXW	READW121
4000	FORMAT(15H1THE SUBSCRIPT ,I3, ' ON THE W-ARRAY INPUT IS OUT OF BOREADW122	
	1UNDS. ALLOWABLE VALUES ARE -8 THROUGH, ',I4, ' )	READW123
	CALL EXIT	READW124
C		READW125
5	READ(LINEX,70) DEG,KM,NM,FEET,CYCLE,PER,MSKMS	READW126
70	FORMAT(7A)	READW127
	W(NW)=WWW	READW128
C		READW129
C	CHECK FOR A 'TERRAIN RELATIVE' HEIGHT SPECIFICATION.	READW130
C	IF SO ADD FLAG VALUE 10**40 TO BE TESTED FOR LATER IN 'RAYTRC'	READW131
C		READW132
	IF(MSKMS.EQ.'T' .AND. WWW.EQ.0.0) W(NW)=1.E-40	READW133
	IF(WWW.EQ.0.0) GO TO 4	READW134
	IF(MSKMS.EQ.'T') WWW=WWW*1.E40	READW135
C		READW136
C	CHECK FOR KEYWORD UNITS SPECIFICATION, IF SO PERFORM CONVERSION	READW137
C		READW138
	IF(.NOT.UCON(KU,LINEX(:10),CONV)) GO TO 60	READW139
75	W(NW)=WWW*CONV	READW140
	GO TO 4	READW141

C			
60	IF (DEG.EQ.'1')	WWW=WWW*RAD	READW142
	IF (KM.EQ.'1')	WWW=WWW/EARTH	READW143
	IF (NM.EQ.'1')	WWW=WWW*1.852	READW144
	IF (FEET.EQ.'1')	WWW=WWW*3.048006096E-4	READW145
	IF (CYCLE.EQ.'1')	WWW=WWW*PIT2	READW146
	IF (PER.EQ.'1')	WWW=PIT2/WWW	READW147
	IF (MSKMS.EQ.'1')	WWW=WWW*1.E-3	READW148
	W(NW)=WWW		READW149
	GO TO 4		READW150
C			READW151
10	IF (.NOT.AB)	RETURN	READW152
	PRINT	1200	READW153
1200	FORMAT(' A DATA FORMATTING ERROR PREVENTS CONTINUED EXECUTION')		READW154
	CALL	EXIT	READW155
C			READW156
	ENTRY	SETW(XX)	READW157
C			READW158
	THIS ENTRY IS CALLED ONCE BEFORE THE FIRST RUN SET IS READ		READW159
C			READW160
	INITIALIZE SOME MATHEMATICAL CONSTANTS		READW161
	PI=4.0*ATAN(1.0)		READW162
	PIT2=2.*PI		READW163
	PID2=PI/2.		READW164
	DEGS=180./PI		READW165
	RAD=PI/180.		READW166
	ALN10=ALOG(10.)		READW167
CC*****	INITIALIZE SOME VARIABLES IN THE W ARRAY		READW168
	MAXW=NWARSZ		READW169
	CALL CLEAR(W,MAXW)		READW170
	PLON=0.		READW171
	PLAT=PID2		READW172
	EARTH=6370.		READW173
	INTYP=3.		READW174
	MAXERR=1.E-4		READW175
	ERATIO=50.		READW176
	STEP1=1.		READW177
	STPMAX=100.		READW178
	STPMIN=1.E-8		READW179
	FACTR=0.5		READW180
	HITLET=.15		READW181
	MAXSTP=1000.0		READW182
	HOP=1.		READW183
	HMAX=500.0		READW184
	EXTINC=999.999		READW185
	PAGLN=66.0		READW186
C			READW187
	CALL	SETUCON	READW188
C			READW189
	RETURN		READW190
C			READW191
	ENTRY	SETOVR(XX)	READW192
C			READW193
	THIS ENTRY IS CALLED AFTER EACH RUN SET IS READ		READW194
C			READW195
	PERFORM OVERRIDE ASSIGNMENTS TO W-ELEMENTS		READW196
C	CALL	OVERRD(MAXSTP,0.0,1000.0,WCOMTS(23),2,1)	

CALL OVERRD(ERATIO,0.0,50.0,WCOMTS(43),2,1)	READW197
CALL OVERRD(FACTR,0.0,0.5,WCOMTS(47),2,1)	READW198
CALL OVERRD(SKIP,0.0,BIGVAL,WCOMTS(71),2,1)	READW199
CALL OVERRD(HITLET,0.0,.15,WCOMTS(75),2,1)	READW200
IF(PAGLN.LT.30.0) PAGLN=0.0	READW201
CALL OVERRD(PAGLN,0.0,66.0,WCOMTS(77),2,1)	READW202
CALL OVERRD(PFACTR,0.0,1.0,WCOMTS(82),2,1)	READW203
RETURN	READW204
C	READW205
ENTRY PRINTW(XX)	READW206
C THIS ENTRY IS CALLED AFTER EACH RUN SET IS READ	READW207
C TO PRINT VALUES OF THE W-ARRAY IN A FORMAT WHICH SHOWS	READW208
C FULL ACCURACY AND THE EFFECTS OF ANY CONVERSIONS OR OVERRIDES.	READW209
C	READW210
C GO TO NEXT PAGE, PUT OUT COPY OF INPUT DATA FOR THIS RUN SET	READW211
C ASSUMING WE HAD A TEMPORARY FILE TO USE	READW212
C	READW213
IF(NDEVTMP.LE.0) GO TO 1065	READW214
CALL NEWPAG(NPAG,INT(PAGLN),PC)	READW215
LNSXPG=LINES+INT(PAGLN)	READW216
CALL PUTHDR(3,PC,NPAG)	READW217
CALL PUTDVR(3)	READW218
CALL PUTKKB(3,1)	READW219
CALL PUTKCT(3,'INPUT DATA FILE FOR RUN SET NUMBER'	READW220
1 //NUMSTG(NSET,1,'(I5)'))	READW221
CALL PUTKKB(3,1)	READW222
CALL PUTDVR(3)	READW223
CALL PUTKKB(3,1)	READW224
REWIND NDEVTMP	READW225
C	READW226
1060 READ(NDEVTMP,'(A)',END=1065) LINEX	READW227
IF(LINES.GE.LNSXPG) THEN	READW228
CALL NEWPAG(NPAG,INT(PAGLN),PC)	READW229
LNSXPG=LINES+INT(PAGLN)	READW230
CALL PUTHDR(3,PC,NPAG)	READW231
CALL PUTKKB(3,1)	READW232
ENDIF	READW233
CALL PUTKST(3,' //LINEX)	READW234
GO TO 1060	READW235
1065 CONTINUE	READW236
C	READW237
C GO TO NEXT PAGE, PUT OUT W-ELEMENTS SHOWING FULL PRECISION	READW238
C USE A TWO COLUMN FORMAT	READW239
C	READW240
CALL NEWPAG(NPAG,INT(PAGLN),PC)	READW241
CALL PUTHDR(3,PC,NPAG)	READW242
CALL PUTDVR(3)	READW243
CALL PUTKKB(3,1)	READW244
CALL PUTKCT(3,'INITIAL VALUES FOR THE W ARRAY')	READW245
CALL PUTKCT(3,'ONLY NONZERO VALUES PRINTED'	READW246
1 //' -- ALL ANGLES IN RADIANS')	READW247
CALL PUTKKB(3,1)	READW248
CALL PUTDVR(3)	READW249
LINSPP=INT(PAGLN)-7	READW250
C	READW251

	WFRMT='(BZ,I3,E14.7,A)'	
	IF(NFRMAT.EQ.0) WFRMT='(I4,E24.15,A)'	READW252
C		READW253
	NWE=0	READW254
C	ALLOW MAXIMUM OF 10 PAGES OF OUTPUT(1 IS ENOUGH)	READW255
	DO 18 NPGS=1,10	READW256
C	ALLOW 3 LINES FOR INSIDE HEADER(SEE BELOW)	READW257
	LINSPP=LINSPP-3	READW258
C	NEXT ELEMENT TO SCAN IS ONE MORE THAN LAST ONE	READW259
	LWE=NWE+1	READW260
C		READW261
C	INITIALIZE SECOND COLUMN START INDEX	READW262
	NXCL=0	READW263
C	INITIALIZE TOTAL ELEMENT COUNTER	READW264
	NELS=0	READW265
C	LOOP TO FIND BREAK POINTS FOR FIRST/SECOND COLUMNS	READW266
	DO 14 I=LWE,MAXW	READW267
	IF(W(I).EQ.0.0) GO TO 14	READW268
	NWE=I	READW269
	NELS=NELS+1	READW270
	IF(NELS.EQ.LINSPP) NXCL=I	READW271
	IF(NELS.EQ.2*LINSPP) GO TO 15	READW272
14	CONTINUE	READW273
15	IF(NELS.EQ.0) GO TO 22	READW274
C		READW275
	IF(NPGS.GT.1) THEN	READW276
	CALL NEWPAG(NPAG,INT(PAGLN),PC)	READW277
	CALL PUTHDR(3,PC,NPAG)	READW278
	LINSPP=INT(PAGLN)-1	READW279
	ENDIF	READW280
C		READW281
C	INSERT 'INNER' HEADER	READW282
	CALL PUTKBK(3,2)	READW283
	STMP1=' N W(N)'	READW284
	CALL PUTKST(3,STMP1(:65)//' '//STMP1)	READW285
C		READW286
	NX=NXCL-1	READW287
	IF(NX.LT.LWE) NX=NWE	READW288
	DO 17 NW=LWE,NX	READW289
	NCOMT=MINO(NW,MXCMTS)	READW290
	IF(W(NW).NE.0) THEN	READW291
	WRITE(STMP1,WFRMT) NW,W(NW),WNOTES(WCOMTS(NCOMT))	READW292
	STMP2=' '	READW293
	IF(NXCL.EQ.0) GO TO 23	READW294
	DO 19 I=NXCL,MAXW	READW295
	IF(W(I).NE.0) THEN	READW296
	NCOMT=MINO(I,MXCMTS)	READW297
	WRITE(STMP2,WFRMT) I,W(I),WNOTES(WCOMTS(NCOMT))	READW298
	NXCL=I+1	READW299
	GO TO 23	READW300
	ENDIF	READW301
19	CONTINUE	READW302
23	CALL PUTKST(3,STMP1(:65)//' '//STMP2)	READW303
	ENDIF	READW304
17	CONTINUE	READW305
		READW306

	IF(NELS.EQ.0) GO TO 22	READW307
18	CONTINUE	READW308
C		READW309
22	CONTINUE	READW310
	END	READW311

	SUBROUTINE CLEAR(A,N)	CLEAR 2
C	SET N ELEMENTS OF ARRAY A TO ZERO	CLEAR 3
	REAL A(N)	CLEAR 4
	IF(N.LE.0) RETURN	CLEAR 5
	DO 10 I=1,N	CLEAR 6
10	A(I)=0.0	CLEAR 7
	RETURN	CLEAR 8
	END	CLEAR 9

	FUNCTION ND2B(INDEC)	ND2B 2
C		ND2B 3
C	CONVERT A NUMERIC DECIMAL DIGIT STRING TO A BIT STRING	ND2B 4
C	WITH EACH BIT SET BY A CORRESPONDING DECIMAL DIGIT.	ND2B 5
C		ND2B 6
	ND2B=0	ND2B 7
	IF(INDEC.LE.0) RETURN	ND2B 8
	M=INDEC	ND2B 9
	MB=1	ND2B 10
C		ND2B 11
10	IF(MOD(M,10).NE.0) ND2B=ND2B+MB	ND2B 12
	MB=MB*2	ND2B 13
	M=M/10	ND2B 14
	IF(M.GT.0) GO TO 10	ND2B 15
	END	ND2B 16

	LOGICAL FUNCTION UCON(JC1,U,CONV)	UCON 2
	LOGICAL SETUCON	UCON 3
C	PROVIDES KEYWORD UNITS CONVERSION FOR W-ARRAY INPUT.	UCON 4
C	UNITS SPECIFICATION MUST BE IN THE FORM 'DV UN' WHERE DV IS THE	UCON 5
C	TYPE OF VARIABLE(SUCH AS AN FOR ANGLE) AND UN IS THE UNITS CHOICE	UCON 6
C	SUCH AS RD FOR RADIANS). RETURN VALUE IS THE CONVERSION FACTOR.	UCON 7
C	COMMON DECK "UCON" INSERTED HERE	CUCON 2
	COMMON/UCONV/CNVV(4,4)	CUCON 4
	CHARACTER PCV*3,CNVC*2	CUCON 5
	COMMON/UCONC/PCV(4),CNVC(4,4)	CUCON 6
C	COMMON DECK "CONST" INSERTED HERE	CCONST 2
	COMMON/PCONST/CREF,RGAS,GAMMA	CCONST 4

C	COMMON/MCONST/PI,PIT2,PID2,DEGS,RAD,ALN10	CCONST	5
	COMMON DECK "WWR" INSERTED HERE	CWWR	2
	PARAMETER (NWARSZ=1000)	CWW1	3
	COMMON/WW/ID(10),MAXW,W(NWARSZ)	CWW1	4
	REAL MAXSTP,MAXERR,INTYP,LLAT,LLON	CWW2	2
	EQUIVALENCE (EARTH, W(1)), (RAY, W(2)), (XMTRH, W(3)), (TLAT, W(4)),	CWW2	3
	1 (TLON, W(5)), (OW, W(6)), (FBEG, W(7)), (FEND, W(8)), (FSTEP, W(9)),	CWW2	4
	2 (AZ1, W(10)), (AZBEG, W(11)), (AZEND, W(12)), (AZSTEP, W(13)),	CWW2	5
	3 (BETA, W(14)), (ELBEG, W(15)), (ELEND, W(16)), (ELSTEP, W(17)),	CWW2	6
	8 (RCVRH, W(20)),	CWW2	7
	4 (ONLY, W(21)), (HOP, W(22)), (MAXSTP, W(23)), (PLAT, W(24)), (PLON, W(25))	CWW2	8
	5, (HMAX, W(26)), (RAYFNC, W(29)), (EXTINC, W(33)),	CWW2	9
	6 (HMIN, W(27)), (RGMAX, W(28)),	CWW2	10
	8 (INTYP, W(41)), (MAXERR, W(42)), (ERATIO, W(43)),	CWW2	11
	6 (STEP1, W(44)), (STPMAX, W(45)), (STPMIN, W(46)), (FACTR, W(47)),	CWW2	12
	7 (SKIP, W(71)), (RAYSET, W(72)), (PRTSRP, W(74)), (HITLET, W(75))	CWW2	13
	9, (BINRAY, W(76)), (PAGLN, W(77)), (PLT, W(81)), (PFACTR, W(82)),	CWW2	14
	1 (LLAT, W(83)), (LLON, W(84)), (RLAT, W(85)), (RLON, W(86))	CWW2	15
	2, (TIC, W(87)), (HB, W(88)), (HT, W(89)), (TICV, W(96))	CWW2	16
	CHARACTER U*(*), PU*3, PV*2	UCON	11
C	DATA NPV,NPU/3,4/	UCON	12
	UCON=.FALSE.	UCON	13
	CONV=1.0	UCON	14
C	READ(U,100) PU,PV	UCON	15
100	FORMAT(A,A)	UCON	16
C	DO 2010 J=1,NPV	UCON	17
2010	IF(PU.EQ.PCV(J)) GO TO 2015	UCON	18
	JC1=4	UCON	19
	RETURN	UCON	20
2015	JC1=J	UCON	21
	DO 2020 K=1,NPU	UCON	22
2020	IF(PV.EQ.CNVC(J,K)) GO TO 2025	UCON	23
	JC1=4	UCON	24
	RETURN	UCON	25
2025	UCON=.TRUE.	UCON	26
	CONV=CNVV(JC1,K)	UCON	27
	RETURN	UCON	28
C	INITIAL CONVERSION CONSTANTS	UCON	29
C	ENTRY SETUCON(JC1,U,CONV)	UCON	30
	SETUCON=.TRUE.	UCON	31
C	CNVV(1,2) = RAD	UCON	32
	CNVV(1,3) = 1.0/EARTH	UCON	33
	CNVV(2,2) = 1.0E-3	UCON	34
	CNVV(2,3) = 3.048006096E-4	UCON	35
	CNVV(2,4) = 1.852	UCON	36
	CNVV(3,2) = PIT2	UCON	37
	CNVV(3,3) = PIT2*1.0E3	UCON	38
	CNVV(3,4) = PIT2*RAD	UCON	39
	END	UCON	40
		UCON	41
		UCON	42
		UCON	43
		UCON	44
		UCON	45

	SUBROUTINE TRACE		TRACE 3
C		VERSION 3/4/86	TRACE 4
C	CALCULATES ONE RAYPATH FOR THE REQUESTED NUMBER OF HOPS		TRACE 5
C	(CROSSINGS OR CLOSEST APPROACH TO RECEIVER SURFACE; A CLOSEST		TRACE 6
C	APPROACH COUNTS AS TWO HOPS).		TRACE 7
C	THIS VERSION IS LIMITED TO USE WITH ATMOSPHERIC MODELS		TRACE 8
	REAL NORYST		TRACE 9
	PARAMETER (NORYST=0.0,MXPRGS=200)		TRACE 10
C			TRACE 11
C	COMMON /RK/ N,STEP,MODE,E1MAX,E1MIN,E2MAX,E2MIN,FACT,RSTART		TRACE 12
C	COMMON DECK "FLAG" INSERTED HERE		TRACE 13
	LOGICAL NEWWR,NEWWP,NEWTRC,PENET		TRACE 14
C	COMMON /FLG/ NTYP,NEWWR,NEWWP,NEWTRC,PENET,LINES,IHOP,HPUNCH		TRACE 15
C	COMMON DECK "TRAC" INSERTED HERE		CTRAC 2
	LOGICAL GROUND,SURF,PERIGE,THERE,MINDIS,NEWRAY		CTRAC 4
	COMMON /TRAC/ GROUND,SURF,PERIGE,THERE,MINDIS,NEWRAY,SMT,OSMT		CTRAC 5
	COMMON/TRAC/ROLD(20),DROLD(20),TOLD,ZDOT,D2Z,RAD,RAD1		CTRAC 6
C	COMMON DECK "RR" INSERTED HERE		TRACE 17
	REAL MODREC		TRACE 18
	COMMON/RR/ MODREC(4)		TRACE 19
	COMMON/RR/F,PFR,PFRP,PFRTH,PFRPH		TRACE 20
	COMMON/RR/PFTH,PFPH,PFTHTH,PFPHPH,PFTHPH,FSELECT,FTIME		TRACE 21
C	COMMON DECK "GG" INSERTED HERE		TRACE 22
	REAL MODG		TRACE 23
	COMMON/GG/MODG(4)		TRACE 24
	COMMON/GG/G,PGR,PGRP,PGRTH,PGRPH		TRACE 25
	COMMON/GG/PGTH,PGPH,PGTHTH,PGPHPH,PGTHPH,GSELECT,GTIME		TRACE 26
C	COMMON DECK "RKTIME" INSERTED HERE		TRACE 27
	COMMON/CRKTIME/RKTIME		TRACE 28
C	COMMON DECK "RINPLEX" INSERTED HERE		TRACE 29
	REAL KAY2,KAY2I		TRACE 30
	COMPLEX PNP,POLAR,LPOLAR		TRACE 31
	LOGICAL SPACE		TRACE 32
	COMMON /RIN/ MODRIN(8),RAYNAME(2,3),TYPE(3),SPACE		TRACE 33
	COMMON/RIN/OMEGMIN,OMEGMAX,KAY2,KAY2I		TRACE 34
	COMMON/RIN/PNP(10),POLAR,LPOLAR,SGN		TRACE 35
	COMMON R(20),T,STP,DRDT(20)		TRACE 36
C	COMMON DECK "WWR" INSERTED HERE		TRACE 37
	PARAMETER (NWARSZ=1000)		TRACE 38
	COMMON/WW/ID(10),MAXW,W(NWARSZ)		TRACE 39
	REAL MAXSTP,MAXERR,INTYP,LLAT,LLON		TRACE 40
	EQUIVALENCE (EARTH,W(1)),(RAY,W(2)),(XMTRH,W(3)),(TLAT,W(4)),		TRACE 41
1	(TLON,W(5)),(OW,W(6)),(FBEG,W(7)),(FEND,W(8)),(FSTEP,W(9)),		TRACE 42
2	(AZ1,W(10)),(AZBEG,W(11)),(AZEND,W(12)),(AZSTEP,W(13)),		TRACE 43
3	(BETA,W(14)),(ELBEG,W(15)),(ELEND,W(16)),(ELSTEP,W(17)),		TRACE 44
8	(RCVRH,W(20)),		TRACE 45
4	(ONLY,W(21)),(HOP,W(22)),(MAXSTP,W(23)),(PLAT,W(24)),(PLON,W(25))		TRACE 46
5,	(HMAX,W(26)),(RAYFNC,W(29)),(EXTINC,W(33)),		TRACE 47
6	(HMIN,W(27)),(RGMAX,W(28)),		TRACE 48
8	(INTYP,W(41)),(MAXERR,W(42)),(ERATIO,W(43)),		TRACE 49
6	(STEP1,W(44)),(STPMAX,W(45)),(STPMIN,W(46)),(FACTR,W(47)),		TRACE 50

	7 (SKIP,W(71)), (RAYSET,W(72)), (PRTSRP,W(74)), (HITLET,W(75))	TRACE 51
	9 , (BINRAY,W(76)), (PAGLN,W(77)), (PLT,W(81)), (PFACTR,W(82)),	TRACE 52
	1 (LLAT,W(83)), (LLON,W(84)), (RLAT,W(85)), (RLON,W(86))	TRACE 53
	2, (TIC,W(87)), (HB,W(88)), (HT,W(89)), (TICV,W(96))	TRACE 54
C	THE FOLLOWING IS A LOCAL COMMON ONLY	TRACE 55
C	COMMON DECK "TRLOCAL" INSERTED HERE	TRACE 56
	COMMON/TRLOCAL/RSIGN,HOME,FDOT,GDOT,GOLD,GDOLD	TRACE 57
	LOGICAL PCROSS,HOME,WASNT	TRACE 58
	LOGICAL LAUNCH,APOGEE,PLTENB,EXTON	TRACE 59
	EQUIVALENCE (R(2),TH),(R(3),PHI)	TRACE 60
C		TRACE 61
	CHARACTER*10 XCOND,DEFCND	TRACE 62
	PARAMETER (DEFCND=' MAX HOPS')	TRACE 63
C		TRACE 64
	REAL PRGHST(3,MXPRGS)	TRACE 65
	EQUIVALENCE(RKTIME,IRKTIME), (APOG,PRIGEE,W(80))	TRACE 66
	DATA GROUND/.FALSE./	TRACE 67
C		TRACE 68
C	INCREMENT EVENT COUNT	TRACE 69
	IRKTIME=IRKTIME+1	TRACE 70
	PLTENB=APOG.EQ.0.0	TRACE 71
C	ENABLE EXTINCTION TEST IF LIMIT IS SET AND VARIABLE IS BEING INTE	TRACE 72
	EXTON=(EXTINC.GT.0.0) .AND. (W(58).NE.0.0)	TRACE 73
C	POINT INDEX TO ABSORTION VARIABLE	TRACE 74
	NR=7	TRACE 75
	IF(W(57).NE.0.0) NR=8	TRACE 76
	RMAX=HMAX+EARTHTR	TRACE 77
	RMIN=HMIN+EARTHTR	TRACE 78
	NHOP=HOP	TRACE 79
	MAX=MAXSTP	TRACE 80
	NSKIP=SKIP	TRACE 81
C*****	INITIALIZE PARAMETERS FOR INTEGRATION SUBROUTINE RKAM	TRACE 82
	MODE=INTYP	TRACE 83
	STEP=STEP1	TRACE 84
	E1MAX=MAXERR	TRACE 85
	E1MIN=MAXERR/ERATIO	TRACE 86
	E2MAX=STPMAX	TRACE 87
	E2MIN=STPMIN	TRACE 88
	FACT=FACTR	TRACE 89
	RSTART=1.	TRACE 90
	CALL HAMLTN	TRACE 91
	FDOT=DOT(F)	TRACE 92
C		TRACE 93
C	CHECK FOR EQUALITY WITH RECEIVER HEIGHT WITHIN MACHINE PRECISION	TRACE 94
	THERE=F.EQ.0.0	TRACE 95
C		TRACE 96
	HOME=FDOT*F.GE.0.	TRACE 97
C*****	IHOP=0 TELLS PRINTR TO PRINT HEADING AND PUNCH A TRANSMITTER	TRACE 98
C*****	RAYSET AND NEWTRC=TRUE TELLS RAYPLT TO START A NEW RAY	TRACE 99
	NEWTRC=.TRUE.	TRACE100
	IHOP=0	TRACE101
C*****	RESET PERIGEE PLOT COUNTER	TRACE102
	NPRGS=0	TRACE103
C	USE CURRENT RELATIVE POSITION OF RAY TO PREDICT	TRACE104
C	SIGN OF NEXT INTERSECTION OF RAY WITH RECEIVER HEIGHT	TRACE105

C	(WILL SOON BE REVERSED).	TRACE106
	RSIGN=SIGN(1.0,F)	TRACE107
C	IF RAY IS LAUNCHED FROM RECEIVER HEIGHT, USE DIRECTION INSTEAD	TRACE108
	IF(THERE) RSIGN=SIGN(1.0,FDOT)	TRACE109
	GDOT=DOT(G)	TRACE110
C	TEST CASE FOR RECEIVER ON THE GROUND	TRACE111
	IF(F.EQ.G) RSIGN=1.0	TRACE112
C	IF RECEIVER IS ON TERRAIN THEN DIRECTION OF FIRST	TRACE113
C	RECEIVER CROSSING IS DOWNWARD	TRACE114
	CALL PRINTR('TXMTR',RAYSET)	TRACE115
	IF (PLTENB) CALL RAYPLT	TRACE116
	NEWRAY=.TRUE.	TRACE117
	STHO=SIN(TH)	TRACE118
	CTHO=COS(TH)	TRACE119
	PHIO=PHI	TRACE120
C		TRACE121
C	SET DEFAULT RAY EVENTS FOR 'PRINTR'	TRACE122
	XCOND=DEFCND	TRACE123
	XSET=NORYST	TRACE124
C		TRACE125
C	***** LOOP ON NUMBER OF HOPS	TRACE126
10	IHOP=IHOP+1	TRACE127
C	REVERSE SIGN AT EACH CROSSING OF RECEIVER HEIGHT	TRACE128
	RSIGN=-RSIGN	TRACE129
	IF (IHOP.GT.NHOP) GO TO 100	TRACE130
	PENET=.FALSE.	TRACE131
C	***** LOOP ON MAXIMUM NUMBER OF STEPS PER HOP	TRACE132
	DO 79 J=1,MAX	TRACE133
C	LAUNCH=TRUE ONLY WHEN TRANSMITTER ON GROUND WITH DOWNWARD	TRACE134
C	TRANSMISSION(POSSIBLE ONLY ON 1ST STEP).	TRACE135
	LAUNCH=G.EQ.0.0 .AND. GDOT.LT.0.0	TRACE136
C		TRACE137
C	SAVE CURRENT STATE VALUES FOR LATER COMPARISONS	TRACE138
12	DO 13 L=1,6	TRACE139
	ROLD(L)=R(L)	TRACE140
13	DROLD(L)=DRDT(L)	TRACE141
	FDOLD=FDOT	TRACE142
	GDOLD=GDOT	TRACE143
	FOLD=F	TRACE144
	GOLD=G	TRACE145
	TOLD=T	TRACE146
C		TRACE147
C	PROCESS NEXT RAY POINT	TRACE148
	CALL RKAM	TRACE149
	FDOT=DOT(F)	TRACE150
	WASNT=.NOT.HOME	TRACE151
	HOME=FDOT*F.GE.0.	TRACE152
C		TRACE153
C		TRACE154
C	LOOK FOR DOWNGOING CROSSING OF RECEIVER SURFACE	TRACE155
	IF(.NOT.LAUNCH.AND.F.LT.0.0.AND.RSIGN.LT.0.0) GO TO 50	TRACE156
C	CHECK FOR CASE OF CLOSEST APPROACH	TRACE157
	IF (HOME.AND.WASNT) GO TO 30	TRACE158
C	DETERMINE IF A GROUND CROSSING HAS OCCURED	TRACE159
	IF(PCROSS(G,GDOT)) GO TO 20	TRACE160

C	LOOK FOR UPGOING CROSSING OF RECEIVER SURFACE	TRACE161
	IF(.NOT.LAUNCH.AND.F.GT.0.0.AND.RSIGN.GT.0.0) GO TO 50	TRACE162
	GO TO 18	TRACE163
C		TRACE164
C	CHECK FOR PERIGEE CONDITION	TRACE165
18	IF (DROLD(1).GE.0..OR.DRDT(1).LE.0.) GO TO 25	TRACE166
	CALL PRINTR(' PERIGEE ',NORYST)	TRACE167
	IF(PRIGEE.EQ.0.0) GO TO 25	TRACE168
C		TRACE169
	IF(NPRGS.GE.MXPRGS) CALL STOPIT('PRG LIMIT')	TRACE170
	NPRGS=NPRGS+1	TRACE171
	CALL RMOVE(PRGHST(1,NPRGS),R,3)	TRACE172
C		TRACE173
25	APOGEE=DROLD(1).GT.0..AND.DRDT(1).LT.0.	TRACE174
	PLTENB=APOG.EQ.0.0.OR.APOGEE	TRACE175
C		TRACE176
	IF(APOGEE) CALL PRINTR(' APOGEE ',NORYST)	TRACE177
	IF (DROLD(2)*DRDT(2).LT.0.) CALL PRINTR(' MAX LAT ',NORYST)	TRACE178
	IF (DROLD(3)*DRDT(3).LT.0.) CALL PRINTR(' MAX LONG ',NORYST)	TRACE179
	DO 14 I=4,6	TRACE180
	IF (ROLD(I)*R(I).LT.0.) CALL PRINTR(' WAVE REV',NORYST)	TRACE181
14	CONTINUE	TRACE182
	GO TO 75	TRACE183
C*****	RAY WENT UNDERGROUND	TRACE184
C	USE 'FULL' REGULAR PARABOLIC FIT(ENTRY 'FIT')	TRACE185
20	CALL RCROSS(-1.,G,GDOT,'GGRND REF',GROUND)	TRACE186
	GO TO 75	TRACE187
C*****	RAY MAY HAVE MADE A CLOSEST APPROACH	TRACE188
C	USE 'FULL' REGULAR PARABOLIC FIT	TRACE189
30	CALL FIT(F,FOLD,FDOLD)	TRACE190
	IF(RAD.GE.0.0) GO TO 501	TRACE191
C	ESTIMATE TIME OF CLOSEST APPROACH	TRACE192
	TP=T-ZDOT/D2Z	TRACE193
	CALL GRAZE(F,RSIGN,TP)	TRACE194
	FDOT=ZDOT	TRACE195
	IF (THERE) GO TO 51	TRACE196
C		TRACE197
C	SET DRDT(1)=0 TO AVOID INCORRECT APOGEE OR PERIGEE PRINTOUT, A NEW	TRACE198
C	VALUE WILL BE COMPUTED BEFORE FURTHER ANALYSIS IS DONE	TRACE199
40	DRDT(1)=0.	TRACE200
	HPUNCH=R(1)-EARTH	TRACE201
	CALL PRINTR('MMIN DIST',RAYSET)	TRACE202
	IF(PLTENB) CALL RAYPLT	TRACE203
	IF (IHOP.GE.NHOP) GO TO 100	TRACE204
	IHOP=IHOP+1	TRACE205
	RSIGN=-RSIGN	TRACE206
	CALL PRINTR ('MMIN DIST',RAYSET)	TRACE207
	GO TO 89	TRACE208
C*****	RAY CROSSED RECEIVER HEIGHT	TRACE209
50	CALL FIT(F,FOLD,FDOLD)	TRACE210
C	ESTIMATE GROUP TIME WHEN RAY CROSSES RECEIVER HEIGHT	TRACE211
C	(IN THE CORRECT DIRECTION).	TRACE212
501	TC=T-2.0*F/(ZDOT+SIGN(RAD1,RSIGN))	TRACE213
	CALL BACKUP(F,RSIGN,TC)	TRACE214
	FDOT=ZDOT	TRACE215

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IF(.NOT.THERE) GO TO 40
51 HPUNCH=R(1)-EARTHTR                                TRACE216
CALL PRINTR('RRCVR      ',RAYSET)                    TRACE217
IF (PLTENB) CALL RAYPLT                                TRACE218
IF (GET(F).NE.GET(G)) GO TO 89                        TRACE219
C RECEIVER IS ON TERRAINE                              TRACE220
IF (IHOP.GE.NHOP) GO TO 100                          TRACE221
IHOP=IHOP+1                                           TRACE222
RSIGN=-RSIGN                                           TRACE223
C***** GROUND REFLECT                                TRACE224
CALL REFLECT(G)                                       TRACE225
CALL HAMLTN                                           TRACE226
FDOT=DOT(F)                                           TRACE227
RSTART=1.                                             TRACE228
HPUNCH=R(1)-EARTHTR                                TRACE229
CALL PRINTR('GGRND REF',RAYSET)                      TRACE230
THERE=.TRUE.                                         TRACE231
HPUNCH=R(1)-EARTHTR                                TRACE232
CALL PRINTR ('RRCVR      ',RAYSET)                  TRACE233
GO TO 89                                              TRACE234
C*****                                              TRACE235
75 IF (PLTENB) CALL RAYPLT                            TRACE236
PLTENB=APOG.EQ.0.0                                    TRACE237
IF (EXTON) THEN                                       TRACE238
  IF (R(NR).GE.EXTINC) XCOND='EEXTINC'              TRACE239
ENDIF                                                TRACE240
IF (R(1).GT.RMAX.AND.F.GT.0.0.AND.FDOT.GT.0.) XCOND='UMAX HT' TRACE241
IF (R(1).LT.RMIN.AND.F.LT.0.0.AND.FDOT.LT.0.) XCOND='DMIN HT' TRACE242
RANGE=EARTHTR*ACOS(COS(TH)*CTHO+SIN(TH)*STHO*COS(PHI-PHI0)) TRACE243
IF(RGMAX.GT.0.0.AND.RGMAX.LT.RANGE) XCOND='FMAX RANGE' TRACE244
IF(XCOND.NE.DEFCND) GO TO 90                         TRACE245
C                                                    TRACE246
IF (MOD(J,NSKIP).EQ.0) CALL PRINTR('                ',NORYST) TRACE247
79 CONTINUE                                          TRACE248
C***** EXCEEDED MAXIMUM NUMBER OF STEPS             TRACE249
HPUNCH=R(1)-EARTHTR                                TRACE250
CALL PRINTR('SSTEP MAX',RAYSET)                    TRACE251
GO TO 100                                           TRACE252
C*****                                              TRACE253
89 HOME=.TRUE.                                       TRACE254
GDOT=DOT(G)                                          TRACE255
GO TO 10                                            TRACE256
C***** RAY PENETRATED COMPUTATIONAL AREA BOUNDARY AND WAS HEADING OUT TRACE257
90 PENET=.TRUE.                                       TRACE258
HPUNCH=R(1)-EARTHTR                                TRACE259
XSET=RAYSET                                          TRACE260
C                                                    TRACE261
C NORMAL EXIT                                        TRACE262
100 CALL PRINTR(XCOND,XSET)                          TRACE263
IF(NPRGS.LE.0) RETURN                               TRACE264
C                                                    TRACE265
CALL DASH                                           TRACE266
NEWTRC=.TRUE.                                       TRACE267
DO 110 I=1,NPRGS                                     TRACE268
CALL RMOVE(R,PRGHST(1,I),3)                         TRACE269
                                                    TRACE270

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110	CALL RAYPLT	TRACE271
C	CALL RESET('DASH')	TRACE272
	END	TRACE273
		TRACE274
C	LOGICAL FUNCTION PCROSS(Z,ZDT)	TRACE275
C	RETURNS 'TRUE' IF PARABOLIC 'FIT2'(SEE 'FIT' ROUTINE)	TRACE276
C	INDICATES CROSSING OF SURFACE 'Z'.	TRACE277
	REAL ZDT(3)	TRACE278
C	COMMON DECK "TRAC" INSERTED HERE	CTRAC 2
	LOGICAL GROUND,SURF,PERIGE,THERE,MINDIS,NEWRAY	CTRAC 4
	COMMON /TRAC/ GROUND,SURF,PERIGE,THERE,MINDIS,NEWRAY,SMT,OSMT	CTRAC 5
	COMMON/TRAC/ROLD(20),DROLD(20),TOLD,ZDOT,D2Z,RAD,RAD1	CTRAC 6
C		TRACE280
C	USE SPECIAL PARABOLIC FIT GIVING 'SMT' AND 'OSMT'	TRACE281
	ZDT(1)=DOT(Z)	TRACE282
	PCROSS=.TRUE.	TRACE283
	IF(Z.LT.0.0) GO TO 20	TRACE284
	IF(ZDT(1).LE.0.0.OR.ZDT(3).GE.0.0) GO TO 15	TRACE285
	CALL FIT2(Z,ZDT(2),ZDT(3))	TRACE286
	IF(SMT.GT.Z.OR.OSMT.GT.ZDT(2)) GO TO 20	TRACE287
C		TRACE288
15	PCROSS=.FALSE.	TRACE289
20	RETURN	TRACE290
	END	TRACE291
C	SUBROUTINE RCROSS(S,Z,ZDT,EVENT,QMODE)	TRACE292
C	FIND ESTIMATED CROSSING POINT OF SURFACE 'Z' THEN USE	TRACE293
C	ROUTINE 'BACKUP' TO GO THERE AND PERFORM A RAY REFLECTION	TRACE294
C	WITH ROUTINE 'REFLECT'.	TRACE295
C	EXTENDS RAY PROPAGATION TO INTERSECTION WITH REFLECTING SURFACE	TRACE296
C	Z AND CALLS 'REFLECT' TO OBTAIN VECTOR COMPONENTS.	TRACE297
C		TRACE298
	CHARACTER EVENT*8	TRACE299
	REAL ZDT(3)	TRACE300
	LOGICAL QMODE	TRACE301
C	COMMON DECK "TRAC" INSERTED HERE	CTRAC 2
	LOGICAL GROUND,SURF,PERIGE,THERE,MINDIS,NEWRAY	CTRAC 4
	COMMON /TRAC/ GROUND,SURF,PERIGE,THERE,MINDIS,NEWRAY,SMT,OSMT	CTRAC 5
	COMMON/TRAC/ROLD(20),DROLD(20),TOLD,ZDOT,D2Z,RAD,RAD1	CTRAC 6
C	COMMON DECK "RR" INSERTED HERE	TRACE303
	REAL MODREC	TRACE304
	COMMON/RR/ MODREC(4)	TRACE305
	COMMON/RR/F,PFR,PFRR,PFRTH,PFRPH	TRACE306
	COMMON/RR/PFTH,PFPH,PFTHTH,PFPHPH,PFTHPH,FSELECT,FTIME	TRACE307
C	COMMON DECK "WWR" INSERTED HERE	TRACE308
	PARAMETER (NWARSZ=1000)	TRACE309

	COMMON/WW/ID(10),MAXW,W(NWARSZ)	TRACE310
	REAL MAXSTP,MAXERR,INTYP,LLAT,LLON	TRACE311
	EQUIVALENCE (EARTH, W(1)), (RAY, W(2)), (XMTRH, W(3)), (TLAT, W(4)),	TRACE312
	1 (TLON, W(5)), (OW, W(6)), (FBEG, W(7)), (FEND, W(8)), (FSTEP, W(9)),	TRACE313
	2 (AZ1, W(10)), (AZBEG, W(11)), (AZEND, W(12)), (AZSTEP, W(13)),	TRACE314
	3 (BETA, W(14)), (ELBEG, W(15)), (ELEND, W(16)), (ELSTEP, W(17)),	TRACE315
	8 (RCVRH, W(20)),	TRACE316
	4 (ONLY, W(21)), (HOP, W(22)), (MAXSTP, W(23)), (PLAT, W(24)), (PLON, W(25))	TRACE317
	5, (HMAX, W(26)), (RAYFNC, W(29)), (EXTINC, W(33)),	TRACE318
	6 (HMIN, W(27)), (RGMX, W(28)),	TRACE319
	8 (INTYP, W(41)), (MAXERR, W(42)), (ERATIO, W(43)),	TRACE320
	6 (STEP1, W(44)), (STPMAX, W(45)), (STPMIN, W(46)), (FACTR, W(47)),	TRACE321
	7 (SKIP, W(71)), (RAYSET, W(72)), (PRTSRP, W(74)), (HITLET, W(75))	TRACE322
	9, (BINRAY, W(76)), (PAGLN, W(77)), (PLT, W(81)), (PFACTR, W(82)),	TRACE323
	1 (LLAT, W(83)), (LLON, W(84)), (RLAT, W(85)), (RLON, W(86))	TRACE324
	2, (TIC, W(87)), (HB, W(88)), (HT, W(89)), (TICV, W(96))	TRACE325
C	COMMON DECK "FLAG" INSERTED HERE	TRACE326
	LOGICAL NEWWR, NEWWP, NEWTRC, PENET	TRACE327
	COMMON /FLG/ NTYP, NEWWR, NEWWP, NEWTRC, PENET, LINES, IHOP, HPUNCH	TRACE328
	COMMON R(20), T, STP, DRDT(20)	TRACE329
	COMMON /RK/ N, STEP, MODE, E1MAX, E1MIN, E2MAX, E2MIN, FACT, RSTART	TRACE330
	LOGICAL HOME	TRACE331
C	COMMON DECK "TRLOCAL" INSERTED HERE	TRACE332
	COMMON/TRLOCAL/RSIGN, HOME, FDOT, GDOT, GOLD, GDOLD	TRACE333
C		TRACE334
	IF(QMODE) GO TO 60	TRACE335
	CALL FIT(Z, ZDT(2), ZDT(3))	TRACE336
	TC=T-2.0*Z/(ZDOT-RAD1)	TRACE337
	CALL BACKUP(Z, -1., TC)	TRACE338
C*****	GROUND REFLECT	TRACE339
60	CALL REFLECT(Z)	TRACE340
	CALL HAMLTN	TRACE341
	ZDT(1)=DOT(Z)	TRACE342
	FDOT=DOT(F)	TRACE343
	HOME=FDOT*F.GE.0.0	TRACE344
	RSTART=1.	TRACE345
	HPUNCH=R(1)-EARTH	TRACE346
	CALL PRINTR(EVENT, RAYSET)	TRACE347
	IF(F.NE.Z) RETURN	TRACE348
C	AVOID RECEIVER CROSSING AT THE TRANSMITTER IF RECEIVER ON TERRAIN	TRACE349
	RSIGN=S	TRACE350
	HOME=.TRUE.	TRACE351
	END	TRACE352
	SUBROUTINE HAMLTN	HAMLTN 2
C*****	CALCULATES HAMILTONS EQUATIONS FOR RAY TRACING	HAMLTN 3
C	AND OTHER QUANTITIES TO BE INTEGRATED	HAMLTN 4
C	COMMON DECK "GG" INSERTED HERE	CGG 2
	REAL MODG	CGG 4
	COMMON/GG/MODG(4)	CGG 5
	COMMON/GG/G, PGR, PGRR, PGRTH, PGRPH	CGG 6

	COMMON/GG/PGTH,PGPH,PGTHTH,PGPHPH,PGTHPH,GSELECT,GTIME	CGG	7
C	COMMON DECK "CONST" INSERTED HERE	CCONST	2
	COMMON/PCONST/CREF,RGAS,GAMMA	CCONST	4
	COMMON/MCONST/PI,PIT2,PID2,DEGS,RAD,ALN10	CCONST	5
C	COMMON DECK "RINREAL" INSERTED HERE	CRINREA2	
	LOGICAL SPACE	CRINREA4	
	REAL LPOLAR,LPOLRI,KPHK,KPHKI,KAY2,KAY2I	CRINREA5	
	CHARACTER DISPM*6	CRINREA6	
	COMMON/RINPL/DISPM	CRINREA7	
	COMMON /RIN/ MODRIN(8),RAYNAME(2,3),TYPE(3),SPACE	CRINREA8	
	COMMON/RIN/OMEGMIN,OMEGMAX,KAY2,KAY2I,	CRINREA9	
	1 H,HI,PHT,PHTI,PHR,PHRI,PHTH,PHTHI,PHPH,PHPHI	CRINRE10	
	2, PHOW,PHOWI,PHKR,PHKRI,PHKTH,PHKTI, PHKPH,PHKPI	CRINRE11	
	3 ,KPHK,KPHKI,POLAR,POLARI,LPOLAR,LPOLRI,SGN	CRINRE12	
	COMMON R(20),T,STP,DRDT(20)	HAMLTN	8
	PARAMETER (NWARSZ=1000)	CWW1	3
	COMMON/WW/ID(10),MAXW,W(NWARSZ)	CWW1	4
	EQUIVALENCE (TH,R(2)),(PH,R(3)),(KR,R(4)),(KTH,R(5)),(KPH,R(6)),	HAMLTN10	
	1 (DTHDT,DRDT(2)),(DPHDT,DRDT(3)),(DKRDT,DRDT(4)),(DKTHDT,DRDT(5)),	HAMLTN11	
	2 (DKPHDT,DRDT(6)),(HMAX,W(26)),(OW,W(6))	HAMLTN12	
	REAL KR,KTH,KPH	HAMLTN13	
	STH=SIN(TH)	HAMLTN14	
	CTH=SIN(PID2-TH)	HAMLTN15	
	RSTH=R(1)*STH	HAMLTN16	
	RCTH=R(1)*CTH	HAMLTN17	
	CALL DISPER	HAMLTN18	
	DENPHC=1.0/(PHOW*CREF)	HAMLTN19	
	DRDT(1)=-PHKR*DENPHC	HAMLTN20	
	DTHDT=-PHKTH*DENPHC/R(1)	HAMLTN21	
	DPHDT=-PHKPH*DENPHC/RSTH	HAMLTN22	
	DKRDT=PHR*DENPHC+KTH*DTHDT+KPH*STH*DPHDT	HAMLTN23	
	DKTHDT=(PHTH*DENPHC-KTH*DRDT(1)+KPH*RCTH*DPHDT)/R(1)	HAMLTN24	
	DKPHDT=(PHPH*DENPHC-KPH*STH*DRDT(1)-KPH*RCTH*DTHDT)/RSTH	HAMLTN25	
	NR=6	HAMLTN26	
C*****	PHASE PATH	HAMLTN27	
	IF (W(57).EQ.0.) GO TO 10	HAMLTN28	
	NR=NR+1	HAMLTN29	
	DRDT(NR)=- KPHK/PHOW/OW	HAMLTN30	
C*****	ABSORPTION	HAMLTN31	
	10 IF (W(58).EQ.0.) GO TO 15	HAMLTN32	
	NR=NR+1	HAMLTN33	
	DRDT(NR)= 10./ALN10*KPHK*KAY2I/(KR*KR+KTH*KTH+KPH*KPH)*DENPHC	HAMLTN34	
C*****	DOPPLER SHIFT	HAMLTN35	
	15 IF (W(59).EQ.0.) GO TO 20	HAMLTN36	
	NR=NR+1	HAMLTN37	
	DRDT(NR)=-PHT*DENPHC/PIT2	HAMLTN38	
C*****	GEOMETRICAL PATH LENGTH	HAMLTN39	
	20 IF (W(60).EQ.0.) GO TO 25	HAMLTN40	
	NR=NR+1	HAMLTN41	
	DRDT(NR)=SQRT(PHKR**2+PHKTH**2+PHKPH**2)*ABS(DENPHC)	HAMLTN42	
C*****	TERRAIN FUNCTION AS COMPLETE INTEGRAL	HAMLTN43	
25	IF(ABS(W(61))+ABS(W(62))+ABS(W(63))+ABS(W(64)).EQ.0.0) GO TO 45	HAMLTN44	
	CALL TOPOG	HAMLTN45	
C		HAMLTN46	
	IF(W(61).EQ.0.) GO TO 30	HAMLTN47	

NR=NR+1	HAMLTN48
DRDT(NR)=PGR*DRDT(1)+PGTH*DTHDT+PGPH*DPHDT	HAMLTN49
C***** TERRAIN TIME DERIVATIVES AS COMPLETE INTEGRALS	HAMLTN50
30 IF(W(62).EQ.0.) GO TO 35	HAMLTN51
NR=NR+1	HAMLTN52
C DERIVATIVE WITH RESPECT TO R	HAMLTN53
DRDT(NR)=PGR*DRDT(1)+PGRTH*DTHDT+PGRPH*DPHDT	HAMLTN54
35 IF(W(63).EQ.0.) GO TO 40	HAMLTN55
NR=NR+1	HAMLTN56
C DERIVATIVE WITH RESPECT TO THETA	HAMLTN57
DRDT(NR)=PGRTH*DRDT(1)+PGTHTH*DTHDT+PGTHPH*DPHDT	HAMLTN58
40 IF(W(64).EQ.0.) GO TO 45	HAMLTN59
NR=NR+1	HAMLTN60
C DERIVATIVE WITH RESPECT TO PHI	HAMLTN61
DRDT(NR)=PGRPH*DRDT(1)+PGTHPH*DTHDT+PGPHPH*DPHDT	HAMLTN62
C***** OTHER CALCULATIONS	HAMLTN63
45 CONTINUE	HAMLTN64
RETURN	HAMLTN65
END	HAMLTN66

SUBROUTINE RKAM	RKAM	2
C KEEPS TRACK OF INTERNAL INTEGRATION STEPS PERFORMED BY THE RKAM1	RKAM	3
C ROUTINE AND MAKES THEM AVAILABLE TO CALLING ROUTINES.	RKAM	4
COMMON/RKAMS/XV(5),FV(4,20),YU(5,20),EPM,ALPHA,MM	RKAM	5
C COMMON DECK "RK" INSERTED HERE	CRK	2
C DEFINE SIZE REQUIRED FOR RAY STATE SAVE ARRAY	CRK	4
PARAMETER (LRKAMS=87+2*100,NXRKMS=12+LRKAMS,MXEQPT=21)	CRK	5
PARAMETER (NRKSAV=NXRKMS+MXEQPT-1)	CRK	6
COMMON /RK/ NEQS,STEP,MODE,E1MAX,E1MIN,E2MAX,E2MIN,FACT,RSTART	CRK	7
C COMMON DECK "RKTIME" INSERTED HERE	CRKTIME2	
COMMON/CRKTIME/RKTIME	CRKTIME4	
COMMON Y(20),T,SPACE,DYDT(20)	RKAM	8
REAL RV(1)	RKAM	9
DOUBLE PRECISION YU	RKAM	10
EQUIVALENCE(RKTIME,IRKTIME),(RV,R)	RKAM	11
C	RKAM	12
REAL SVBUF(NRKSAV)	RKAM	13
LOGICAL SAVED	RKAM	14
C	RKAM	15
DATA SAVED/.FALSE./	RKAM	16
C PERFORM CLOCK ADVANCE(SEE 'GET' ROUTINE)	RKAM	17
IRKTIME=IRKTIME+1	RKAM	18
C	RKAM	19
IF(RSTART.NE.0.0 .OR. MODE.LE.2) GO TO 250	RKAM	20
C	RKAM	21
NV=NV+1	RKAM	22
IF(NV.LE.4) GO TO 300	RKAM	23
C	RKAM	24
250 TOLD=T	RKAM	25
C PERFORM NUMERICAL INTEGRATION TO TIME 'T'	RKAM	26
CALL RKAM1	RKAM	27

	IF(MODE.LE.2) GO TO 400	RKAM	28
	IF(RSTART.NE.0.0) GO TO 260	RKAM	29
C	SEARCH FOR REQUESTED VALUE IN PIPELINE	RKAM	30
C	TAKING SIGN OF 'STEP' INTO ACCOUNT.	RKAM	31
	TUP=TOLD+.25*STEP	RKAM	32
	DO 150 NV=1,3	RKAM	33
	IF(SPACE.GT.0.0.AND.TUP.LT.XV(NV)) GO TO 300	RKAM	34
	IF(SPACE.LT.0.0.AND.TUP.GT.XV(NV)) GO TO 300	RKAM	35
150	CONTINUE	RKAM	36
C	GOT IT ALREADY, RETURN	RKAM	37
	GO TO 400	RKAM	38
C		RKAM	39
260	NV=1	RKAM	40
C	RETRIEVE REQUESTED VALUES FROM PIPELINE	RKAM	41
300	T=XV(NV)	RKAM	42
	DO 350 I=1,NEQS	RKAM	43
	Y(I)=YU(NV,I)	RKAM	44
350	DYDT(I)=FV(NV,I)	RKAM	45
C		RKAM	46
C	STANDARD EXIT SEQUENCE	RKAM	47
400	RETURN	RKAM	48
C		RKAM	49
	ENTRY RKSAVE(SVBUF)	RKAM	50
C		RKAM	51
	SVBUF(1)=NV	RKAM	52
	SVBUF(2)=NEQS	RKAM	53
	SVBUF(3)=MM	RKAM	54
	SVBUF(4)=SPACE	RKAM	55
	SVBUF(5)=MODE	RKAM	56
	CALL RMOVE(SVBUF(6),E1MAX,6)	RKAM	57
	CALL RMOVE(SVBUF(12),XV,LRKAMS)	RKAM	58
	CALL RMOVE(SVBUF(NXRKMS),Y,MXEQPT)	RKAM	59
C		RKAM	60
	SAVED=.TRUE.	RKAM	61
	RETURN	RKAM	62
	ENTRY RKRSTR(SVBUF)	RKAM	63
C		RKAM	64
	IF(.NOT.SAVED) RETURN	RKAM	65
C		RKAM	66
	NV=SVBUF(1)	RKAM	67
	NEQS=SVBUF(2)	RKAM	68
	MM=SVBUF(3)	RKAM	69
	SPACE=SVBUF(4)	RKAM	70
	MODE=SVBUF(5)	RKAM	71
	CALL RMOVE(E1MAX,SVBUF(6),6)	RKAM	72
	CALL RMOVE(XV,SVBUF(12),LRKAMS)	RKAM	73
	CALL RMOVE(Y,SVBUF(NXRKMS),MXEQPT)	RKAM	74
C		RKAM	75
	WRITE(3,*) 'RESTORING NV,NEQS,MM,ALPHA,T='	RKAM	76
1	,NV,NEQS,MM,ALPHA,T	RKAM	77
	RETURN	RKAM	78
	END	RKAM	79

	SUBROUTINE RKAM1	RKAM1 2
C	NUMERICAL INTEGRATION OF DIFFERENTIAL EQUATIONS	RKAM1 3
C	THIS ROUTINE IS A MODIFICATION OF RKAMSUB, WHICH WAS WRITTEN	RKAM1 4
C	BY G.J. LASTMAN AND IS AVAILABLE THROUGH THE CDC CO-OP LIBRARY	RKAM1 5
C	AS 'D2 UTEX RKAMSUB'.	RKAM1 6
	COMMON /RK/ NN,SPACE,MODE,E1MAX,E1MIN,E2MAX,E2MIN,FACT,RSTART	RKAM1 7
	COMMON Y(20),T,STEP,DYDT(20)	RKAM1 8
	COMMON/RKAMS/XV(5),FV(4,20),YU(5,20),EPM,ALPHA,MM	RKAM1 9
	DIMENSION DELY(4,20),BET(4)	RKAM1 10
	DOUBLE PRECISION YU	RKAM1 11
C	IF (RSTART.EQ.0.) GO TO 1000	RKAM1 12
	LL=1	RKAM1 13
	MM=1	RKAM1 14
	IF (MODE.EQ.1) MM=4	RKAM1 15
	ALPHA=T	RKAM1 16
	EPM=0.0	RKAM1 17
	BET(1)=0.5	RKAM1 18
	BET(2)=0.5	RKAM1 19
	BET(3)=1.0	RKAM1 20
	BET(4)=0.0	RKAM1 21
	STEP=SPACE	RKAM1 22
	R=19.0/270.0	RKAM1 23
	XV(MM)=T	RKAM1 24
	IF (E1MIN.LE.0.) E1MIN=E1MAX/50.	RKAM1 25
	IF (FACT.LE.0.) FACT=0.5	RKAM1 26
	CALL HAMLTN	RKAM1 27
	DO 320 I=1,NN	RKAM1 28
	FV(MM,I)=DYDT(I)	RKAM1 29
320	YU(MM,I)=Y(I)	RKAM1 30
	RSTART=0.	RKAM1 31
	GO TO 1001	RKAM1 32
1000	IF (MODE.NE.1) GO TO 2000	RKAM1 33
C		RKAM1 34
C	RUNGE-KUTTA	RKAM1 35
1001	DO 1034 K=1,4	RKAM1 36
	DO 1350 I=1,NN	RKAM1 37
	DELY(K,I)=STEP*FV(MM,I)	RKAM1 38
	Z=YU(MM,I)	RKAM1 39
1350	Y(I)=Z+BET(K)*DELY(K,I)	RKAM1 40
	T=BET(K)*STEP+XV(MM)	RKAM1 41
	CALL HAMLTN	RKAM1 42
	DO 1034 I=1,NN	RKAM1 43
1034	FV(MM,I)=DYDT(I)	RKAM1 44
	DO 1039 I=1,NN	RKAM1 45
	DEL=(DELY(1,I)+2.0*DELY(2,I)+2.0*DELY(3,I)+DELY(4,I))/6.0	RKAM1 46
1039	YU(MM+1,I)=YU(MM,I)+DEL	RKAM1 47
	MM=MM+1	RKAM1 48
	XV(MM)=XV(MM-1)+STEP	RKAM1 49
	DO 1400 I=1,NN	RKAM1 50
1400	Y(I)=YU(MM,I)	RKAM1 51
	T=XV(MM)	RKAM1 52
	CALL HAMLTN	RKAM1 53
		RKAM1 54

	IF (MODE.EQ.1) GO TO 42	RKAM1 55
	DO 150 I=1,NN	RKAM1 56
150	FV(MM,I)=DYDT(I)	RKAM1 57
	IF (MM.LE.3) GO TO 1001	RKAM1 58
C		RKAM1 59
C	ADAMS-MOULTON	RKAM1 60
2000	DO 2048 I=1,NN	RKAM1 61
	DEL=STEP*(55.*FV(4,I)-59.*FV(3,I)+37.*FV(2,I)-9.*FV(1,I))/24.	RKAM1 62
	Y(I)=YU(4,I)+DEL	RKAM1 63
2048	DELY(1,I)=Y(I)	RKAM1 64
	T=XV(4)+STEP	RKAM1 65
	CALL HAMLTN	RKAM1 66
	XV(5)=T	RKAM1 67
	DO 2051 I=1,NN	RKAM1 68
	DEL=STEP*(9.*DYDT(I)+19.*FV(4,I)-5.*FV(3,I)+FV(2,I))/24.	RKAM1 69
	YU(5,I)=YU(4,I)+DEL	RKAM1 70
2051	Y(I)=YU(5,I)	RKAM1 71
	CALL HAMLTN	RKAM1 72
	IF (MODE.LE.2) GO TO 42	RKAM1 73
C		RKAM1 74
C	ERROR ANALYSIS	RKAM1 75
	SSE=0.0	RKAM1 76
	DO 3033 I=1,NN	RKAM1 77
	EPSIL=R*ABS(Y(I)-DELY(1,I))	RKAM1 78
	IF (MODE.EQ.3.AND.Y(I).NE.0.) EPSIL=EPSIL/ABS(Y(I))	RKAM1 79
	IF (SSE.LT.EPSIL) SSE=EPSIL	RKAM1 80
3033	CONTINUE	RKAM1 81
	IF (ELMAX.GT.SSE) GO TO 3035	RKAM1 82
	IF (ABS(STEP).LE.E2MIN) GO TO 42	RKAM1 83
	LL=1	RKAM1 84
	MM=1	RKAM1 85
	STEP=STEP*FACT	RKAM1 86
	GO TO 1001	RKAM1 87
3035	IF (LL.LE.1.OR.SSE.GE.E1MIN.OR.E2MAX.LE.ABS(STEP)) GO TO 42	RKAM1 88
	LL=2	RKAM1 89
	MM=3	RKAM1 90
	XV(2)=XV(3)	RKAM1 91
	XV(3)=XV(5)	RKAM1 92
	DO 5363 I=1,NN	RKAM1 93
	FV(2,I)=FV(3,I)	RKAM1 94
	FV(3,I)=DYDT(I)	RKAM1 95
	YU(2,I)=YU(3,I)	RKAM1 96
5363	YU(3,I)=YU(5,I)	RKAM1 97
	STEP=2.0*STEP	RKAM1 98
	GO TO 1001	RKAM1 99
C		RKAM1100
C	EXIT ROUTINE	RKAM1101
42	LL=2	RKAM1102
	MM=4	RKAM1103
	DO 12 K=1,3	RKAM1104
	XV(K)=XV(K+1)	RKAM1105
	DO 12 I=1,NN	RKAM1106
	FV(K,I)=FV(K+1,I)	RKAM1107
12	YU(K,I)=YU(K+1,I)	RKAM1108
	XV(4)=XV(5)	RKAM1109

	DO 52 I=1,NN	
	FV(4,I)=DYDT(I)	RKAM1110
52	YU(4,I)=YU(5,I)	RKAM1111
	IF (MODE.LE.2) RETURN	RKAM1112
	E=ABS(XV(4)-ALPHA)	RKAM1113
	IF (E.LE.EPM+.25*STEP) GO TO 2000	RKAM1114
	EPM=E	RKAM1115
	RETURN	RKAM1116
	END	RKAM1117
		RKAM1118

	SUBROUTINE BACKUP(Z,RSIGN,TC)	BACKUP 2
C	MOVES THE RAY TO THE CLOSEST INTERSECTION WITH THE RECEIVER	BACKUP 3
C	OR TERRAIN SURFACE(VARIABLES 'FSELECT' OR 'GSELECT' IN LABELED	BACKUP 4
C	COMMONS /RR/ OR /GG/, RESPECTIVELY, TELL WHICH KIND OF SURFACE).	BACKUP 5
C		BACKUP 6
	CHARACTER*9 NBAK,NGRAZ,NTRY	BACKUP 7
C		BACKUP 8
	PARAMETER (PRNZTL=0.5E-4,PRNDZTL=1.E-6)	BACKUP 9
C		BACKUP 10
	COMMON /RK/ N,STEP,MODE,E1MAX,E1MIN,E2MAX,E2MIN,FACT,RSTART	BACKUP 11
C	COMMON DECK "TRAC" INSERTED HERE	CTRAC 2
	LOGICAL GROUND,SURF,PERIGE,THERE,MINDIS,NEWRAY	CTRAC 4
	COMMON /TRAC/ GROUND,SURF,PERIGE,THERE,MINDIS,NEWRAY,SMT,OSMT	CTRAC 5
	COMMON/TRAC/ROLD(20),DROLD(20),TOLD,ZDOT,D2Z,RAD,RAD1	CTRAC 6
	COMMON R(20),T,STP,DRDT(20)	BACKUP 13
	PARAMETER (NWARSZ=1000)	CWW1 3
	COMMON/WW/ID(10),MAXW,W(NWARSZ)	CWW1 4
	EQUIVALENCE (EARTH,W(1)),(INTYP,W(41)),(STEP1,W(44))	BACKUP 15
	REAL KR	BACKUP 16
	EQUIVALENCE (KR,R(4)),(DKRDT,DRDT(4))	BACKUP 17
	REAL INTYP	BACKUP 18
	LOGICAL PCNTRL	BACKUP 19
	DATA NBAK,NGRAZ/' BACK UP0', ' GRAZE 1'/	BACKUP 20
C		BACKUP 21
	NTRY=NBAK	BACKUP 22
	GO TO 100	BACKUP 23
C		BACKUP 24
	ENTRY GRAZE(Z,RSIGN,TC)	BACKUP 25
	NTRY=NGRAZ	BACKUP 26
C		BACKUP 27
	DEFINE BASE STEP SIZE	BACKUP 28
100	STPB=STP	BACKUP 29
C		BACKUP 30
	DEFINE BACKUP LOCATION TOLERANCES BASED ON INTEGRATION MODE	BACKUP 31
C		BACKUP 32
	IF(MODE.LT.3) THEN	BACKUP 33
	TOL=STEP1	BACKUP 34
	ELSEIF(MODE.EQ.3) THEN	BACKUP 35
	TOL=ABS(E1MAX*STPB)	BACKUP 36
	ELSE	BACKUP 37
	TOL=E1MAX	BACKUP 38

ENDIF	BACKUP39
C USE THIS OR MINIMUM STEP SIZE WHICHEVER IS LESS	BACKUP40
TOL=AMIN1(TOL,FACT*E2MIN)	BACKUP41
C	BACKUP42
PCNTRL=W(73).NE.0.0	BACKUP43
THERE=.TRUE.	BACKUP44
C STEP TO ESTIMATED CROSSING AT TC.	BACKUP45
C***** DIAGNOSTIC PRINTOUT	BACKUP46
IF(PCNTRL) CALL PRINTR (NTRY,0.)	BACKUP47
STEP=TC-T	BACKUP48
STEP=SIGN(AMIN1(ABS(STPB),ABS(STEP)),STEP)	BACKUP49
MODE=1	BACKUP50
RSTART=1	BACKUP51
TOLD=T	BACKUP52
CALL RMOVE(DROLD,DRDT,3)	BACKUP53
ZDOLD=DOT(Z)	BACKUP54
CALL RKAM	BACKUP55
RSTART=1.0	BACKUP56
ZDOT=DOT(Z)	BACKUP57
IF(NTRY.EQ.NGRAZ .OR. RSIGN*ZDOT.LE.0.0) GO TO 12	BACKUP58
C	BACKUP59
C***** FIND NEAREST INTERSECTION OF RAY WITH THE HEIGHT HS	BACKUP60
DO 10 I=1,10	BACKUP61
STEP=-Z/ZDOT	BACKUP62
STEP=SIGN(AMIN1(ABS(STPB),ABS(STEP)),STEP)	BACKUP63
IF (ABS(Z).LT.PRNZTL .AND. ABS(STEP).LT.TOL) GO TO 60	BACKUP64
C***** DIAGNOSTIC PRINTOUT	BACKUP65
IF(PCNTRL) CALL PRINTR(' BACK UP1',0.)	BACKUP66
MODE=1	BACKUP67
RSTART=1.	BACKUP68
TOLD=T	BACKUP69
CALL RMOVE(DROLD,DRDT,3)	BACKUP70
ZDOLD=ZDOT	BACKUP71
CALL RKAM	BACKUP72
ZDOT=DOT(Z)	BACKUP73
10 RSTART=1.	BACKUP74
C	BACKUP75
C***** FIND NEAREST CLOSEST APPROACH OF RAY TO THE HEIGHT HS	BACKUP76
12 THERE=.FALSE.	BACKUP77
DO 20 I=1,10	BACKUP78
C DO 'LOCAL' PARABOLIC FIT	BACKUP79
CALL FIT3(Z,ZOLD,ZDOLD)	BACKUP80
STEP=-ZDOT/D2Z	BACKUP81
STEP=SIGN(AMIN1(ABS(STPB),ABS(STEP)),STEP)	BACKUP82
IF (ABS(ZDOT).LE.PRNDZTL .AND. ABS(STEP).LT.TOL) GO TO 60	BACKUP83
C***** DIAGNOSTIC PRINTOUT	BACKUP84
IF(PCNTRL) CALL PRINTR (' GRAZE 1 ',0.)	BACKUP85
MODE=1	BACKUP86
RSTART=1.	BACKUP87
TOLD=T	BACKUP88
CALL RMOVE(DROLD,DRDT,3)	BACKUP89
ZOLD=Z	BACKUP90
ZDOLD=ZDOT	BACKUP91
CALL RKAM	BACKUP92
RSTART=1.	BACKUP93

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      IF (D2Z*Z.LT.0.) GO TO 30
      IF (KPARLEL(Z).EQ.0.0) GO TO 60
20  CONTINUE
      WRITE(3,350)
350  FORMAT(' ***** COULDN'T FIND CLOSEST APPROACH IN 10 STEPS')
      GO TO 60
C
      30 CONTINUE
C***** DIAGNOSTIC PRINTOUT
      IF(PCNTRL) CALL PRINTR (' BACK UP2',0.)
      MODE=1
C***** ESTIMATE DISTANCE TO NEAREST INTERSECTION GOING THE RIGHT
C***** DIRECTION OF RAY WITH HEIGHT HS
      CALL FIT3(Z,ZOLD,ZDOLD)
      STEP=(-ZDOT+RSIGN*RAD1)/D2Z
      RSTART=1.
      CALL RKAM
      RSTART=1.
C***** FIND NEAREST INTERSECTION OF RAY WITH HEIGHT HS
      DO 40 I=1,10
      ZDOT=DOT(Z)
      STEP=-Z/ZDOT
      STEP=SIGN(AMIN1(ABS(STPB),ABS(STEP)),STEP)
      IF (ABS(Z).LT.PRNZTL .AND. ABS(STEP).LT.TOL) GO TO 50
C***** DIAGNOSTIC PRINTOUT
      IF(PCNTRL) CALL PRINTR (' BACK UP3',0.)
      MODE=1
      RSTART=1.
      CALL RKAM
40  RSTART=1.
50  THERE=.TRUE.
C***** RESET STANDARD MODE AND INTEGRATION TYPE
60  MODE=INTYP
      STEP=STPB
      RETURN
      END

```

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BACKUP94
BACKUP95
BACKUP96
BACKUP97
BACKUP98
BACKUP99
BACKU100
BACKU101
BACKU102
BACKU103
BACKU104
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BACKU120
BACKU121
BACKU122
BACKU123
BACKU124
BACKU125
BACKU126
BACKU127
BACKU128
BACKU129

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C      FUNCTION REFLECT(Z)
C      COMPUTES NORMAL AND PARALLEL COMPONENTS OF THE K-VECTOR AT
C      REFLECTION POINTS TO A SURFACE. WIND EFFECTS ARE INCLUDED.
C
      REAL Z(12),KPARLEL,KNORM
C      COMMON DECK "CC" INSERTED HERE
      REAL MODC
C      COMMON/CC/MODC(4),CS,PCST,PCSR,PCSTH,PCSPH
C      COMMON DECK "WW" INSERTED HERE
      PARAMETER (NWARSZ=1000)
      COMMON/WW/ID(10),MAXW,W(NWARSZ)
      REAL MAXSTP,MAXERR,INTYP,LLAT,LLON
      EQUIVALENCE (EARTH,W(1)),(RAY,W(2)),(XMTRH,W(3)),(TLAT,W(4)),
1 (TLON,W(5)),(OW,W(6)),(FBEG,W(7)),(FEND,W(8)),(FSTEP,W(9)),

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```

REFLECT2
REFLECT3
REFLECT4
REFLECT5
REFLECT6
CCC      2
CCC      4
CCC      5
CWWR     2
CWW1     3
CWW1     4
CWW2     2
CWW2     3
CWW2     4

```

	2 (AZ1,W(10)), (AZBEG,W(11)), (AZEND,W(12)), (AZSTEP,W(13)),	CWW2	5
	3 (BETA,W(14)), (ELBEG,W(15)), (ELEND,W(16)), (ELSTEP,W(17)),	CWW2	6
	8 (RCVRH,W(20)),	CWW2	7
	4 (ONLY,W(21)), (HOP,W(22)), (MAXSTP,W(23)), (PLAT,W(24)), (PLON,W(25))	CWW2	8
	5, (HMAX,W(26)), (RAYFNC,W(29)), (EXTINC,W(33)),	CWW2	9
	6 (HMIN,W(27)), (RGMX,W(28)),	CWW2	10
	8 (INTYP,W(41)), (MAXERR,W(42)), (ERATIO,W(43)),	CWW2	11
	6 (STEP1,W(44)), (STPMAX,W(45)), (STPMIN,W(46)), (FACTR,W(47)),	CWW2	12
	7 (SKIP,W(71)), (RAYSET,W(72)), (PRTSRP,W(74)), (HITLET,W(75))	CWW2	13
	9, (BINRAY,W(76)), (PAGLN,W(77)), (PLT,W(81)), (PFACTR,W(82)),	CWW2	14
	1 (LLAT,W(83)), (LLON,W(84)), (RLAT,W(85)), (RLON,W(86))	CWW2	15
	2, (TIC,W(87)), (HB,W(88)), (HT,W(89)), (TICV,W(96))	CWW2	16
C	COMMON DECK "RKAM" INSERTED HERE	RKAMCOM2	
	REAL KR, KTH, KPH	RKAMCOM4	
	COMMON/R, TH, PH, KR, KTH, KPH, RKVARS(14), TPULSE, CSTEP, DRDT(20)	RKAMCOM5	
C	COMMON DECK "UU" INSERTED HERE	CUU	2
	REAL MODU	CUU	4
	COMMON/UU/MODU(4)	CUU	5
	1, V, PVT, PVR, PVTH, PVPH	CUU	6
	2, VR, PVRT, PVRR, PVRTH, PVRPH	CUU	7
	3, VTH, PVTHT, PVTHR, PVTHTH, PVTHPH	CUU	8
	4, VPH, PVPHT, PVPHR, PVPHTH, PVPHPH	CUU	9
C	COMMON DECK "FNDR" INSERTED HERE	CFNDR	2
	COMMON/FNDR/NZ, NPZR, NPZRR, NPZRTH, NPZRPH, NPZTH, NPZPH, NPZTHTH	CFNDR	4
	COMMON/FNDR/NPZPHPH, NPZTHPH, NSELECT, NTIME	CFNDR	5
C		REFLEC12	
	REAL NR, NTH, NPH, KRNR, KPARR, KPARTH, KPARPH	REFLEC13	
C		REFLEC14	
	IENTRY=1	REFLEC15	
	REFLECT=0.0	REFLEC16	
	GO TO 5	REFLEC17	
C		REFLEC18	
	ENTRY KPARLEL(Z)	REFLEC19	
	KPARLEL=0.0	REFLEC20	
	IENTRY=2	REFLEC21	
	GO TO 5	REFLEC22	
C		REFLEC23	
	ENTRY KNORM(Z)	REFLEC24	
	KNORM=0.0	REFLEC25	
	IENTRY=3	REFLEC26	
C		REFLEC27	
5	Z(1)=GET(Z)	REFLEC28	
	NR=Z(NPZR)	REFLEC29	
	NTH=Z(NPZTH)/R	REFLEC30	
	NPH=Z(NPZPH)/(R*SIN(TH))	REFLEC31	
C		REFLEC32	
	CALL RENORM(NR,1.0,3)	REFLEC33	
C	COMPUTE THE NORMAL COMPONENT OF K-VECTOR TO SURFACE	REFLEC34	
	KRNR=KR*NR+KTH*NTH+KPH*NPH	REFLEC35	
	IF(IENTRY.NE.3) GO TO 8	REFLEC36	
C	IF ENTRY 3 THEN WE ARE DONE	REFLEC37	
	REFLECT=KRNR	REFLEC38	
	RETURN	REFLEC39	
C		REFLEC40	
C	COMPUTE THE PARALLEL VECTOR COMPONENT	REFLEC41	

8	KPARR=KR-KRNR*NR	REFLEC42
	KPARTH=KTH-KRNR*NTH	REFLEC43
	KPARPH=KPH-KRNR*NPH	REFLEC44
C		REFLEC45
	IF(IENTRY.NE.2) GO TO 10	REFLEC46
	REFLECT=ABS(KPARR)+ABS(KPARTH)+ABS(KPARPH)	REFLEC47
	RETURN	REFLEC48
C		REFLEC49
10	OWIPAR=OW-KPARR*VR-KPARTH*VTH-KPARPH*VPH	REFLEC50
	VNR=VR*NR+VTH*NTH+VPH*NPH	REFLEC51
C		REFLEC52
	FCTR=2.0*(KRNR+OWIPAR*VNR/(CS-VNR*VNR))	REFLEC53
	KR=KR-FCTR*NR	REFLEC54
	KTH=KTH-FCTR*NTH	REFLEC55
	KPH=KPH-FCTR*NPH	REFLEC56
	END	REFLEC57
C	SUBROUTINE FIT(Z,ZOLD,ZDOLD)	FIT 2
C	COMPUTES THREE TYPES OF PARABOLIC FITS TO RAY PATH RELATIVE	FIT 3
C	TO TERRAIN.	FIT 4
C		FIT 5
	REAL Z(12)	FIT 6
C	COMMON DECK "RKAM" INSERTED HERE	RKAMCOM2
	REAL KR,KTH,KPH	RKAMCOM4
	COMMON//R,TH,PH,KR,KTH,KPH,RKVAR(14),TPULSE,CSTEP,DRDT(20)	RKAMCOM5
C	COMMON DECK "TRAC" INSERTED HERE	CTRAC 2
	LOGICAL GROUND,SURF,PERIGE,THERE,MINDIS,NEWRAY	CTRAC 4
	COMMON/TRAC/ GROUND,SURF,PERIGE,THERE,MINDIS,NEWRAY,SMT,OSMT	CTRAC 5
	COMMON/TRAC/ROLD(20),DOLD(20),TOLD,ZDOT,D2Z,RAD,RAD1	CTRAC 6
C	COMMON DECK "FNDR" INSERTED HERE	CFNDR 2
	COMMON/FNDR/NZ,NPZR,NPZRR,NPZRTH,NPZRPH,NPZTH,NPZPH,NPZTHTH	CFNDR 4
C	COMMON/FNDR/NPZPHPH,NPZTHPH,NSELECT,NTIME	CFNDR 5
	REAL D2(3)	FIT 10
C		FIT 11
C	USE FIT OF APPENDIX 'J' OF REPORT 'WPL-103' WHICH USES	FIT 12
C	WEIGHTED ESTIMATE OF 1ST DERIVATIVE.	FIT 13
C		FIT 14
	IENTRY=1	FIT 15
	GO TO 5	FIT 16
C		FIT 17
C	USE MODIFIED FIT REQUIRING HEIGHTS OF PARABOLA VERTICES FROM	FIT 18
C	CURRENT AND PREVIOUS RAY POINTS.	FIT 19
	ENTRY FIT2(Z,ZOLD,ZDOLD)	FIT 20
	IENTRY=2	FIT 21
	GO TO 5	FIT 22
C		FIT 23
C	USE FIT OF APPENDIX U(LOCAL VALUE OF 1ST DERIVATIVE)	FIT 24
	ENTRY FIT3(Z,ZOLD,ZDOLD)	FIT 25
	IENTRY=3	FIT 26
C		FIT 27
		FIT 28

5	ZDOT=DOT(Z)	FIT	29
C		FIT	30
	DTI=1.0/(TPULSE-TOLD)	FIT	31
	DO 10 I=1,3	FIT	32
10	D2(I)=(DRDT(I)-DROLD(I))*DTI	FIT	33
C		FIT	34
	D2Z=Z(NPZR)*D2(1)+Z(NPZTH)*D2(2)+Z(NPZPH)*D2(3)	FIT	35
1	+Z(NPZRR)*DRDT(1)*DRDT(1)	FIT	36
1	+Z(NPZTHH)*DRDT(2)*DRDT(2)	FIT	37
1	+Z(NPZPHH)*DRDT(3)*DRDT(3)	FIT	38
1	+2.0*(Z(NPZRTH)*DRDT(1)*DRDT(2)	FIT	39
1	+Z(NPZRPH)*DRDT(1)*DRDT(3)	FIT	40
1	+Z(NPZTHPH)*DRDT(2)*DRDT(3) )	FIT	41
C		FIT	42
C	THE STATEMENTS FROM HERE TO 'END FIT' IMPLEMENT THE	FIT	43
C	PARABOLIC FITS IN EQUATIONS J.1 AND U.3 OF THE TEXT.	FIT	44
C		FIT	45
	IF(IENTRY.NE.2) GO TO 30	FIT	46
	SMT=0.	FIT	47
	IF(D2Z.NE.0.) SMT=0.5*ZDOT*ZDOT/D2Z	FIT	48
C	USE FIT U.3 AT THE PREVIOUS POINT OF RAY PATH	FIT	49
	OSMT=0.	FIT	50
	IF(D2Z.NE.0.) OSMT=0.5*ZDOLD*ZDOLD/D2Z	FIT	51
	GO TO 2000	FIT	52
C		FIT	53
C	IMPLEMENTATION OF FIT FOR EQUATION J.1	FIT	54
C		FIT	55
30	IF(IENTRY.EQ.3) GO TO 1000	FIT	56
	ZDOTM=.5*(ZDOT+ZDOLD)	FIT	57
C	IMPLEMENT TESTS OF EQUATIONS J.2 AND J.3	FIT	58
	IF(ABS(ZDOTM).LE..05*ABS(ZDOT)) GO TO 1000	FIT	59
	FCTR=(Z(NZ)-ZOLD)*DTI/ZDOTM	FIT	60
	D2Z=FCTR*D2Z	FIT	61
	ZDOT=FCTR*ZDOT	FIT	62
C	END FIT	FIT	63
C		FIT	64
C	COMMON CODE FOR FIT AND FIT3	FIT	65
1000	RAD=ZDOT*ZDOT-2.0*Z(NZ)*D2Z	FIT	66
	RAD1=SQRT(AMAX1(RAD,0.0))	FIT	67
C		FIT	68
2000	CONTINUE	FIT	69
C		FIT	70
	END	FIT	71
	FUNCTION GET1(Z)	GET	14
C	FUNCTIONALLY THE SAME AS 'GET' PROGRAM, SEE DOCUMENTATION THERE	GET	15
C	NEEDED BECAUSE RECEIVER MODELS WILL CALL GET TO OBTAIN TERRAIN VA	GET	16
C	BUT THEY THEMSELVES ARE CALLED VIA GET. HENCE HAVE RE-ENTRANCE	GET	17
C	PROBLEM.	GET	18
C		GET	19
	REAL Z(*)	GET	20

	REAL PF(10),PG(10)	GET 21
C	COMMON DECK "RKAM" INSERTED HERE	RKAMCOM2
	REAL KR,KTH,KPH	RKAMCOM4
	COMMON//R,TH,PH,KR,KTH,KPH,RKVAR(14),TPULSE,CSTEP,DRDT(20)	RKAMCOM5
C	COMMON DECK "FNDR" INSERTED HERE	CFNDR 2
	COMMON/FNDR/NZ,NPZR,NPZRR,NPZRTH,NPZRPH,NPZTH,NPZPH,NPZTHTH	CFNDR 4
	COMMON/FNDR/NPZPHPH,NPZTHPH,NSELECT,NTIME	CFNDR 5
C	COMMON DECK "RR" INSERTED HERE	CRR 2
	REAL MODREC	CRR 4
	COMMON/RR/ MODREC(4)	CRR 5
	COMMON/RR/F,PFR,PFRR,PFRTTH,PFRRPH	CRR 6
	COMMON/RR/PFTH,PFPH,PFTHTH,PFPHPH,PFTHPH,FSELECT,FTIME	CRR 7
C	COMMON DECK "GG" INSERTED HERE	CGG 2
	REAL MODG	CGG 4
	COMMON/GG/MODG(4)	CGG 5
	COMMON/GG/G,PGR,PGRR,PGRTH,PGRPH	CGG 6
	COMMON/GG/PGTH,PGPH,PGTHTH,PGPHPH,PGTHPH,GSELECT,GTIME	CGG 7
C	COMMON DECK "RKTIME" INSERTED HERE	CRKTIME2
	COMMON/CRKTIME/RKTIME	CRKTIME4
C		GET 27
C	COMMON DECK "RMACH" INSERTED HERE	CRMACH 2
	COMMON/CRMACH/RMACH(5)	CRMACH 4
	EQUIVALENCE(RKTIME,IRKTIME)	GET 29
C	COMMON DECK "WWR" INSERTED HERE	CWWR 2
	PARAMETER (NWARSZ=1000)	CWW1 3
	COMMON/WW/ID(10),MAXW,W(NWARSZ)	CWW1 4
	REAL MAXSTP,MAXERR,INTYP,LLAT,LLON	CWW2 2
	EQUIVALENCE (EARTH,W(1)),(RAY,W(2)),(XMTRH,W(3)),(TLAT,W(4)),	CWW2 3
	1 (TLON,W(5)),(OW,W(6)),(FBEG,W(7)),(FEND,W(8)),(FSTEP,W(9)),	CWW2 4
	2 (AZ1,W(10)),(AZBEG,W(11)),(AZEND,W(12)),(AZSTEP,W(13)),	CWW2 5
	3 (BETA,W(14)),(ELBEG,W(15)),(ELEND,W(16)),(ELSTEP,W(17)),	CWW2 6
	8 (RCVRH,W(20)),	CWW2 7
	4 (ONLY,W(21)),(HOP,W(22)),(MAXSTP,W(23)),(PLAT,W(24)),(PLON,W(25))	CWW2 8
	5,(HMAX,W(26)),(RAYFNC,W(29)),(EXTINC,W(33)),	CWW2 9
	6 (HMIN,W(27)),(RGMAX,W(28)),	CWW2 10
	8 (INTYP,W(41)),(MAXERR,W(42)),(ERATIO,W(43)),	CWW2 11
	6 (STEP1,W(44)),(STPMAX,W(45)),(STPMIN,W(46)),(FACTR,W(47)),	CWW2 12
	7 (SKIP,W(71)),(RAYSET,W(72)),(PRTSRP,W(74)),(HITLET,W(75))	CWW2 13
	9 ,(BINRAY,W(76)),(PAGLN,W(77)),(PLT,W(81)),(PFACTR,W(82)),	CWW2 14
	1 (LLAT,W(83)),(LLON,W(84)),(RLAT,W(85)),(RLON,W(86))	CWW2 15
	2,(TIC,W(87)),(HB,W(88)),(HT,W(89)),(TICV,W(96))	CWW2 16
C		GET 31
	COMMON/CGET/ZERO	GET 32
C		GET 33
	IENTRY=1	GET 34
	GO TO 5	GET 35
C		GET 36
	ENTRY DOT1(Z)	GET 37
	IENTRY=2	GET 38
5	CONTINUE	GET 39
	IF(ZERO.EQ.0.0) ZERO=EARTH*RMACH(3)*2.0	GET 40
C		GET 41
	IF(ITEST(Z(NTIME)).EQ.IRKTIME) GO TO 10	GET 42
C		GET 43
	IF(Z(NSELECT).EQ.FSELECT) CALL RECEIVER	GET 44

	IF(Z(NSELECT).EQ.GSELECT) CALL TOPOG	GET	45
	Z(NTIME)=RKTIME	GET	46
C	REMOVE MACHINE ROUND OFF NOISE FROM EXACT RECEIVER LOCATIONS	GET	47
	IF(ABS(Z(NZ)).LE.ZERO) Z(NZ)=0.0	GET	48
C		GET	49
10	IF(IENTRY.NE.1) GO TO 20	GET	50
	GET1=Z(NZ)	GET	51
	RETURN	GET	52
C		GET	53
20	GET1=Z(NPZR)*DRDT(1)+Z(NPZTH)*DRDT(2)+Z(NPZPH)*DRDT(3)	GET	54
	RETURN	GET	55
	ENTRY GETST1(Z)	GET	56
C		GET	57
C	FORCE LOAD THE GET ROUTINE	GET	58
	CALL GET	GET	59
	END	GET	60
	FUNCTION GET(Z)	GET	61
C	'GET' AND ENTRY 'DOT' PROVIDE A CONTROL METHOD FOR AVOIDING	GET	62
C	REDUNDANT CALLS TO THE TERRAIN AND RECEIVER MODELS. THE VALUES	GET	63
C	RETURNED ARE THE FUNCTION VALUES FOR 'F' OR 'G' OR THEIR DERIVATI	GET	64
C	(VIA 'DOT' ENTRY). UNNECESSARY CALLS ARE ELIMINATED THROUGH USE	GET	65
C	OF 'TIME OF CALL' VARIABLES WHICH ARE COMPARED WITH THE CURRENT	GET	66
C	LAST CALL TIME MAINTAINED BY THE 'RKAM' PROGRAM. WHEN VALUES ARE	GET	67
C	NOT CURRENT THEY ARE UPDATED BY CALLS TO THE APPROPRIATE ROUTINES	GET	68
C		GET	69
	REAL Z(*),PF(10),PG(10)	GET	70
C	COMMON DECK "RKAM" INSERTED HERE	RKAMCOM2	
	REAL KR,KTH,KPH	RKAMCOM4	
	COMMON//R,TH,PH,KR,KTH,KPH,RKVAR(14),TPULSE,CSTEP,DRDT(20)	RKAMCOM5	
C	COMMON DECK "FNDR" INSERTED HERE	CFNDR 2	
	COMMON/FNDR/NZ,NPZR,NPZRR,NPZRTH,NPZRPH,NPZTH,NPZPH,NPZTHTH	CFNDR 4	
	COMMON/FNDR/NPZPHPH,NPZTHPH,NSELECT,NTIME	CFNDR 5	
C	COMMON DECK "RR" INSERTED HERE	CRR 2	
	REAL MODREC	CRR 4	
	COMMON/RR/ MODREC(4)	CRR 5	
	COMMON/RR/F,PFR,PFRR,PFRTH,PFRPH	CRR 6	
	COMMON/RR/PFTH,PFPH,PFTHTH,PFPHPH,PFTHPH,FSELECT,FTIME	CRR 7	
C	COMMON DECK "GG" INSERTED HERE	CGG 2	
	REAL MODG	CGG 4	
	COMMON/GG/MODG(4)	CGG 5	
	COMMON/GG/G,PGR,PGRR,PGRTH,PGRPH	CGG 6	
	COMMON/GG/PGTH,PGPH,PGTHTH,PGPHPH,PGTHPH,GSELECT,GTIME	CGG 7	
C	COMMON DECK "RKTIME" INSERTED HERE	CRKTIME2	
	COMMON/CRKTIME/RKTIME	CRKTIME4	
C		GET	76
C	COMMON DECK "RMACH" INSERTED HERE	CRMACH 2	
	COMMON/CRMACH/RMACH(5)	CRMACH 4	
	EQUIVALENCE(RKTIME,IRKTIME)	GET	78
C		GET	79
C	COMMON DECK "WWR" INSERTED HERE	CWWR 2	

	PARAMETER (NWARSZ=1000)		
	COMMON/WW/ID(10),MAXW,W(NWARSZ)	CWW1	3
	REAL MAXSTP,MAXERR,INTYP,LLAT,LLON	CWW1	4
	EQUIVALENCE (EARTH, W(1)), (RAY, W(2)), (XMTRH, W(3)), (TLAT, W(4)),	CWW2	2
	1 (TLON, W(5)), (OW, W(6)), (FBEG, W(7)), (FEND, W(8)), (FSTEP, W(9)),	CWW2	3
	2 (AZ1, W(10)), (AZBEG, W(11)), (AZEND, W(12)), (AZSTEP, W(13)),	CWW2	4
	3 (BETA, W(14)), (ELBEG, W(15)), (ELEND, W(16)), (ELSTEP, W(17)),	CWW2	5
	8 (RCVRH, W(20)),	CWW2	6
	4 (ONLY, W(21)), (HOP, W(22)), (MAXSTP, W(23)), (PLAT, W(24)), (PLON, W(25))	CWW2	7
	5, (HMAX, W(26)), (RAYFNC, W(29)), (EXTINC, W(33)),	CWW2	8
	6 (HMIN, W(27)), (RGMX, W(28)),	CWW2	9
	8 (INTYP, W(41)), (MAXERR, W(42)), (ERATIO, W(43)),	CWW2	10
	6 (STEP1, W(44)), (STPMAX, W(45)), (STPMIN, W(46)), (FACTR, W(47)),	CWW2	11
	7 (SKIP, W(71)), (RAYSET, W(72)), (PRTSRP, W(74)), (HITLET, W(75)),	CWW2	12
	9, (BINRAY, W(76)), (PAGLN, W(77)), (PLT, W(81)), (PFACTR, W(82)),	CWW2	13
	1 (LLAT, W(83)), (LLON, W(84)), (RLAT, W(85)), (RLON, W(86))	CWW2	14
	2, (TIC, W(87)), (HB, W(88)), (HT, W(89)), (TICV, W(96))	CWW2	15
C		CWW2	16
	COMMON/CGET/ZERO	GET	81
C		GET	82
	EQUIVALENCE (PF, PFR), (PG, PGR)	GET	83
	DATA PF, PG/1.0, 9*0.0, 1.0, 9*0.0/	GBL	2
	DATA NZ, NPZR, NPZRR, NPZPTH, NPZPH, NPZTH, NPZPH, NPZTH, NPZTH	GBL	3
	1, NPZPH, NPZTH, NSELECT, NTIME	GBL	4
	2 /1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12/	GBL	5
	DATA FTIME, GTIME, FSELECT, GSELECT/2*-1.0, 8HRECEIVER, 7HTERRAIN /	GBL	6
	DATA ZERO/0.0/	GBL	7
C		GBL	8
	IENTRY=1	GET	86
	GO TO 5	GET	87
C		GET	88
	ENTRY DOT(Z)	GET	89
	IENTRY=2	GET	90
5	CONTINUE	GET	91
	IF(ZERO.EQ.0.0) ZERO=EARTH*RMACH(3)*2.0	GET	92
C		GET	93
	IF(ITEST(Z(NTIME)).EQ.IRKTIME) GO TO 10	GET	94
C		GET	95
	IF(Z(NSELECT).EQ.FSELECT) CALL RECEIVER	GET	96
	IF(Z(NSELECT).EQ.GSELECT) CALL TOPOG	GET	97
	Z(NTIME)=RKTIME	GET	98
C		GET	99
	REMOVE MACHINE ROUND OFF NOISE FROM EXACT RECEIVER LOCATIONS	GET	100
	IF(ABS(Z(NZ)).LE.ZERO) Z(NZ)=0.0	GET	101
C		GET	102
10	IF(IENTRY.NE.1) GO TO 20	GET	103
	GET=Z(NZ)	GET	104
	RETURN	GET	105
C		GET	106
20	GET=Z(NPZR)*DRDT(1)+Z(NPZTH)*DRDT(2)+Z(NPZPH)*DRDT(3)	GET	107
	RETURN	GET	108
	ENTRY DFCNCL(Z)	GET	109
C		GET	110
C	FORCE LOAD THE MACHINE DEPENDENT CONSTANTS(SEE MODULE 'DFCNST')	GET	111
C		GET	112
	CALL DFCNST	GET	113

END

GET 114

	FUNCTION ITEST(I)	ITEST 2
C	USED TO PASS INTEGER VALUES THROUGH FOR VARIABLES TYPED REAL	ITEST 3
C	(AS IN MIXED REAL/INTEGER ARRAYS)	ITEST 4
	ITEST=I	ITEST 5
	END	ITEST 6
	SUBROUTINE CONBLK	CONBLK 3
C	DATA INITIALIZATION AND FILE OPENING SERVICE ROUTINE	CONBLK 4
C		CONBLK 5
C	COMMON DECK "HDR" INSERTED HERE	CHDR 2
	CHARACTER*10 INITID*80,DAT,TOD	CHDR 4
	COMMON/HDR/SEC	CHDR 5
	COMMON/HDRC/INITID,DAT,TOD	CHDR 6
C		CONBLK 9
C	COMMON DECK "CPROCFL" INSERTED HERE	CPROCFL2
	INTEGER PMX,PNTBL,PITBL,PFRMTBL,IDSP(10)	CPROCFL4
C	PARAMETER DECK "PGROUPS"	PGROUPS2
	PARAMETER (NCHPG1=11,NWPV=250,NSPGP=NCHPG1+2*NWPV+1)	PGROUPS3
	PARAMETER (MNGRP=9,MXGRP=69,MXLIST=MXGRP-MNGRP+2)	PGROUPS4
	COMMON/PROCFL/LIST(MXLIST)	CPROCFL6
	COMMON/PROCFL/PMX,PNTBL(10),PITBL(10),PFRMTBL(10),PGP(NSPGP)	CPROCFL7
	EQUIVALENCE (PGP,IDSP)	CPROCFL8
C	COMMON DECK "CC" INSERTED HERE	CCC 2
	REAL MODC	CCC 4
	COMMON/CC/MODC(4),CS,PCST,PCSR,PCSTH,PCSPH	CCC 5
C	COMMON DECK "GG" INSERTED HERE	CGG 2
	REAL MODG	CGG 4
	COMMON/GG/MODG(4)	CGG 5
	COMMON/GG/G,PGR,PGRR,PGRTH,PGRPH	CGG 6
	COMMON/GG/PGTH,PGPH,PGTHTH,PGPHPH,PGTHPH,GSELECT,GTIME	CGG 7
C	COMMON DECK "RR" INSERTED HERE	CRR 2
	REAL MODREC	CRR 4
	COMMON/RR/MODREC(4)	CRR 5
	COMMON/RR/F,PFR,PFRR,PFRTH,PFRPH	CRR 6
	COMMON/RR/PFTH,PFPH,PFTHTH,PFPHPH,PFTHPH,FSELECT,FTIME	CRR 7
C	COMMON DECK "TT" INSERTED HERE	CTT 2
	REAL MODT	CTT 4
	COMMON/TT/MODT(4),T,PTT,PTR,PTTH,PTPH	CTT 5
C	COMMON DECK "UU" INSERTED HERE	CUU 2
	REAL MODU	CUU 4
	COMMON/UU/MODU(4)	CUU 5
	1 ,V ,PVT ,PVR ,PVTH ,PVPH	CUU 6
	2 ,VR ,PVRT ,PVRR ,PVRTH ,PVRPH	CUU 7
	3 ,VTH ,PVTHTH ,PVTHR ,PVTHTH ,PVTHPH	CUU 8
	4 ,VPH ,PVPHT ,PVPHR ,PVPHTH ,PVPHPH	CUU 9

C		CONBLK16
C	COMMON DECK "RAYDEV" INSERTED HERE	CRAYDEV2
C	DEVICE ASSIGNED TO RAYTRC INPUT FILE	CRAYDEV4
	COMMON/RAYDEV/NRYIND,NDEVTMP,NFRMAT,NDEVGRP,NDEVBIN	CRAYDEV5
C	COMMON DECK "CUCON" INSERTED HERE	CUCON 2
	COMMON/UCONV/CNVV(4,4)	CUCON 4
	CHARACTER PCV*3,CNVC*2	CUCON 5
	COMMON/UCONC/PCV(4),CNVC(4,4)	CUCON 6
C		CONBLK19
C	COMMON DECK "SS" INSERTED HERE	CSS 2
	REAL MODSURF	CSS 4
	COMMON/SS/ MODSURF(4)	CSS 5
	COMMON/SS/U,PUR,PURR,PURTH,PURPH	CSS 6
	COMMON/SS/PUTH,PUPH,PUTHTH,PUPHPH,PUTHPH,USELECT,UTIME	CSS 7
C	COMMON DECK "CONST" INSERTED HERE	CCONST 2
	COMMON/PCONST/CREG,RGAS,GAMMA	CCONST 4
	COMMON/MCONST/PI,PIT2,PID2,DEGS,RAD,ALN10	CCONST 5
C	COMMON DECK "WWR" INSERTED HERE	CWWR 2
	PARAMETER (NWARSZ=1000)	CWW1 3
	COMMON/WW/ID(10),MAXW,W(NWARSZ)	CWW1 4
	REAL MAXSTP,MAXERR,INTYP,LLAT,LLON	CWW2 2
	EQUIVALENCE (EARTH,W(1)),(RAY,W(2)),(XMTRH,W(3)),(TLAT,W(4)),	CWW2 3
	1 (TLON,W(5)),(OW,W(6)),(FBEG,W(7)),(FEND,W(8)),(FSTEP,W(9)),	CWW2 4
	2 (AZ1,W(10)),(AZBEG,W(11)),(AZEND,W(12)),(AZSTEP,W(13)),	CWW2 5
	3 (BETA,W(14)),(ELBEG,W(15)),(ELEND,W(16)),(ELSTEP,W(17)),	CWW2 6
	8 (RCVRH,W(20)),	CWW2 7
	4 (ONLY,W(21)),(HOP,W(22)),(MAXSTP,W(23)),(PLAT,W(24)),(PLON,W(25))	CWW2 8
	5,(HMAX,W(26)),(RAYFNC,W(29)),(EXTINC,W(33)),	CWW2 9
	6 (HMIN,W(27)),(RGMX,W(28)),	CWW2 10
	8 (INTYP,W(41)),(MAXERR,W(42)),(ERATIO,W(43)),	CWW2 11
	6 (STEP1,W(44)),(STPMX,W(45)),(STPMIN,W(46)),(FACTR,W(47)),	CWW2 12
	7 (SKIP,W(71)),(RAYSET,W(72)),(PRTSRP,W(74)),(HITLET,W(75))	CWW2 13
	9 ,(BINRAY,W(76)),(PAGLN,W(77)),(PLT,W(81)),(PFACTR,W(82)),	CWW2 14
	1 (LLAT,W(83)),(LLON,W(84)),(RLAT,W(85)),(RLON,W(86))	CWW2 15
	2,(TIC,W(87)),(HB,W(88)),(HT,W(89)),(TICV,W(96))	CWW2 16
C	COMMON DECK "B9" INSERTED HERE	CB8 2
	INTEGER GMX,GNTBL,GITBL,GFRMTBL,IDSG(10)	CB8 4
	COMMON/B9/GMX,GNTBL(10),GITBL(10),GFRMTBL(10),GGP(113)	CB8 5
	EQUIVALENCE (GGP,IDSG),(ANG,GGP(11))	CB8 6
C	COMMON DECK "B2" INSERTED HERE	CB2 2
	INTEGER DUMX,DUNTBL,DUITBL,DUFRMTB,IDSU(10)	CB2 4
	COMMON/B2/DUMX,DUNTBL(10),DUITBL(10),DUFRMTB(10),DUGP(10)	CB2 5
	EQUIVALENCE (DUGP,IDSU)	CB2 6
C	COMMON DECK "B4" INSERTED HERE	CB4 2
	INTEGER DCMX,DCNTBL,DCITBL,DCFRMTB,IDSDC(10)	CB4 4
	COMMON/B4/DCMX,DCNTBL(10),DCITBL(10),DCFRMTB(10),DCGP(10)	CB4 5
	EQUIVALENCE (DCGP,IDSDC)	CB4 6
C	COMMON DECK "B6" INSERTED HERE	CB6 2
	INTEGER DTMX,DTNTBL,DTITBL,DTFRMTB,IDSDT(10)	CB6 4
	COMMON/B6/DTMX,DTNTBL(10),DTITBL(10),DTFRMTB(10),DTGP(10)	CB6 5
	EQUIVALENCE (DTGP,IDSDT)	CB6 6
C	COMMON DECK "B1" INSERTED HERE	CB1 2
	INTEGER UMX,UNTBL,UITBL,UFRMTBL,IDSU(10)	CB1 4
	COMMON/B1/UMX,UNTBL(10),UITBL(10),UFRMTBL(10),UGP(10)	CB1 5
	EQUIVALENCE (UGP,IDSU)	CB1 6

C	COMMON DECK "B3" INSERTED HERE	CB3	2
	INTEGER CMX,CNTBL,CITBL,CFRMTBL,IDSC(10)	CB3	4
	COMMON/B3/CMX,CNTBL(10),CITBL(10),CFRMTBL(10),CGP(512)	CB3	5
	EQUIVALENCE (CGP,IDSC),(ANC,CGP(11))	CB3	6
C	COMMON DECK "B5" INSERTED HERE	CB5	2
	INTEGER TMX,TNTBL,TITBL,TFRMTBL,IDST(10)	CB5	4
	COMMON/B5/TMX,TNTBL(10),TITBL(10),TFRMTBL(10),TGP(262)	CB5	5
	EQUIVALENCE (TGP,IDST),(ANT,TGP(11))	CB5	6
C	COMMON DECK "B7" INSERTED HERE	CB7	2
	INTEGER MMX,MNTBL,MITBL,MFRMTBL,IDSM(10)	CB7	4
	REAL MGP	CB7	5
	COMMON/B7/MMX,MNTBL(10),MITBL(10),MFRMTBL(10),MGP(10)	CB7	6
	EQUIVALENCE (MGP,IDSM)	CB7	7
C	COMMON DECK "RINPLEX" INSERTED HERE	CRINPLE2	
	REAL KAY2,KAY2I	CRINPLE4	
	COMPLEX PNP,POLAR,LPOLAR	CRINPLE5	
	LOGICAL SPACE	CRINPLE6	
	CHARACTER DISPM*6	CRINPLE7	
	COMMON/RINPL/DISPM	CRINPLE8	
	COMMON /RIN/ MODRIN(8),RAYNAME(2,3),TYPE(3),SPACE	CRINPLE9	
	COMMON/RIN/OMEGMIN,OMEGMAX,KAY2,KAY2I	CRINPL10	
	COMMON/RIN/PNP(10),POLAR,LPOLAR,SGN	CRINPL11	
C	COMMON DECK "MM" INSERTED HERE	CMM	2
	REAL M,MODM	CMM	4
	COMMON/MM/MODM(4),M,PMT,PMR,PMTH,PMPH	CMM	5
C	COMMON DECK "PP" INSERTED HERE	CPP	2
	REAL MODP	CPP	4
	COMMON/PP/MODP(4),P,PPT,PPR,PPTH,PPPH	CPP	5
C	COMMON DECK "AA" INSERTED HERE	CAA	2
	REAL MODA	CAA	4
	REAL MU,MUPT,MUPR,MUPTH,MUPPH	CAA	5
	REAL KAP,KAPPT,KAPPR,KAPPTH,KAPPPH	CAA	6
	COMMON/AA/MODA(4),MU,MUPT,MUPR,MUPTH,MUPPH	CAA	7
	COMMON/AA/KAP,KAPPT,KAPPR,KAPPTH,KAPPPH	CAA	8
C	COMMON DECK "FLAG" INSERTED HERE	CFLAG	2
	LOGICAL NEWWR,NEWWP,NEWTRC,PENET	CFLAG	4
	COMMON /FLG/ NTYP,NEWWR,NEWWP,NEWTRC,PENET,LINES,IHOP,HPUNCH	CFLAG	5
	COMMON/FLGP/NSET	CFLAG	6
C	COMMON DECK "RKTIME" INSERTED HERE	CRKTIME2	
	COMMON/CRKTIME/RKTIME	CRKTIME4	
C		CONBLK37	
C	COMMON/RAYCON/MCONP	CONBLK38	
C		CONBLK39	
C	EQUIVALENCE (RKTIME,IRKTIME)	CONBLK40	
C		CONBLK41	
C	COMMON DECK "B10" INSERTED HERE	CB9	2
	INTEGER DGMX,DGNTBL,DGITBL,DGFRMTB,IDSDG(10)	CB9	4
	COMMON/B10/DGMX,DGNTBL(10),DGITBL(10),DGFRMTB(10),DGPP(10)	CB9	5
	EQUIVALENCE (DGPP,IDSDG)	CB9	6
C	COMMON DECK "B8" INSERTED HERE	CB10	2
	INTEGER RMX,RNTBL,RITBL,RFRMTBL,IDSR(10)	CB10	4
	COMMON/B8/RMX,RNTBL(10),RITBL(10),RFRMTBL(10),RGP(10)	CB10	5
	EQUIVALENCE (RGP,IDSR)	CB10	6
C	COMMON DECK "CB17" INSERTED HERE	CB17	2
	INTEGER VMX,VNTBL,VITBL,VFRMTBL,IDSV(10)	CB17	4

	COMMON/B17/VMX,VNTBL(10),VITBL(10),VFRMTBL(10),VGP(53)	CB17	5
	EQUIVALENCE (VGP,IDSU),(ANV,VGP(11))	CB17	6
C	COMMON DECK "CB18" INSERTED HERE	CB18	2
	INTEGER DVMX,DVNTBL,DVITBL,DVFRMTB,IDSU(10)	CB18	4
	COMMON/B18/DVMX,DVNTBL(10),DVITBL(10),DVFRMTB(10),DVGP(11)	CB18	5
	EQUIVALENCE (DVGP,IDSU),(ANDV,DVGP(11))	CB18	6
C	COMMON DECK "CB19" INSERTED HERE	CB19	2
	INTEGER PRMX,PRNTBL,PRITBL,PRFRMTB,IDSPR(10)	CB19	4
	COMMON/B19/PRMX,PRNTBL(10),PRITBL(10),PRFRMTB(10),PRGP(11)	CB19	5
	EQUIVALENCE (PRGP,IDSPR),(ANP,PRGP(11))	CB19	6
C	COMMON DECK "CB20" INSERTED HERE	CB20	2
	INTEGER DPMX,DPNTBL,DPITBL,DPFRMTB,IDSU(10)	CB20	4
	COMMON/B20/DPMX,DPNTBL(10),DPITBL(10),DPFRMTB(10),DPGP(11)	CB20	5
	EQUIVALENCE (DPGP,IDSU),(ANDP,DPGP(11))	CB20	6
	REAL KVECT(22)	CONBLK48	
	REAL VSET(20)	CONBLK49	
	EQUIVALENCE (KVECT,KAY2),(VSET,V)	CONBLK50	
C		CONBLK51	
	DATA KVECT/22*0.0/	CONBLK52	
	DATA RAYNAME/6*1H /	CONBLK53	
	DATA VSET/20*0.0/	CONBLK54	
	DATA OMEGMIN,OMEGMAX/0.0,0.0/	CONBLK55	
	DATA POLAR,LPOLAR/(0.0,0.0),(1.0,0.0)/	CONBLK56	
C		CONBLK57	
	DATA IRKTIME/0/	CONBLK58	
	DATA MCONP/0/	CONBLK59	
	DATA CREF,GAMMA,RGAS/1.0,1.4,8.31436E-3/	CONBLK60	
	DATA NRYIND,NDEVTMP,NFRMAT,NDEVGRP,NDEVBIN/8,4,0,10,11/	CONBLK61	
	DATA PCV/'AN','LN','FQ',' ' /	CONBLK62	
	DATA CNVC/'RD','KM','RD',' ' /	CONBLK63	
1	,'DG','M','HZ',' ' /	CONBLK64	
2	,'KM','FT','KH',' ' /	CONBLK65	
3	,' ','NM','DG',' ' /	CONBLK66	
	DATA CNVV /16*1.0 /	CONBLK67	
C		CONBLK68	
	DATA IDSDC,IDSU,IDSU,ISDC,ISDM,ISU,ISU,ISG/80*1H /	CONBLK69	
	DATA IDSDG,IDSU,IDSU,ISPR,ISU,ISU,ISU/60*1H /	CONBLK70	
	DATA MODG/7HNO MODL,0.0,7HNO MODL,0.0/	CONBLK71	
	DATA MODREC/7HNO MODL,0.0,7HNO MODL,0.0/	CONBLK72	
	DATA MODC/7HNO MODL,0.0,7HNO MODL,0.0/	CONBLK73	
	DATA MODM/7HNO MODL,0.0,7HNO MODL,0.0/	CONBLK74	
	DATA MODT/7HNO MODL,0.0,7HNO MODL,0.0/	CONBLK75	
	DATA MODU/7HNO MODL,0.0,7HNO MODL,0.0/	CONBLK76	
	DATA MODC/7HNO MODL,0.0,7HNO MODL,0.0/	CONBLK77	
	DATA MODT/7HNO MODL,0.0,7HNO MODL,0.0/	CONBLK78	
	DATA MODM/7HNO MODL,0.0,7HNO MODL,0.0/	CONBLK79	
	DATA MODP/7HNO MODL,0.0,7HNO MODL,0.0/	CONBLK80	
	DATA MODA/7HNO MODL,0.0,7HNO MODL,0.0/	CONBLK81	
C		CONBLK82	
	RETURN	CONBLK91	
C		CONBLK92	
	ENTRY STDINI	CONBLK93	
	CALL OPNREP(NDEVTMP,'TAPE4')	CONBLK94	
	CALL OPNURP(NDEVBIN,'TAPE6')	CONBLK95	
	CALL OPNREP(9,'PUNCH')	CONBLK96	

C	ENTRY STDINT	CONBLK97
	OPEN(UNIT=NRYIND,FILE='DINP',STATUS='OLD',ERR=1000)	CONBLK98
	REWIND NRYIND	CONBLK99
	CALL OPNREP(2,'OUTPUT')	CONBL100
	CALL OPNREP(3,'DOUTP')	CONBL101
	CALL OPNURP(NDEVGRP,'TAPE5')	CONBL102
C		CONBL103
C	TEMPORARY WE HOPE, TO MAKE CRAY VERSION WORK	CONBL104
	FSELECT=8HRECEIVER	CONBL105
	GSELECT=7HTERRAIN	CONBL106
C	INITIALIZE RAYSET FILE	CONBL107
	READ(NRYIND,'(A)',END=1000) INITID	CONBL108
	CALL SETW	CONBL109
	CALL SYSDAT(DAT)	CONBL110
	CALL SYSTIM(TOD)	CONBL111
	CALL SYSSEC(SEC)	CONBL112
C	INITIALIZE POINT MODEL LIST	CONBL113
	LIST(1)=1	CONBL114
	LIST(2)=0	CONBL115
C	FILL FORMAT CONTROL ARRAYS	CONBL116
	PNTBL(1)=1	CONBL117
C	ALLOW FOR AN 80 CHARACTER IDENT STRING(A8)	CONBL118
	PNTBL(2)=NCHPG1	CONBL119
C	ALLOW MAXIMUM 250 WORD PER VARIABLE	CONBL120
	PITBL(2)=NWPV	CONBL121
C	FOR BOTH X AND Y PLUS 1 FOR NUMBER OF VARIABLES	CONBL122
	PNTBL(3)=NSPGP	CONBL123
	RETURN	CONBL124
1000	STOP 'DINP FORMAT ERROR'	CONBL125
	END	CONBL126
		CONBL127

	LOGICAL FUNCTION WCHANGE(W1,W2)	
	REAL W1(400),W2(400)	WCHANGE2
C		WCHANGE3
C	WCHANGE PROVIDES A TEST AGAINST TWO W-ARRAYS	WCHANGE4
C	IF BOTH WOULD PRODUCE THE SAME SET OF RAYS BY RAYTRC THEN RESULT	WCHANGE5
C	IS <FALSE>.	WCHANGE6
C		WCHANGE7
	INTEGER NDX(8)	WCHANGE8
C		WCHANGE9
	DATA NGRPS,NDX/8, 1,17, 21,26, 41,47, 100,399/	WCHANG10
C		WCHANG11
	WCHANGE=.FALSE.	WCHANG12
	DO 20 N=1,NGRPS,2	WCHANG13
	N1=NDX(N)	WCHANG14
	N2=NDX(N+1)	WCHANG15
	DO 20 I=N1,N2	WCHANG16
	WCHANGE=W1(I).NE.W2(I)	WCHANG17
	IF(WCHANGE) RETURN	WCHANG18
20	CONTINUE	WCHANG19
		WCHANG20



	PARAMETER (LRKAMS=87+2*100,NXRKMS=12+LRKAMS,MXEQPT=21)	CRK	5
	PARAMETER (NRKSAV=NXRKMS+MXEQPT-1)	CRK	6
	COMMON /RK/ NEQS,STEP,MODE,ELMAX,ELMIN,E2MAX,E2MIN,FACT,RSTART	CRK	7
C	COMMON DECK "CERR" INSERTED HERE	CERR	2
	COMMON/ERR/NERG,NERR,NERT,NERP	CERR	3
C	COMMON DECK "GG" INSERTED HERE	CGG	2
	REAL MODG	CGG	4
	COMMON/GG/MODG(4)	CGG	5
	COMMON/GG/G,PGR,PGRR,PGRTH,PGRPH	CGG	6
	COMMON/GG/PGTH,PGPH,PGTHTH,PGPHPH,PGTHPH,GSELECT,GTIME	CGG	7
C	COMMON DECK "CONST" INSERTED HERE	CCONST	2
	COMMON/PCONST/CREF,RGAS,GAMMA	CCONST	4
	COMMON/MCONST/PI,PIT2,PID2,DEGS,RAD,ALN10	CCONST	5
C	COMMON DECK "FLAG" INSERTED HERE	CFLAG	2
	LOGICAL NEWWR,NEWWP,NEWTRC,PENET	CFLAG	4
	COMMON /FLG/ NTYP,NEWWR,NEWWP,NEWTRC,PENET,LINES,IHOP,HPUNCH	CFLAG	5
	COMMON/FLGP/NSET	CFLAG	6
C	COMMON DECK "RINPLEX" INSERTED HERE	CRINPLE2	
	REAL KAY2,KAY2I	CRINPLE4	
	COMPLEX PNP,POLAR,LPOLAR	CRINPLE5	
	LOGICAL SPACE	CRINPLE6	
	CHARACTER DISPM*6	CRINPLE7	
	COMMON/RINPL/DISPM	CRINPLE8	
	COMMON /RIN/ MODRIN(8),RAYNAME(2,3),TYPE(3),SPACE	CRINPLE9	
	COMMON/RIN/OMEGMIN,OMEGMAX,KAY2,KAY2I	CRINPL10	
	COMMON/RIN/PNP(10),POLAR,LPOLAR,SGN	CRINPL11	
C	COMMON DECK "RKAM" INSERTED HERE	RKAMCOM2	
	REAL KR,KTH,KPH	RKAMCOM4	
	COMMON//R,TH,PH,KR,KTH,KPH,RKVAR(14),TPULSE,CSTEP,DRDT(20)	RKAMCOM5	
C	COMMON DECK "WW" INSERTED HERE	CWW	2
	PARAMETER (NWARSZ=1000)	CWW1	3
	COMMON/WW/ID(10),MAXW,W(NWARSZ)	CWW1	4
	REAL MAXSTP,MAXERR,INTYP,LLAT,LLON	CWW2	2
	EQUIVALENCE (EARTH,W(1)),(RAY,W(2)),(XMTRH,W(3)),(TLAT,W(4)),	CWW2	3
	1 (TLON,W(5)),(OW,W(6)),(FBEG,W(7)),(FEND,W(8)),(FSTEP,W(9)),	CWW2	4
	2 (AZ1,W(10)),(AZBEG,W(11)),(AZEND,W(12)),(AZSTEP,W(13)),	CWW2	5
	3 (BETA,W(14)),(ELBEG,W(15)),(ELEND,W(16)),(ELSTEP,W(17)),	CWW2	6
	8 (RCVRH,W(20)),	CWW2	7
	4 (ONLY,W(21)),(HOP,W(22)),(MAXSTP,W(23)),(PLAT,W(24)),(PLON,W(25))	CWW2	8
	5,(HMAX,W(26)),(RAYFNC,W(29)),(EXTINC,W(33)),	CWW2	9
	6 (HMIN,W(27)),(RGMAX,W(28)),	CWW2	10
	8 (INTYP,W(41)),(MAXERR,W(42)),(ERATIO,W(43)),	CWW2	11
	6 (STEP1,W(44)),(STPMAX,W(45)),(STPMIN,W(46)),(FACTR,W(47)),	CWW2	12
	7 (SKIP,W(71)),(RAYSET,W(72)),(PRTSRP,W(74)),(HITLET,W(75))	CWW2	13
	9 ,(BINRAY,W(76)),(PAGLN,W(77)),(PLT,W(81)),(PFACTR,W(82)),	CWW2	14
	1 (LLAT,W(83)),(LLON,W(84)),(RLAT,W(85)),(RLON,W(86))	CWW2	15
	2,(TIC,W(87)),(HB,W(88)),(HT,W(89)),(TICV,W(96))	CWW2	16
	REAL MMODEL,MFORM,MID	CWW3	2
C		CWW3	3
C	WIND 100-124	CWW3	4
	EQUIVALENCE (W(100),UMODEL),(W(101),UFORM),(W(102),UID)	CWW3	5
C		CWW3	6
C	DELTA WIND 125-149	CWW3	7
	EQUIVALENCE (W(125),DUMODEL),(W(126),DUFORM),(W(127),DUID)	CWW3	8
C		CWW3	9

C	SOUND SPEED 150-174	CWW3 10
	EQUIVALENCE (W(150),CMODEL), (W(151),CFORM), (W(152),CID)	CWW3 11
	EQUIVALENCE (W(153),REFC)	CWW3 12
C		CWW3 13
C	DELTA SOUND SPEED 175-199	CWW3 14
	EQUIVALENCE (W(175),DCMODEL), (W(176),DCFORM), (W(177),DCID)	CWW3 15
C		CWW3 16
C	TEMPERATURE 200-224	CWW3 17
	EQUIVALENCE (W(200),TMODEL), (W(201),TFORM), (W(202),TID)	CWW3 18
C		CWW3 19
C	DELTA TEMPERATURE 225-249	CWW3 20
	EQUIVALENCE (W(225),DTMODEL), (W(226),DTFORM), (W(227),DTID)	CWW3 21
C		CWW3 22
C	MOLECULAR 250-274	CWW3 23
	EQUIVALENCE (W(250),MMODEL), (W(251),MFORM), (W(252),MID)	CWW3 24
C		CWW3 25
C	RECEIVER HEIGHT 275-299	CWW3 26
	EQUIVALENCE (W(275),RMODEL), (W(276),RFORM), (W(277),RID)	CWW3 27
C		CWW3 28
C	TOPOGRAPHY 300-324	CWW3 29
	EQUIVALENCE (W(300),GMODEL), (W(301),GFORM), (W(302),GID)	CWW3 30
C		CWW3 31
C	DELTA TOPOGRAPHY 325-349	CWW3 32
	EQUIVALENCE (W(325),GUMODEL), (W(326),GUFORM), (W(327),GUID)	CWW3 33
C		CWW3 34
C	UPPER SURFACE TOPOGRAPHY 350-374	CWW3 35
	EQUIVALENCE (W(350),SMODEL), (W(351),SFORM), (W(352),SID)	CWW3 36
C	PLOT ENHANCEMENTS CONTROL PARAMETERS	CWW3 37
C		CWW3 38
	EQUIVALENCE (W(490),XFQMDL), (W(491),YFQMDL)	CWW3 39
C	ABSORPTION 500-524	CWW3 40
	EQUIVALENCE (W(500),AMODEL), (W(501),AFORM), (W(502),AID)	CWW3 41
C		CWW3 42
C	DELTA ABSORPTION 525-549	CWW3 43
	EQUIVALENCE (W(525),DAMODEL), (W(526),DAFORM), (W(527),DAID)	CWW3 44
C		CWW3 45
C	PRESSURE 550-574	CWW3 46
	EQUIVALENCE (W(550),PMODEL), (W(551),PFORM), (W(552),PID)	CWW3 47
C		CWW3 48
C	DELTA PRESSURE 575-599	CWW3 49
	EQUIVALENCE (W(575),DPMODEL), (W(576),DPFORM), (W(577),DPID)	CWW3 50
C		CWW3 51
	EQUIVALENCE (T,TPULSE), (PHI,PH), (TH,THETA)	PRINTR20
	DATA	PRINTR21
2	HEADRS(7)/' PHASE TIME'//,UNITS(7)/' SEC'//	PRINTR22
3	,HEADRS(8)/' ABSORPTION'//,UNITS(8)/' DB'//	PRINTR23
4	,HEADRS(9)/' DOPPLER'//,UNITS(9)/' C/S'//	PRINTR24
5	,HEADRS(10)/' PATH LENGTH'//,UNITS(10)/' KM'//	PRINTR25
6	,HEADRS(11)/' TERRAIN'//,UNITS(11)/' '/	PRINTR26
7	,HEADRS(12)/' TERRAIN PGR'//,UNITS(12)/' '/	PRINTR27
8	,HEADRS(13)/' TERRAIN PGT'//,UNITS(13)/' '/	PRINTR28
9	,HEADRS(14)/' TERRAIN PGP'//,UNITS(14)/' '/	PRINTR29
C		PRINTR30
C	ROUND-OFF FUNCTION	PRINTR31
	ROUND(X)=SIGN(ABS(X)+0.5,X)	PRINTR32

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C
  NWHY=EVENT(2:)
  GO TO 10
C
C  INITIALIZATION ENTRY POINT FOR PRINTR. CALLED FOR EACH NEW
C  W-ARRAY.
  ENTRY IPRINTR
C
C***** NEW W ARRAY -- REINITIALIZE
  NEWWP=.FALSE.
  SPL=SIN (PLON-TLON)
  CPL=SIN (PID2-(PLON-TLON))
  SP=SIN (PLAT)
  CP=SIN (PID2-PLAT)
  SL=SIN (TLAT)
  CL=SIN (PID2-TLAT)
C***** MATRIX TO ROTATE COORDINATES
  GO(1,1)=CPL*SP*CL-CP*SL
  GO(1,2)=SPL*SP
  GO(1,3)=-SL*SP*CPL-CL*CP
  GO(2,1)=-SPL*CL
  GO(2,2)=CPL
  GO(2,3)=SL*SPL
  GO(3,1)=CL*CP*CPL+SP*SL
  GO(3,2)=CP*SPL
  GO(3,3)=-SL*CP*CPL+SP*CL
  DENM=GO(1,1)*GO(2,2)*GO(3,3)+GO(1,2)*GO(3,1)*GO(2,3)
  1 +GO(2,1)*GO(3,2)*GO(1,3)-GO(2,2)*GO(3,1)*GO(1,3)
  2 -GO(1,2)*GO(2,1)*GO(3,3)-GO(1,1)*GO(3,2)*GO(2,3)
C***** THE MATRIX G1 IS THE INVERSE OF THE MATRIX G
  G1(1,1)=(GO(2,2)*GO(3,3)-GO(3,2)*GO(2,3))/DENM
  G1(1,2)=(GO(3,2)*GO(1,3)-GO(1,2)*GO(3,3))/DENM
  G1(1,3)=(GO(1,2)*GO(2,3)-GO(2,2)*GO(1,3))/DENM
  G1(2,1)=(GO(3,1)*GO(2,3)-GO(2,1)*GO(3,3))/DENM
  G1(2,2)=(GO(1,1)*GO(3,3)-GO(3,1)*GO(1,3))/DENM
  G1(2,3)=(GO(2,1)*GO(1,3)-GO(1,1)*GO(2,3))/DENM
  G1(3,1)=(GO(2,1)*GO(3,2)-GO(3,1)*GO(2,2))/DENM
  G1(3,2)=(GO(3,1)*GO(1,2)-GO(1,1)*GO(3,2))/DENM
  G1(3,3)=(GO(1,1)*GO(2,2)-GO(2,1)*GO(1,2))/DENM
  RO=EARTH+XMTRH
C***** CARTESIAN COORDINATES OF TRANSMITTER
  XR=RO*GO(1,1)
  YR=RO*GO(2,1)
  ZR=RO*GO(3,1)
  CTHR=GO(3,1)
  STHR=SIN (ACOS (CTHR))
  PHIR=ATAN2 (YR, XR)
  ALPH=ATAN2 (GO(3,2), GO(3,3))
C*****
  NR=0
  NP=0
  NERG=0
  NERR=0
  NERT=0
  NERP=0
  PRINTR33
  PRINTR34
  PRINTR35
  PRINTR36
  PRINTR37
  PRINTR38
  PRINTR39
  PRINTR40
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  PRINTR85
  PRINTR86
  PRINTR87

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C      INSURE NO GARBLE IN HEADERS                                PRINTR88
      HEAD(1)=' '                                                PRINTR89
      UNIT(1)=' '                                                PRINTR90
C
      DO 7 NN=7,20                                               PRINTR91
      IF (W(NN+50).EQ.0.) GO TO 7                                PRINTR92
C***** DEPENDENT VARIABLE NUMBER NN IS BEING INTEGRATED      PRINTR93
C***** NR IS THE NUMBER OF DEPENDENT VARIABLES BEING INTEGRATED PRINTR94
      NR=NR+1                                                    PRINTR95
C      ENABLE SELECTED RELATIVE ERROR PRINTOUTS FOR TERRAIN(G) OR PRINTR96
C      ITS DERIVATIVES WITH RESPECT TO (R)ANGE, (T)HETA OR (P)HI. PRINTR97
      IF(NN.EQ.11) NERG=NR                                        PRINTR98
      IF(NN.EQ.12) NERR=NR                                        PRINTR99
      IF(NN.EQ.13) NERT=NR                                        PRINT100
      IF(NN.EQ.14) NERP=NR                                        PRINT101
      IF (W(NN+50).NE.2.) GO TO 7                                PRINT102
C***** DEPENDENT VARIABLE NUMBER NN IS BEING INTEGRATED AND PRINTED. PRINT103
C***** NP IS THE NUMBER OF DEPENDENT VARIABLES BEING INTEGRATED AND PRINT104
C***** PRINTED                                                 PRINT105
      NP=NP+1                                                    PRINT106
C***** SAVE THE INDEX OF THE DEPENDENT VARIABLE TO PRINT      PRINT107
      NPR(NP)=NR                                                 PRINT108
      HEAD(NP)=HEADRS (NN)                                       PRINT109
      HEAD(NP)=HEADRS (NN)                                       PRINT110
      UNIT(NP)=UNITS (NN)                                         PRINT111
7 CONTINUE                                                       PRINT112
      NPM=MINO (NP, 3)                                           PRINT113
      NP1=NPM+1                                                  PRINT114
      P=0.0                                                       PRINT115
      ABSORB=0.0                                                 PRINT116
      DOPP=0.0                                                   PRINT117
      NEQS=NR+6                                                  PRINT118
      RETURN                                                       PRINT119
C
      ENTRY PRNHD1(CC)                                           PRINT120
C      PRINT PRINTR HEADER 1                                     PRINT121
C      IF NO OUTPUT NEEDED EXIT NOW                             PRINT122
      IF(PRTSRP.NE.0.0) RETURN                                   PRINT123
C
C      ADD NUMBER OF LINES NEEDED FOR THIS HEADER              PRINT124
      PC=CC                                                       PRINT125
      IF(CC.EQ.'1') CALL NEWPAG(NPAG,INT(PAGLN),PC)             PRINT126
      LINES=LINES+3                                              PRINT127
C***** PRINT COLUMN HEADINGS                                    PRINT128
C
      WRITE(3,1100) PC,(HEAD(NN),NN=1,NPM)                       PRINT129
C
C      WRITE(3,1100) PC,(HEAD(NN),NN=1,NPM)                       PRINT130
1100 FORMAT ( A,T25,'ELEVATION',T54,'AZIMUTH',T71,'ELEVATION'/   PRINT131
3 ,T20,2('ABOVE',6X),T53,'DEVIATION',T72,'ANGLE'/ ' ERROR EVENT' PRINT132
4 ,T20,'SEA LEVEL TERRAIN RANGE',4X,2('XMTR LOCAL',5X),        PRINT133
5 'PULSE TIME',3A12)                                           PRINT134
C
      WRITE(3,1150) (UNIT(NN),NN=1,NPM)                          PRINT135
1150 FORMAT(13X,3(8X,'KM'),2X,2(6X,'DEG',5X,'DEG'),T88        PRINT136
1 , 'SEC',3X,3(3X,A7,2X))                                       PRINT137
                                                                    PRINT138
                                                                    PRINT139
                                                                    PRINT140
                                                                    PRINT141
                                                                    PRINT142

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C          RETURN PRINT143
C          ENTRY PRNHD2(CC) PRINT144
C          PRINT PRINTR HEADER 1 PRINT145
C          IF NO OUTPUT NEEDED EXIT NOW PRINT146
C          IF(PRTSRP.NE.0.0) RETURN PRINT147
C          PAGE BY HALF LENGTH PRINT148
C          LINSPP=PAGLN/2 PRINT149
C          IF(LINSPP.LT.40) LINSPP=PAGLN PRINT150
C          PC=CC PRINT151
C          IF(CC.EQ.'1') CALL NEWPAG(NPAG,LINSPP,PC) PRINT152
C          ADD NUMBER OF LINES NEEDED FOR THIS SUBHEADER PRINT153
C          LINES=LINES+1 PRINT154
C          IF(ELEND.GE.ELBEG+ELSTEP) THEN PRINT155
C              WRITE(3,'(A,'ELEVATION ANGLE OF TRANSMISSION =' PRINT156
1              ,F10.4,' ' DEG''')' ) PC,BETA*DEGS PRINT157
C          ELSEIF(AZEND.GE.AZBEG+AZSTEP) THEN PRINT158
C              WRITE(3,'(A,'AZIMUTH ANGLE OF TRANSMISSION =' PRINT159
1              ,F10.4,' ' DEG''')' ) PC,AZ1*DEGS PRINT160
C          ENDIF PRINT161
C          RETURN PRINT162
C          IF PRINTING SUPPRESSED AND RAYSETS OFF NOTHING TO DO PRINT163
C          IF(PRTSRP.NE.0.0 .AND. CARD.EQ.0.0) RETURN PRINT164
C          CALL DISPER PRINT165
C          IF (CARD.EQ.0.0 .OR. IHOP.NE.0) GO TO 12 PRINT166
C***** OUTPUT A TRANSMITTER RAYSET PRINT167
C          NOTE: THIS IS A SPECIAL CASE, ALL OTHER RAY EVENTS ARE PRINT168
C          OUTPUT AT CODE 'PUNCH A RAYSET' BELOW. PRINT169
C          PRINT170
C          TLOND=TLON*DEGS PRINT171
C          IF (TLOND.LT.0.) TLOND=TLOND+360. PRINT172
C          TLATD=TLAT*DEGS PRINT173
C          IF (TLATD.LT.0.) TLATD=TLATD+360. PRINT174
C          AZ=AZ1*DEGS PRINT175
C          EL=BETA*DEGS PRINT176
C          NHOP=HOP PRINT177
C          NXMTRH=ROUND(XMTRH*1.E4) PRINT178
C          NTLATD=ROUND(TLATD*1.E3) PRINT179
C          NTLOND=ROUND(TLOND*1.E3) PRINT180
C          NRCVRH=ROUND(RCVRH*1.E4) PRINT181
C          NF=ROUND(OW*1.E4) PRINT182
C          NAZ=ROUND(AZ*1.E5) PRINT183
C          NEL=ROUND(EL*1.E5) PRINT184
C          NPOLAR1=ROUND(REAL(POLAR)*1.E2) PRINT185
C          NPOLAR2=ROUND(AIMAG(POLAR)*1.E2) PRINT186
C          WRITE(9,1201) ID(1),TYPE(NTYP),NXMTRH,NTLATD,NTLOND,NRCVRH,NF,NAZ PRINT187
1          ,NEL,NPOLAR1,NPOLAR2,NHOP,'T' PRINT188
1201 FORMAT(A3,A1,I9,2I6,2I9,2I10,5X,I5,I4,I2,A1) PRINT189
C***** PRINT190
12          V=1.E10 PRINT191
C          OBTAIN THE WORST ERROR OF THOSE ENABLED. PRINT192
C          IF (KAY2.NE.0.) V=(KR**2+KTH**2+KPH**2)/KAY2-1. PRINT193
C          PRINT194
C          PRINT195
C          PRINT196
C          PRINT197

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ERT=1HK
V=RERR(V,ERT,'G',NERG,G)
V=RERR(V,ERT,'R',NERR,PGR)
V=RERR(V,ERT,'T',NERT,PGTH)
V=RERR(V,ERT,'P',NERP,PGPH)
C
H=R-EARTH
STH=SIN (THETA)
CTH=SIN (PID2-THETA)
C***** CARTESIAN COORDINATES OF RAY POINT, ORIGIN AT TRANSMITTER
XP=R*STH*SIN (PID2-PHI)-XR
YP=R*STH*SIN (PHI)-YR
ZP=R*CTH-ZR
C***** CARTESIAN COORDINATES OF RAY POINT, ORIGIN AT TRANSMITTER AND
C***** ROTATED
EPS=XP*G1(1,1)+YP*G1(1,2)+ZP*G1(1,3)
ETA=XP*G1(2,1)+YP*G1(2,2)+ZP*G1(2,3)
ZETA=XP*G1(3,1)+YP*G1(3,2)+ZP*G1(3,3)
RCE2=ETA**2+ZETA**2
RCE=SQRT (RCE2)
C***** GROUND RANGE
RANGE=EARTH*ATAN2 (RCE,EARTH+EPS+XMTRH)
C***** ANGLE OF WAVE NORMAL WITH LOCAL HORIZONTAL
ELL=ATAN2 (KR,SQRT (KTH**2+KPH**2))*DEGS
C***** STRAIGHT LINE DISTANCE FROM TRANSMITTER TO RAY POINT
SR=SQRT (RCE2+EPS**2)
C***** TERRAIN RELATIVE HEIGHT
GRH=GET(G)/PGR
C
REPORT GROUP TIME AS FIRST 'OPTION'
RPRINT(1)=T
IF (NP1.LT.2) GO TO 16
C
ADD MORE OPTIONS IF REQUESTED
DO 15 I=2,NP1
NN=NPR(I-1)
15 RPRINT(I)=RKVAR(NN)
C
16 IF(V.GE.0.0) THEN
WRITE(TMP,'(A1,E7.2)') ERT,V
ELSE
WRITE(TMP,'(A1,E7.1)') ERT,V
ENDIF
C
DETERMINE WHERE TO PUT A SPACE
C
AT BEGINNING OR END OF 1ST 2 VALUES
KT=1
IF(TMP(1:1).EQ.'K') KT=2
C
IF (SR.GE.1.E-6) GO TO 20
C***** TOO CLOSE TO TRANSMITTER TO CALCULATE DIRECTION FROM
C***** TRANSMITTER
IF(PRTSRP.EQ.0.0)
1 WRITE(3,1500)TMP(KT:9),NWHY,H,GRH,RANGE,ELL,(RPRINT(NN),NN=1,NP1)
1500 FORMAT (1X,A8,A8,2F10.4,F11.4,26X,F8.3,4F12.4)
C
SET RAYSET VARIABLES TO UNDEFINED VALUES FOR FLAGS
AZDEV=999.0
AZA=999.0

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PRINT198
PRINT199
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PRINT250
PRINT251
PRINT252

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GO TO 40
C***** ELEVATION ANGLE OF RAY POINT FROM TRANSMITTER
20 EL=ATAN2(EPS,RCE)*DEGS
IF (RCE.GE.1.E-6) GO TO 30
C***** NEARLY DIRECTLY ABOVE OR BELOW TRANSMITTER. CAN NOT CALCULATE
C***** AZIMUTH DIRECTION FROM TRANSMITTER ACCURATELY
IF(PRTSRP.EQ.0.0)
1 WRITE(3,2500)TMP(KT:9),NWHY,H,GRH,RANGE,EL,ELL
2 ,(RPRINT(NN),NN=1,NP1)
2500 FORMAT (1X,A8,A8,2F10.4,F11.4,17X,F9.3,F8.3,
1 4F12.4)
GO TO 40
C***** AZIMUTH ANGLE OF RAY POINT FROM TRANSMITTER
30 ANGA=ATAN2(ETA,ZETA)
AZDEV=180.-AMOD(540.-(AZ1-ANGA)*DEGS,360.)
IF (KTH.NE.0..OR.KPH.NE.0.) GO TO 34
C***** WAVE NORMAL IS VERTICAL, SO AZIMUTH DIRECTION CANNOT BE
C***** CALCULATED
IF(PRTSRP.EQ.0.0)
1 WRITE(3,3000)TMP(KT:9),NWHY,H,GRH,RANGE,AZDEV,EL,ELL,(RPRINT(NN),
1 NN=1,NP1)
3000 FORMAT (1X,A8,A8,2F10.4,F11.4,F9.3,8X,F9.3,F8.3,
1 4F12.4)
GO TO 40
34 ANA=ANGA-ALPH
SANA=SIN(ANA)
SPHI=SANA*STHR/STH
CPHI=-SIN(PID2-ANA)*SIN(PID2-(PHI-PHIR))+SANA*SIN(PHI-PHIR)
1 *CTHR
AZA=180.-AMOD(540.-(ATAN2(SPHI,CPHI)-ATAN2(KPH,KTH))*DEGS,360.)
IF(PRTSRP.EQ.0.0)
1 WRITE(3,3500)TMP(KT:9),NWHY,H,GRH,RANGE,AZDEV,AZA,EL,ELL
2 ,(RPRINT(NN),NN=1,NP1)
3500 FORMAT (1X,A8,A8,2F10.4,F11.4,2(F9.3,F8.3),
1 4F12.4)
C*****
40 LINES=LINES+1
IF (NP.LE.3) GO TO 45
C***** ADDITIONAL LINE TO PRINT REMAINING DEPENDENT INTEGRATION
C***** VARIABLES
IF(PRTSRP.EQ.0.0)
1 WRITE(3,4000)(RPRINT(NN),NN=4,NP)
4000 FORMAT (99X,3F12.4)
LINES=LINES+1
C
C IF NO 'CARDS' WANTED OR AT TRANSMITTER, NO RAYSET OUTPUT
C
45 IF (CARD.EQ.0.0 .OR. IHOP.LT.1) RETURN
C
C***** PUNCH A RAYSET
IF (AZDEV.LT.-90.) AZDEV=AZDEV+360.
IF (AZA.LT.-90.) AZA=AZA+360.
NR=0
IF (W(57).EQ.0.) GO TO 47
C***** PHASE PATH

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PRINT253
PRINT254
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PRINT304
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PRINT306
PRINT307

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NR=NR+1	PRINT308
P=RKVAR(S(NR))	PRINT309
47 IF (W(58).EQ.0.) GO TO 48	PRINT310
C***** ABSORPTION	PRINT311
NR=NR+1	PRINT312
ABSORB=RKVAR(S(NR))	PRINT313
C***** DOPPLER SHIFT	PRINT314
48 IF (W(59).NE.0.) DOPP=RKVAR(S(NR+1))	PRINT315
NHPUNCH=ROUND(HPUNCH*1.E4)	PRINT316
NRANGE=ROUND(RANGE*1.E4)	PRINT317
NAZDEV=ROUND(AZDEV*1.E3)	PRINT318
NAZA=ROUND(AZA*1.E3)	PRINT319
NELL=ROUND(ELL*1.E3)	PRINT320
IF(NWHY.EQ.'GRND REF') NELL =	PRINT321
1 ROUND((PID2 - ACOS(KNORM(G)/SQRT(KR*KR+KTH*KTH+KPH*KPH)))	PRINT322
2 *DEGS*1.E3)	PRINT323
NABSORB=AMIN1(999999.0,ROUND(ABSORB*1.E3))	PRINT324
NDOPP=ROUND(DOPP*1.E3)	PRINT325
NPOLAR1=ROUND(REAL(POLAR)*1.E2)	PRINT326
NPOLAR2=ROUND(AIMAG(POLAR)*1.E2)	PRINT327
JP=ROUND(P*1.E5)	PRINT328
JT=ROUND(T*1.E5)	PRINT329
WRITE(9,4501) NHPUNCH,NRANGE,NAZDEV,NAZA,NELL,JT,JP,NABSORB	PRINT330
1 ,NDOPP,NPOLAR1,NPOLAR2,IHOP,EVENT(1:1)	PRINT331
4501 FORMAT(2I9,3I6,2I10,2I6,I5,I4,I2,A1)	PRINT332
RETURN	PRINT333
END	PRINT334

SUBROUTINE ATMOSHD	ATMOSHD2
C PRINTS PAGE HEADINGS	ATMOSHD3
C IF W(72) IS NEGATIVE, ONLY ONE HEADER OUTPUT IS INCLUDED IN RAYSE	ATMOSHD4
CHARACTER PCC*1,PC*1,BLANKS*100,DIVIDR*132,BANNER(8)*80	ATMOSHD5
CHARACTER NUMSTG*80,STMP*80	ATMOSHD6
LOGICAL NOPUNCH	ATMOSHD7
INTEGER STRIM	ATMOSHD8
C	ATMOSHD9
C TWO ENTRY POINTS ARE PROVIDED. ONE FOR THE FIRST PAGE HEADER	ATMOSH10
C OF THE COMPUTATIONAL PRINTOUT AND FOR THE RAYSET FILE. THE	ATMOSH11
C SECOND ENTRY IS FOR ALL SUBSEQUENT PAGES OF THE COMPUTATIONAL	ATMOSH12
C PRINTOUT.	ATMOSH13
C	ATMOSH14
C COMMON DECK "AA" INSERTED HERE	CAA 2
REAL MODA	CAA 4
REAL MU,MUPT,MUPR,MUPTH,MUPPH	CAA 5
REAL KAP,KAPPT,KAPPR,KAPPTH,KAPPPH	CAA 6
COMMON/AA/MODA(4),MU,MUPT,MUPR,MUPTH,MUPPH	CAA 7
COMMON/AA/KAP,KAPPT,KAPPR,KAPPTH,KAPPPH	CAA 8
C COMMON DECK "PP" INSERTED HERE	CPP 2
REAL MODP	CPP 4
COMMON/PP/MODP(4),P,PPT,PPR,PPTH,PPPH	CPP 5
C	ATMOSH17

C	COMMON DECK "SS" INSERTED HERE	CSS	2
	REAL MODSURF	CSS	4
	COMMON/SS/ MODSURF(4)	CSS	5
	COMMON/SS/U, PUR, PURR, PURTH, PURPH	CSS	6
	COMMON/SS/PUTH, PUPH, PUTHTH, PUPHPH, PUTHPH, USELECT, UTIME	CSS	7
C	COMMON DECK "CONST" INSERTED HERE	CCONST	2
	COMMON/PCONST/CREF, RGAS, GAMMA	CCONST	4
	COMMON/MCONST/PI, PIT2, PID2, DEGS, RAD, ALN10	CCONST	5
C	COMMON DECK "WWR" INSERTED HERE	CWWR	2
	PARAMETER (NWAR SZ=1000)	CWW1	3
	COMMON/WW/ID(10), MAXW, W(NWAR SZ)	CWW1	4
	REAL MAXSTP, MAXERR, INTYP, LLAT, LLON	CWW2	2
	EQUIVALENCE (EARTH, W(1)), (RAY, W(2)), (XMTRH, W(3)), (TLAT, W(4)),	CWW2	3
	1 (TLON, W(5)), (OW, W(6)), (FBEG, W(7)), (FEND, W(8)), (FSTEP, W(9)),	CWW2	4
	2 (AZ1, W(10)), (AZBEG, W(11)), (AZEND, W(12)), (AZSTEP, W(13)),	CWW2	5
	3 (BETA, W(14)), (ELBEG, W(15)), (ELEND, W(16)), (ELSTEP, W(17)),	CWW2	6
	8 (RCVRH, W(20)),	CWW2	7
	4 (ONLY, W(21)), (HOP, W(22)), (MAXSTP, W(23)), (PLAT, W(24)), (PLON, W(25))	CWW2	8
	5, (HMAX, W(26)), (RAYFNC, W(29)), (EXTINC, W(33)),	CWW2	9
	6 (HMIN, W(27)), (RGMAX, W(28)),	CWW2	10
	8 (INTYP, W(41)), (MAXERR, W(42)), (ERATIO, W(43)),	CWW2	11
	6 (STEP1, W(44)), (STPMAX, W(45)), (STPMIN, W(46)), (FACTR, W(47)),	CWW2	12
	7 (SKIP, W(71)), (RAYSET, W(72)), (PRTSRP, W(74)), (HITLET, W(75))	CWW2	13
	9, (BINRAY, W(76)), (PAGLN, W(77)), (PLT, W(81)), (PFACTR, W(82)),	CWW2	14
	1 (LLAT, W(83)), (LLON, W(84)), (RLAT, W(85)), (RLON, W(86))	CWW2	15
	2, (TIC, W(87)), (HB, W(88)), (HT, W(89)), (TICV, W(96))	CWW2	16
C	COMMON DECK "GG" INSERTED HERE	CGG	2
	REAL MODG	CGG	4
	COMMON/GG/MODG(4)	CGG	5
	COMMON/GG/G, PGR, PGRR, PGRTH, PGRPH	CGG	6
	COMMON/GG/PGTH, PGPH, PGTHTH, PGPHPH, PGTHPH, GSELECT, GTIME	CGG	7
C	COMMON DECK "RR" INSERTED HERE	CRR	2
	REAL MODREC	CRR	4
	COMMON/RR/ MODREC(4)	CRR	5
	COMMON/RR/F, PFR, PFRR, PFRTH, PFRPH	CRR	6
	COMMON/RR/PFTH, PFPH, PFTHTH, PFPHPH, PFTHPH, FSELECT, FTIME	CRR	7
C	COMMON DECK "B9" INSERTED HERE	CB8	2
	INTEGER GMX, GNTBL, GITBL, GFRMTBL, IDSG(10)	CB8	4
	COMMON/B9/GMX, GNTBL(10), GITBL(10), GFRMTBL(10), GGP(113)	CB8	5
	EQUIVALENCE (GGP, IDSG), (ANG, GGP(11))	CB8	6
C	COMMON DECK "B2" INSERTED HERE	CB2	2
	INTEGER DUMX, DUNTBL, DUITBL, DUFRMTB, IDSDU(10)	CB2	4
	COMMON/B2/DUMX, DUNTBL(10), DUITBL(10), DUFRMTB(10), DUGP(10)	CB2	5
	EQUIVALENCE (DUGP, IDSDU)	CB2	6
C	COMMON DECK "B4" INSERTED HERE	CB4	2
	INTEGER DCMX, DCNTBL, DCITBL, DCFRMTB, IDSDC(10)	CB4	4
	COMMON/B4/DCMX, DCNTBL(10), DCITBL(10), DCFRMTB(10), DCGP(10)	CB4	5
	EQUIVALENCE (DCGP, IDSDC)	CB4	6
C	COMMON DECK "B6" INSERTED HERE	CB6	2
	INTEGER DTMX, DTNTBL, DTITBL, DTFRMTB, IDSDT(10)	CB6	4
	COMMON/B6/DTMX, DTNTBL(10), DTITBL(10), DTFRMTB(10), DTGP(10)	CB6	5
	EQUIVALENCE (DTGP, IDSDT)	CB6	6
C	COMMON DECK "B1" INSERTED HERE	CB1	2
	INTEGER UMX, UNTBL, UITBL, UFRMTBL, IDSU(10)	CB1	4
	COMMON/B1/UMX, UNTBL(10), UITBL(10), UFRMTBL(10), UGP(10)	CB1	5

	EQUIVALENCE (UGP,IDSU)	CB1	6
C	COMMON DECK "B3" INSERTED HERE	CB3	2
	INTEGER CMX,CNTBL,CITBL,CFRMTBL,IDSC(10)	CB3	4
	COMMON/B3/CMX,CNTBL(10),CITBL(10),CFRMTBL(10),CGP(512)	CB3	5
	EQUIVALENCE (CGP, IDSC), (ANC,CGP(11))	CB3	6
C	COMMON DECK "B5" INSERTED HERE	CB5	2
	INTEGER TMX,TNTBL,TITBL,TFRMTBL,IDST(10)	CB5	4
	COMMON/B5/TMX,TNTBL(10),TITBL(10),TFRMTBL(10),TGP(262)	CB5	5
	EQUIVALENCE (TGP, IDST), (ANT,TGP(11))	CB5	6
C	COMMON DECK "B7" INSERTED HERE	CB7	2
	INTEGER MMX,MNTBL,MITBL,MFRMTBL,IDSM(10)	CB7	4
	REAL MGP	CB7	5
	COMMON/B7/MMX,MNTBL(10),MITBL(10),MFRMTBL(10),MGP(10)	CB7	6
	EQUIVALENCE (MGP, IDSM)	CB7	7
C	COMMON DECK "HDR" INSERTED HERE	CHDR	2
	CHARACTER*10 INITID*80,DAT,TOD	CHDR	4
	COMMON/HDR/SEC	CHDR	5
	COMMON/HDR/INITID,DAT,TOD	CHDR	6
C	COMMON DECK "RINPLEX" INSERTED HERE	CRINPLE2	
	REAL KAY2,KAY2I	CRINPLE4	
	COMPLEX PNP,POLAR,LPOLAR	CRINPLE5	
	LOGICAL SPACE	CRINPLE6	
	CHARACTER DISPM*6	CRINPLE7	
	COMMON/RINPL/DISPM	CRINPLE8	
	COMMON /RIN/ MODRIN(8),RAYNAME(2,3),TYPE(3),SPACE	CRINPLE9	
	COMMON/RIN/OMEGMIN,OMEGMAX,KAY2,KAY2I	CRINPL10	
	COMMON/RIN/PNP(10),POLAR,LPOLAR,SGN	CRINPL11	
C	COMMON DECK "CC" INSERTED HERE	CCC	2
	REAL MODC	CCC	4
	COMMON/CC/MODC(4),CS,PCST,PCSR,PCSTH,PCSPH	CCC	5
C	COMMON DECK "MM" INSERTED HERE	CMM	2
	REAL M,MODM	CMM	4
	COMMON/MM/MODM(4),M,PMT,PMR,PMTH,PMPH	CMM	5
C	COMMON DECK "FLAG" INSERTED HERE	CFLAG	2
	LOGICAL NEWWR,NEWWP,NEWTRC,PENET	CFLAG	4
	COMMON /FLG/ NTYP,NEWWR,NEWWP,NEWTRC,PENET,LINES,IHOP,HPUNCH	CFLAG	5
	COMMON/FLGP/NSET	CFLAG	6
C	COMMON DECK "TT" INSERTED HERE	CTT	2
	REAL MODT	CTT	4
	COMMON/TT/MODT(4),T,PTT,PTR,PTTH,PTPH	CTT	5
C	COMMON DECK "UU" INSERTED HERE	CUU	2
	REAL MODU	CUU	4
	COMMON/UU/MODU(4)	CUU	5
	1 ,V ,PVT ,PVR ,PVTH ,PVPH	CUU	6
	2 ,VR ,PVRT ,PVRR ,PVRTH ,PVRPH	CUU	7
	3 ,VTH ,PVTHT ,PVTHR ,PVTHTH ,PVTHPH	CUU	8
	4 ,VPH ,PVPHT ,PVPHR ,PVPHTH ,PVPHPH	CUU	9
C		ATMOSH38	
C	COMMON DECK "B10" INSERTED HERE	CB9	2
	INTEGER DGMX,DGNTBL,DGITBL,DGFRMTB,IDSDG(10)	CB9	4
	COMMON/B10/DGMX,DGNTBL(10),DGITBL(10),DGFRMTB(10),DGGP(10)	CB9	5
	EQUIVALENCE (DGGP, IDSDG)	CB9	6
C	COMMON DECK "B8" INSERTED HERE	CB10	2
	INTEGER RMX,RNTBL,RITBL,RFRMTBL,IDSR(10)	CB10	4
	COMMON/B8/RMX,RNTBL(10),RITBL(10),RFRMTBL(10),RGP(10)	CB10	5

	EQUIVALENCE (RGP, IDSR)	CB10	6
C	COMMON DECK "CB17" INSERTED HERE	CB17	2
	INTEGER VMX, VNTBL, VITBL, VFRMTBL, IDSV(10)	CB17	4
	COMMON/B17/VMX, VNTBL(10), VITBL(10), VFRMTBL(10), VGP(53)	CB17	5
	EQUIVALENCE (VGP, IDSV), (ANV, VGP(11))	CB17	6
C	COMMON DECK "CB18" INSERTED HERE	CB18	2
	INTEGER DVMX, DVNTBL, DVITBL, DVFRMTB, IDSDV(10)	CB18	4
	COMMON/B18/DVMX, DVNTBL(10), DVITBL(10), DVFRMTB(10), DVGP(11)	CB18	5
	EQUIVALENCE (DVGP, IDSDV), (ANDV, DVGP(11))	CB18	6
C	COMMON DECK "CB19" INSERTED HERE	CB19	2
	INTEGER PRMX, PRNTBL, PRITBL, PRFRMTB, IDSPR(10)	CB19	4
	COMMON/B19/PRMX, PRNTBL(10), PRITBL(10), PRFRMTB(10), PRGP(11)	CB19	5
	EQUIVALENCE (PRGP, IDSPR), (ANP, PRGP(11))	CB19	6
C	COMMON DECK "CB20" INSERTED HERE	CB20	2
	INTEGER DPMX, DPNTBL, DPITBL, DPFRMTB, IDSDP(10)	CB20	4
	COMMON/B20/DPMX, DPNTBL(10), DPITBL(10), DPFRMTB(10), DPGP(11)	CB20	5
	EQUIVALENCE (DPGP, IDSDP), (ANDP, DPGP(11))	CB20	6
C		ATMOSH45	
C	PARAMETER (NBNRLS=8, NBLNS=8)	ATMOSH46	
		ATMOSH47	
	DATA BLANKS/' '/	ATMOSH48	
	DATA BANNER/	ATMOSH49	
	1 '***** H A R P A *****'	ATMOSH50	
	2 , 'HAMILTONIAN ACOUSTIC RAY-TRACING PROGRAM FOR THE ATMOSPHERE'	ATMOSH51	
	3 , ' '	ATMOSH52	
	4 , 'BY'	ATMOSH53	
	5 , 'R. M. JONES, J. P. RILEY AND T. M. GEORGES'	ATMOSH54	
	6 , 'WAVE PROPAGATION LABORATORY'	ATMOSH55	
	7 , 'NATIONAL OCEANIC AND ATMOSPHERIC ADMINISTRATION'	ATMOSH56	
	8 , 'BOULDER, COLORADO 80303'/'	ATMOSH57	
	DATA NOPUNCH/.FALSE./	ATMOSH58	
	DATA IBLK/1H /	ATMOSH59	
C		ATMOSH60	
	ENTRY HEADER1	ATMOSH61	
C		ATMOSH62	
C	COMPUTE EFFECTIVE LINES COUNT BASED ON FIXED PAGE SIZE	ATMOSH63	
	CALL NEWPAG(NPAG, INT(PAGLN), PC)	ATMOSH64	
	CALL SFILL(DIVIDR, LEN(DIVIDR), '-')	ATMOSH65	
	DIVIDR(1:1)=' '	ATMOSH66	
	NTYP=2	ATMOSH67	
	IF(RAY.NE.0.0) NTYP=2.0+SIGN(1.0, RAY)	ATMOSH68	
C		ATMOSH69	
1600	FORMAT(2(2(A8, F7.1, 1X), 2X))	ATMOSH70	
	CALL PUTKST(3, '1')	ATMOSH71	
	1 //DAT//TOD//BLANKS(:100)//'PAGE'//NUMSTG(NPAG, 1, '(I5)')	ATMOSH72	
	CALL PUTKST(3, DIVIDR)	ATMOSH73	
	CALL PUTKBK(3, 1)	ATMOSH74	
	DO 15 I=1, NBNRLS	ATMOSH75	
15	CALL PUTKCT(3, BANNER(I))	ATMOSH76	
	CALL PUTKBK(3, 1)	ATMOSH77	
	CALL PUTKST(3, DIVIDR)	ATMOSH78	
	CALL PUTKBK(3, NBLNS)	ATMOSH79	
C		ATMOSH80	
	CALL PUTKST(3, BLANKS(:57)//'RUN SET NUMBER'	ATMOSH81	
1	//NUMSTG(NSET, 1, '(I5)')	ATMOSH82	

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CALL PUTKBK(3,1)
WRITE(STMP,'(10A8)') ID
CALL PUTKST(3,BLANKS(:52)//'ATMOSPHERIC MODEL ID -- '//STMP(:3))
CALL PUTKBK(3,1)
CALL PUTKST(3,
1 BLANKS(:25)//'ATMOSPHERIC MODEL DESCRIPTION -- '//STMP(7:))
CALL PUTKBK(3,1)

WRITE(STMP,'(2A8)') (RAYNAME(I,NTYP),I=1,2)
CALL PUTKST(3,STMP)
CALL PUTKBK(3,1)
CALL PUTKST(3,DIVIDR)
CALL PUTKBK(3,1)
CALL PUTKST(3,
1 BLANKS(:8)//'MODEL
1 //' DESCRIPTION')
CALL PUTKST(3,
1 BLANKS(:8)//'TYPE
CALL PUTKBK(3,1)
CALL PUTKST(3,DIVIDR)
CALL PUTKBK(3,1)
CALL PUTKST(3,' DISPERSION RELATION
1 //BLANKS(:16)//NUMSTG(MODRIN,8,'(8A8)'))
CALL PUTDES(3,'BACKGROUND WIND VELOCITY',MODU,IDSU)
CALL PUTDES(3,'WIND VELOCITY PERTURBATION',MODU(3),IDSDU)
CALL PUTDES(3,'BACKGROUND SOUND SPEED',MODC,IDSC)
CALL PUTDES(3,'SOUND SPEED PERTURBATION',MODC(3),IDSDC)
CALL PUTDES(3,'BACKGROUND TEMPERATURE',MODT,IDST)
CALL PUTDES(3,'TEMPERATURE PERTURBATION',MODT(3),IDSdT)
CALL PUTDES(3,'MOLECULAR WEIGHT',MODM,IDSM)
CALL PUTDES(3,'BACKGROUND TERRAIN',MODG,IDSG)
CALL PUTDES(3,'TERRAIN PERTURBATION',MODG(3),IDSDG)
CALL PUTKST(3,' BACKGROUND VISCOSITY/')
CALL PUTDES(3,' THERMAL CONDUCTIVITY',MODA,IDSV)
CALL PUTKST(3,' VISCOSITY/THERMAL')
CALL PUTDES(3,' CONDUCTIVITY PERTURBATION',MODA(3),IDSdV)
CALL PUTDES(3,'BACKGROUND PRESSURE',MODP,IDSPR)
CALL PUTDES(3,'PRESSURE PERTURBATION',MODP(3),IDSDP)
CALL PUTDES(3,'RECEIVER SURFACE',MODREC,IDSr)
CALL PUTKST(3,DIVIDR)

NOPUNCH=NOPUNCH.AND.RAYSET.LT.0.0
IF(NOPUNCH) RETURN
NOPUNCH=RAYSET.LT.0.0

WRITE(9,1200) ID,DAT,TOD
WRITE(9,1600) MODU,MODC,MODT,MODM,MODP,MODA
1 ,MODG,MODREC
IF(IDSU(1) .NE. IBLK) WRITE(9,1200) IDSU
IF(IDSDU(1) .NE. IBLK) WRITE(9,1200) IDSDU
IF(IDSC(1) .NE. IBLK) WRITE(9,1200) IDSC
IF(IDSDC(1) .NE. IBLK) WRITE(9,1200) IDSDC
IF(IDST(1) .NE. IBLK) WRITE(9,1200) IDST
IF(IDSDT(1) .NE. IBLK) WRITE(9,1200) IDSdT
IF(IDSM(1) .NE. IBLK) WRITE(9,1200) IDSM

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ATMOSH83
ATMOSH84
ATMOSH85
ATMOSH86
ATMOSH87
ATMOSH88
ATMOSH89
ATMOSH90
ATMOSH91
ATMOSH92
ATMOSH93
ATMOSH94
ATMOSH95
ATMOSH96
ATMOSH97
ATMOSH98
ATMOSH99
ATMOS100
ATMOS101
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ATMOS132
ATMOS133
ATMOS134
ATMOS135
ATMOS136
ATMOS137

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	IF(IDSG(1) .NE. IBLK) WRITE(9,1200) IDSG	ATMOS138
C		ATMOS139
	1000 FORMAT (A1,10A8,24X,2A,' PAGE',I4)	ATMOS140
	1200 FORMAT(10A8,2(A8,2X))	ATMOS141
C		ATMOS142
	RETURN	ATMOS143
C		ATMOS144
	ENTRY HEADER2	ATMOS145
C		ATMOS146
C	COMPUTE EFFECTIVE LINES COUNT BASED ON FIXED PAGE SIZE	ATMOS147
	CALL NEWPAG(NPAG,INT(PAGLN),PC)	ATMOS148
	LINES=LINES+5	ATMOS149
C		ATMOS150
	WRITE(3,1000) PC,ID,DAT,TOD,NPAG	ATMOS151
	WRITE(3,2400) AZ1*DEGS,TLAT*DEGS,OW/PIT2,BETA*DEGS	ATMOS152
	1 ,TLON*DEGS,MAXERR	ATMOS153
	2400 FORMAT (	ATMOS154
	1 /' AZIMUTH ANGLE OF TRANSMISSION =',F12.6,' DEG'	ATMOS155
	2 ,' TRANSMITTER LATITUDE =',F12.6,' DEG'	ATMOS156
	3 ,' FREQUENCY =',F12.6,' HZ'	ATMOS157
	4 /' ELEVATION ANGLE OF TRANSMISSION =',F12.6,' DEG'	ATMOS158
	5 ,' TRANSMITTER LONGITUDE =',F12.6,' DEG'	ATMOS159
	6 ,' SINGLE STEP ERROR =',1PG13.6/)	ATMOS160
C		ATMOS161
	RETURN	ATMOS162
C		ATMOS163
	ENTRY PUTDVR(NUNIT)	ATMOS164
	CALL PUTKST(NUNIT,DIVIDR)	ATMOS165
	RETURN	ATMOS166
C		ATMOS167
	ENTRY PUTHDR(NUNIT,PCC,NP)	ATMOS168
	CALL PUTKST(NUNIT,	ATMOS169
	1 PCC//DAT//TOD//BLANKS(:100)//'PAGE'//NUMSTG(NP,1,'(I5)'))	ATMOS170
	RETURN	ATMOS171
	END	ATMOS172

	SUBROUTINE PUTDES(NUNIT,DES,MOD,ID)	PUTDES 2
	CHARACTER DES*(*),TITLE*30,SMODL*20,NUMSTG*80	PUTDES 3
	REAL MOD(2),ID(10)	PUTDES 4
	TITLE=DES	PUTDES 5
	WRITE(SMODL,'(A8,F10.2)') MOD	PUTDES 6
	CALL PUTKST(NUNIT, ' '//TITLE//SMODL//NUMSTG(ID,10,'(10A8)'))	PUTDES 7
	END	PUTDES 8

	CHARACTER*80 FUNCTION NUMSTG(V,N,FRM)	NUMSTG 2
	INTEGER V(N)	NUMSTG 3
	CHARACTER FRM*(*)	NUMSTG 4

	NUMSTG=' '		
	WRITE(NUMSTG,FRM) V		NUMSTG 5
	RETURN		NUMSTG 6
	END		NUMSTG 7
			NUMSTG 8
	SUBROUTINE SFILL(STG, LN, C)		SFILL 2
	CHARACTER STG*(*), C*1		SFILL 3
C			SFILL 4
	DO 10 I=1, LN		SFILL 5
10	STG(I:I)=C		SFILL 6
	RETURN		SFILL 7
	END		SFILL 8
	INTEGER FUNCTION STRIM(C)		STRIM 2
	CHARACTER*(*) C		STRIM 3
C			STRIM 4
	L=LEN(C)		STRIM 5
	DO 100 I=L, 1, -1		STRIM 6
100	IF(C(I:I) .NE. ' ') GO TO 200		STRIM 7
	I=0		STRIM 8
200	STRIM=I		STRIM 9
	END		STRIM 10
	FUNCTION RERR(V, ERT, ELAB, NKV, PREF)		RERR 2
C	RETURNS RELATIVE ERROR OF VARIABLE RKVAR(NKV) IF PREF<>0 AND		RERR 3
C	THE ERROR IS GREATER THAN PREVIOUS ERROR 'V'.		RERR 4
C	COMMON DECK "RKAM" INSERTED HERE		RKAMCOM2
	REAL KR, KTH, KPH		RKAMCOM4
C	COMMON//R, TH, PH, KR, KTH, KPH, RKVARS(14), TPULSE, CSTEP, DRDT(20)		RKAMCOM5
	RERR=V		RERR 6
	IF(NKV.LE.0) RETURN		RERR 7
	IF(PREF.EQ.0.) RETURN		RERR 8
	V1=RKVARS(NKV)/PREF-1.		RERR 9
	IF(ABS(V1).LT.ABS(V)) RETURN		RERR 10
C			RERR 11
	ERT=ELAB		RERR 12
	RERR=V1		RERR 13
	END		RERR 14
			RERR 15

	SUBROUTINE ERROR(ROUTIN,STR,VAL)	RERROR 2
C	REPORTS ERROR CONDITIONS AND STOPS PROGRAM.	RERROR 3
C		RERROR 4
	PRINT 10,ROUTIN,STR,VAL	RERROR 5
10	FORMAT(39H ERROR CONDITION IN RAYTRACE ROUTINE <	RERROR 6
	1 ,A8,10H> DUE TO " ,A10,9H", VALUE= ,F8.2)	RERROR 7
	STOP	RERROR 8
	END	RERROR 9

	SUBROUTINE STOPIT(A)	STOPIT 2
C	PRINTS CONDITION AND STOPS PROGRAM	STOPIT 3
C	AFTER CALLING THE SYSTEM POST MORTEM DUMP.	STOPIT 4
C		STOPIT 5
	CHARACTER A*(*)	STOPIT 6
C		STOPIT 7
	PRINT 100, A	STOPIT 8
	CALL MORTEM	STOPIT 9
100	FORMAT('*** STOPIT WITH CONDITION <',A,'>')	STOPIT10
	STOP	STOPIT11
	END	STOPIT12

	SUBROUTINE PUTKST(NUNIT,STRG)	PUTKST 2
C	WRITE LINE OF OUTPUT TO PRINTER UNIT ADDING TO LINE COUNT	PUTKST 3
C		PUTKST 4
	CHARACTER STRG*(*)	PUTKST 5
	CHARACTER BLANKS*100,STMP*80	PUTKST 6
	INTEGER STRIM	PUTKST 7
	CHARACTER PC*1	PUTKST 8
C		PUTKST 9
C	COMMON DECK "FLAG" INSERTED HERE	CFLAG 2
	LOGICAL NEWWR,NEWWP,NEWTRC,PENET	CFLAG 4
	COMMON /FLG/ NTYP,NEWWR,NEWWP,NEWTRC,PENET,LINES,IHOP,HPUNCH	CFLAG 5
	COMMON/FLGP/NSET	CFLAG 6
C		PUTKST11
	DATA BLANKS/' '/	PUTKST12
C		PUTKST13
C	PUT OUT A STRING WITH LINE COUNT INCREMENT	PUTKST14
	LINES=LINES+1	PUTKST15
	LN=MIN0(LEN(STRG),132)	PUTKST16
	WRITE(NUNIT,'(A)') STRG(:LN)	PUTKST17
	RETURN	PUTKST18
C		PUTKST19
	ENTRY PUTKCT(NUNIT,STRG)	PUTKST20
C	PUT OUT A CENTERED LINE AND COUNT	PUTKST21
	NTRM=MAX0(1,STRIM(STRG))	PUTKST22
	NBLKS=66-(NTRM+1)/2	PUTKST23

	LINES=LINES+1	PUTKST24
	LN=MINO(NTRM,132-NBLKS)	PUTKST25
	STMP=STRG	PUTKST26
	WRITE(NUNIT,'(A)') BLANKS(:NBLKS)//STMP(:LN)	PUTKST27
	RETURN	PUTKST28
C	ENTRY PUTKKBK(NUNIT,NBKS)	PUTKST29
C	PUT A BLANK LINE TO PRINTER	PUTKST30
	LINES=LINES+1	PUTKST31
	DO 100 I=1,NBKS	PUTKST32
100	WRITE(NUNIT,'(1X)')	PUTKST33
	RETURN	PUTKST34
C		PUTKST35
	ENTRY NEWPAG(NP,LINSPP,PC)	PUTKST36
C	THE LOGIC HERE ASSUMES THAT A FORM FEED IS ALWAYS NEEDED	PUTKST37
	PC='1'	PUTKST38
C	COMPUTE EFFECTIVE LINES COUNT AFTER NEXT FORM FEED	PUTKST39
	NPAG=(LINES+LINSPP-1)/LINSPP	PUTKST40
	LINES=NPAG*LINSPP	PUTKST41
	NP=NPAG+1	PUTKST42
	RETURN	PUTKST43
	END	PUTKST44
		PUTKST45

	SUBROUTINE OPNREP(IUN,FNAME)	OPNREP 2
C	CYBER VERSION OF OPEN FOR REPLACE	OPNREP 3
C	SINCE THIS OPERATION SEEMS TO BE COMPILER DEPENDENT	OPNREP 4
C	WE MAKE A SUBROUTINE OUT OF IT.	OPNREP 5
C	THIS OPEN OPERATION ALLOWS FOR AN EXISTING VERSION OF	OPNREP 6
C	A FILE. IF THE FILE EXISTS IT IS OVERWRITTEN.	OPNREP 7
	CHARACTER*(*) FNAME	OPNREP 8
	OPEN(IUN,FILE=FNAME)	OPNREP 9
	REWIND IUN	OPNREP10
	RETURN	OPNREP11
	ENTRY OPNURP(IUN,FNAME)	OPNREP12
	OPEN(IUN,FILE=FNAME,FORM='UNFORMATTED')	OPNREP13
	REWIND IUN	OPNREP14
	END	OPNREP15

	SUBROUTINE OVERRD(VAR,TST,DEFT,NFLG,NFVLEQ,NFVLNE)	OVERRD 2
C	OVERWRITE SUPPORT ROUTINE	OVERRD 3
C	TEST 'VAR' AGAINST 'TST', IF EQUAL SET TO DEFAULT 'DEFT'	OVERRD 4
C	AND ALSO SET INTEGER FLAG 'NFLG' TO VALUE 'NFVLEQ' ELSE 'NFVLNE'	OVERRD 5
C		OVERRD 6
	IF(VAR.EQ.TST) THEN	OVERRD 7
	VAR=DEFT	OVERRD 8
	NFLG=NFVLEQ	OVERRD 9
		OVERRD10

	ELSE	OVERRD11
	NFLG=NFVLNE	OVERRD12
	ENDIF	OVERRD13
	RETURN	OVERRD14
	END	OVERRD15
	SUBROUTINE SFILTR(C,S,KSET)	SFILTR 2
	CHARACTER*(*) C,S,KSET	SFILTR 3
C	LN=LEN(C)	SFILTR 4
	J=0	SFILTR 5
	DO 10 I=1, LN	SFILTR 6
	IF(INDEX(KSET,C(I:I)).EQ.0) THEN	SFILTR 7
	J=J+1	SFILTR 8
	S(J:J)=C(I:I)	SFILTR 9
	ENDIF	SFILTR10
10	CONTINUE	SFILTR11
	RETURN	SFILTR12
	END	SFILTR13
		SFILTR14
	FUNCTION ALCOSH(X)	ALCOSH 2
C	COMPUTE LOG(COSH(X)) AND USE LARGE ARGUMENT APPROXIMATION	ALCOSH 3
C	WHEN POSSIBLE.	ALCOSH 4
	DATA ALOG2/.6931471806/	ALCOSH 5
C		ALCOSH 6
	IF(ABS(X).GT.50.0) GO TO 10	ALCOSH 7
	EX=EXP(X)	ALCOSH 8
	ALCOSH=ALOG((EX+1.0/EX)*.5)	ALCOSH 9
	RETURN	ALCOSH10
10	ALCOSH=ABS(X)-ALOG2	ALCOSH11
	END	ALCOSH12
	SUBROUTINE GAUSEL (C,NRD,NRR,NCC,NSF)	GAUSEL 2
C	MATRIX INVERSION BY METHOD OF GAUSSIAN PIVOT	GAUSEL 3
C	SOLVES NCC-NRR SETS OF NRR EQUATIONS	GAUSEL 4
C	***** SAME AS SUBROUTINE GAUSSEL WRITTEN BY L. DAVID LEWIS *****	GAUSEL 5
	DIMENSION C(NRD,NCC),L(128,2)	GAUSEL 6
C	BITS = 2.**-18	GAUSEL 7
	DATA BITS/3.8146972656E-6/	GAUSEL 8
	NR=NRR	GAUSEL 9
	NC=NCC	GAUSEL10
	IF(NC.LT.NR.OR.NR.GT.128.OR.NR.LE.0) CALL EXIT	GAUSEL11
C		GAUSEL12

C	INITIALIZE.	
	NSF=0	GAUSEL13
	NRM=NR-1	GAUSEL14
	NRP=NR+1	GAUSEL15
	D=1.	GAUSEL16
	LSD=1	GAUSEL17
	DO 1 KR=1,NR	GAUSEL18
	L(KR,1)=KR	GAUSEL19
1	L(KR,2)=0	GAUSEL20
	IF(NR.EQ.1) GO TO 42	GAUSEL21
C		GAUSEL22
C	ELIMINATION PHASE.	GAUSEL23
	DO 41 KP=1,NRM	GAUSEL24
	KPP=KP+1	GAUSEL25
	PM=0.	GAUSEL26
	MPN=0	GAUSEL27
C		GAUSEL28
C	SEARCH COLUMN KP FROM DIAGONAL DOWN FOR MAX PIVOT.	GAUSEL29
	DO 2 KR=KP,NR	GAUSEL30
	LKR=L(KR,1)	GAUSEL31
	PT=ABS(C(LKR,KP))	GAUSEL32
	IF(PT.LE.PM) GO TO 2	GAUSEL33
	PM=PT	GAUSEL34
	MPN=KR	GAUSEL35
	LMP=LKR	GAUSEL36
2	CONTINUE	GAUSEL37
C		GAUSEL38
C	IF MAX PIVOT IS ZERO, MATRIX IS SINGULAR.	GAUSEL39
	IF(MPN.EQ.0) GO TO 9	GAUSEL40
	NSF=NSF+1	GAUSEL41
	IF(MPN.EQ.KP) GO TO 3	GAUSEL42
C		GAUSEL43
C	NEW ROW NUMBER KP HAS MAX PIVOT.	GAUSEL44
	LSD=-LSD	GAUSEL45
	L(KP,2)=L(KP,1)	GAUSEL46
	L(MPN,1)=L(KP,1)	GAUSEL47
	L(KP,1)=LMP	GAUSEL48
C		GAUSEL49
C	ROW OPERATIONS TO ZERO COLUMN KP BELOW DIAGONAL.	GAUSEL50
3	MKP=L(KP,1)	GAUSEL51
	P=C(MKP,KP)	GAUSEL52
	D=D*P	GAUSEL53
	DO 41 KR=KPP,NR	GAUSEL54
	MKR=L(KR,1)	GAUSEL55
	Q=C(MKR,KP)/P	GAUSEL56
	IF(Q.EQ.0.) GO TO 41	GAUSEL57
C		GAUSEL58
C	SUBTRACT Q * PIVOT ROW FROM ROW KR.	GAUSEL59
	DO 4 LC=KPP,NC	GAUSEL60
	R=Q*C(MKP,LC)	GAUSEL61
	C(MKR,LC)=C(MKR,LC)-R	GAUSEL62
4	IF(ABS(C(MKR,LC)).LT.ABS(R)*BITS) C(MKR,LC)=0.	GAUSEL63
41	CONTINUE	GAUSEL64
C		GAUSEL65
C	LOWER RIGHT HAND CORNER.	GAUSEL66
		GAUSEL67

42	LNR=L(NR,1)	GAUSEL68
	P=C(LNR,NR)	GAUSEL69
	IF(P.EQ.0.) GO TO 9	GAUSEL70
	NSF=NSF+1	GAUSEL71
	D=D*P*LSD	GAUSEL72
	IF(NR.EQ.NC) GO TO 8	GAUSEL73
C		GAUSEL74
C	BACK SOLUTION PHASE.	GAUSEL75
	DO 61 MC=NRP,NC	GAUSEL76
	C(LNR,MC)=C(LNR,MC)/P	GAUSEL77
	IF(NR.EQ.1) GO TO 61	GAUSEL78
	DO 6 LL=1,NRM	GAUSEL79
	KR=NR-LL	GAUSEL80
	MR=L(KR,1)	GAUSEL81
	KRP=KR+1	GAUSEL82
	DO 5 MS=KRP,NR	GAUSEL83
	LMS=L(MS,1)	GAUSEL84
	R=C(MR,MS)*C(LMS,MC)	GAUSEL85
	C(MR,MC)=C(MR,MC)-R	GAUSEL86
5	IF(ABS(C(MR,MC)).LT.ABS(R)*BITS) C(MR,MC)=0.	GAUSEL87
6	C(MR,MC)=C(MR,MC)/C(MR,KR)	GAUSEL88
61	CONTINUE	GAUSEL89
C		GAUSEL90
C	SHUFFLE SOLUTION ROWS BACK TO NATURAL ORDER.	GAUSEL91
	DO 71 LL=1,NRM	GAUSEL92
	KR=NR-LL	GAUSEL93
	MKR=L(KR,2)	GAUSEL94
	IF(MKR.EQ.0) GO TO 71	GAUSEL95
	MKP=L(KR,1)	GAUSEL96
	DO 7 LC=NRP,NC	GAUSEL97
	Q=C(MKR,LC)	GAUSEL98
	C(MKR,LC)=C(MKP,LC)	GAUSEL99
7	C(MKP,LC)=Q	GAUSE100
71	CONTINUE	GAUSE101
C		GAUSE102
C	NORMAL AND SINGULAR RETURNS. GOOD SOLUTION COULD HAVE D=0.	GAUSE103
8	C(1,1)=D	GAUSE104
	GO TO 91	GAUSE105
9	C(1,1)=0.	GAUSE106
91	RETURN	GAUSE107
	END	GAUSE108

	SUBROUTINE RAYPLT	RAYPLT 2
C	MAIN PLOTTING PROGRAM; INITIALIZES, READS INPUT, PLOTS	RAYPLT 3
C	PROJECTIONS OF RAYS ON A VERTICAL OR HORIZONTAL PLANE.	RAYPLT 4
C	ABS(PLT)=1. PLOTS PROJECTION OF RAYPATH ON VERTICAL PLANE	RAYPLT 5
C	RECTANGULAR EXPANSION BY FACTOR 'PFACTR'	RAYPLT 6
C	=2. PLOTS PROJECTION OF RAYPATH ON GROUND	RAYPLT 7
C	=3. VERTICAL PROJECTION USING RADIAL EXPANSION BY FACTOR	RAYPLT 8
C	'PFACTR'	RAYPLT 9
C	COMMON DECK "FILEC" INSERTED HERE	CFILEC 2

	COMMON /FILEC/NPLTDP	CFILEC 4
	COMMON /PLT/ XL, XR, YB, YT, PRESET	RAYPLT11
	COMMON/PLT/RMIN, RMAX, ALPHA, APLT	RAYPLT12
C		RAYPLT13
C	COMMON DECK "CONST" INSERTED HERE	CCONST 2
	COMMON/PCONST/CREF, RGAS, GAMMA	CCONST 4
	COMMON/MCONST/PI, PIT2, PID2, DEGS, RAD, ALN10	CCONST 5
C	COMMON DECK "FLAG" INSERTED HERE	CFLAG 2
	LOGICAL NEWWR, NEWWP, NEWTRC, PENET	CFLAG 4
	COMMON /FLG/ NTYP, NEWWR, NEWWP, NEWTRC, PENET, LINES, IHOP, HPUNCH	CFLAG 5
	COMMON/FLGP/NSET	CFLAG 6
C	COMMON DECK "RKAM" INSERTED HERE	RKAMCOM2
	REAL KR, KTH, KPH	RKAMCOM4
	COMMON//R, TH, PH, KR, KTH, KPH, RKVARS(14), TPULSE, CSTEP, DRDT(20)	RKAMCOM5
C	COMMON DECK "WW" INSERTED HERE	CWW 2
	PARAMETER (NWARSZ=1000)	CWW1 3
	COMMON/WW/ID(10), MAXW, W(NWARSZ)	CWW1 4
	REAL MAXSTP, MAXERR, INTYP, LLAT, LLON	CWW2 2
	EQUIVALENCE (EARTH, W(1)), (RAY, W(2)), (XMTRH, W(3)), (TLAT, W(4)),	CWW2 3
1	(TLON, W(5)), (OW, W(6)), (FBEG, W(7)), (FEND, W(8)), (FSTEP, W(9)),	CWW2 4
2	(AZ1, W(10)), (AZBEG, W(11)), (AZEND, W(12)), (AZSTEP, W(13)),	CWW2 5
3	(BETA, W(14)), (ELBEG, W(15)), (ELEND, W(16)), (ELSTEP, W(17)),	CWW2 6
8	(RCVRH, W(20)),	CWW2 7
4	(ONLY, W(21)), (HOP, W(22)), (MAXSTP, W(23)), (PLAT, W(24)), (PLON, W(25))	CWW2 8
5	(HMAX, W(26)), (RAYFNC, W(29)), (EXTINC, W(33)),	CWW2 9
6	(HMIN, W(27)), (RGMAX, W(28)),	CWW2 10
8	(INTYP, W(41)), (MAXERR, W(42)), (ERATIO, W(43)),	CWW2 11
6	(STEP1, W(44)), (STPMAX, W(45)), (STPMIN, W(46)), (FACTR, W(47)),	CWW2 12
7	(SKIP, W(71)), (RAYSET, W(72)), (PRTSRP, W(74)), (HITLET, W(75))	CWW2 13
9	, (BINRAY, W(76)), (PAGLN, W(77)), (PLT, W(81)), (PFACTOR, W(82)),	CWW2 14
1	(LLAT, W(83)), (LLON, W(84)), (RLAT, W(85)), (RLON, W(86))	CWW2 15
2	, (TIC, W(87)), (HB, W(88)), (HT, W(89)), (TICV, W(96))	CWW2 16
	REAL MMODEL, MFORM, MID	CWW3 2
C		CWW3 3
C	WIND 100-124	CWW3 4
	EQUIVALENCE (W(100), UMODEL), (W(101), UFORM), (W(102), UID)	CWW3 5
C		CWW3 6
C	DELTA WIND 125-149	CWW3 7
	EQUIVALENCE (W(125), DUMODEL), (W(126), DUFORM), (W(127), DUID)	CWW3 8
C		CWW3 9
C	SOUND SPEED 150-174	CWW3 10
	EQUIVALENCE (W(150), CMODEL), (W(151), CFORM), (W(152), CID)	CWW3 11
	EQUIVALENCE (W(153), REFC)	CWW3 12
C		CWW3 13
C	DELTA SOUND SPEED 175-199	CWW3 14
	EQUIVALENCE (W(175), DCMODEL), (W(176), DCFORM), (W(177), DCID)	CWW3 15
C		CWW3 16
C	TEMPERATURE 200-224	CWW3 17
	EQUIVALENCE (W(200), TMODEL), (W(201), TFORM), (W(202), TID)	CWW3 18
C		CWW3 19
C	DELTA TEMPERATURE 225-249	CWW3 20
	EQUIVALENCE (W(225), DTMODEL), (W(226), DTFORM), (W(227), DTID)	CWW3 21
C		CWW3 22
C	MOLECULAR 250-274	CWW3 23
	EQUIVALENCE (W(250), MMODEL), (W(251), MFORM), (W(252), MID)	CWW3 24

C		CWW3	25
C	RECEIVER HEIGHT 275-299	CWW3	26
C	EQUIVALENCE (W(275),RMODEL), (W(276),RFORM), (W(277),RID)	CWW3	27
C		CWW3	28
C	TOPOGRAPHY 300-324	CWW3	29
C	EQUIVALENCE (W(300),GMODEL), (W(301),GFORM), (W(302),GID)	CWW3	30
C		CWW3	31
C	DELTA TOPOGRAPHY 325-349	CWW3	32
C	EQUIVALENCE (W(325),GUMODEL), (W(326),GUFORM), (W(327),GUID)	CWW3	33
C		CWW3	34
C	UPPER SURFACE TOPOGRAPHY 350-374	CWW3	35
C	EQUIVALENCE (W(350),SMODEL), (W(351),SFORM), (W(352),SID)	CWW3	36
C	PLOT ENHANCEMENTS CONTROL PARAMETERS	CWW3	37
C		CWW3	38
C	EQUIVALENCE (W(490),XFQMDL), (W(491),YFQMDL)	CWW3	39
C	ABSORPTION 500-524	CWW3	40
C	EQUIVALENCE (W(500),AMODEL), (W(501),AFORM), (W(502),AID)	CWW3	41
C		CWW3	42
C	DELTA ABSORPTION 525-549	CWW3	43
C	EQUIVALENCE (W(525),DAMODEL), (W(526),DAFORM), (W(527),DAID)	CWW3	44
C		CWW3	45
C	PRESSURE 550-574	CWW3	46
C	EQUIVALENCE (W(550),PMODEL), (W(551),PFORM), (W(552),PID)	CWW3	47
C		CWW3	48
C	DELTA PRESSURE 575-599	CWW3	49
C	EQUIVALENCE (W(575),DPMODEL), (W(576),DPFORM), (W(577),DPID)	CWW3	50
C		CWW3	51
C	REAL LTIC	RAYPLT18	
C	INTEGER IWDMP(411)	RAYPLT19	
C	EQUIVALENCE (IWDMP, ID)	RAYPLT20	
C		RAYPLT21	
C	EXTERNAL PLOT, PLTLB, PLTLBN, PLTHLB	RAYPLT22	
C		RAYPLT23	
C	DATA NWDSRK/4/	RAYPLT24	
C		RAYPLT25	
C	IF (.NOT.NEWWR) GO TO 8	RAYPLT26	
C	APLT=ABS (PLT)	RAYPLT27	
C		RAYPLT28	
C	NEW W ARRAY -- REINITIALIZE	RAYPLT29	
C	NEWWR=.FALSE.	RAYPLT30	
C	PRESET=1.	RAYPLT31	
C	IF NO ACTIVE PLOTTING, WE ARE STILL DUMPING DATA	RAYPLT32	
C	IF (PLT.EQ.0) GO TO 5	RAYPLT33	
C	INITIALIZE ANNOTATION MODEL	RAYPLT34	
C	CONVERT COORDINATES OF VERTICAL PLANE FROM GEOGRAPHIC TO GEOMAGNETIC	RAYPLT35	
C	SW=SIN (PLAT)	RAYPLT36	
C	CW=SIN (PID2-PLAT)	RAYPLT37	
C	SLM=SIN (LLAT)	RAYPLT38	
C	CLM=SIN (PID2-LLAT)	RAYPLT39	
C	SRM=SIN (RLAT)	RAYPLT40	
C	CRM=SIN (PID2-RLAT)	RAYPLT41	
C	CDPHI=SIN (PID2-(LLON-PLON))	RAYPLT42	
C	PHL=ATAN2 (SIN (LLON-PLON)*CLM, CDPHI*SW*CLM-CW*SLM)	RAYPLT43	
C	CTHL=CDPHI*CW*CLM+SW*SLM	RAYPLT44	
C	STHL=SIN (ACOS (CTHL))	RAYPLT45	

	CDPHI=SIN (PID2-(RLON-PLON))	RAYPLT46
	PHR=ATAN2(SIN (RLON-PLON)*CRM, CDPHI*SW*CRM-CW*SRM)	RAYPLT47
	CTHR=CDPHI*CW*CRM+SW*SRM	RAYPLT48
	STHR=SIN (ACOS (CTHR))	RAYPLT49
	CLR=C*THL*CTHR+STHL*STHR*SIN (PID2-(PHL-PHR))	RAYPLT50
	ALPHA=.5*ACOS (CLR)	RAYPLT51
	SLR=SQRT (1.-CLR**2)	RAYPLT52
C		RAYPLT53
	IF (APLT.EQ.2.) GO TO 3	RAYPLT54
C		RAYPLT55
C	VERTICAL PROJECTIONS ONLY	RAYPLT56
	T=HB	RAYPLT57
	HB=AMIN1(T, HT)	RAYPLT58
	HT=AMAX1(T, HT)	RAYPLT59
	RMIN=EARTH*HB	RAYPLT60
	YT1=YT	RAYPLT61
	RMAX=EARTH*HT	RAYPLT62
C		RAYPLT63
	IF(APLT.NE.4.) GO TO 100	RAYPLT64
C		RAYPLT65
C	SCALE FOR CARTESIAN PROJECTION(=4)	RAYPLT66
	XR=ALPHA	RAYPLT67
	XR1=XR	RAYPLT68
	XL=-XR	RAYPLT69
	XL1=XL	RAYPLT70
	YB=RMIN	RAYPLT71
	YT=RMAX	RAYPLT72
	GO TO 5	RAYPLT73
C		RAYPLT74
C	PROJECTIONS 1 AND 3	RAYPLT75
100	XR1=RMIN*SIN (ALPHA)	RAYPLT76
	XL1=-XR1	RAYPLT77
	YB=RMIN*SIN (PID2-ALPHA)	RAYPLT78
	IF (APLT.EQ.3.) RMAX=RMIN+(RMAX-RMIN)*PFACTR	RAYPLT79
	XR=AMAX1 (RMAX*SIN(ALPHA), (RMAX-YB)/2.)	RAYPLT80
	XL=-XR	RAYPLT81
	YT1=RMAX*(YB/RMIN)	RAYPLT82
	YT=2.0*XR	RAYPLT83
	IF (APLT.EQ.1) YT=YT/PFACTR	RAYPLT84
	YT=YT+YB	RAYPLT85
	GO TO 5	RAYPLT86
C		RAYPLT87
C	HORIZONTAL PROJECTION(=2)	RAYPLT88
3	ALPH1=ATAN2 (STHR*SIN (PHR-PHL), (CTHR-C*THL*CLR)/STHL)	RAYPLT89
	XL=0.0	RAYPLT90
	XL1=0.0	RAYPLT91
	XR=EARTH*2.0*ALPHA	RAYPLT92
	XR1=XR	RAYPLT93
C USE	90% OF X-RANGE FOR Y-RANGE	RAYPLT94
	RMAX=0.5*(0.90*XR)/PFACTR	RAYPLT95
	YT=RMAX	RAYPLT96
	RMIN=-RMAX	RAYPLT97
	YB=RMIN	RAYPLT98
C		RAYPLT99
5	IF(NPLTDP.LE.0) GO TO 8	RAYPL100

	WRITE(NPLTDP) 1,NWDSRK,1,411	RAYPL101
	WRITE(NPLTDP) (IWDMP(I),I=1,411)	RAYPL102
C		RAYPL103
8	NEW=0	RAYPL104
	IF (NEWTRC) NEW=1	RAYPL105
	NEWTRC=.FALSE.	RAYPL106
C		RAYPL107
	IF(NPLTDP.LE.0) GO TO 88	RAYPL108
	IF(NEW.NE.1) GO TO 84	RAYPL109
	WRITE(NPLTDP) 1,NWDSRK,17,25	RAYPL110
	WRITE(NPLTDP) (IWDMP(I),I=17,25)	RAYPL111
C		RAYPL112
84	WRITE(NPLTDP) 3-NEW,R,TH,PH	RAYPL113
C		RAYPL114
88	IF(PLT.EQ.0) RETURN	RAYPL115
C		RAYPL116
	STH=SIN (TH)	RAYPL117
	CTH=SIN (PID2-TH)	RAYPL118
	CR=CTHR*CTH+STHR*STH*SIN (PID2-(PHR-PH))	RAYPL119
	CL=CTHL*CTH+STHL*STH*SIN (PID2-(PHL-PH))	RAYPL120
	CEA=ATAN2 (CR-CL*CLR,CL*SLR)	RAYPL121
C		RAYPL122
	IF(APLT.NE.4.) GO TO 150	RAYPL123
	CALL PLOT(CEA-ALPHA,R,NEW)	RAYPL124
	RETURN	RAYPL125
C		RAYPL126
150	IF(APLT.EQ.2.) GO TO 10	RAYPL127
	RX=R	RAYPL128
	IF(APLT.EQ.3.) RX=RMIN+(R-RMIN)*PFACTR	RAYPL129
	CALL PLOT(CEA-ALPHA,RX,NEW)	RAYPL130
	RETURN	RAYPL131
C		RAYPL132
10	SL=SQRT(AMAX1(0.,1.-CL**2))	RAYPL133
	TMP1=STH*SIN (PH-PHL)	RAYPL134
	TMP2=(CTH-CTHL*CL)/STHL	RAYPL135
	ALPH2=0.	RAYPL136
	IF (TMP1.NE.0..OR.TMP2.NE.0.) ALPH2=ATAN2(TMP1,TMP2)	RAYPL137
	CALL PLOT (EARTH*CEA,EARTH*ASIN(SL*SIN (ALPH1-ALPH2)),NEW)	RAYPL138
	RETURN	RAYPL139
C		RAYPL140
C	DRAW AXES AND CALL FOR LABELING AND TERMINATION OF THIS PLOT	RAYPL141
	ENTRY ENDPLT	RAYPL142
C		RAYPL143
C	IF NEWWR IS STILL TRUE, NO PLOTS WHERE PRODUCED	RAYPL144
	IF(NEWWR) RETURN	RAYPL145
	NEWWR=.TRUE.	RAYPL146
C		RAYPL147
C	SIGNAL END OF PLOT	RAYPL148
	IF(NPLTDP.GT.0) WRITE(NPLTDP) 4,(NWDSRK,I=2,NWDSRK)	RAYPL149
C		RAYPL150
	IF(PLT.EQ.0) RETURN	RAYPL151
C		RAYPL152
	TICKX=0.01*(YT-YB)	RAYPL153
	DTIC=TIC*EARTH	RAYPL154
	CALL SETXY(APLT,-ALPHA,RMIN,ALPHA,RMAX)	RAYPL155

C	IF(APLT.EQ.4.) GO TO 200	RAYPL156
	IF(APLT.EQ.2.) GO TO 25	RAYPL157
C		RAYPL158
C	CURVLINEAR PROJECTIONS(=1,3)	RAYPL159
	CALL ARCTIC(-ALPHA,ALPHA,RMIN,TICKX,PLTHLB)	RAYPL160
	CALL ARCTIC(-ALPHA,ALPHA,RMAX,-TICKX,PLTHLB)	RAYPL161
	GO TO 300	RAYPL162
C		RAYPL163
C	CARTESIAN PROJECTION PUT IN BOTTOM BOUNDARY	RAYPL164
200	CALL TIKLINE(-ALPHA,RMIN,ALPHA,RMIN,TIC,-TICKX,PLTHLB)	RAYPL165
C	PUT IN TOP BOUNDARY	RAYPL166
	CALL TIKLINE(-ALPHA,RMAX,ALPHA,RMAX,TIC,TICKX,PLTHLB)	RAYPL167
C		RAYPL168
300	TIKL=.02*ALPHA	RAYPL169
	LTIC=TICV	RAYPL170
	IF(APLT.EQ.3.) LTIC=TICV*PFACTR	RAYPL171
C	PUT IN LEFT BOUNDARY	RAYPL172
	CALL TIKLINE(-ALPHA,RMIN,-ALPHA,RMAX,LTIC,TIKL,PLTLB)	RAYPL173
C	PUT IN RIGHT BOUNDARY	RAYPL174
	CALL TIKLINE(ALPHA,RMIN,ALPHA,RMAX,LTIC,-TIKL,PLTLBN)	RAYPL175
C		RAYPL176
	GO TO 50	RAYPL177
C	DRAW TICKS, BOX FOR HORIZONTAL PLOT	RAYPL178
25	CALL DRAWTKS(DTIC,TICV,XL,XR,YB,YT,PLOT)	RAYPL179
C		RAYPL180
50	IF(APLT.EQ.2.0) THEN	RAYPL181
	CALL PLTANOT(ID,OW/PIT2,XFQMDL,YFQMDL,XL,YB,XR,YT,DEGS,	RAYPL182
2	LLAT,LLON,RLAT,RLON,HB,HT,APLT,DTIC,DTIC/PFACTR,PLOT)	RAYPL183
	ELSE	RAYPL184
	CALL PLTANOT(ID,OW/PIT2,XFQMDL,YFQMDL,-ALPHA,RMIN,ALPHA,RMAX,	RAYPL185
2	DEGS,LLAT,LLON,RLAT,RLON,HB,HT,APLT,DTIC,TICV,PLOT)	RAYPL186
	ENDIF	RAYPL187
C		RAYPL188
	CALL LABPLT	RAYPL189
	CALL PLTEND	RAYPL190
	RETURN	RAYPL191
	END	RAYPL192
		RAYPL193

	SUBROUTINE PLOT (X,Y,NEW)	PLOT	2
C	PLOTS ONE VECTOR FROM CURRENT PLOT POSITION TO POINT(X,Y)	PLOT	3
C	TAKING BORDER CROSSINGS INTO ACCOUNT.	PLOT	4
	COMMON /PLT/ XMINO,XMAXO,YMINO,YMAXO,RESET	PLOT	5
	COMMON/PLT/RMIN,RMAX,ALPHA,APLT	PLOT	6
	COMMON /DD/ INT,IOR,IT,IS,IC,ICC,IX,IY	PLOT	7
C	DEFINE NOMINAL PLOTTING AREA(ZERO SUFFIXES) AND AN	PLOT	8
C	OUTER CLIPPING BOUNDARY BEYOND WHICH NO VECTORS EXTEND.	PLOT	9
	DATA XOLD,YOLD/0.0,0.0/	PLOT	10
C	90% FOR Y RANGE	PLOT	11
C		PLOT	12
C	COMPUTE SCALE FACTORS	PLOT	13

1	IF (RESET.EQ.0.) GO TO 5	PLOT 14
	RESET=0.	PLOT 15
	IF (APLT.EQ.2.) THEN	PLOT 16
	MRNGE=723	PLOT 17
	MINX0=165	PLOT 18
	MINY0=140	PLOT 19
	ELSE	PLOT 20
	MRNGE=813	PLOT 21
	MINX0=165	PLOT 22
	MINY0=140	PLOT 23
	ENDIF	PLOT 24
	IF (APLT.EQ.4.) MINY0=0	PLOT 25
C		PLOT 26
	MAXX0=MINX0+MRNGE	PLOT 27
	MAXY0=MINY0+MRNGE	PLOT 28
C		PLOT 29
	XSCALE=(MAXX0-MINX0)/(XMAX0-XMIN0)	PLOT 30
	YSCALE=(MAXY0-MINY0)/(YMAX0-YMIN0)	PLOT 31
	XMIN=XMIN0	PLOT 32
	YMIN=YMIN0	PLOT 33
	XMAX=XMAX0	PLOT 34
	YMAX=YMAX0	PLOT 35
	IF (APLT.EQ.2.) GO TO 5	PLOT 36
C		PLOT 37
	XMIN=-ALPHA	PLOT 38
	XMAX=ALPHA	PLOT 39
	YMIN=RMIN	PLOT 40
	YMAX=RMAX	PLOT 41
	IF (APLT.NE.4) GO TO 5	PLOT 42
	YSCALE=.85*YSCALE	PLOT 43
	MINY0=MINY0+60	PLOT 44
C		PLOT 45
C	START A NEW LINE	PLOT 46
C	HORIZONTAL DISPLACEMENT	PLOT 47
5	XS=X-XOLD	PLOT 48
	YS=Y-YOLD	PLOT 49
	S=1.0	PLOT 50
	IF (NEW.EQ.0) GO TO 10	PLOT 51
	IF (X.GE.XMIN.AND.X.LE.XMAX.AND.Y.GE.YMIN.AND.Y.LE.YMAX) GO TO 48	PLOT 52
	GO TO 50	PLOT 53
C		PLOT 54
10	IF (XS) 11,12,16	PLOT 55
C	NEGATIVE	PLOT 56
11	X1=XMAX	PLOT 57
	X2=XMIN	PLOT 58
	GO TO 20	PLOT 59
C	ZERO	PLOT 60
12	IF (YS) 13,50,14	PLOT 61
13	S1=(YMAX-YOLD)/YS	PLOT 62
	S2=(YMIN-YOLD)/YS	PLOT 63
	GO TO 40	PLOT 64
14	S1=(YMIN-YOLD)/YS	PLOT 65
	S2=(YMAX-YOLD)/YS	PLOT 66
	GO TO 40	PLOT 67
C	POSITIVE	PLOT 68

16	X1=XMIN X2=XMAX	PLOT 69
C		PLOT 70
C	VERTICAL DISPLACEMENT	PLOT 71
20	IF (YS) 21,22,26	PLOT 72
C	NEGATIVE	PLOT 73
21	Y1=YMAX	PLOT 74
	Y2=YMIN	PLOT 75
	GO TO 30	PLOT 76
C	ZERO	PLOT 77
22	S1=(X1-XOLD)/XS	PLOT 78
	S2=(X2-XOLD)/XS	PLOT 79
	GO TO 40	PLOT 80
C	POSITIVE	PLOT 81
26	Y1=YMIN	PLOT 82
	Y2=YMAX	PLOT 83
C		PLOT 84
30	S1=AMAX1((X1-XOLD)/XS,(Y1-YOLD)/YS)	PLOT 85
	S2=AMIN1((X2-XOLD)/XS,(Y2-YOLD)/YS)	PLOT 86
C		PLOT 87
C	PLOT LINE -- CHECKING FOR BORDER CROSSINGS	PLOT 88
40	IF (S2.LT.0..OR.S1.GT.1.) GO TO 50	PLOT 89
	IF (S1.LT.0.) GO TO 42	PLOT 90
C	PREVIOUS POINT OFF GRAPH	PLOT 91
	XP=XOLD+XS*S1	PLOT 92
	YP=YOLD+YS*S1	PLOT 93
	IF(APLT.EQ.2.0.OR.APLT.EQ.4.0) GO TO 41	PLOT 94
	T=XP	PLOT 95
	XP=YP*SIN(T)	PLOT 96
	YP=YP*COS(T)	PLOT 97
C		PLOT 98
41	IX=MINX0+(XP-XMIN0)*XSCALE+0.5	PLOT 99
	IY=MINY0+(YP-YMIN0)*YSCALE+0.5	PLOT 100
	CALL DDBP	PLOT 101
	GO TO 48	PLOT 102
C		PLOT 103
42	IF (S2.GT.1.) GO TO 48	PLOT 104
C	CURRENT POINT OFF GRAPH	PLOT 105
	S=S2	PLOT 106
C	CURRENT POINT ON GRAPH	PLOT 107
48	XP=XOLD+XS*S	PLOT 108
	YP=YOLD+YS*S	PLOT 109
	IF(APLT.EQ.2.0.OR.APLT.EQ.4.0) GO TO 49	PLOT 110
	T=XP	PLOT 111
	XP=YP*SIN(T)	PLOT 112
	YP=YP*COS(T)	PLOT 113
49	IX=MINX0+(XP-XMIN0)*XSCALE+0.5	PLOT 114
	IY=MINY0+(YP-YMIN0)*YSCALE+0.5	PLOT 115
	IF(NEW.EQ.0) CALL DDVC	PLOT 116
	IF(NEW.NE.0) CALL DDBP	PLOT 117
C		PLOT 118
C	EXIT ROUTINE	PLOT 119
50	XOLD=X	PLOT 120
	YOLD=Y	PLOT 121
	RETURN	PLOT 122
		PLOT 123

C		PLOT 124
C	TERMINATE THE CURRENT PLOT	PLOT 125
	ENTRY PLTEND(X,Y,NEW)	PLOT 126
	CALL DDFR	PLOT 127
C		PLOT 128
	RETURN	PLOT 129
	END	PLOT 130
	SUBROUTINE LABPLT	LABPLT 2
C	LABEL THE CURRENT PLOT	LABPLT 3
	CHARACTER*80 LABEL,CHID	LABPLT 4
	CHARACTER*4 ANGRANG,ANOTE	LABPLT 5
C	COMMON DECK "SS" INSERTED HERE	CSS 2
	REAL MODSURF	CSS 4
	COMMON/SS/ MODSURF(4)	CSS 5
	COMMON/SS/U, PUR, PURR, PURTH, PURPH	CSS 6
	COMMON/SS/PUTH, PUPH, PUTHTH, PUPHPH, PUTHPH, USELECT, UTIME	CSS 7
C	COMMON DECK "GG" INSERTED HERE	CGG 2
	REAL MODG	CGG 4
	COMMON/GG/MODG(4)	CGG 5
	COMMON/GG/G, PGR, PGRR, PGRTH, PGRPH	CGG 6
	COMMON/GG/PGTH, PGPH, PGTHTH, PGPHPH, PGTHPH, GSELECT, GTIME	CGG 7
C	COMMON DECK "RR" INSERTED HERE	CRR 2
	REAL MODREC	CRR 4
	COMMON/RR/ MODREC(4)	CRR 5
	COMMON/RR/F, PFR, PFRR, PFRTH, PFRPH	CRR 6
	COMMON/RR/PFTH, PFPH, PFTHTH, PFPHPH, PFTHPH, FSELECT, FTIME	CRR 7
C	COMMON DECK "UU" INSERTED HERE	CUU 2
	REAL MODU	CUU 4
	COMMON/UU/MODU(4)	CUU 5
	1 ,V ,PVT ,PVR ,PVTH ,PVPH	CUU 6
	2 ,VR ,PVRT ,PVRR ,PVRTH ,PVRPH	CUU 7
	3 ,VTH ,PVTHT ,PVTHR ,PVTHTH ,PVTHPH	CUU 8
	4 ,VPH ,VPHHT ,VPHHR ,VPHHTH ,VPHPH	CUU 9
C	COMMON DECK "CC" INSERTED HERE	CCC 2
	REAL MODC	CCC 4
	COMMON/CC/MODC(4) , CS , PCST , PCSR , PCSTH , PCSPH	CCC 5
C	COMMON DECK "TT" INSERTED HERE	CTT 2
	REAL MODT	CTT 4
	COMMON/TT/MODT(4) , T , PTT , PTR , PTH , PTPH	CTT 5
C	COMMON DECK "MM" INSERTED HERE	CMM 2
	REAL M,MODM	CMM 4
	COMMON/MM/MODM(4) , M , PMT , PMR , PMTH , PMPH	CMM 5
C	COMMON DECK "HDR" INSERTED HERE	CHDR 2
	CHARACTER*10 INITID*80,DAT,TOD	CHDR 4
	COMMON/HDR/SEC	CHDR 5
	COMMON/HDR/INITID,DAT,TOD	CHDR 6
C	COMMON DECK "RINPLEX" INSERTED HERE	CRINPLE2
	REAL KAY2,KAY2I	CRINPLE4
	COMPLEX PNP,POLAR,LPOLAR	CRINPLE5
	LOGICAL SPACE	CRINPLE6

	CHARACTER DISPM*6		CRINPLE7
	COMMON/RINPL/DISPM		CRINPLE8
	COMMON /RIN/ MODRIN(8), RAYNAME(2,3), TYPE(3), SPACE		CRINPLE9
	COMMON/RIN/OMEGMIN, OMEGMAX, KAY2, KAY2I		CRINPL10
	COMMON/RIN/PNP(10), POLAR, LPOLAR, SGN		CRINPL11
	COMMON /DD/ INT, IOR, IT, IS, IC, ICC, IX, IY		LABPLT15
C	COMMON DECK "CONST" INSERTED HERE		CCONST 2
	COMMON/PCONST/CREF, RGAS, GAMMA		CCONST 4
	COMMON/MCONST/PI, PIT2, PID2, DEGS, RAD, ALN10		CCONST 5
C	COMMON DECK "FLAG" INSERTED HERE		CFLAG 2
	LOGICAL NEWWR, NEWWP, NEWTRC, PENET		CFLAG 4
	COMMON /FLG/ NTYP, NEWWR, NEWWP, NEWTRC, PENET, LINES, IHOP, HPUNCH		CFLAG 5
	COMMON/FLGP/NSET		CFLAG 6
C	COMMON DECK "WW" INSERTED HERE		CWW 2
	PARAMETER (NWARSZ=1000)		CWW1 3
	COMMON/WW/ID(10), MAXW, W(NWARSZ)		CWW1 4
	REAL MAXSTP, MAXERR, INTYP, LLAT, LLON		CWW2 2
	EQUIVALENCE (EARTH, W(1)), (RAY, W(2)), (XMTRH, W(3)), (TLAT, W(4)),		CWW2 3
	1 (TLON, W(5)), (OW, W(6)), (FBEG, W(7)), (FEND, W(8)), (FSTEP, W(9)),		CWW2 4
	2 (AZ1, W(10)), (AZBEG, W(11)), (AZEND, W(12)), (AZSTEP, W(13)),		CWW2 5
	3 (BETA, W(14)), (ELBEG, W(15)), (ELEND, W(16)), (ELSTEP, W(17)),		CWW2 6
	8 (RCVRH, W(20)),		CWW2 7
	4 (ONLY, W(21)), (HOP, W(22)), (MAXSTP, W(23)), (PLAT, W(24)), (PLON, W(25))		CWW2 8
	5, (HMAX, W(26)), (RAYFNC, W(29)), (EXTINC, W(33)),		CWW2 9
	6 (HMIN, W(27)), (RGMAX, W(28)),		CWW2 10
	8 (INTYP, W(41)), (MAXERR, W(42)), (ERATIO, W(43)),		CWW2 11
	6 (STEP1, W(44)), (STPMAX, W(45)), (STPMIN, W(46)), (FACTR, W(47)),		CWW2 12
	7 (SKIP, W(71)), (RAYSET, W(72)), (PRTSRP, W(74)), (HITLET, W(75))		CWW2 13
	9, (BINRAY, W(76)), (PAGLN, W(77)), (PLT, W(81)), (PFACTR, W(82)),		CWW2 14
	1 (LLAT, W(83)), (LLON, W(84)), (RLAT, W(85)), (RLON, W(86))		CWW2 15
	2, (TIC, W(87)), (HB, W(88)), (HT, W(89)), (TICV, W(96))		CWW2 16
	REAL MMODEL, MFORM, MID		CWW3 2
C			CWW3 3
C	WIND 100-124		CWW3 4
	EQUIVALENCE (W(100), UMODEL), (W(101), UFORM), (W(102), UID)		CWW3 5
C			CWW3 6
C	DELTA WIND 125-149		CWW3 7
	EQUIVALENCE (W(125), DUMODEL), (W(126), DUFORM), (W(127), DUID)		CWW3 8
C			CWW3 9
C	SOUND SPEED 150-174		CWW3 10
	EQUIVALENCE (W(150), CMODEL), (W(151), CFORM), (W(152), CID)		CWW3 11
	EQUIVALENCE (W(153), REFC)		CWW3 12
C			CWW3 13
C	DELTA SOUND SPEED 175-199		CWW3 14
	EQUIVALENCE (W(175), DCMODEL), (W(176), DCFORM), (W(177), DCID)		CWW3 15
C			CWW3 16
C	TEMPERATURE 200-224		CWW3 17
	EQUIVALENCE (W(200), TMODEL), (W(201), TFORM), (W(202), TID)		CWW3 18
C			CWW3 19
C	DELTA TEMPERATURE 225-249		CWW3 20
	EQUIVALENCE (W(225), DTMODEL), (W(226), DTFORM), (W(227), DTID)		CWW3 21
C			CWW3 22
C	MOLECULAR 250-274		CWW3 23
	EQUIVALENCE (W(250), MMODEL), (W(251), MFORM), (W(252), MID)		CWW3 24
C			CWW3 25

C	RECEIVER HEIGHT 275-299	CWW3 26
	EQUIVALENCE (W(275),RMODEL), (W(276),RFORM), (W(277),RID)	CWW3 27
C		CWW3 28
C	TOPOGRAPHY 300-324	CWW3 29
	EQUIVALENCE (W(300),GMODEL), (W(301),GFORM), (W(302),GID)	CWW3 30
C		CWW3 31
C	DELTA TOPOGRAPHY 325-349	CWW3 32
	EQUIVALENCE (W(325),GUMODEL), (W(326),GUFORM), (W(327),GUID)	CWW3 33
C		CWW3 34
C	UPPER SURFACE TOPOGRAPHY 350-374	CWW3 35
	EQUIVALENCE (W(350),SMODEL), (W(351),SFORM), (W(352),SID)	CWW3 36
C	PLOT ENHANCEMENTS CONTROL PARAMETERS	CWW3 37
C		CWW3 38
	EQUIVALENCE (W(490),XFQMDL), (W(491),YFQMDL)	CWW3 39
C	ABSORPTION 500-524	CWW3 40
	EQUIVALENCE (W(500),AMODEL), (W(501),AFORM), (W(502),AID)	CWW3 41
C		CWW3 42
C	DELTA ABSORPTION 525-549	CWW3 43
	EQUIVALENCE (W(525),DAMODEL), (W(526),DAFORM), (W(527),DAID)	CWW3 44
C		CWW3 45
C	PRESSURE 550-574	CWW3 46
	EQUIVALENCE (W(550),PMODEL), (W(551),PFORM), (W(552),PID)	CWW3 47
C		CWW3 48
C	DELTA PRESSURE 575-599	CWW3 49
	EQUIVALENCE (W(575),DPMODEL), (W(576),DPFORM), (W(577),DPID)	CWW3 50
C		CWW3 51
C		LABPLT19
C	COMMON DECK "AA" INSERTED HERE	CAA 2
	REAL MODA	CAA 4
	REAL MU, MUPT, MUPR, MUPTH, MUPPH	CAA 5
	REAL KAP, KAPPT, KAPPR, KAPPTH, KAPPPH	CAA 6
	COMMON/AA/MODA(4), MU, MUPT, MUPR, MUPTH, MUPPH	CAA 7
	COMMON/AA/KAP, KAPPT, KAPPR, KAPPTH, KAPPPH	CAA 8
C	COMMON DECK "PP" INSERTED HERE	CPP 2
	REAL MODP	CPP 4
	COMMON/PP/MODP(4), P, PPT, PPR, PPTH, PPPH	CPP 5
C		LABPLT22
	WRITE(LABEL,900) ID	LABPLT23
900	FORMAT(10A8)	LABPLT24
	CHID=LABEL	LABPLT25
	LABEL=CHID(5:)	LABPLT26
	IOR=0	LABPLT27
	IT=0	LABPLT28
	IS=2	LABPLT29
	IX=0	LABPLT30
	IY=1023	LABPLT31
	CALL DDTEXT(8,LABEL)	LABPLT32
	IX=1090	LABPLT33
	IY=0	LABPLT34
	CALL DDTEXT(2,DAT)	LABPLT35
	IY=1023	LABPLT36
	F=OW/PIT2	LABPLT37
	NANGLE=10	LABPLT38
	ANGRANG='EL ='	LABPLT39
	ANOTE='AZ ='	LABPLT40

ANEL=0.	LABPLT41
IF(ELSTEP.NE.0.0) ANEL=(ELEND-ELBEG)/ELSTEP+1.5	LABPLT42
IF(ANEL.GT.1.0.OR.PLT.LT.0.0) GO TO 100	LABPLT43
ANGRANG='AZ ='	LABPLT44
ANOTE='EL ='	LABPLT45
NANGLE=14	LABPLT46
100 WRITE(LABEL,1300) CHID(1:3),F,ANOTE,W(NANGLE)*DEGS	LABPLT47
1300 FORMAT('MODEL = ',A,' ,FREQ = ',F9.3,' HZ, ',A,F7.3,' DEG')	LABPLT48
IX=0	LABPLT49
IY=IY-32	LABPLT50
CALL DDTEXT(7,LABEL)	LABPLT51
C	LABPLT52
C INDEX OF OPPOSITE ANGLE	LABPLT53
NANGLE=(10+14-NANGLE)+1	LABPLT54
NANGLE2=NANGLE+2	LABPLT55
WRITE(LABEL,1400) ANGRANG,(W(I)*DEGS,I=NANGLE,NANGLE2)	LABPLT56
1400 FORMAT(A,F7.2,' DEG TO',F7.2,' DEG, STEP = ',F7.2,' DEG')	LABPLT57
IY=IY-32	LABPLT58
CALL DDTEXT(7,LABEL)	LABPLT59
C	LABPLT60
WRITE(LABEL,1500) XMTRH,TLAT*DEGS,TLON*DEGS	LABPLT61
1500 FORMAT('XMTR HT = ',F6.2,' KM ,LAT = ',F6.2,' DEG, LONG = '	LABPLT62
1    ,F6.2,' DEG')	LABPLT63
IY=IY-32	LABPLT64
CALL DDTEXT(7,LABEL)	LABPLT65
C	LABPLT66
IY=IY-32	LABPLT67
WRITE(LABEL,'(10A8)') MODRIN	LABPLT68
CALL DDTEXT(8,LABEL)	LABPLT69
C	LABPLT70
IX=1050	LABPLT71
CALL DDTEXT(1,'MODELS')	LABPLT72
IY=IY-15	LABPLT73
C	LABPLT74
LOOP FOR 8 MODELS AND PERTURBATIONS	LABPLT75
DO 1700 K=1,16	LABPLT76
I=(K-1)/2+1	LABPLT77
C	LABPLT78
GENERATE ALTERNATING 1,2;3,4 SERIES FOR MODEL AND PERTURBATION	LABPLT79
J1=2*(K+1-I*2)+1	LABPLT80
J2=J1+1	LABPLT81
IF(I.EQ.1) WRITE(LABEL,1600) (MODU(J),J=J1,J2)	LABPLT82
IF(I.EQ.2) WRITE(LABEL,1600) (MODC(J),J=J1,J2)	LABPLT83
IF(I.EQ.3) WRITE(LABEL,1600) (MODT(J),J=J1,J2)	LABPLT84
IF(I.EQ.4 .AND. J1.EQ.1)	LABPLT85
1 WRITE(LABEL,1600) (MODM(J),J=J1,J2)	LABPLT86
C	LABPLT87
IF(I.EQ.5) WRITE(LABEL,1600) (MODG(J),J=J1,J2)	LABPLT88
IF(I.EQ.6) WRITE(LABEL,1600) (MODA(J),J=J1,J2)	LABPLT89
IF(I.EQ.7) WRITE(LABEL,1600) (MODP(J),J=J1,J2)	LABPLT90
C NO FURTHER OUTPUT FOR MODELS WITHOUT PERTURBATIONS	LABPLT91
IF(J1.GT.1) GO TO 1610	LABPLT92
IF(I.EQ.8) WRITE(LABEL,1600) (MODREC(J),J=J1,J2)	LABPLT93
1600 FORMAT(2(2(A8,2X,F5.1,1X),2X))	LABPLT94
C	LABPLT95
1610 IF(LABEL(1:1).EQ.' ') GO TO 1700	
IY=IY-32	

1700	CALL DDTEXT(2,LABEL)	LABPLT96
C	LABEL(1:1)=' '	LABPLT97
	END	LABPLT98
		LABPLT99

C	SUBROUTINE PLTHLB(X,Y,NC)	PLTHLB 2
C	HORIZONTAL TICK ANNOTATION ROUTINE FOR RAYPLOT.	PLTHLB 3
C		PLTHLB 4
	EXTERNAL PLOT	PLTHLB 5
C		PLTHLB 6
	CALL PLTANH(X,Y,NC,PLOT)	PLTHLB 7
	END	PLTHLB 8
		PLTHLB 9

C	SUBROUTINE PLTANH(X,Y,NC,PLOT)	PLTANH 2
C	TIC LABELING ROUTINE FOR HORIZONTAL PLOT PROJECTIONS	PLTANH 3
C		PLTANH 4
	CHARACTER ANNOT*10	PLTANH 5
	COMMON/DD/IN,IOR,IT,IS,IC,ICC,IX,IY	PLTANH 6
C	COMMON DECK "WWR" INSERTED HERE	PLTANH 7
	PARAMETER (NWARSZ=1000)	CWWR 2
	COMMON/WW/ID(10),MAXW,W(NWARSZ)	CWW1 3
	REAL MAXSTP,MAXERR,INTYP,LLAT,LLON	CWW1 4
	EQUIVALENCE (EARTH,W(1)),(RAY,W(2)),(XMTRH,W(3)),(TLAT,W(4)),	CWW2 2
	1 (TLON,W(5)),(OW,W(6)),(FBEG,W(7)),(FEND,W(8)),(FSTEP,W(9)),	CWW2 3
	2 (AZ1,W(10)),(AZBEG,W(11)),(AZEND,W(12)),(AZSTEP,W(13)),	CWW2 4
	3 (BETA,W(14)),(ELBEG,W(15)),(ELEND,W(16)),(ELSTEP,W(17)),	CWW2 5
	8 (RCVRH,W(20)),	CWW2 6
	4 (ONLY,W(21)),(HOP,W(22)),(MAXSTP,W(23)),(PLAT,W(24)),(PLON,W(25))	CWW2 7
	5,(HMAX,W(26)),(RAYFNC,W(29)),(EXTINC,W(33)),	CWW2 8
	6 (HMIN,W(27)),(RGMAX,W(28)),	CWW2 9
	8 (INTYP,W(41)),(MAXERR,W(42)),(ERATIO,W(43)),	CWW2 10
	6 (STEP1,W(44)),(STPMAX,W(45)),(STPMIN,W(46)),(FACTR,W(47)),	CWW2 11
	7 (SKIP,W(71)),(RAYSET,W(72)),(PRTSRP,W(74)),(HITLET,W(75))	CWW2 12
	9 ,(BINRAY,W(76)),(PAGLN,W(77)),(PLT,W(81)),(PFACTR,W(82)),	CWW2 13
	1 (LLAT,W(83)),(LLON,W(84)),(RLAT,W(85)),(RLON,W(86))	CWW2 14
	2,(TIC,W(87)),(HB,W(88)),(HT,W(89)),(TICV,W(96))	CWW2 15
C	COMMON DECK "CONST" INSERTED HERE	CWW2 16
	COMMON/PCONST/CREG,RGAS,GAMMA	CCONST 2
	COMMON/MCONST/PI,PIT2,PID2,DEGS,RAD,ALN10	CCONST 4
	COMMON/LABCLT/PROJCT,THMIN,THMAX,RMIN,RMAX	CCONST 5
C		PLTANH10
	COMMON/RAYCON/MCONP	PLTANH11
C		PLTANH12
		PLTANH13
C		PLTANH14
	DATA LNC/-100/	PLTANH15

<pre> C      IF(NC.LE.0 .OR. NC.GT.2) GO TO 100 C      NORMALIZE LETTER SIZE FACTOR TO .15 INCHES       HLETF=HITLET/.15 C       IF(LNC.NE.NC) LICM=-100       LNC=NC C       CALL PLOT(X,Y,1)       IX=IX-80*HLETF       ICM=IX       IF(NC.GT.1) THEN           ICM=IY           IX=IX-40       ENDIF C       INSURE THAT OVERLAPS OF ANNOTATIONS DO NOT OCCUR       IF(IABS(ICM-LICM).LT.INT(80*HLETF)) GO TO 100 C       IF(PROJECT.EQ.2.0) GO TO 25       IF(HB.GE.0.0.AND.Y.GT.(RMIN+RMAX)/2) GO TO 100       IF(HB.LT.0.0.AND.Y.LT.(RMIN+RMAX)/2) GO TO 100 C 25     F=DEGS       TMP=(THMAX-THMIN)*DEGS       IF(TMP.LT.10.) F =EARTH       FT=F       IF(PROJECT.EQ.2.0 .AND. MCONP.EQ.0) F=F/EARTH       V=X-THMIN       IF(NC.GT.1) V=Y-(RMIN+RMAX)/2.       IF(ABS(AMOD(TIC*FT+.0001,1.)).GT..001) GO TO 60 C       WRITE(ANNOT,50) INT(V*F+SIGN(.5,V))       FORMAT(I5)       GO TO 90 C 60     WRITE(ANNOT,80) V*F       FORMAT(F8.2) C 90     LICM=ICM C      ALLOW 8 RASTERS FOR THE LETTER HEIGHT       H=HB       IF(PROJECT.EQ.2.0) H=0.       IF(NC.EQ.1) IY=IY-8*HLETF-SIGN(52.,H)       IOR=0 95     FORMAT(3G13.6,2I5,1X,A10) 99     FORMAT(2G13.6,5I5,1X,A10)       CALL DDTEXT(1,ANNOT) C 100    CALL PLOT(X,Y,MIN0(1,NC))       END </pre>	<pre> PLTANH16 PLTANH17 PLTANH18 PLTANH19 PLTANH20 PLTANH21 PLTANH22 PLTANH23 PLTANH24 PLTANH25 PLTANH26 PLTANH27 PLTANH28 PLTANH29 PLTANH30 PLTANH31 PLTANH32 PLTANH33 PLTANH34 PLTANH35 PLTANH36 PLTANH37 PLTANH38 PLTANH39 PLTANH40 PLTANH41 PLTANH42 PLTANH43 PLTANH44 PLTANH45 PLTANH46 PLTANH47 PLTANH48 PLTANH49 PLTANH50 PLTANH51 PLTANH52 PLTANH53 PLTANH54 PLTANH55 PLTANH56 PLTANH57 PLTANH58 PLTANH59 PLTANH60 PLTANH61 PLTANH62 PLTANH63 PLTANH64 PLTANH65 PLTANH66 </pre>
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	SUBROUTINE SETXY (PROJ, XMIN, YMIN, XMAX, YMAX)	SETXY 2
C	PLOT INITIALIZATION; SETS PROJECTION PARAMETERS	SETXY 3
C		SETXY 4
	COMMON/LABCLT/PROJCT, THMIN, THMAX, RMIN, RMAX	SETXY 5
C		SETXY 6
C		SETXY 7
C	INITIAL ANNOTATION MODEL	SETXY 8
	CALL SETANN	SETXY 9
C		SETXY 10
	PROJECT=PROJ	SETXY 11
	THMIN=XMIN	SETXY 12
	RMIN=YMIN	SETXY 13
	THMAX=XMAX	SETXY 14
	RMAX=YMAX	SETXY 15
	END	SETXY 16
	SUBROUTINE TIKLINE (XL1, YB, XL, YT1, TICV, TIKSZ, PLOT)	TIKLINE2
C	DRAWS STRAIGHT LINE WITH TICKS AT INTERVALS	TIKLINE3
C		TIKLINE4
C		TIKLINE5
	XDF=XL-XL1	TIKLINE6
	YDF=YT1-YB	TIKLINE7
	DST=SQRT (XDF*XDF+YDF*YDF)	TIKLINE8
	TICE=DST	TIKLINE9
	T=0.0	TIKLINE10
	IF (TICV.EQ.0.0) GO TO 50	TIKLINE11
	TICE=TICV	TIKLINE12
	T=TIKSZ/TICV	TIKLINE13
C		TIKLINE14
50	TICVX=TICE*XDF/DST	TIKLINE15
	TICVY=TICE*YDF/DST	TIKLINE16
	TX=TICVY*T	TIKLINE17
	TY=-TICVX*T	TIKLINE18
	NTIC=1+DST/TICE	TIKLINE19
	CALL PLOT (XL1, YB, -1)	TIKLINE20
	DO 100 I=0, NTIC-1	TIKLINE21
	X=XL1+I*TICVX	TIKLINE22
	Y=YB+I*TICVY	TIKLINE23
	CALL PLOT (X, Y, 0)	TIKLINE24
	CALL PLOT (X+TX, Y+TY, 0)	TIKLINE25
100	CALL PLOT (X, Y, 1)	TIKLINE26
	CALL PLOT (XL, YT1, 0)	TIKLINE27
	CALL PLOT (XL, YT1, 1)	TIKLINE28
	END	TIKLINE29
	SUBROUTINE PLTANOT (ID, FREQ, XMF, YMF, XL, YB, XR, YT	PLTANOT2

1	, DEGS, LLAT, LLON, RLAT, RLON, ALTLOW, ALTHI, PLT, DTICH, DTICV, PLOT)	PLTANOT3
C	PUTS STANDARD ANNOTATIONS ON PLOTS	PLTANOT4
C		PLTANOT5
	COMMON/LABCLT/PROJCT, THMIN, THMAX, RMIN, RMAX	PLTANOT6
	REAL LLAT, LLON	PLTANOT7
	CHARACTER LABEL*80	PLTANOT8
	COMMON /DD/ INT, IOR, IT, IS, IC, ICC, IX, IY	PLTANOT9
C	COMMON DECK "ANNOT" INSERTED HERE	ANNOT 2
	CHARACTER*10 ANOTES, HNOTES	ANNOT 4
	COMMON/ANNCTL/LENA(4), LENHA(3)	ANNOT 5
	COMMON/ANNCTC/ANOTES(2,4), HNOTES(4,3)	ANNOT 6
C		PLTANO11
	IF(PLT.EQ.2. .OR. XMF.LE.0.0 .OR. YMF.LE.0.0) GO TO 45	PLTANO12
	CALL PLOT(XL+XMF*(XR-XL), YB+YMF*(YT-YB), 1)	PLTANO13
	IF(FREQ.LE.0.0) GO TO 30	PLTANO14
C		PLTANO15
	WRITE(LABEL,25) FREQ	PLTANO16
25	FORMAT('FREQ =', F9.3)	PLTANO17
	CALL DDTEXT(2, LABEL)	PLTANO18
	IY=IY+40	PLTANO19
C		PLTANO20
30	WRITE(LABEL,35) ID	PLTANO21
35	FORMAT('MODEL = ', A3)	PLTANO22
	CALL DDTEXT(2, LABEL)	PLTANO23
C		PLTANO24
45	NSPY=97	PLTANO25
	IOR=0	PLTANO26
C		PLTANO27
C	FIRST THE LOW ALTITUDE-LATITUDE ANNOTATION	PLTANO28
50	CALL PLOT(XL, YB, 1)	PLTANO29
	IX=IX-155	PLTANO30
	IY=IY-NSPY	PLTANO31
	WRITE(LABEL,1840) DEGS*LLON	PLTANO32
	CALL DDTEXT(2, LABEL)	PLTANO33
	WRITE(LABEL,1850) DEGS*LLAT	PLTANO34
	IY=IY-32	PLTANO35
	CALL DDTEXT(2, LABEL)	PLTANO36
C		PLTANO37
C	NEXT THE RIGHT LATITUDE ANNOTATION	PLTANO38
	CALL PLOT(XR, YB, 1)	PLTANO39
	IX=IX-130	PLTANO40
	IY=IY-NSPY	PLTANO41
	WRITE(LABEL,1840) DEGS*RLON	PLTANO42
	CALL DDTEXT(2, LABEL)	PLTANO43
	WRITE(LABEL,1850) DEGS*RLAT	PLTANO44
	IY=IY-32	PLTANO45
	CALL DDTEXT(2, LABEL)	PLTANO46
C		PLTANO47
	XMID=(XL+XR)/2.0	PLTANO48
	IF(PLT.EQ.2.0) GO TO 55	PLTANO49
C		PLTANO50
C	PUT THE HORIZONTAL TIC LABEL	PLTANO51
	Y=YT	PLTANO52
	IF(ALTLOW.GE.0.0) Y=YB	PLTANO53
	CALL PLOT(XMID, Y, 1)	PLTANO54

C	IF(ALTLOW.LT.0.0) IY=IY+80	PLTANO55
	IF(ALTLOW.GE.0.0) IY=IY-95	PLTANO56
	GO TO 60	PLTANO57
C		PLTANO58
55	CALL PLOT(XMID,YB,1)	PLTANO59
	IY=IY-95	PLTANO60
C		PLTANO61
60	IX=IX-235	PLTANO62
	NOTEA=1	PLTANO63
	TMP=(THMAX-THMIN)*DEGS	PLTANO64
	IF(TMP.GT.10.) NOTEA=2	PLTANO65
C		PLTANO66
	CALL DDTEXT (LENHA(NOTEA),HNOTES(1,NOTEA))	PLTANO67
C		PLTANO68
C	PUT THE VERTICAL TIC LABEL	PLTANO69
	CALL PLOT(XL,(YB+YT)/2.0,1)	PLTANO70
	IOR=1	PLTANO71
	IF(PLT.NE.2.) GO TO 100	PLTANO72
C		PLTANO73
C	HORIZONTAL PLOT PUT Y-AXIS ANNOTATION	PLTANO74
C		PLTANO75
	IX=IX-125	PLTANO76
	IY=200	PLTANO77
	CALL DDTEXT (LENHA(3),HNOTES(1,3))	PLTANO78
	GO TO 200	PLTANO79
C		PLTANO80
100	IX=IX-125	PLTANO81
	IY=IY-75	PLTANO82
	NOTEA=1	PLTANO83
	IF(ALTLOW.GE.0.0) NOTEA=3	PLTANO84
	IF(ABS(ALTHI-ALTLOW).GE.1.) NOTEA=NOTEA+1	PLTANO85
	CALL DDTEXT (LENA(NOTEA),ANOTES(1,NOTEA))	PLTANO86
C		PLTANO87
200	IOR=0	PLTANO88
1840	FORMAT(F7.2,' DEG E.')	PLTANO89
1850	FORMAT(F7.2,' DEG N.')	PLTANO90
C		PLTANO91
	END	PLTANO92
		PLTANO93

C	SUBROUTINE DRAWTKS (DTICH,DTICV,XLPR,XR,YBPR,YT,PLOT)	DRAWTKS2
C	HORIZONTAL PLOT PROJECTION SUPPORT ROUTINE.	DRAWTKS3
C	DRAW BOUNDARY TO PLOT AREA, TICS AND TIC LABELS.	DRAWTKS4
C		DRAWTKS5
	EXTERNAL PLOT	DRAWTKS6
C		DRAWTKS7
	XL=XLPR	DRAWTKS8
	YB=YBPR	DRAWTKS9
	YMID=.5*(YB+YT)	DRAWTK10
	TICX=.01*(YT-YB)	DRAWTK11
		DRAWTK12

	TICY=.01*(XR-XL)	DRAWTK13
	YBP=YB	DRAWTK14
	IF(DTICV.GT.0.) YBP=YMID-AINT((YMID-YB)/DTICV)*DTICV	DRAWTK15
C		DRAWTK16
	NTICX=(XR-XL)/DTICH	DRAWTK17
	NTICY=1	DRAWTK18
	IF(DTICV.GT.0.) NTICY=(YT-YBP+DTICV)/DTICV	DRAWTK19
C&	PRINT *,"DRAWTKS ",XLPR,XR,YBPR,YBP,YT,DTICH,DTICV,NTICX,NTICY	DRAWTK20
	IOF=0	DRAWTK21
C		DRAWTK22
C	TWO PASSES BOTTOM AND LEFT THEN TOP AND RIGHT	DRAWTK23
	DO 100 J=1,2	DRAWTK24
	CALL PLOT(XL,YBPR,1)	DRAWTK25
	DO 30 I=1,NTICY	DRAWTK26
	Y=YBP+(I-1)*DTICV	DRAWTK27
	CALL PLOT(XL,Y,0)	DRAWTK28
	CALL PLOT(XL+TICY,Y,0)	DRAWTK29
30	CALL PLTANH(XL,Y,IOF+2,PLOT)	DRAWTK30
	CALL PLOT(XL,YT,0)	DRAWTK31
C		DRAWTK32
	CALL PLOT(XLPR,YB,1)	DRAWTK33
C		DRAWTK34
	DO 40 I=1,NTICX	DRAWTK35
	X=XLPR+I*DTICH	DRAWTK36
	CALL PLOT(X,YB,0)	DRAWTK37
	CALL PLOT(X,YB+TICX,0)	DRAWTK38
	CALL PLTANH(X,YB,IOF+1,PLOT)	DRAWTK39
40	CALL PLOT(X,YB,1)	DRAWTK40
	CALL PLOT(XR,YB,0)	DRAWTK41
	YB=YT	DRAWTK42
	XL=XR	DRAWTK43
	TICX=-TICX	DRAWTK44
	TICY=-TICY	DRAWTK45
100	IOF=10	DRAWTK46
C		DRAWTK47
	CALL PLOT(XLPR,YMID,1)	DRAWTK48
	CALL PLOT(XR,YMID,0)	DRAWTK49
	END	DRAWTK50

	SUBROUTINE PLTLB(X,PY,NCP)	PLTLB 2
C	PUT VERTICAL TIC ANNOTATIONS ON RAY PLOT	PLTLB 3
C	THIS IS A SPECIAL PURPOSE SUBSTITUTE FOR THE 'PLOT' ROUTINE	PLTLB 4
C	IT COMPUTES THE NEAREST ROUNDED TIC POSITIONS FOR VERTICAL LINES.	PLTLB 5
C	WHEN THE NC PARAMETER IS > 0 AN ANNOTATION IS GENERATED	PLTLB 6
C	AT THE TIC POSITION. THE ADDITIONAL NC VALUE < 0 ALLOWS FOR	PLTLB 7
C	SIMPLE PEN UP MOTION TO THE X,Y POSITION.	PLTLB 8
C		PLTLB 9
	CHARACTER ANNOT*10	PLTLB 10
C		PLTLB 11
C	COMMON DECK "WWR" INSERTED HERE	CWWR 2
	PARAMETER (NWARSZ=1000)	CWW1 3

	COMMON/WW/ID(10),MAXW,W(NWARSZ)	CWW1	4
	REAL MAXSTP,MAXERR,INTYP,LLAT,LLON	CWW2	2
	EQUIVALENCE (EARTH,W(1)),(RAY,W(2)),(XMTRH,W(3)),(TLAT,W(4)),	CWW2	3
	1 (TLON,W(5)),(OW,W(6)),(FBEG,W(7)),(FEND,W(8)),(FSTEP,W(9)),	CWW2	4
	2 (AZ1,W(10)),(AZBEG,W(11)),(AZEND,W(12)),(AZSTEP,W(13)),	CWW2	5
	3 (BETA,W(14)),(ELBEG,W(15)),(ELEND,W(16)),(ELSTEP,W(17)),	CWW2	6
	8 (RCVRH,W(20)),	CWW2	7
	4 (ONLY,W(21)),(HOP,W(22)),(MAXSTP,W(23)),(PLAT,W(24)),(PLON,W(25))	CWW2	8
	5,(HMAX,W(26)),(RAYFNC,W(29)),(EXTINC,W(33)),	CWW2	9
	6 (HMIN,W(27)),(RGMAX,W(28)),	CWW2	10
	8 (INTYP,W(41)),(MAXERR,W(42)),(ERATIO,W(43)),	CWW2	11
	6 (STEP1,W(44)),(STPMAX,W(45)),(STPMIN,W(46)),(FACTR,W(47)),	CWW2	12
	7 (SKIP,W(71)),(RAYSET,W(72)),(PRTSRP,W(74)),(HITLET,W(75))	CWW2	13
	9 ,(BINRAY,W(76)),(PAGLN,W(77)),(PLT,W(81)),(PFACTR,W(82)),	CWW2	14
	1 (LLAT,W(83)),(LLON,W(84)),(RLAT,W(85)),(RLON,W(86))	CWW2	15
	2,(TIC,W(87)),(HB,W(88)),(HT,W(89)),(TICV,W(96))	CWW2	16
	COMMON /DD/ IINT,IOR,IT,IS,IC,ICC,IX,IY	PLTLB	13
	COMMON/LABCLT/PROJCT,THMIN,THMAX,RMIN,RMAX	PLTLB	14
C		PLTLB	15
	DATA LIY/-100/	PLTLB	16
C		PLTLB	17
	NC=NCP	PLTLB	18
	GO TO 10	PLTLB	19
C		PLTLB	20
	ENTRY PLTLBN(X,PY,NCP)	PLTLB	21
	NC=0	PLTLB	22
C		PLTLB	23
10	Y=PY	PLTLB	24
C		PLTLB	25
	IF(NCP.LT.0) GO TO 200	PLTLB	26
	F=1.	PLTLB	27
	IF(AMAX1(ABS(RMAX-EARTH),ABS(RMIN-EARTH)).LT.1.) F=1000.	PLTLB	28
	Y=INT((Y-EARTH)*F)/F+EARTH	PLTLB	29
	IF(NC.EQ.0) GO TO 100	PLTLB	30
C		PLTLB	31
	V=Y	PLTLB	32
	IF(PROJCT.EQ.3.) V=RMIN+(Y-RMIN)/PFACTR	PLTLB	33
C		PLTLB	34
	IF(ABS(AINT(TICV*F)-TICV*F).GT..001) GO TO 60	PLTLB	35
	WRITE(ANNOT,50) INT(ABS(V-EARTH)*F)	PLTLB	36
50	FORMAT(I3)	PLTLB	37
	GO TO 90	PLTLB	38
C		PLTLB	39
60	WRITE(ANNOT,80) ABS(V-EARTH)*F	PLTLB	40
80	FORMAT(F6.2)	PLTLB	41
C		PLTLB	42
90	CALL PLOT(X,PY,1)	PLTLB	43
	CALL PLOT(X,Y,1)	PLTLB	44
C		PLTLB	45
	INSURE THAT OVERLAPS OF ANNOTATIONS DO NOT OCCUR	PLTLB	46
	IF(IABS(IY-LIY).LT.80) GO TO 100	PLTLB	47
	LIY=IY	PLTLB	48
	IX=IX-100	PLTLB	49
	IOR=0	PLTLB	50
	CALL DDTEXT(1,ANNOT)	PLTLB	51
C			

100	CALL PLOT(X,Y,NC)	PLTLB 52
	RETURN	PLTLB 53
C		PLTLB 54
200	CALL PLOT(X,Y,1)	PLTLB 55
	RETURN	PLTLB 56
	END	PLTLB 57
C	SUBROUTINE ARCTIC(THMIN,THMAX,HEIGHT,TICY,PLOT)	ARCTIC 2
C	DRAW RANGE AXIS IN RAY TRACE PLOT. INCLUDES ANY CURVILINEAR	ARCTIC 3
C	PROJECTIONS PROVIDED IN DDGRAPH.	ARCTIC 4
C	COMMON DECK "WWR" INSERTED HERE	CWWR 2
	PARAMETER (NWARSZ=1000)	CWW1 3
	COMMON/WW/ID(10),MAXW,W(NWARSZ)	CWW1 4
	REAL MAXSTP,MAXERR,INTYP,LLAT,LLON	CWW2 2
	EQUIVALENCE (EARTH, W(1)), (RAY, W(2)), (XMTRH, W(3)), (TLAT, W(4)),	CWW2 3
1	(TLON, W(5)), (OW, W(6)), (FBEG, W(7)), (FEND, W(8)), (FSTEP, W(9)),	CWW2 4
2	(AZ1, W(10)), (AZBEG, W(11)), (AZEND, W(12)), (AZSTEP, W(13)),	CWW2 5
3	(BETA, W(14)), (ELBEG, W(15)), (ELEND, W(16)), (ELSTEP, W(17)),	CWW2 6
8	(RCVRH, W(20)),	CWW2 7
4	(ONLY, W(21)), (HOP, W(22)), (MAXSTP, W(23)), (PLAT, W(24)), (PLON, W(25))	CWW2 8
5,	(HMAX, W(26)), (RAYFNC, W(29)), (EXTINC, W(33)),	CWW2 9
6	(HMIN, W(27)), (RGMX, W(28)),	CWW2 10
8	(INTYP, W(41)), (MAXERR, W(42)), (ERATIO, W(43)),	CWW2 11
6	(STEP1, W(44)), (STPMAX, W(45)), (STPMIN, W(46)), (FACTR, W(47)),	CWW2 12
7	(SKIP, W(71)), (RAYSET, W(72)), (PRTSRP, W(74)), (HITLET, W(75))	CWW2 13
9	, (BINRAY, W(76)), (PAGLN, W(77)), (PLT, W(81)), (PFACTR, W(82)),	CWW2 14
1	(LLAT, W(83)), (LLON, W(84)), (RLAT, W(85)), (RLON, W(86))	CWW2 15
2,	(TIC, W(87)), (HB, W(88)), (HT, W(89)), (TICV, W(96))	CWW2 16
	COMMON /DDSCALE/ XMIN, XMAX, YMIN, YMAX, MINX, MAXX, MINY, MAXY, SCX, SCY,	ARCTIC 6
1	NSCX, NXCX, MSCX, MSCY, ISCX, ISCY	ARCTIC 7
C		ARCTIC 8
	NTIC=2	ARCTIC 9
	IF(TIC.NE.0.) NTIC=1+(THMAX-THMIN)/TIC	ARCTIC10
	NLINE=MAX0(2,100/NTIC)	ARCTIC11
C		ARCTIC12
	TICN=TIC/(NLINE-2)	ARCTIC13
	DO 10 I=1,NTIC	ARCTIC14
	X=THMIN+(I-1)*TIC	ARCTIC15
	CALL PLOT(X,HEIGHT+TICY,1)	ARCTIC16
	DO 10 J=2,NLINE	ARCTIC17
	XJ=X+(J-2)*TICN	ARCTIC18
	IF(XJ.GT.THMAX) GO TO 15	ARCTIC19
10	CALL PLOT(XJ,HEIGHT,0)	ARCTIC20
C		ARCTIC21
15	CALL PLOT(THMAX,HEIGHT,0)	ARCTIC22
	CALL PLOT(THMAX,HEIGHT+TICY,1)	ARCTIC23
	RETURN	ARCTIC24
	END	ARCTIC25

	BLOCK DATA PLOTBL	PLOTBL 2
C	BLOCK DATA INITIALIZING PLOT ROUTINE COUNTERS AND	PLOTBL 3
C	EXTREME VALUES VARIABLES.	PLOTBL 4
	COMMON/KNKN/KNBP,KNVC,KNDT	PLOTBL 5
	COMMON/DDLIM/MXIX,MXIY,MNIX,MNIY	PLOTBL 6
	DATA MXIX,MXIY,MNIX,MNIY/2*-1000,2*1000/	PLOTBL 7
	DATA KNBP,KNVC,KNDT/3*0/	PLOTBL 8
	END	PLOTBL 9

	SUBROUTINE DDINIT(N,TEXT)	DDINIT 2
C	INITIALIZES PLOTTING PROCESS(DDPLOT)	DDINIT 3
C	WRITE PARAMETERS TO GRAPHICS CALLS FILE	DDINIT 4
C	COMMON DECK "RAYDEV" INSERTED HERE	CRAYDEV2
C	DEVICE ASSIGNED TO RAYTRC INPUT FILE	CRAYDEV4
	COMMON/RAYDEV/NRYIND,NDEVTMP,NFRMAT,NDEVGRP,NDEVBIN	CRAYDEV5
	CHARACTER TEXT*(*)	DDINIT 6
C		DDINIT 7
	DATA IDD/0/	DDINIT 8
10	FORMAT(5A10)	DDINIT 9
	IF(IDD.EQ.0) REWIND NDEVGRP	DDINIT10
	IDD=1	DDINIT11
	WRITE(NDEVGRP) 0,0,0	DDINIT12
	WRITE(NDEVGRP) M,LEN(TEXT),TEXT	DDINIT13
	END	DDINIT14

	SUBROUTINE DDBP	DDBP 2
C	SETS A VECTOR ORIGIN(DDPLOT)	DDBP 3
C	WRITE PARAMETERS TO GRAPHICS CALLS FILE	DDBP 4
C	COMMON DECK "RAYDEV" INSERTED HERE	CRAYDEV2
C	DEVICE ASSIGNED TO RAYTRC INPUT FILE	CRAYDEV4
	COMMON/RAYDEV/NRYIND,NDEVTMP,NFRMAT,NDEVGRP,NDEVBIN	CRAYDEV5
	COMMON/DD/IN,IOR,IT,IS,IC,ICC,IX,IY	DDBP 6
	COMMON/KNKN/KNBP,KNVC,KNDT	DDBP 7
	COMMON/DDLIM/MXIX,MXIY,MNIX,MNIY	DDBP 8
	MNIX=MIN0(MNIX,IX)	DDBP 9
	MXIX=MAX0(MXIX,IX)	DDBP 10
	MNIY=MIN0(MNIY,IY)	DDBP 11
	MXIY=MAX0(MXIY,IY)	DDBP 12
	IF(IX.LT.0.OR.IX.GT.1023.OR.IY.LT.0.OR.IY.GT.1023	DDBP 13
1	) PRINT 10,'DDBP ',KNBP,IX,IY	DDBP 14
10	FORMAT(A10,3I5)	DDBP 15
	KNBP=KNBP+1	DDBP 16
	WRITE(NDEVGRP) 1,IX,IY	DDBP 17
	END	DDBP 18

	SUBROUTINE DDVC	DDVC 2
C	PLOTS A VECTOR(DDPLOT)	DDVC 3
C	WRITE PARAMETERS TO GRAPHICS CALLS FILE	DDVC 4
C	COMMON DECK "RAYDEV" INSERTED HERE	CRAYDEV2
C	DEVICE ASSIGNED TO RAYTRC INPUT FILE	CRAYDEV4
	COMMON/RAYDEV/NRYIND,NDEVTMP,NFRMAT,NDEVGRP,NDEVBIN	CRAYDEV5
	COMMON/DD/IN, IOR, IT, IS, IC, ICC, IX, IY	DDVC 6
	COMMON/KNKN/KNBP,KNVC,KNDT	DDVC 7
	COMMON/DDLIM/MXIX,MXIY,MNIX,MNIY	DDVC 8
	MNIX=MINO(MNIX,IX)	DDVC 9
	MXIX=MAXO(MXIX,IX)	DDVC 10
	MNIY=MINO(MNIY,IY)	DDVC 11
	MXIY=MAXO(MXIY,IY)	DDVC 12
	IF(IX.LT.0.OR.IX.GT.1023.OR.IY.LT.0.OR.IY.GT.1023	DDVC 13
10	1 ) PRINT 10,'DDVC ',KNVC,IX,IY	DDVC 14
	FORMAT(A10,3I5)	DDVC 15
	KNVC=KNVC+1	DDVC 16
	WRITE(NDEVGRP) 2,IX,IY	DDVC 17
	END	DDVC 18

	SUBROUTINE DDTEXT(N,TEXT)	DDTEXT 2
C	WRITES A CHARACTER ARRAY PACKED A10(DDPLOT)	DDTEXT 3
C	WRITE PARAMETERS TO GRAPHICS CALLS FILE	DDTEXT 4
C	COMMON DECK "RAYDEV" INSERTED HERE	CRAYDEV2
C	DEVICE ASSIGNED TO RAYTRC INPUT FILE	CRAYDEV4
	COMMON/RAYDEV/NRYIND,NDEVTMP,NFRMAT,NDEVGRP,NDEVBIN	CRAYDEV5
	CHARACTER TEXT*(*)	DDTEXT 6
	COMMON/DD/IN, IOR, IT, IS, IC, ICC, IX, IY	DDTEXT 7
	COMMON/KNKN/KNBP,KNVC,KNDT	DDTEXT 8
100	FORMAT(A10,2I5,I2,1X,8A10)	DDTEXT 9
	KNDT=KNDT+1	DDTEXT10
	WRITE(NDEVGRP) 3,IX,IY	DDTEXT11
	WRITE(NDEVGRP) IOR,N,N*10,(TEXT(I:I),I=1,N*10)	DDTEXT12
	END	DDTEXT13

	SUBROUTINE DDTAB	DDTAB 2
C	INITIALIZES TABULAR PLOTTING(DDPLOT)	DDTAB 3
C	WRITE PARAMETERS TO GRAPHICS CALLS FILE	DDTAB 4
C	COMMON DECK "RAYDEV" INSERTED HERE	CRAYDEV2
C	DEVICE ASSIGNED TO RAYTRC INPUT FILE	CRAYDEV4
	COMMON/RAYDEV/NRYIND,NDEVTMP,NFRMAT,NDEVGRP,NDEVBIN	CRAYDEV5
	END	DDTAB 6

	SUBROUTINE DDFR	DDFR	2
C	ADVANCE ONE PLOTTING FRAME(DDPLOT)	DDFR	3
C	WRITE PARAMETERS TO GRAPHICS CALLS FILE	DDFR	4
C	COMMON DECK "RAYDEV" INSERTED HERE	CRAYDEV2	
C	DEVICE ASSIGNED TO RAYTRC INPUT FILE	CRAYDEV4	
	COMMON/RAYDEV/NRYIND,NDEVTMP,NFRMAT,NDEVGRP,NDEVBIN	CRAYDEV5	
10	FORMAT(A10)	DDFR	6
	WRITE(NDEVGRP) -2,0,0	DDFR	7
	END	DDFR	8

	SUBROUTINE DDEND	DDEND	2
C	EMPTIES PLOT BUFFER AND RELEASES PLOTTING COMMAND FILE(DDPLOT)	DDEND	3
C	WRITE PARAMETERS TO GRAPHICS CALLS FILE	DDEND	4
C	COMMON DECK "RAYDEV" INSERTED HERE	CRAYDEV2	
C	DEVICE ASSIGNED TO RAYTRC INPUT FILE	CRAYDEV4	
	COMMON/RAYDEV/NRYIND,NDEVTMP,NFRMAT,NDEVGRP,NDEVBIN	CRAYDEV5	
	COMMON/KNKN/KNBP,KNVC,KNDT	DDEND	6
	COMMON/DDLIM/MXIX,MXIY,MNIX,MNIY	DDEND	7
10	FORMAT(3A10,5I5)	DDEND	8
	WRITE(NDEVGRP) -1,0,0	DDEND	9
	END	DDEND	10

	SUBROUTINE DASH	DASH	2
C	ACTIVATE DASHED LINE CONNECTIONS(DISSPLA)	DASH	3
C	WRITE PARAMETERS TO GRAPHICS CALLS FILE	DASH	4
C	COMMON DECK "RAYDEV" INSERTED HERE	CRAYDEV2	
C	DEVICE ASSIGNED TO RAYTRC INPUT FILE	CRAYDEV4	
	COMMON/RAYDEV/NRYIND,NDEVTMP,NFRMAT,NDEVGRP,NDEVBIN	CRAYDEV5	
	WRITE(NDEVGRP) 37,0,0	DASH	6
	END	DASH	7

	SUBROUTINE RESET(S)	RESET	2
C	RESETS AN OPTION TO ITS DEFAULT VALUE(DISSPLA)	RESET	3
C	WRITE PARAMETERS TO GRAPHICS CALLS FILE	RESET	4
C	COMMON DECK "RAYDEV" INSERTED HERE	CRAYDEV2	
C	DEVICE ASSIGNED TO RAYTRC INPUT FILE	CRAYDEV4	
	COMMON/RAYDEV/NRYIND,NDEVTMP,NFRMAT,NDEVGRP,NDEVBIN	CRAYDEV5	
	CHARACTER S*10	RESET	6
	WRITE(NDEVGRP) 38,0,0	RESET	7

WRITE(NDEVGRP) S  
END

RESET 8  
RESET 9

SUBROUTINE HEIGHT(H)  
SETS REFERENCE CHARACTER HEIGHT IN INCHES(DISSPLA)  
WRITE PARAMETERS TO GRAPHICS CALLS FILE  
COMMON DECK "RAYDEV" INSERTED HERE  
DEVICE ASSIGNED TO RAYTRC INPUT FILE  
COMMON/RAYDEV/NRYIND,NDEVTMP,NFRMAT,NDEVGRP,NDEVBIN  
WRITE(NDEVGRP) 13,H,0  
END

HEIGHT 2  
HEIGHT 3  
HEIGHT 4  
CRAYDEV2  
CRAYDEV4  
CRAYDEV5  
HEIGHT 6  
HEIGHT 7

SUBROUTINE MX1ALF(T1,T2)  
SPECIFY USE OF ALTERNATE CHARACTER SET NUMBER 1(DISSPLA)  
WRITE PARAMETERS TO GRAPHICS CALLS FILE  
COMMON DECK "RAYDEV" INSERTED HERE  
DEVICE ASSIGNED TO RAYTRC INPUT FILE  
COMMON/RAYDEV/NRYIND,NDEVTMP,NFRMAT,NDEVGRP,NDEVBIN  
WRITE(NDEVGRP) 11,T1,T2  
END

MX1ALF 2  
MX1ALF 3  
MX1ALF 4  
CRAYDEV2  
CRAYDEV4  
CRAYDEV5  
MX1ALF 6  
MX1ALF 7

SUBROUTINE MX2ALF(T1,T2)  
SPECIFY USE OF ALTERNATE CHARACTER SET NUMBER 2(DISSPLA)  
WRITE PARAMETERS TO GRAPHICS CALLS FILE  
COMMON DECK "RAYDEV" INSERTED HERE  
DEVICE ASSIGNED TO RAYTRC INPUT FILE  
COMMON/RAYDEV/NRYIND,NDEVTMP,NFRMAT,NDEVGRP,NDEVBIN  
WRITE(NDEVGRP) 12,T1,T2  
END

MX2ALF 2  
MX2ALF 3  
MX2ALF 4  
CRAYDEV2  
CRAYDEV4  
CRAYDEV5  
MX2ALF 6  
MX2ALF 7

SUBROUTINE SCMPLEX  
SPECIFY USE OF SIMPLEX CHARACTER SET(DISSPLA)  
WRITE PARAMETERS TO GRAPHICS CALLS FILE  
COMMON DECK "RAYDEV" INSERTED HERE  
DEVICE ASSIGNED TO RAYTRC INPUT FILE  
COMMON/RAYDEV/NRYIND,NDEVTMP,NFRMAT,NDEVGRP,NDEVBIN  
WRITE(NDEVGRP) 10,0,0  
END

SCMPLEX 2  
SCMPLEX 3  
SCMPLEX 4  
CRAYDEV2  
CRAYDEV4  
CRAYDEV5  
SCMPLEX 6  
SCMPLEX 7

## DISPERSION-RELATION ROUTINES (Tape File 4)

	SUBROUTINE ANWNL	ANWNL	8
C	DISPERSION RELATION FOR ACOUSTIC WAVES NO WIND, NO LOSSES	ANWNL	9
C	COMMON DECK "RKAM" INSERTED HERE	RKAMCOM2	
	REAL KR, KTH, KPH	RKAMCOM4	
	COMMON//R, TH, PH, KR, KTH, KPH, RKVARS(14), TPULSE, CSTEP, DRDT(20)	RKAMCOM5	
C	COMMON DECK "CC" INSERTED HERE	CCC	2
	REAL MODC	CCC	4
	COMMON/CC/MODC(4), CS, PCST, PCSR, PCSTH, PCSPH	CCC	5
C	COMMON DECK "CONST" INSERTED HERE	CCONST	2
	COMMON/PCONST/CREF, RGAS, GAMMA	CCONST	4
	COMMON/MCONST/PI, PIT2, PID2, DEGS, RAD, ALN10	CCONST	5
C	COMMON DECK "RK" INSERTED HERE	CRK	2
C	DEFINE SIZE REQUIRED FOR RAY STATE SAVE ARRAY	CRK	4
	PARAMETER (LRKAMS=87+2*100, NXRKMS=12+LRKAMS, MXEQPT=21)	CRK	5
	PARAMETER (NRKSAV=NXRKMS+MXEQPT-1)	CRK	6
	COMMON /RK/ NEQS, STEP, MODE, E1MAX, E1MIN, E2MAX, E2MIN, FACT, RSTART	CRK	7
C	COMMON DECK "RINREAL" INSERTED HERE	CRINREA2	
	LOGICAL SPACE	CRINREA4	
	REAL LPOLAR, LPOLRI, KPHK, KPHKI, KAY2, KAY2I	CRINREA5	
	CHARACTER DISPM*6	CRINREA6	
	COMMON/RINPL/DISPM	CRINREA7	
	COMMON /RIN/ MODRIN(8), RAYNAME(2,3), TYPE(3), SPACE	CRINREA8	
	COMMON/RIN/OMEGMIN, OMEGMAX, KAY2, KAY2I,	CRINREA9	
	1 H, HI, PHT, PHTI, PHR, PHRI, PHTH, PHTHI, PPH, PPHI	CRINRE10	
	2, PHOW, PHOWI, PHKR, PHKRI, PHKTH, PHKTI, PHKPH, PHKPI	CRINRE11	
	3, KPHK, KPHKI, POLAR, POLARI, LPOLAR, LPOLRI, SGN	CRINRE12	
C	COMMON DECK "UU" INSERTED HERE	CUU	2
	REAL MODU	CUU	4
	COMMON/UU/MODU(4)	CUU	5
	1, V, PVT, PVR, PVTH, PVPH	CUU	6
	2, VR, PVRT, PVRR, PVRTH, PVRP	CUU	7
	3, VTH, PVTHT, PVTHR, PVTHTH, PVTHPH	CUU	8
	4, VPH, PVPHT, PVPHR, PVPHTH, PVPHPH	CUU	9
C	COMMON DECK "WW" INSERTED HERE	CWW	2
	PARAMETER (NWARSZ=1000)	CWW1	3
	COMMON/WW/ID(10), MAXW, W(NWARSZ)	CWW1	4
	REAL MAXSTP, MAXERR, INTYP, LLAT, LLON	CWW2	2
	EQUIVALENCE (EARTH, W(1)), (RAY, W(2)), (XMTRH, W(3)), (TLAT, W(4)),	CWW2	3
	1 (TLON, W(5)), (OW, W(6)), (FBEG, W(7)), (FEND, W(8)), (FSTEP, W(9)),	CWW2	4
	2 (AZ1, W(10)), (AZBEG, W(11)), (AZEND, W(12)), (AZSTEP, W(13)),	CWW2	5
	3 (BETA, W(14)), (ELBEG, W(15)), (ELEND, W(16)), (ELSTEP, W(17)),	CWW2	6
	8 (RCVRH, W(20)),	CWW2	7
	4 (ONLY, W(21)), (HOP, W(22)), (MAXSTP, W(23)), (PLAT, W(24)), (PLON, W(25))	CWW2	8
	5, (HMAX, W(26)), (RAYFNC, W(29)), (EXTINC, W(33)),	CWW2	9
	6 (HMIN, W(27)), (RGMAX, W(28)),	CWW2	10
	8 (INTYP, W(41)), (MAXERR, W(42)), (ERATIO, W(43)),	CWW2	11
	6 (STEP1, W(44)), (STPMAX, W(45)), (STPMIN, W(46)), (FACTR, W(47)),	CWW2	12
	7 (SKIP, W(71)), (RAYSET, W(72)), (PRTSRP, W(74)), (HITLET, W(75))	CWW2	13
	9, (BINRAY, W(76)), (PAGLN, W(77)), (PLT, W(81)), (PFACTR, W(82)),	CWW2	14
	1 (LLAT, W(83)), (LLON, W(84)), (RLAT, W(85)), (RLON, W(86))	CWW2	15
	2, (TIC, W(87)), (HB, W(88)), (HT, W(89)), (TICV, W(96))	CWW2	16
	REAL MMODEL, MFORM, MID	CWW3	2
C		CWW3	3
C	WIND 100-124	CWW3	4
	EQUIVALENCE (W(100), UMODEL), (W(101), UFORM), (W(102), UID)	CWW3	5

C			CWW3	6
C	DELTA WIND	125-149	CWW3	7
	EQUIVALENCE	(W(125),DUMODEL), (W(126),DUFORM), (W(127),DUID)	CWW3	8
C			CWW3	9
C	SOUND SPEED	150-174	CWW3	10
	EQUIVALENCE	(W(150),CMODEL), (W(151),CFORM), (W(152),CID)	CWW3	11
	EQUIVALENCE	(W(153),REFC)	CWW3	12
C			CWW3	13
C	DELTA SOUND SPEED	175-199	CWW3	14
	EQUIVALENCE	(W(175),DCMODEL), (W(176),DCFORM), (W(177),DCID)	CWW3	15
C			CWW3	16
C	TEMPERATURE	200-224	CWW3	17
	EQUIVALENCE	(W(200),TMODEL), (W(201),TFORM), (W(202),TID)	CWW3	18
C			CWW3	19
C	DELTA TEMPERATURE	225-249	CWW3	20
	EQUIVALENCE	(W(225),DTMODEL), (W(226),DTFORM), (W(227),DTID)	CWW3	21
C			CWW3	22
C	MOLECULAR	250-274	CWW3	23
	EQUIVALENCE	(W(250),MMODEL), (W(251),MFORM), (W(252),MID)	CWW3	24
C			CWW3	25
C	RECEIVER HEIGHT	275-299	CWW3	26
	EQUIVALENCE	(W(275),RMODEL), (W(276),RFORM), (W(277),RID)	CWW3	27
C			CWW3	28
C	TOPOGRAPHY	300-324	CWW3	29
	EQUIVALENCE	(W(300),GMODEL), (W(301),GFORM), (W(302),GID)	CWW3	30
C			CWW3	31
C	DELTA TOPOGRAPHY	325-349	CWW3	32
	EQUIVALENCE	(W(325),GUMODEL), (W(326),GUFORM), (W(327),GUID)	CWW3	33
C			CWW3	34
C	UPPER SURFACE TOPOGRAPHY	350-374	CWW3	35
	EQUIVALENCE	(W(350),SMODEL), (W(351),SFORM), (W(352),SID)	CWW3	36
C		PLOT ENHANCEMENTS CONTROL PARAMETERS	CWW3	37
C			CWW3	38
	EQUIVALENCE	(W(490),XFQMDL), (W(491),YFQMDL)	CWW3	39
C	ABSORPTION	500-524	CWW3	40
	EQUIVALENCE	(W(500),AMODEL), (W(501),AFORM), (W(502),AID)	CWW3	41
C			CWW3	42
C	DELTA ABSORPTION	525-549	CWW3	43
	EQUIVALENCE	(W(525),DAMODEL), (W(526),DAFORM), (W(527),DAID)	CWW3	44
C			CWW3	45
C	PRESSURE	550-574	CWW3	46
	EQUIVALENCE	(W(550),PMODEL), (W(551),PFORM), (W(552),PID)	CWW3	47
C			CWW3	48
C	DELTA PRESSURE	575-599	CWW3	49
	EQUIVALENCE	(W(575),DPMODEL), (W(576),DPFORM), (W(577),DPID)	CWW3	50
C			CWW3	51
C			ANWNL	17
	REAL KS,MKS		ANWNL	18
	REAL KVECT(24)		ANWNL	19
	REAL VSET(20)		ANWNL	20
	EQUIVALENCE(KVECT,KAY2), (VSET,V)		ANWNL	21
C			ANWNL	22
	DATA MODRIN/8HACOUSTIC ,8H WAVE ** ,8H** NO WI ,8HND *** N		ANNBL	2
1	,8HO LOSSES ,3*1H /		ANNBL	3
	DATA DISPM/'ANWNL'/		ANNBL	4

C	DATA TYPE/3*1H0 /	ANNBL 5
	ENTRY IDISPER	ANWNL 25
	CALL ISPEED	ANWNL 26
	CALL IRECVR	ANWNL 27
	CALL ITOPOG	ANWNL 28
	CALL ISURFAC	ANWNL 29
	RETURN	ANWNL 30
C		ANWNL 31
	ENTRY DISPER	ANWNL 32
	ENTRY RINDEX	ANWNL 33
C		ANWNL 34
	SPACE=.FALSE.	ANWNL 35
C		ANWNL 36
	KS=KR*KR+KTH*KTH+KPH*KPH	ANWNL 37
C		ANWNL 38
	SOUND SPEED	ANWNL 39
	CALL SPEED	ANWNL 40
	OWS=OW*OW	ANWNL 41
	KAY2=OWS/CS	ANWNL 42
C		ANWNL 43
	H=OW*OW - CS*KS	ANWNL 44
	MKS=-KS	ANWNL 45
	PHT=MKS*PCST	ANWNL 46
	PHR=MKS*PCSR	ANWNL 47
	PHTH=MKS*PCSTH	ANWNL 48
	PHPH=MKS*PCSPH	ANWNL 49
C		ANWNL 50
	PHOW=2.0*OW	ANWNL 51
	CS2=-2.0*CS	ANWNL 52
	PHKR=CS2*KR	ANWNL 53
	PHKTH=CS2*KTH	ANWNL 54
	PHKPH=CS2*KPH	ANWNL 55
	KPHK=CS2*KS	ANWNL 56
	RETURN	ANWNL 57
	END	ANWNL 58

	SUBROUTINE AWWNL	AWWNL 8
C	DISPERSION RELATION FOR ACOUSTIC WAVES WITH WIND, NO LOSSES	AWWNL 9
C	COMMON DECK "RKAM" INSERTED HERE	RKAMCOM2
	REAL KR, KTH, KPH	RKAMCOM4
	COMMON//R, TH, PH, KR, KTH, KPH, RKVARS(14), TPULSE, CSTEP, DRDT(20)	RKAMCOM5
C	COMMON DECK "CC" INSERTED HERE	CCC 2
	REAL MODC	CCC 4
	COMMON/CC/MODC(4), CS, PCST, PCSR, PCSTH, PCSPH	CCC 5
C	COMMON DECK "CONST" INSERTED HERE	CCONST 2
	COMMON/PCONST/CREF, RGAS, GAMMA	CCONST 4
	COMMON/MCONST/PI, PIT2, PID2, DEGS, RAD, ALN10	CCONST 5
C	COMMON DECK "RK" INSERTED HERE	CRK 2
C	DEFINE SIZE REQUIRED FOR RAY STATE SAVE ARRAY	CRK 4
	PARAMETER (LRKAMS=87+2*100, NXRKMS=12+LRKAMS, MXEQPT=21)	CRK 5
	PARAMETER (NRKSAV=NXRKMS+MXEQPT-1)	CRK 6

C	COMMON /RK/ NEQS,STEP,MODE,E1MAX,E1MIN,E2MAX,E2MIN,FACT,RSTART	CRK	7
	COMMON DECK "RINREAL" INSERTED HERE	CRINREA2	
	LOGICAL SPACE	CRINREA4	
	REAL LPOLAR,LPOLRI,KPHK,KPHKI,KAY2,KAY2I	CRINREA5	
	CHARACTER DISPM*6	CRINREA6	
	COMMON/RINPL/DISPM	CRINREA7	
	COMMON /RIN/ MODRIN(8),RAYNAME(2,3),TYPE(3),SPACE	CRINREA8	
	COMMON/RIN/OMEGMIN,OMEGMAX,KAY2,KAY2I,	CRINREA9	
	1 H,HI,PHT,PHTI,PHR,PHRI,PHTH,PHTHI,PHPH,PHPHI	CRINRE10	
	2, PHOW,PHOWI,PHKR,PHKRI,PHKTH,PHKTI,PHKPH,PHKPI	CRINRE11	
	3 ,KPHK,KPHKI,POLAR,POLARI,LPOLAR,LPOLRI,SGN	CRINRE12	
C	COMMON DECK "UU" INSERTED HERE	CUU	2
	REAL MODU	CUU	4
	COMMON/UU/MODU(4)	CUU	5
	1 ,V ,PVT ,PVR ,PVTH ,PVPH	CUU	6
	2 ,VR ,PVRT ,PVRR ,PVTRH ,PVRPH	CUU	7
	3 ,VTH ,PVTH, PVTHR, PVTHH, PVTHPH	CUU	8
	4 ,VPH ,VPH, VPHR, VPHH, VPHPH	CUU	9
C	COMMON DECK "WW" INSERTED HERE	CWW	2
	PARAMETER (NWARSZ=1000)	CWW1	3
	COMMON/WW/ID(10),MAXW,W(NWARSZ)	CWW1	4
	REAL MAXSTP,MAXERR,INTYP,LLAT,LLON	CWW2	2
	EQUIVALENCE (EARTH, W(1)), (RAY, W(2)), (XMTRH, W(3)), (TLAT, W(4)),	CWW2	3
	1 (TLON, W(5)), (OW, W(6)), (FBEG, W(7)), (FEND, W(8)), (FSTEP, W(9)),	CWW2	4
	2 (AZ1, W(10)), (AZBEG, W(11)), (AZEND, W(12)), (AZSTEP, W(13)),	CWW2	5
	3 (BETA, W(14)), (ELBEG, W(15)), (ELEND, W(16)), (ELSTEP, W(17)),	CWW2	6
	8 (RCVRH, W(20)),	CWW2	7
	4 (ONLY, W(21)), (HOP, W(22)), (MAXSTP, W(23)), (PLAT, W(24)), (PLON, W(25))	CWW2	8
	5, (HMAX, W(26)), (RAYFNC, W(29)), (EXTINC, W(33)),	CWW2	9
	6 (HMIN, W(27)), (RGMAX, W(28)),	CWW2	10
	8 (INTYP, W(41)), (MAXERR, W(42)), (ERATIO, W(43)),	CWW2	11
	6 (STEP1, W(44)), (STPMAX, W(45)), (STPMIN, W(46)), (FACTR, W(47)),	CWW2	12
	7 (SKIP, W(71)), (RAYSET, W(72)), (PRTSRP, W(74)), (HITLET, W(75))	CWW2	13
	9 , (BINRAY, W(76)), (PAGLN, W(77)), (PLT, W(81)), (PFACTR, W(82)),	CWW2	14
	1 (LLAT, W(83)), (LLON, W(84)), (RLAT, W(85)), (RLON, W(86))	CWW2	15
	2, (TIC, W(87)), (HB, W(88)), (HT, W(89)), (TICV, W(96))	CWW2	16
	REAL MMODEL,MFORM,MID	CWW3	2
C		CWW3	3
C	WIND 100-124	CWW3	4
	EQUIVALENCE (W(100),UMODEL), (W(101),UFORM), (W(102),UID)	CWW3	5
C		CWW3	6
C	DELTA WIND 125-149	CWW3	7
	EQUIVALENCE (W(125),DUMODEL), (W(126),DIFORM), (W(127),DUID)	CWW3	8
C		CWW3	9
C	SOUND SPEED 150-174	CWW3	10
	EQUIVALENCE (W(150),CMODEL), (W(151),CFORM), (W(152),CID)	CWW3	11
	EQUIVALENCE (W(153),REFC)	CWW3	12
C		CWW3	13
C	DELTA SOUND SPEED 175-199	CWW3	14
	EQUIVALENCE (W(175),DCMODEL), (W(176),DCFORM), (W(177),DCID)	CWW3	15
C		CWW3	16
C	TEMPERATURE 200-224	CWW3	17
	EQUIVALENCE (W(200),TMODEL), (W(201),TFORM), (W(202),TID)	CWW3	18
C		CWW3	19
C	DELTA TEMPERATURE 225-249	CWW3	20

C	EQUIVALENCE (W(225),DTMODEL), (W(226),DTFORM), (W(227),DTID)	CWW3	21
C	MOLECULAR 250-274	CWW3	22
C	EQUIVALENCE (W(250),MMODEL), (W(251),MFORM), (W(252),MID)	CWW3	23
C	RECEIVER HEIGHT 275-299	CWW3	24
C	EQUIVALENCE (W(275),RMODEL), (W(276),RFORM), (W(277),RID)	CWW3	25
C	TOPOGRAPHY 300-324	CWW3	26
C	EQUIVALENCE (W(300),GMODEL), (W(301),GFORM), (W(302),GID)	CWW3	27
C	DELTA TOPOGRAPHY 325-349	CWW3	28
C	EQUIVALENCE (W(325),GUMODEL), (W(326),GUFORM), (W(327),GUID)	CWW3	29
C	UPPER SURFACE TOPOGRAPHY 350-374	CWW3	30
C	EQUIVALENCE (W(350),SMODEL), (W(351),SFORM), (W(352),SID)	CWW3	31
C	PLOT ENHANCEMENTS CONTROL PARAMETERS	CWW3	32
C	EQUIVALENCE (W(490),XFQMDL), (W(491),YFQMDL)	CWW3	33
C	ABSORPTION 500-524	CWW3	34
C	EQUIVALENCE (W(500),AMODEL), (W(501),AFORM), (W(502),AID)	CWW3	35
C	DELTA ABSORPTION 525-549	CWW3	36
C	EQUIVALENCE (W(525),DAMODEL), (W(526),DAFORM), (W(527),DAID)	CWW3	37
C	PRESSURE 550-574	CWW3	38
C	EQUIVALENCE (W(550),PMODEL), (W(551),PFORM), (W(552),PID)	CWW3	39
C	DELTA PRESSURE 575-599	CWW3	40
C	EQUIVALENCE (W(575),DPMODEL), (W(576),DPFORM), (W(577),DPID)	CWW3	41
C	REAL KS, KV	CWW3	42
C	REAL KVECT(24)	CWW3	43
C	EQUIVALENCE(KVECT, KAY2)	CWW3	44
C	DATA MODRIN/SHACOUSTIC ,8H WAVE ** ,8H* WITH W ,8HIND ****	CWW3	45
C	1 ,8H** NO LO ,4HSSES ,2*1H /	CWW3	46
C	DATA DISPM/'AWWNL' /	CWW3	47
C	DATA TYPE/3*1H1 /	CWW3	48
C	ENTRY IDISPER	CWW3	49
C	CALL ISPEED	CWW3	50
C	CALL IWINDR	CWW3	51
C	CALL IRECVR	CWW3	52
C	CALL ITOPOG	CWW3	53
C	CALL ISURFAC	CWW3	54
C	RETURN	CWW3	55
C	ENTRY DISPER	CWW3	56
C	SPACE=.FALSE.	CWW3	57
C	KS=KR*KR+KTH*KTH+KPH*KPH	CWW3	58
C	WIND VELOCITY	CWW3	59

	CALL WINDR	AWWNL 39
	KV=KR*VR+KTH*VTH+KPH*VPH	AWWNL 40
	VLS=KV*KV/KS	AWWNL 41
C	SOUND SPEED	AWWNL 42
	CALL SPEED	AWWNL 43
	OWS=OW*OW	AWWNL 44
	KAY2=OWS/(SQRT(CS)+KV/SQRT(KS))**2	AWWNL 45
C		AWWNL 46
	OWI=OW-KV	AWWNL 47
	H=OWI*OWI - CS*KS	AWWNL 48
	POWIT=-KR*PVRT - KTH*PVTHT - KPH*PVPHT	AWWNL 49
	PHT=2.0*OWI*POWIT - KS*PCST	AWWNL 50
	POWIR=-KR*PVR - KTH*PVTHR - KPH*PVPHR	AWWNL 51
	PHR=2.0*OWI*POWIR - KS*PCSR	AWWNL 52
	POWITH=-KR*PVRTH - KTH*PVTHTH - KPH*PVPHTH	AWWNL 53
	PHTH=2.0*OWI*POWITH - KS*PCSTH	AWWNL 54
	POWIPH=-KR*PVRPH - KTH*PVTHPH - KPH*PVPHPH	AWWNL 55
	PHPH=2.0*OWI*POWIPH - KS*PCSPH	AWWNL 56
C		AWWNL 57
	PHOW=2.0*OWI	AWWNL 58
	PHKR=-2.0*(OWI*VR + CS*KR)	AWWNL 59
	PHKTH=-2.0*(OWI*VTH + CS*KTH)	AWWNL 60
	PHKPH=-2.0*(OWI*VPH + CS*KPH)	AWWNL 61
	KPHK=-2.0*(OWI*KV + CS*KS)	AWWNL 62
	RETURN	AWWNL 63
	END	AWWNL 64

	SUBROUTINE ANWWL	ANWWL 8
C	DISPERSION RELATION FOR ACOUSTIC WAVES NO WIND, WITH LOSSES	ANWWL 9
C	COMMON DECK "RKAM" INSERTED HERE	RKAMCOM2
	REAL KR, KTH, KPH	RKAMCOM4
	COMMON//R, TH, PH, KR, KTH, KPH, RKVARS(14), TPULSE, CSTEP, DRDT(20)	RKAMCOM5
C	COMMON DECK "CC" INSERTED HERE	CCC 2
	REAL MODC	CCC 4
	COMMON/CC/MODC(4), CS, PCST, PCSR, PCSTH, PCSPH	CCC 5
C	COMMON DECK "CONST" INSERTED HERE	CCONST 2
	COMMON/PCONST/CREF, RGAS, GAMMA	CCONST 4
	COMMON/MCONST/PI, PIT2, PID2, DEGS, RAD, ALN10	CCONST 5
C	COMMON DECK "RK" INSERTED HERE	CRK 2
C	DEFINE SIZE REQUIRED FOR RAY STATE SAVE ARRAY	CRK 4
	PARAMETER (LRKAMS=87+2*100, NXRKMS=12+LRKAMS, MXEQPT=21)	CRK 5
	PARAMETER (NRKSAV=NXRKMS+MXEQPT-1)	CRK 6
	COMMON /RK/ NEQS, STEP, MODE, E1MAX, E1MIN, E2MAX, E2MIN, FACT, RSTART	CRK 7
C	COMMON DECK "RINREAL" INSERTED HERE	CRINREA2
	LOGICAL SPACE	CRINREA4
	REAL LPOLAR, LPOLRI, KPHK, KPHKI, KAY2, KAY2I	CRINREA5
	CHARACTER DISPM*6	CRINREA6
	COMMON/RINPL/DISPM	CRINREA7
	COMMON /RIN/ MODRIN(8), RAYNAME(2,3), TYPE(3), SPACE	CRINREA8
	COMMON/RIN/OMEGMIN, OMEGMAX, KAY2, KAY2I,	CRINREA9
1	H, HI, PHT, PHTI, PHR, PHRI, PHTH, PHTHI, PHPH, PHPHI	CRINRE10

	2, PHOW, PHOWI, PHKR, PHKRI, PHKTH, PHKTI, PHKPH, PHKPI	CRINRE11
	3, KPHK, KPHKI, POLAR, POLARI, LPOLAR, LPOLRI, SGN	CRINRE12
C	COMMON DECK "UU" INSERTED HERE	CUU 2
	REAL MODU	CUU 4
	COMMON/UU/MODU(4)	CUU 5
	1, V, PVT, PVR, PVTH, PVPH	CUU 6
	2, VR, PVRT, PVRR, PVRTH, PVRP	CUU 7
	3, VTH, PVTHT, PVTHR, PVTHTH, PVTHPH	CUU 8
	4, VPH, PVPHT, PVPHR, PVPHTH, PVPHPH	CUU 9
C	COMMON DECK "WW" INSERTED HERE	CWW 2
	PARAMETER (NWARSZ=1000)	CWW1 3
	COMMON/WW/ID(10), MAXW, W(NWARSZ)	CWW1 4
	REAL MAXSTP, MAXERR, INTYP, LLAT, LLON	CWW2 2
	EQUIVALENCE (EARTH, W(1)), (RAY, W(2)), (XMTRH, W(3)), (TLAT, W(4)),	CWW2 3
	1 (TLON, W(5)), (OW, W(6)), (FBEG, W(7)), (FEND, W(8)), (FSTEP, W(9)),	CWW2 4
	2 (AZ1, W(10)), (AZBEG, W(11)), (AZEND, W(12)), (AZSTEP, W(13)),	CWW2 5
	3 (BETA, W(14)), (ELBEG, W(15)), (ELEND, W(16)), (ELSTEP, W(17)),	CWW2 6
	8 (RCVRH, W(20)),	CWW2 7
	4 (ONLY, W(21)), (HOP, W(22)), (MAXSTP, W(23)), (PLAT, W(24)), (PLON, W(25))	CWW2 8
	5, (HMAX, W(26)), (RAYFNC, W(29)), (EXTINC, W(33)),	CWW2 9
	6 (HMIN, W(27)), (RGMAX, W(28)),	CWW2 10
	8 (INTYP, W(41)), (MAXERR, W(42)), (ERATIO, W(43)),	CWW2 11
	6 (STEP1, W(44)), (STPMAX, W(45)), (STPMIN, W(46)), (FACTR, W(47)),	CWW2 12
	7 (SKIP, W(71)), (RAYSET, W(72)), (PRTSRP, W(74)), (HITLET, W(75))	CWW2 13
	9, (BINRAY, W(76)), (PAGLN, W(77)), (PLT, W(81)), (PFACTR, W(82)),	CWW2 14
	1 (LLAT, W(83)), (LLON, W(84)), (RLAT, W(85)), (RLON, W(86))	CWW2 15
	2, (TIC, W(87)), (HB, W(88)), (HT, W(89)), (TICV, W(96))	CWW2 16
	REAL MMODEL, MFORM, MID	CWW3 2
C		CWW3 3
C	WIND 100-124	CWW3 4
	EQUIVALENCE (W(100), UMODEL), (W(101), UFORM), (W(102), UID)	CWW3 5
C		CWW3 6
C	DELTA WIND 125-149	CWW3 7
	EQUIVALENCE (W(125), DUMODEL), (W(126), DUFORM), (W(127), DUID)	CWW3 8
C		CWW3 9
C	SOUND SPEED 150-174	CWW3 10
	EQUIVALENCE (W(150), CMODEL), (W(151), CFORM), (W(152), CID)	CWW3 11
	EQUIVALENCE (W(153), REFC)	CWW3 12
C		CWW3 13
C	DELTA SOUND SPEED 175-199	CWW3 14
	EQUIVALENCE (W(175), DCMODEL), (W(176), DCFORM), (W(177), DCID)	CWW3 15
C		CWW3 16
C	TEMPERATURE 200-224	CWW3 17
	EQUIVALENCE (W(200), TMODEL), (W(201), TFORM), (W(202), TID)	CWW3 18
C		CWW3 19
C	DELTA TEMPERATURE 225-249	CWW3 20
	EQUIVALENCE (W(225), DTMODEL), (W(226), DTFORM), (W(227), DTID)	CWW3 21
C		CWW3 22
C	MOLECULAR 250-274	CWW3 23
	EQUIVALENCE (W(250), MMODEL), (W(251), MFORM), (W(252), MID)	CWW3 24
C		CWW3 25
C	RECEIVER HEIGHT 275-299	CWW3 26
	EQUIVALENCE (W(275), RMODEL), (W(276), RFORM), (W(277), RID)	CWW3 27
C		CWW3 28
C	TOPOGRAPHY 300-324	CWW3 29

C	EQUIVALENCE (W(300),GMODEL), (W(301),GFORM), (W(302),GID)	CWW3	30
C	DELTA TOPOGRAPHY 325-349	CWW3	31
C	EQUIVALENCE (W(325),GUMODEL), (W(326),GUFORM), (W(327),GUID)	CWW3	32
C	UPPER SURFACE TOPOGRAPHY 350-374	CWW3	33
C	EQUIVALENCE (W(350),SMODEL), (W(351),SFORM), (W(352),SID)	CWW3	34
C	PLOT ENHANCEMENTS CONTROL PARAMETERS	CWW3	35
C	EQUIVALENCE (W(490),XFQMDL), (W(491),YFQMDL)	CWW3	36
C	ABSORPTION 500-524	CWW3	37
C	EQUIVALENCE (W(500),AMODEL), (W(501),AFORM), (W(502),AID)	CWW3	38
C	DELTA ABSORPTION 525-549	CWW3	39
C	EQUIVALENCE (W(525),DAMODEL), (W(526),DAFORM), (W(527),DAID)	CWW3	40
C	PRESSURE 550-574	CWW3	41
C	EQUIVALENCE (W(550),PMODEL), (W(551),PFORM), (W(552),PID)	CWW3	42
C	DELTA PRESSURE 575-599	CWW3	43
C	EQUIVALENCE (W(575),DPMODEL), (W(576),DPFORM), (W(577),DPID)	CWW3	44
C		CWW3	45
C	COMMON DECK "AA" INSERTED HERE	CWW3	46
C	REAL MODA	CWW3	47
C	REAL MU, MUPT, MUPR, MUPTH, MUPPH	CWW3	48
C	REAL KAP, KAPPT, KAPPR, KAPPTH, KAPPPH	CWW3	49
C	COMMON/AA/MODA(4), MU, MUPT, MUPR, MUPTH, MUPPH	CWW3	50
C	COMMON/AA/KAP, KAPPT, KAPPR, KAPPTH, KAPPPH	CWW3	51
C		ANWWL	17
C	COMMON DECK "PP" INSERTED HERE	CAA	2
C	REAL MODP	CAA	4
C	COMMON/PP/MODP(4), P, PPT, PPR, PPTH, PPPH	CAA	5
C		CAA	6
C	COMMON DECK "MM" INSERTED HERE	CAA	7
C	REAL M, MODM	CAA	8
C	COMMON/MM/MODM(4), M, PMT, PMR, PMTH, PMPH	ANWWL	19
C		CPP	2
C	REAL KS, MKS	CPP	4
C	REAL KVECT(24)	CPP	5
C	REAL VSET(20)	ANWWL	21
C	EQUIVALENCE(KVECT, KAY2), (VSET, V)	CMM	2
C		CMM	4
C	DATA MODRIN/8HACOUSTIC, 8H WAVE **, 8H** NO WI, 8HND *** W	CMM	5
C	1, 8HWITH LOS, 3HSES, 2*1H /	ANWWL	23
C	DATA DISPM/'ANWWL' /	ANWWL	24
C	DATA TYPE/3*1H2 /	ANWWL	25
C	ENTRY IDISPER	ANWWL	26
C	CALL ISPEED	ANWWL	27
C	CALL IRECVR	ANWWL	28
C	CALL ITOPOG	ANWBL	2
C	CALL ISURFAC	ANWBL	3
C	CALL IPRES	ANWBL	4
		ANWBL	5
		ANWWL	31
		ANWWL	32
		ANWWL	33
		ANWWL	34
		ANWWL	35
		ANWWL	36
		ANWWL	37
		ANWWL	38

	CALL IABSRP	ANWWL 39
	RETURN	ANWWL 40
C	ENTRY DISPER	ANWWL 41
	ENTRY RINDEX	ANWWL 42
C		ANWWL 43
	SPACE=.FALSE.	ANWWL 44
C		ANWWL 45
	KS=KR*KR+KTH*KTH+KPH*KPH	ANWWL 46
C	SOUND SPEED	ANWWL 47
	CALL SPEED	ANWWL 48
	OWS=OW*OW	ANWWL 49
	KAY2=OWS/CS	ANWWL 50
C		ANWWL 51
	H=OW*OW - CS*KS	ANWWL 52
	MKS=-KS	ANWWL 53
	PHT=MKS*PCST	ANWWL 54
	PHR=MKS*PCSR	ANWWL 55
	PHTH=MKS*PCSTH	ANWWL 56
	PHPH=MKS*PCSPH	ANWWL 57
C		ANWWL 58
	PHOW=2.0*OW	ANWWL 59
	CS2=-2.0*CS	ANWWL 60
	PHKR=CS2*KR	ANWWL 61
	PHKTH=CS2*KTH	ANWWL 62
	PHKPH=CS2*KPH	ANWWL 63
	KPHK=CS2*KS	ANWWL 64
C		ANWWL 65
	CALL PRES	ANWWL 66
	CALL ABSRP	ANWWL 67
	GMS=GAMMA-1.0	ANWWL 68
	KAY2I=- (OWI / (GAMMA * P)) * (4. / 3. * MU + GMS * GMS * M / (GAMMA * RGAS) * KAP) * KAY2	ANWWL 69
	RETURN	ANWWL 70
	END	ANWWL 71
		ANWWL 72

	SUBROUTINE AWWWL	AWWWL 8
C	DISPERSION RELATION FOR ACOUSTIC WAVES WITH WIND, WITH LOSSES	AWWWL 9
C	COMMON DECK "RKAM" INSERTED HERE	RKAMCOM2
	REAL KR, KTH, KPH	RKAMCOM4
	COMMON//R, TH, PH, KR, KTH, KPH, RKVARS (14), TPULSE, CSTEP, DRDT (20)	RKAMCOM5
C	COMMON DECK "CC" INSERTED HERE	CCC 2
	REAL MODC	CCC 4
	COMMON/CC/MODC (4), CS, PCST, PCSR, PCSTH, PCSPH	CCC 5
C	COMMON DECK "CONST" INSERTED HERE	CCONST 2
	COMMON/PCONST/CREF, RGAS, GAMMA	CCONST 4
	COMMON/MCONST/PI, PIT2, PID2, DEGS, RAD, ALN10	CCONST 5
C	COMMON DECK "RK" INSERTED HERE	CRK 2
C	DEFINE SIZE REQUIRED FOR RAY STATE SAVE ARRAY	CRK 4
	PARAMETER (LRKAMS=87+2*100, NXRKMS=12+LRKAMS, MXEQPT=21)	CRK 5
	PARAMETER (NRKSAV=NXRKMS+MXEQPT-1)	CRK 6
	COMMON /RK/ NEQS, STEP, MODE, E1MAX, E1MIN, E2MAX, E2MIN, FACT, RSTART	CRK 7

C	COMMON DECK "RINREAL" INSERTED HERE	CRINREA2
	LOGICAL SPACE	CRINREA4
	REAL LPOLAR,LPOLRI,KPHK,KPHKI,KAY2,KAY2I	CRINREA5
	CHARACTER DISPM*6	CRINREA6
	COMMON/RINPL/DISPM	CRINREA7
	COMMON /RIN/ MODRIN(8),RAYNAME(2,3),TYPE(3),SPACE	CRINREA8
	COMMON/RIN/OMEGMIN,OMEGMAX,KAY2,KAY2I,	CRINREA9
	1 H,HI,PHT,PHTI,PHR,PHRI,PHTH,PHTHI,PHPH,PHPHI	CRINRE10
	2, PHOW,PHOWI,PHKR,PHKRI,PHKTH,PHKTI,PHKPH,PHKPI	CRINRE11
	3 ,KPHK,KPHKI,POLAR,POLARI,LPOLAR,LPOLRI,SGN	CRINRE12
C	COMMON DECK "UU" INSERTED HERE	CUU 2
	REAL MODU	CUU 4
	COMMON/UU/MODU(4)	CUU 5
	1 ,V ,PVT ,PVR ,PVTH ,PVPH	CUU 6
	2 ,VR ,PVRT ,PVRR ,PVTRH ,PVRPH	CUU 7
	3 ,VTH,PVTHT,PVTHR,PVTHTH,PVTHPH	CUU 8
	4 ,VPH,PVPHT,PVPHR,PVPHTH,PVPHPH	CUU 9
C	COMMON DECK "WW" INSERTED HERE	CWW 2
	PARAMETER (NWARSZ=1000)	CWW1 3
	COMMON/WW/ID(10),MAXW,W(NWARSZ)	CWW1 4
	REAL MAXSTP,MAXERR,INTYP,LLAT,LLON	CWW2 2
	EQUIVALENCE (EARTH,W(1)),(RAY,W(2)),(XMTRH,W(3)),(TLAT,W(4)),	CWW2 3
	1 (TLON,W(5)),(OW,W(6)),(FBEG,W(7)),(FEND,W(8)),(FSTEP,W(9)),	CWW2 4
	2 (AZ1,W(10)),(AZBEG,W(11)),(AZEND,W(12)),(AZSTEP,W(13)),	CWW2 5
	3 (BETA,W(14)),(ELBEG,W(15)),(ELEND,W(16)),(ELSTEP,W(17)),	CWW2 6
	8 (RCVRH,W(20)),	CWW2 7
	4 (ONLY,W(21)),(HOP,W(22)),(MAXSTP,W(23)),(PLAT,W(24)),(PLON,W(25))	CWW2 8
	5,(HMAX,W(26)),(RAYFNC,W(29)),(EXTINC,W(33)),	CWW2 9
	6 (HMIN,W(27)),(RGMAX,W(28)),	CWW2 10
	8 (INTYP,W(41)),(MAXERR,W(42)),(ERATIO,W(43)),	CWW2 11
	6 (STEP1,W(44)),(STPMAX,W(45)),(STPMIN,W(46)),(FACTR,W(47)),	CWW2 12
	7 (SKIP,W(71)),(RAYSET,W(72)),(PRTSRP,W(74)),(HITLET,W(75))	CWW2 13
	9 ,(BINRAY,W(76)),(PAGLN,W(77)),(PLT,W(81)),(PFACTR,W(82)),	CWW2 14
	1 (LLAT,W(83)),(LLON,W(84)),(RLAT,W(85)),(RLON,W(86))	CWW2 15
	2,(TIC,W(87)),(HB,W(88)),(HT,W(89)),(TICV,W(96))	CWW2 16
	REAL MMODEL,MFORM,MID	CWW3 2
C		CWW3 3
C	WIND 100-124	CWW3 4
	EQUIVALENCE (W(100),UMODEL),(W(101),UFORM),(W(102),UID)	CWW3 5
C		CWW3 6
C	DELTA WIND 125-149	CWW3 7
	EQUIVALENCE (W(125),DUMODEL),(W(126),DIFORM),(W(127),DUID)	CWW3 8
C		CWW3 9
C	SOUND SPEED 150-174	CWW3 10
	EQUIVALENCE (W(150),CMODEL),(W(151),CFORM),(W(152),CID)	CWW3 11
	EQUIVALENCE (W(153),REFC)	CWW3 12
C		CWW3 13
C	DELTA SOUND SPEED 175-199	CWW3 14
	EQUIVALENCE (W(175),DCMODEL),(W(176),DCFORM),(W(177),DCID)	CWW3 15
C		CWW3 16
C	TEMPERATURE 200-224	CWW3 17
	EQUIVALENCE (W(200),TMODEL),(W(201),TFORM),(W(202),TID)	CWW3 18
C		CWW3 19
C	DELTA TEMPERATURE 225-249	CWW3 20
	EQUIVALENCE (W(225),DTMODEL),(W(226),DTFORM),(W(227),DTID)	CWW3 21

C		CWW3	22
C	MOLECULAR 250-274	CWW3	23
	EQUIVALENCE (W(250),MMODEL), (W(251),MFORM), (W(252),MID)	CWW3	24
C		CWW3	25
C	RECEIVER HEIGHT 275-299	CWW3	26
	EQUIVALENCE (W(275),RMODEL), (W(276),RFORM), (W(277),RID)	CWW3	27
C		CWW3	28
C	TOPOGRAPHY 300-324	CWW3	29
	EQUIVALENCE (W(300),GMODEL), (W(301),GFORM), (W(302),GID)	CWW3	30
C		CWW3	31
C	DELTA TOPOGRAPHY 325-349	CWW3	32
	EQUIVALENCE (W(325),GUMODEL), (W(326),GUFORM), (W(327),GUID)	CWW3	33
C		CWW3	34
C	UPPER SURFACE TOPOGRAPHY 350-374	CWW3	35
	EQUIVALENCE (W(350),SMODEL), (W(351),SFORM), (W(352),SID)	CWW3	36
C	PLOT ENHANCEMENTS CONTROL PARAMETERS	CWW3	37
C		CWW3	38
	EQUIVALENCE (W(490),XFQMDL), (W(491),YFQMDL)	CWW3	39
C	ABSORPTION 500-524	CWW3	40
	EQUIVALENCE (W(500),AMODEL), (W(501),AFORM), (W(502),AID)	CWW3	41
C		CWW3	42
C	DELTA ABSORPTION 525-549	CWW3	43
	EQUIVALENCE (W(525),DAMODEL), (W(526),DAFORM), (W(527),DAID)	CWW3	44
C		CWW3	45
C	PRESSURE 550-574	CWW3	46
	EQUIVALENCE (W(550),PMODEL), (W(551),PFORM), (W(552),PID)	CWW3	47
C		CWW3	48
C	DELTA PRESSURE 575-599	CWW3	49
	EQUIVALENCE (W(575),DPMODEL), (W(576),DPFORM), (W(577),DPID)	CWW3	50
C		CWW3	51
C		AWWWL	17
C	COMMON DECK "AA" INSERTED HERE	CAA	2
	REAL MODA	CAA	4
	REAL MU, MUPT, MUPR, MUPTH, MUPPH	CAA	5
	REAL KAP, KAPPT, KAPPR, KAPPTH, KAPPPH	CAA	6
	COMMON/AA/MODA(4), MU, MUPT, MUPR, MUPTH, MUPPH	CAA	7
	COMMON/AA/KAP, KAPPT, KAPPR, KAPPTH, KAPPPH	CAA	8
C		AWWWL	19
C	COMMON DECK "PP" INSERTED HERE	CPP	2
	REAL MODP	CPP	4
	COMMON/PP/MODP(4), P, PPT, PPR, PPTH, PPPH	CPP	5
C		AWWWL	21
C	COMMON DECK "MM" INSERTED HERE	CMM	2
	REAL M, MODM	CMM	4
	COMMON/MM/MODM(4), M, PMT, PMR, PMTH, PMPH	CMM	5
C		AWWWL	23
	REAL KS, KV	AWWWL	24
	REAL KVECT(24)	AWWWL	25
	EQUIVALENCE(KVECT, KAY2)	AWWWL	26
C		AWWWL	27
	DATA MODRIN/8HACOUSTIC ,8H WAVE ** ,8H* WITH W ,8HIND ****	AWWBL	2
	1 ,8H** WITH ,6HLOSSES ,2*1H /	AWWBL	3
	DATA DISPM/'AWWWL' /	AWWBL	4
	DATA TYPE/3*1H3 /	AWWBL	5
C		AWWWL	30

	ENTRY IDISPER	AWWWL 31
	CALL ISPEED	AWWWL 32
	CALL IWINDR	AWWWL 33
	CALL IRECVR	AWWWL 34
	CALL ITOPOG	AWWWL 35
	CALL ISURFAC	AWWWL 36
C		AWWWL 37
	CALL IPRES	AWWWL 38
	CALL IABSRP	AWWWL 39
	RETURN	AWWWL 40
C		AWWWL 41
	ENTRY DISPER	AWWWL 42
C		AWWWL 43
	SPACE=.FALSE.	AWWWL 44
C		AWWWL 45
	KS=KR*KR+KTH*KTH+KPH*KPH	AWWWL 46
C	WIND VELOCITY	AWWWL 47
	CALL WINDR	AWWWL 48
	KV=KR*VR+KTH*VTH+KPH*VPH	AWWWL 49
	VLS=KV*KV/KS	AWWWL 50
C	SOUND SPEED	AWWWL 51
	CALL SPEED	AWWWL 52
	OWS=OW*OW	AWWWL 53
	KAY2=OWS/(SQRT(CS)+KV/SQRT(KS))**2	AWWWL 54
C		AWWWL 55
	OWI=OW-KV	AWWWL 56
	H=OWI*OWI - CS*KS	AWWWL 57
	POWIT=-KR*PVRT - KTH*PVTH - KPH*PVPHT	AWWWL 58
	PHT=2.0*OWI*POWIT - KS*PCST	AWWWL 59
	POWIR=-KR*PVRR - KTH*PVTHR - KPH*PVPHR	AWWWL 60
	PHR=2.0*OWI*POWIR - KS*PCSR	AWWWL 61
	POWITH=-KR*PVTRTH - KTH*PVTHTH - KPH*PVPHTH	AWWWL 62
	PHTH=2.0*OWI*POWITH - KS*PCSTH	AWWWL 63
	POWIPH=-KR*PVRPH - KTH*PVTHPH - KPH*PVPHPH	AWWWL 64
	PHPH=2.0*OWI*POWIPH - KS*PCSPH	AWWWL 65
C		AWWWL 66
	PHOW=2.0*OWI	AWWWL 67
	PHKR=-2.0*(OWI*VR + CS*KR)	AWWWL 68
	PHKTH=-2.0*(OWI*VTH + CS*KTH)	AWWWL 69
	PHKPH=-2.0*(OWI*VPH + CS*KPH)	AWWWL 70
	KPHK=-2.0*(OWI*KV + CS*KS)	AWWWL 71
C		AWWWL 72
	CALL PRES	AWWWL 73
	CALL ABRP	AWWWL 74
	GMS=GAMMA-1.0	AWWWL 75
	KAY2I=- (OW/(GAMMA*P)) * (4./3.*MU+GMS*GMS*M/(GAMMA*RGAS)*KAP) *KAY2	AWWWL 76
	RETURN	AWWWL 77
	END	AWWWL 78

## ATMOSPHERIC MODEL ROUTINES (Tape File 5)

	SUBROUTINE WLINEAR		WLINEAR8
C	LINEAR WIND VELOCITY PROFILE		WLINEAR9
C	PROVIDES CONSTANT RADIAL, ZONAL AND MERIDONAL WINDS		WLINEA10
C	EXCEPT THAT A POSSIBLE LINEAR HEIGHT GRADIENT OF THE ZONAL		WLINEA11
C	COMPONENT IS ALLOWED.		WLINEA12
C	COMMON DECK "RKAM" INSERTED HERE		RKAMCOM2
	REAL KR, KTH, KPH		RKAMCOM4
	COMMON//R, TH, PH, KR, KTH, KPH, RKVARS (14), TPULSE, CSTEP, DRDT (20)		RKAMCOM5
C	COMMON DECK "UU" INSERTED HERE		CUU 2
	REAL MODU		CUU 4
	COMMON/UU/MODU (4)		CUU 5
	1 ,V ,PVT ,PVR ,PVTH ,PVPH		CUU 6
	2 ,VR ,PVRT ,PVRR ,PVRTH ,PVRPH		CUU 7
	3 ,VTH ,PVTH, PVTHR, PVTHH, PVTHPH		CUU 8
	4 ,VPH, PVPHT, PVPHR, PVPHTH, PVPHPH		CUU 9
C	COMMON DECK "WW" INSERTED HERE		CWW 2
	PARAMETER (NWARSZ=1000)		CWW1 3
	COMMON/WW/ID (10), MAXW, W (NWARSZ)		CWW1 4
	REAL MAXSTP, MAXERR, INTYP, LLAT, LLON		CWW2 2
	EQUIVALENCE (EARTH, W(1)), (RAY, W(2)), (XMTRH, W(3)), (TLAT, W(4)),		CWW2 3
	1 (TLON, W(5)), (OW, W(6)), (FBEG, W(7)), (FEND, W(8)), (FSTEP, W(9)),		CWW2 4
	2 (AZ1, W(10)), (AZBEG, W(11)), (AZEND, W(12)), (AZSTEP, W(13)),		CWW2 5
	3 (BETA, W(14)), (ELBEG, W(15)), (EEND, W(16)), (ELSTEP, W(17)),		CWW2 6
	8 (RCVRH, W(20)),		CWW2 7
	4 (ONLY, W(21)), (HOP, W(22)), (MAXSTP, W(23)), (PLAT, W(24)), (PLON, W(25))		CWW2 8
	5, (HMAX, W(26)), (RAYFNC, W(29)), (EXTINC, W(33)),		CWW2 9
	6 (HMIN, W(27)), (RGMAX, W(28)),		CWW2 10
	8 (INTYP, W(41)), (MAXERR, W(42)), (ERATIO, W(43)),		CWW2 11
	6 (STEP1, W(44)), (STPMAX, W(45)), (STPMIN, W(46)), (FACTR, W(47)),		CWW2 12
	7 (SKIP, W(71)), (RAYSET, W(72)), (PRTSRP, W(74)), (HITLET, W(75))		CWW2 13
	9 , (BINRAY, W(76)), (PAGLN, W(77)), (PLT, W(81)), (PFACTR, W(82)),		CWW2 14
	1 (LLAT, W(83)), (LLON, W(84)), (RLAT, W(85)), (RLON, W(86))		CWW2 15
	2, (TIC, W(87)), (HB, W(88)), (HT, W(89)), (TICV, W(96))		CWW2 16
	REAL MMODEL, MFORM, MID		CWW3 2
C			CWW3 3
C	WIND 100-124		CWW3 4
	EQUIVALENCE (W(100), UMODEL), (W(101), UFORM), (W(102), UID)		CWW3 5
C			CWW3 6
C	DELTA WIND 125-149		CWW3 7
	EQUIVALENCE (W(125), DUMODEL), (W(126), DUFORM), (W(127), DUID)		CWW3 8
C			CWW3 9
C	SOUND SPEED 150-174		CWW3 10
	EQUIVALENCE (W(150), CMODEL), (W(151), CFORM), (W(152), CID)		CWW3 11
	EQUIVALENCE (W(153), REFC)		CWW3 12
C			CWW3 13
C	DELTA SOUND SPEED 175-199		CWW3 14
	EQUIVALENCE (W(175), DCMODEL), (W(176), DCFORM), (W(177), DCID)		CWW3 15
C			CWW3 16
C	TEMPERATURE 200-224		CWW3 17
	EQUIVALENCE (W(200), TMODEL), (W(201), TFORM), (W(202), TID)		CWW3 18
C			CWW3 19
C	DELTA TEMPERATURE 225-249		CWW3 20
	EQUIVALENCE (W(225), DTMODEL), (W(226), DTFORM), (W(227), DTID)		CWW3 21
C			CWW3 22
C	MOLECULAR 250-274		CWW3 23

C	EQUIVALENCE (W(250),MMODEL), (W(251),MFORM), (W(252),MID)	CWW3	24
C	RECEIVER HEIGHT 275-299	CWW3	25
C	EQUIVALENCE (W(275),RMODEL), (W(276),RFORM), (W(277),RID)	CWW3	26
C	TOPOGRAPHY 300-324	CWW3	27
C	EQUIVALENCE (W(300),GMODEL), (W(301),GFORM), (W(302),GID)	CWW3	28
C	DELTA TOPOGRAPHY 325-349	CWW3	29
C	EQUIVALENCE (W(325),GUMODEL), (W(326),GUFORM), (W(327),GUID)	CWW3	30
C	UPPER SURFACE TOPOGRAPHY 350-374	CWW3	31
C	EQUIVALENCE (W(350),SMODEL), (W(351),SFORM), (W(352),SID)	CWW3	32
C	PLOT ENHANCEMENTS CONTROL PARAMETERS	CWW3	33
C	EQUIVALENCE (W(490),XFQMDL), (W(491),YFQMDL)	CWW3	34
C	ABSORPTION 500-524	CWW3	35
C	EQUIVALENCE (W(500),AMODEL), (W(501),AFORM), (W(502),AID)	CWW3	36
C	DELTA ABSORPTION 525-549	CWW3	37
C	EQUIVALENCE (W(525),DAMODEL), (W(526),DAFORM), (W(527),DAID)	CWW3	38
C	PRESSURE 550-574	CWW3	39
C	EQUIVALENCE (W(550),PMODEL), (W(551),PFORM), (W(552),PID)	CWW3	40
C	DELTA PRESSURE 575-599	CWW3	41
C	EQUIVALENCE (W(575),DPMODEL), (W(576),DPFORM), (W(577),DPID)	CWW3	42
C	COMMON DECK "B1" INSERTED HERE	CWW3	43
C	INTEGER UMX, UNTBL, UITBL, UFRMTBL, IDSU(10)	CB1	44
C	COMMON/B1/UMX, UNTBL(10), UITBL(10), UFRMTBL(10), UGP(10)	CB1	45
C	EQUIVALENCE (UGP, IDSU)	CB1	46
C	EQUIVALENCE (W(103), URO)	CB1	47
C	EQUIVALENCE (W(104), UTH0), (W(105), UPH0), (W(106), PUPHZ0)	WLINEA17	48
C	DATA RECOGU/1.0/	WLINEA18	49
C	DATA UMX/1/	WLINEA19	50
C	DATA UNTBL/1, 11, 8*0/	WLINEA20	51
C	DATA UITBL/1, 9*0/	WNEARBL2	52
C	DATA UFRMTBL/1, 9*0/	WNEARBL3	53
C	ENTRY IWINDR	WNEARBL4	54
C	IF(RECOGU .NE. UMODEL)	WNEARBL5	55
C	1 CALL RERROR('SPEED ', 'WRNG MODEL', RECOGU)	WLINEA23	56
C	MODU(1)=7HLINEAR	WLINEA24	57
C	MODU(2)=UID	WLINEA25	58
C	CALL IPWINDR	WLINEA26	59
C	RETURN	WLINEA27	60
C	ENTRY WINDR	WLINEA28	61
C	H = R - EARTH	WLINEA29	62
C		WLINEA30	63
		WLINEA31	64
		WLINEA32	65
		WLINEA33	66
		WLINEA34	67
		WLINEA35	68
		WLINEA36	69
		WLINEA37	70

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C      CALL CLEAR(V,20)
      VR = URO
      VTH = UTHO
      VPH = (UPHO + PUPHZO * H)
      V=SQRT(VR*VR+VTH*VTH+VPH*VPH)
      PVR=PUPHZO
      IF(V.NE.0.0) PVR=VPH/V*PUPHZO
      PVPHR = PUPHZO
      CALL PWINDR
      RETURN
      END

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WLINEA38
WLINEA39
WLINEA40
WLINEA41
WLINEA42
WLINEA43
WLINEA44
WLINEA45
WLINEA46
WLINEA47
WLINEA48
WLINEA49

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C      SUBROUTINE WTIDE
C      WIND VELOCITY MODEL
C      PROVIDES WIND FIELD OF THE ATMOSPHERIC TIDES BY ZONAL AND
C      MERIDONAL HEIGHT PROFILES THAT ARE SINUSOIDAL AND IN PHASE
C      QUADRATURE.
C
C      REAL LAMZ
C      COMMON DECK "RKAM" INSERTED HERE
C      REAL KR,KTH,KPH
C      COMMON//R,TH,PH,KR,KTH,KPH,RKVAR(14),TPULSE,CSTEP,DRDT(20)
C      COMMON DECK "UU" INSERTED HERE
C      REAL MODU
C      COMMON/UU/MODU(4)
1      ,V ,PVT ,PVR ,PVTH ,PVPH
2      ,VR ,PVRT ,PVRR ,PVRTH ,PVRPH
3      ,VTH ,PVTHT ,PVTHR ,PVTHTH ,PVTHPH
4      ,VPH ,PVPHT ,PVPHR ,PVPHTH ,PVPHPH
C      COMMON DECK "WW" INSERTED HERE
C      PARAMETER (NWARSZ=1000)
C      COMMON/WW/ID(10),MAXW,W(NWARSZ)
C      REAL MAXSTP,MAXERR,INTYP,LLAT,LLON
C      EQUIVALENCE (EARTH,W(1)),(RAY,W(2)),(XMTRH,W(3)),(TLAT,W(4)),
1 (TLON,W(5)),(OW,W(6)),(FBEG,W(7)),(FEND,W(8)),(FSTEP,W(9)),
2 (AZ1,W(10)),(AZBEG,W(11)),(AZEND,W(12)),(AZSTEP,W(13)),
3 (BETA,W(14)),(ELBEG,W(15)),(ELEND,W(16)),(ELSTEP,W(17)),
8 (RCVRH,W(20)),
4 (ONLY,W(21)),(HOP,W(22)),(MAXSTP,W(23)),(PLAT,W(24)),(PLON,W(25))
5,(HMAX,W(26)),(RAYFNC,W(29)),(EXTINC,W(33)),
6 (HMIN,W(27)),(RGMX,W(28)),
8 (INTYP,W(41)),(MAXERR,W(42)),(ERATIO,W(43)),
6 (STEP1,W(44)),(STPMAX,W(45)),(STPMIN,W(46)),(FACTR,W(47)),
7 (SKIP,W(71)),(RAYSET,W(72)),(PRTSRP,W(74)),(HITLET,W(75))
9 ,(BINRAY,W(76)),(PAGLN,W(77)),(PLT,W(81)),(PFACTR,W(82)),
1 (LLAT,W(83)),(LLON,W(84)),(RLAT,W(85)),(RLON,W(86))
2,(TIC,W(87)),(HB,W(88)),(HT,W(89)),(TICV,W(96))
C      REAL MMODEL,MFORM,MID
C
C      WIND          100-124

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WTIDE  8
WTIDE  9
WTIDE 10
WTIDE 11
WTIDE 12
WTIDE 13
WTIDE 14
RKAMCOM2
RKAMCOM4
RKAMCOM5
CUU    2
CUU    4
CUU    5
CUU    6
CUU    7
CUU    8
CUU    9
CWW    2
CWW1   3
CWW1   4
CWW2   2
CWW2   3
CWW2   4
CWW2   5
CWW2   6
CWW2   7
CWW2   8
CWW2   9
CWW2  10
CWW2  11
CWW2  12
CWW2  13
CWW2  14
CWW2  15
CWW2  16
CWW3   2
CWW3   3
CWW3   4

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C	EQUIVALENCE (W(100),UMODEL), (W(101),UFORM), (W(102),UID)	CWW3	5
C	DELTA WIND 125-149	CWW3	6
C	EQUIVALENCE (W(125),DUMODEL), (W(126),DUFORM), (W(127),DUID)	CWW3	7
C	SOUND SPEED 150-174	CWW3	8
C	EQUIVALENCE (W(150),CMODEL), (W(151),CFORM), (W(152),CID)	CWW3	9
C	EQUIVALENCE (W(153),REFC)	CWW3	10
C	DELTA SOUND SPEED 175-199	CWW3	11
C	EQUIVALENCE (W(175),DCMODEL), (W(176),DCFORM), (W(177),DCID)	CWW3	12
C	TEMPERATURE 200-224	CWW3	13
C	EQUIVALENCE (W(200),TMODEL), (W(201),TFORM), (W(202),TID)	CWW3	14
C	DELTA TEMPERATURE 225-249	CWW3	15
C	EQUIVALENCE (W(225),DTMODEL), (W(226),DTFORM), (W(227),DTID)	CWW3	16
C	MOLECULAR 250-274	CWW3	17
C	EQUIVALENCE (W(250),MMODEL), (W(251),MFORM), (W(252),MID)	CWW3	18
C	RECEIVER HEIGHT 275-299	CWW3	19
C	EQUIVALENCE (W(275),RMODEL), (W(276),RFORM), (W(277),RID)	CWW3	20
C	TOPOGRAPHY 300-324	CWW3	21
C	EQUIVALENCE (W(300),GMODEL), (W(301),GFORM), (W(302),GID)	CWW3	22
C	DELTA TOPOGRAPHY 325-349	CWW3	23
C	EQUIVALENCE (W(325),GUMODEL), (W(326),GUFORM), (W(327),GUID)	CWW3	24
C	UPPER SURFACE TOPOGRAPHY 350-374	CWW3	25
C	EQUIVALENCE (W(350),SMODEL), (W(351),SFORM), (W(352),SID)	CWW3	26
C	PLOT ENHANCEMENTS CONTROL PARAMETERS	CWW3	27
C	EQUIVALENCE (W(490),XFQMDL), (W(491),YFQMDL)	CWW3	28
C	ABSORPTION 500-524	CWW3	29
C	EQUIVALENCE (W(500),AMODEL), (W(501),AFORM), (W(502),AID)	CWW3	30
C	DELTA ABSORPTION 525-549	CWW3	31
C	EQUIVALENCE (W(525),DAMODEL), (W(526),DAFORM), (W(527),DAID)	CWW3	32
C	PRESSURE 550-574	CWW3	33
C	EQUIVALENCE (W(550),PMODEL), (W(551),PFORM), (W(552),PID)	CWW3	34
C	DELTA PRESSURE 575-599	CWW3	35
C	EQUIVALENCE (W(575),DPMODEL), (W(576),DPFORM), (W(577),DPID)	CWW3	36
C	COMMON DECK "B1" INSERTED HERE	CWW3	37
C	INTEGER UMX,UNTBL,UITBL,UFRMTBL,IDSU(10)	CB1	2
C	COMMON/B1/UMX,UNTBL(10),UITBL(10),UFRMTBL(10),UGP(10)	CB1	4
C	EQUIVALENCE (UGP,IDSU)	CB1	5
C	COMMON DECK "CONST" INSERTED HERE	CB1	6
C	COMMON/PCONST/CREG,RGAS,GAMMA	CCONST	2
C	COMMON/MCONST/PI,PIT2,PID2,DEGS,RAD,ALN10	CCONST	4
C	EQUIVALENCE (W(103),UPHO)	CCONST	5
		WTIDE	20

C	EQUIVALENCE (W(104),UTH0),(W(105),LAMZ),(W(106),TTAU),(W(107),TAU)	WTIDE 21
		WTIDE 22
	DATA RECOGU/5.0/	WTIDE 23
	DATA UMX/1/	WDEBL 2
	DATA UNTBL/1,11,8*0/	WDEBL 3
	DATA UITBL/1,9*0/	WDEBL 4
	DATA UFRMTBL/1,9*0/	WDEBL 5
C		WTIDE 26
C		WTIDE 27
	ENTRY IWINDR	WTIDE 28
C		WTIDE 29
	IF(RECOGU .NE. UMODEL)	WTIDE 30
1	CALL RERROR('SPEED ', 'WRNG MODEL', RECOGU)	WTIDE 31
C		WTIDE 32
	MODU(1)=5HWTIDE	WTIDE 33
	MODU(2)=UID	WTIDE 34
	CALL IPWINDR	WTIDE 35
C		WTIDE 36
	Q=PID2/LAMZ	WTIDE 37
	S=PID2/TAU	WTIDE 38
	RETURN	WTIDE 39
C		WTIDE 40
	ENTRY WINDR	WTIDE 41
C		WTIDE 42
	CALL CLEAR(V,20)	WTIDE 43
C		WTIDE 44
	ARG=PID2*((R-EARTHHR)/LAMZ+TTAU)	WTIDE 45
C		WTIDE 46
	CSA=COS(ARG)	WTIDE 47
	SSA=SIN(ARG)	WTIDE 48
	VTH=UTH0*SSA	WTIDE 49
	VPH=UPH0*CSA	WTIDE 50
C		WTIDE 51
	PVTHR=CSA*Q*UTH0	WTIDE 52
	PVPHR=SSA*Q*UPH0	WTIDE 53
C	V=SQRT(VTH*VTH+VPH*VPH)	WTIDE 54
	PVTHT=CSA*S*UTH0	WTIDE 55
	PVPHT=SSA*S*UPH0	WTIDE 56
	CALL PWINDR	WTIDE 57
	RETURN	WTIDE 58
	END	WTIDE 59
	SUBROUTINE ULOGZ2	ULOGZ2 8
C	LOGARITHMIC WIND VELOCITY PROFILE	ULOGZ2 9
C	SINGULARITY IS AVOIDED BY A LINEAR TANGENT UNIQUELY	ULOGZ210
C	DETERMINED BY CONTINUITY OF VALUE AND SLOPE GOING THROUGH	ULOGZ211
C	THE ORIGIN.	ULOGZ212
	REAL K	ULOGZ213
	EQUIVALENCE (USTAR,W(103)),(K,W(104)),(Z0,W(105))	ULOGZ214
C		ULOGZ215
C	COMMON DECK "RKAM" INSERTED HERE	RKAMCOM2

	REAL KR, KTH, KPH	RKAMCOM4
	COMMON /R, TH, PH, KR, KTH, KPH, RKVARS (14), TPULSE, CSTEP, DRDT (20)	RKAMCOM5
C	COMMON DECK "UU" INSERTED HERE	CUU 2
	REAL MODU	CUU 4
	COMMON /UU /MODU (4)	CUU 5
	1 ,V ,PVT ,PVR ,PVTH ,PVPH	CUU 6
	2 ,VR ,PVRT ,PVRR ,PVTRH ,PVRRH	CUU 7
	3 ,VTH ,PVTH, PVTHR, PVTHH, PVTHPH	CUU 8
	4 ,VPH ,VPH, PVPH, PVPHH, PVPHPH	CUU 9
C	COMMON DECK "WW" INSERTED HERE	CWW 2
	PARAMETER (NWARSZ=1000)	CWW1 3
	COMMON /WW /ID (10), MAXW, W (NWARSZ)	CWW1 4
	REAL MAXSTP, MAXERR, INTYP, LLAT, LLON	CWW2 2
	EQUIVALENCE (EARTH, W(1)), (RAY, W(2)), (XMTRH, W(3)), (TLAT, W(4)),	CWW2 3
	1 (TLON, W(5)), (OW, W(6)), (FBEG, W(7)), (FEND, W(8)), (FSTEP, W(9)),	CWW2 4
	2 (AZ1, W(10)), (AZBEG, W(11)), (AZEND, W(12)), (AZSTEP, W(13)),	CWW2 5
	3 (BETA, W(14)), (ELBEG, W(15)), (ELEND, W(16)), (ELSTEP, W(17)),	CWW2 6
	4 (RCVRH, W(20)),	CWW2 7
	5 (ONLY, W(21)), (HOP, W(22)), (MAXSTP, W(23)), (PLAT, W(24)), (PLON, W(25))	CWW2 8
	6 (HMAX, W(26)), (RAYFNC, W(29)), (EXTINC, W(33)),	CWW2 9
	7 (HMIN, W(27)), (RGMAX, W(28)),	CWW2 10
	8 (INTYP, W(41)), (MAXERR, W(42)), (ERATIO, W(43)),	CWW2 11
	6 (STEP1, W(44)), (STPMAX, W(45)), (STPMIN, W(46)), (FACTR, W(47)),	CWW2 12
	7 (SKIP, W(71)), (RAYSET, W(72)), (PRTSRP, W(74)), (HITLET, W(75))	CWW2 13
	9 , (BINRAY, W(76)), (PAGLN, W(77)), (PLT, W(81)), (PFACTR, W(82)),	CWW2 14
	1 (LLAT, W(83)), (LLON, W(84)), (RLAT, W(85)), (RLON, W(86))	CWW2 15
	2, (TIC, W(87)), (HB, W(88)), (HT, W(89)), (TICV, W(96))	CWW2 16
	REAL MMODEL, MFORM, MID	CWW3 2
C		CWW3 3
C	WIND 100-124	CWW3 4
	EQUIVALENCE (W(100), UMODEL), (W(101), UFORM), (W(102), UID)	CWW3 5
C		CWW3 6
C	DELTA WIND 125-149	CWW3 7
	EQUIVALENCE (W(125), DUMODEL), (W(126), DUFORM), (W(127), DUID)	CWW3 8
C		CWW3 9
C	SOUND SPEED 150-174	CWW3 10
	EQUIVALENCE (W(150), CMODEL), (W(151), CFORM), (W(152), CID)	CWW3 11
	EQUIVALENCE (W(153), REFC)	CWW3 12
C		CWW3 13
C	DELTA SOUND SPEED 175-199	CWW3 14
	EQUIVALENCE (W(175), DCMODEL), (W(176), DCFORM), (W(177), DCID)	CWW3 15
C		CWW3 16
C	TEMPERATURE 200-224	CWW3 17
	EQUIVALENCE (W(200), TMODEL), (W(201), TFORM), (W(202), TID)	CWW3 18
C		CWW3 19
C	DELTA TEMPERATURE 225-249	CWW3 20
	EQUIVALENCE (W(225), DTMODEL), (W(226), DTFORM), (W(227), DTID)	CWW3 21
C		CWW3 22
C	MOLECULAR 250-274	CWW3 23
	EQUIVALENCE (W(250), MMODEL), (W(251), MFORM), (W(252), MID)	CWW3 24
C		CWW3 25
C	RECEIVER HEIGHT 275-299	CWW3 26
	EQUIVALENCE (W(275), RMODEL), (W(276), RFORM), (W(277), RID)	CWW3 27
C		CWW3 28
C	TOPOGRAPHY 300-324	CWW3 29

C	EQUIVALENCE (W(300),GMODEL), (W(301),GFORM), (W(302),GID)	CWW3	30
C	DELTA TOPOGRAPHY 325-349	CWW3	31
C	EQUIVALENCE (W(325),GUMODEL), (W(326),GUFORM), (W(327),GUID)	CWW3	32
C	UPPER SURFACE TOPOGRAPHY 350-374	CWW3	33
C	EQUIVALENCE (W(350),SMODEL), (W(351),SFORM), (W(352),SID)	CWW3	34
C	PLOT ENHANCEMENTS CONTROL PARAMETERS	CWW3	35
C	EQUIVALENCE (W(490),XFQMDL), (W(491),YFQMDL)	CWW3	36
C	ABSORPTION 500-524	CWW3	37
C	EQUIVALENCE (W(500),AMODEL), (W(501),AFORM), (W(502),AID)	CWW3	38
C	DELTA ABSORPTION 525-549	CWW3	39
C	EQUIVALENCE (W(525),DAMODEL), (W(526),DAFORM), (W(527),DAID)	CWW3	40
C	PRESSURE 550-574	CWW3	41
C	EQUIVALENCE (W(550),PMODEL), (W(551),PFORM), (W(552),PID)	CWW3	42
C	DELTA PRESSURE 575-599	CWW3	43
C	EQUIVALENCE (W(575),DPMODEL), (W(576),DPFORM), (W(577),DPID)	CWW3	44
C	COMMON DECK "B1" INSERTED HERE	CWW3	45
C	INTEGER UMX,UNTBL,UITBL,UFRMTBL,IDSU(10)	CB1	46
C	COMMON/B1/UMX,UNTBL(10),UITBL(10),UFRMTBL(10),UGP(10)	CB1	47
C	EQUIVALENCE (UGP,IDSU)	CB1	48
C	COMMON DECK "GG" INSERTED HERE	CB1	49
C	REAL MODG	CGG	50
C	COMMON/GG/MODG(4)	CGG	51
C	COMMON/GG/G, PGR, PGRR, PGRTH, PGRPH	CGG	2
C	COMMON/GG/PGTH, PGPH, PGTHTH, PGPHPH, PGTHPH, GSELECT, GTIME	CGG	3
C	DATA RECOGU/6.0/	CGG	4
C	DATA UMX/1/	ULOGZ221	5
C	DATA UNTBL/1,11,8*0/	UGZ2BL	6
C	DATA UITBL/1,9*0/	UGZ2BL	7
C	DATA UFRMTBL/1,9*0/	UGZ2BL	8
C	ENTRY IWINDR	UGZ2BL	9
C	IF(RECOGU .NE. UMODEL)	ULOGZ224	10
C	1 CALL RERROR('ULOGZ2 ', 'WRNG MODEL', RECOGU)	ULOGZ225	11
C	MODU(1)=6HULOGZ2	ULOGZ226	12
C	MODU(2)=UID	ULOGZ227	13
C	ZOE=Z0*EXP(1.0)	ULOGZ228	14
C	C=USTAR/K	ULOGZ229	15
C	CZOE=C/ZOE	ULOGZ230	16
C	CALL IPWINDR	ULOGZ231	17
C	RETURN	ULOGZ232	18
C	ENTRY WINDR	ULOGZ233	19
C	CALL CLEAR(V,20)	ULOGZ234	20
C	CALL TOPOG	ULOGZ235	21
		ULOGZ236	22
		ULOGZ237	23
		ULOGZ238	24
		ULOGZ239	25
		ULOGZ240	26
		ULOGZ241	27
		ULOGZ242	28

	Z = G/PGR	
	IF(Z.GT.ZOE) GO TO 100	ULOGZ243
C		ULOGZ244
	VPH=CZOE*Z	ULOGZ245
	PVPHR=CZOE*PGR	ULOGZ246
	PVPHTH=CZOE*PGTH	ULOGZ247
	PVPHPH=CZOE*PGPH	ULOGZ248
	GO TO 120	ULOGZ249
C		ULOGZ250
100	VPH=C*ALOG(Z/ZO)	ULOGZ251
	CZ=C/Z	ULOGZ252
	PVPHR=CZ*PGR	ULOGZ253
	PVPHTH=CZ*PGTH	ULOGZ254
	PVPHPH=CZ*PGPH	ULOGZ255
C		ULOGZ256
120	V=ABS(VPH)	ULOGZ257
	PVR=SIGN(PVPHR,VPH)	ULOGZ258
C		ULOGZ259
	CALL PWINDR	ULOGZ260
	RETURN	ULOGZ261
	END	ULOGZ262
		ULOGZ263

	SUBROUTINE VVORTX3	VVORTX39
C	WIND VELOCITY MODEL	VVORTX10
C	VERTICAL VORTEX WIND PERTURBATION WITH VISCOUS CORE AND	VVORTX11
C	MULTIPLIES VELOCITY FIELD BY A GUASSIAN HEIGHT PROFILE.	VVORTX12
C		VVORTX13
C	COMMON DECK "CONST" INSERTED HERE	CCONST 2
	COMMON/PCONST/CREF, RGAS, GAMMA	CCONST 4
	COMMON/MCONST/PI, PIT2, PID2, DEGS, RAD, ALN10	CCONST 5
C	COMMON DECK "RKAM" INSERTED HERE	RKAMCOM2
	REAL KR, KTH, KPH	RKAMCOM4
	COMMON//R, TH, PH, KR, KTH, KPH, RKVARS(14), TPULSE, CSTEP, DRDT(20)	RKAMCOM5
C	COMMON DECK "UU" INSERTED HERE	CUU 2
	REAL MODU	CUU 4
	COMMON/UU/MODU(4)	CUU 5
	1 ,V ,PVT ,PVR ,PVTH ,PVPH	CUU 6
	2 ,VR ,PVRT ,PVRR ,PVRTH ,PVRPH	CUU 7
	3 ,VTH ,PVTHT ,PVTHR ,PVTHTH ,PVTHPH	CUU 8
	4 ,VPH ,PVPHT ,PVPHR ,PVPHTH ,PVPHPH	CUU 9
C	COMMON DECK "WW" INSERTED HERE	CWW 2
	PARAMETER (NWARSZ=1000)	CWW1 3
	COMMON/WW/ID(10), MAXW, W(NWARSZ)	CWW1 4
	REAL MAXSTP, MAXERR, INTYP, LLAT, LLON	CWW2 2
	EQUIVALENCE (EARTH, W(1)), (RAY, W(2)), (XMTRH, W(3)), (TLAT, W(4)),	CWW2 3
	1 (TLON, W(5)), (OW, W(6)), (FBEG, W(7)), (FEND, W(8)), (FSTEP, W(9)),	CWW2 4
	2 (AZ1, W(10)), (AZBEG, W(11)), (AZEND, W(12)), (AZSTEP, W(13)),	CWW2 5
	3 (BETA, W(14)), (ELBEG, W(15)), (ELEND, W(16)), (ELSTEP, W(17)),	CWW2 6
	8 (RCVRH, W(20)),	CWW2 7
	4 (ONLY, W(21)), (HOP, W(22)), (MAXSTP, W(23)), (PLAT, W(24)), (PLON, W(25))	CWW2 8
	5, (HMAX, W(26)), (RAYFNC, W(29)), (EXTINC, W(33)),	CWW2 9

	6 (HMIN,W(27)), (RGMAX,W(28)),	CWW2	10
	8 (INTYP,W(41)), (MAXERR,W(42)), (ERATIO,W(43)),	CWW2	11
	6 (STEPL,W(44)), (STPMAX,W(45)), (STPMIN,W(46)), (FACTR,W(47)),	CWW2	12
	7 (SKIP,W(71)), (RAYSET,W(72)), (PRTSRP,W(74)), (HITLET,W(75))	CWW2	13
	9 , (BINRAY,W(76)), (PAGLN,W(77)), (PLT,W(81)), (PFACTOR,W(82)),	CWW2	14
	1 (LLAT,W(83)), (LLON,W(84)), (RLAT,W(85)), (RLON,W(86))	CWW2	15
	2, (TIC,W(87)), (HB,W(88)), (HT,W(89)), (TICV,W(96))	CWW2	16
	REAL MMODEL,MFORM,MID	CWW3	2
C		CWW3	3
C	WIND 100-124	CWW3	4
	EQUIVALENCE (W(100),UMODEL), (W(101),UFORM), (W(102),UID)	CWW3	5
C		CWW3	6
C	DELTA WIND 125-149	CWW3	7
	EQUIVALENCE (W(125),DUMODEL), (W(126),DUFORM), (W(127),DUID)	CWW3	8
C		CWW3	9
C	SOUND SPEED 150-174	CWW3	10
	EQUIVALENCE (W(150),CMODEL), (W(151),CFORM), (W(152),CID)	CWW3	11
	EQUIVALENCE (W(153),REFC)	CWW3	12
C		CWW3	13
C	DELTA SOUND SPEED 175-199	CWW3	14
	EQUIVALENCE (W(175),DCMODEL), (W(176),DCFORM), (W(177),DCID)	CWW3	15
C		CWW3	16
C	TEMPERATURE 200-224	CWW3	17
	EQUIVALENCE (W(200),TMODEL), (W(201),TFORM), (W(202),TID)	CWW3	18
C		CWW3	19
C	DELTA TEMPERATURE 225-249	CWW3	20
	EQUIVALENCE (W(225),DTMODEL), (W(226),DTFORM), (W(227),DTID)	CWW3	21
C		CWW3	22
C	MOLECULAR 250-274	CWW3	23
	EQUIVALENCE (W(250),MMODEL), (W(251),MFORM), (W(252),MID)	CWW3	24
C		CWW3	25
C	RECEIVER HEIGHT 275-299	CWW3	26
	EQUIVALENCE (W(275),RMODEL), (W(276),RFORM), (W(277),RID)	CWW3	27
C		CWW3	28
C	TOPOGRAPHY 300-324	CWW3	29
	EQUIVALENCE (W(300),GMODEL), (W(301),GFORM), (W(302),GID)	CWW3	30
C		CWW3	31
C	DELTA TOPOGRAPHY 325-349	CWW3	32
	EQUIVALENCE (W(325),GUMODEL), (W(326),GUFORM), (W(327),GUID)	CWW3	33
C		CWW3	34
C	UPPER SURFACE TOPOGRAPHY 350-374	CWW3	35
	EQUIVALENCE (W(350),SMODEL), (W(351),SFORM), (W(352),SID)	CWW3	36
C		CWW3	37
C	PLOT ENHANCEMENTS CONTROL PARAMETERS	CWW3	38
	EQUIVALENCE (W(490),XFQMDL), (W(491),YFQMDL)	CWW3	39
C	ABSORPTION 500-524	CWW3	40
	EQUIVALENCE (W(500),AMODEL), (W(501),AFORM), (W(502),AID)	CWW3	41
C		CWW3	42
C	DELTA ABSORPTION 525-549	CWW3	43
	EQUIVALENCE (W(525),DAMODEL), (W(526),DAFORM), (W(527),DAID)	CWW3	44
C		CWW3	45
C	PRESSURE 550-574	CWW3	46
	EQUIVALENCE (W(550),PMODEL), (W(551),PFORM), (W(552),PID)	CWW3	47
C		CWW3	48
C	DELTA PRESSURE 575-599	CWW3	49

C	EQUIVALENCE (W(575),DPMODEL), (W(576),DPFORM), (W(577),DPID)	CWW3 50
	EQUIVALENCE (U0,W(103)), (R0,W(104)), (TH0,W(105)), (PH0,W(106))	CWW3 51
	EQUIVALENCE (HWIDTH,W(107)), (HVMAX,W(108))	VVORTX18
C	COMMON DECK "B1" INSERTED HERE	VVORTX19
	INTEGER UMX,UNTBL,UITBL,UFRMTBL,IDSU(10)	CB1 2
	COMMON/B1/UMX,UNTBL(10),UITBL(10),UFRMTBL(10),UGP(10)	CB1 4
	EQUIVALENCE (UGP,IDSU)	CB1 5
	DATA RECOGU/9.0/	CB1 6
	DATA UMX/1/	VVORTX21
	DATA UNTBL/1,11,8*0/	VRTX3BL2
	DATA UITBL/1,9*0/	VRTX3BL3
	DATA UFRMTBL/1,9*0/	VRTX3BL4
C		VRTX3BL5
	ENTRY IWINDR	VVORTX24
C		VVORTX25
	IF(RECOGU .NE. UMODEL)	VVORTX26
1	CALL RERROR('SPEED ', 'WRNG MODEL', RECOGU)	VVORTX27
C		VVORTX28
	MODU(1)=7HVVERTX3	VVORTX29
	MODU(2)=UID	VVORTX30
	DENOM=0.0	VVORTX31
	IF(HWIDTH.NE.0.0) DENOM=1.0/HWIDTH**2	VVORTX32
	CALL IPWINDR	VVORTX33
C		VVORTX34
	RETURN	VVORTX35
C		VVORTX36
	ENTRY WINDR	VVORTX37
	CALL CLEAR(V,20)	VVORTX38
	DR=R-EARTH-HVMAX	VVORTX39
	DTH = TH - (PID2-TH0)	VVORTX40
	DPH = PH - PH0	VVORTX41
	RAD2 = EARTH * SQRT(DTH * DTH + DPH * DPH)	VVORTX42
	A = 1.397	VVORTX43
	B = - 1.26	VVORTX44
	EXPO=RAD2/R0	VVORTX45
	EXPO=B*EXPO*EXPO	VVORTX46
	EXB=0.0	VVORTX47
	IF(EXPO .GT. -675.0) EXB = EXP(EXPO)	VVORTX48
	FX=1.-EXB	VVORTX49
	DUM = A * EARTH * U0 * R0 / RAD2 * * 2	VVORTX50
	FZ=EXP(-DR*DR*DENOM)	VVORTX51
	DFDZ=-2.*DR*DENOM	VVORTX52
	DUM=FZ*DUM	VVORTX53
C		VVORTX54
	DUX = FX / RAD2 + RAD2 * B * EXB / R0 * * 2	VVORTX55
	VTH = - DUM * FX * DPH	VVORTX56
	VPH = DUM * FX * DTH	VVORTX57
	V=SQRT(VTH*VTH + VPH*VPH)	VVORTX58
	DUM2=2.*DUM*EARTH*EARTH	VVORTX59
	PVTHTH = DUM2 * DTH * DPH / RAD2 * DUX	VVORTX60
	PVPHPH = - PVTHTH	VVORTX61
	PVTHPH = DPH**2 * DUM2 / RAD2 * DUX -DUM*FX	VVORTX62
	PVPHTH = - DTH**2 * DUM2 / RAD2 * DUX + DUM*FX	VVORTX63
C		VVORTX64
		VVORTX65

	PVTH=(VTH*PVTHTH + VPH*PVPHTH)/V	VVORTX66
	PVPH=(VTH*PVTHPH + VPH*PVPHPH)/V	VVORTX67
C		VVORTX68
	PVTHR=VTH*DFDZ	VVORTX69
	PVPHR=VPH*DFDZ	VVORTX70
	PVR=(VTH*PVTHR+VPH*PVPHR)/V	VVORTX71
C		VVORTX72
	CALL PWINDR	VVORTX73
	RETURN	VVORTX74
	END	VVORTX75
	SUBROUTINE WGAUSS2	WGAUSS28
C	WIND VELOCITY MODEL	WGAUSS29
C	EXPONENTIALLY DECAYING EFFECT IN ALL THREE DIRECTIONS.	WGAUSS10
C	COMMON DECK "CONST" INSERTED HERE	CCONST 2
	COMMON/PCONST/CREF, RGAS, GAMMA	CCONST 4
	COMMON/MCONST/PI, PIT2, PID2, DEGS, RAD, ALN10	CCONST 5
C	COMMON DECK "RKAM" INSERTED HERE	RKAMCOM2
	REAL KR, KTH, KPH	RKAMCOM4
	COMMON//R, TH, PH, KR, KTH, KPH, RKVARS(14), TPULSE, CSTEP, DRDT(20)	RKAMCOM5
C	COMMON DECK "UU" INSERTED HERE	CUU 2
	REAL MODU	CUU 4
	COMMON/UU/MODU(4)	CUU 5
	1 ,V ,PVT ,PVR ,PVTH ,PVPH	CUU 6
	2 ,VR ,PVRT ,PVRR ,PVTRH ,PVRRH	CUU 7
	3 ,VTH ,PVTHH ,PVTHR ,PVTHH ,PVTHPH	CUU 8
	4 ,VPH ,PVPHT ,PVPHR ,PVPHTH ,PVPHPH	CUU 9
C	COMMON DECK "WW" INSERTED HERE	CWW 2
	PARAMETER (NWARSZ=1000)	CWW1 3
	COMMON/WW/ID(10), MAXW, W(NWARSZ)	CWW1 4
	REAL MAXSTP, MAXERR, INTYP, LLAT, LLON	CWW2 2
	EQUIVALENCE (EARTH, W(1)), (RAY, W(2)), (XMTRH, W(3)), (TLAT, W(4)),	CWW2 3
	1 (TLON, W(5)), (OW, W(6)), (FBEG, W(7)), (FEND, W(8)), (FSTEP, W(9)),	CWW2 4
	2 (AZ1, W(10)), (AZBEG, W(11)), (AZEND, W(12)), (AZSTEP, W(13)),	CWW2 5
	3 (BETA, W(14)), (ELBEG, W(15)), (ELEND, W(16)), (ELSTEP, W(17)),	CWW2 6
	8 (RCVRH, W(20)),	CWW2 7
	4 (ONLY, W(21)), (HOP, W(22)), (MAXSTP, W(23)), (PLAT, W(24)), (PLON, W(25))	CWW2 8
	5, (HMAX, W(26)), (RAYFNC, W(29)), (EXTINC, W(33)),	CWW2 9
	6 (HMIN, W(27)), (RGMAX, W(28)),	CWW2 10
	8 (INTYP, W(41)), (MAXERR, W(42)), (ERATIO, W(43)),	CWW2 11
	6 (STEP1, W(44)), (STPMAX, W(45)), (STPMIN, W(46)), (FACTR, W(47)),	CWW2 12
	7 (SKIP, W(71)), (RAYSET, W(72)), (PRTSRP, W(74)), (HITLET, W(75))	CWW2 13
	9 , (BINRAY, W(76)), (PAGLN, W(77)), (PLT, W(81)), (PFACTR, W(82)),	CWW2 14
	1 (LLAT, W(83)), (LLON, W(84)), (RLAT, W(85)), (RLON, W(86))	CWW2 15
	2, (TIC, W(87)), (HB, W(88)), (HT, W(89)), (TICV, W(96))	CWW2 16
	REAL MMODEL, MFORM, MID	CWW3 2
C		CWW3 3
C	WIND 100-124	CWW3 4
	EQUIVALENCE (W(100), UMODEL), (W(101), UFORM), (W(102), UID)	CWW3 5
C		CWW3 6
C	DELTA WIND 125-149	CWW3 7

C	EQUIVALENCE (W(125),DUMODEL), (W(126),DUFORM), (W(127),DUID)	CWW3	8
C	SOUND SPEED 150-174	CWW3	9
C	EQUIVALENCE (W(150),CMODEL), (W(151),CFORM), (W(152),CID)	CWW3	10
C	EQUIVALENCE (W(153),REFC)	CWW3	11
C	DELTA SOUND SPEED 175-199	CWW3	12
C	EQUIVALENCE (W(175),DCMODEL), (W(176),DCFORM), (W(177),DCID)	CWW3	13
C	TEMPERATURE 200-224	CWW3	14
C	EQUIVALENCE (W(200),TMODEL), (W(201),TFORM), (W(202),TID)	CWW3	15
C	DELTA TEMPERATURE 225-249	CWW3	16
C	EQUIVALENCE (W(225),DTMODEL), (W(226),DTFORM), (W(227),DTID)	CWW3	17
C	MOLECULAR 250-274	CWW3	18
C	EQUIVALENCE (W(250),MMODEL), (W(251),MFORM), (W(252),MID)	CWW3	19
C	RECEIVER HEIGHT 275-299	CWW3	20
C	EQUIVALENCE (W(275),RMODEL), (W(276),RFORM), (W(277),RID)	CWW3	21
C	TOPOGRAPHY 300-324	CWW3	22
C	EQUIVALENCE (W(300),GMODEL), (W(301),GFORM), (W(302),GID)	CWW3	23
C	DELTA TOPOGRAPHY 325-349	CWW3	24
C	EQUIVALENCE (W(325),GUMODEL), (W(326),GUFORM), (W(327),GUID)	CWW3	25
C	UPPER SURFACE TOPOGRAPHY 350-374	CWW3	26
C	EQUIVALENCE (W(350),SMODEL), (W(351),SFORM), (W(352),SID)	CWW3	27
C	PLOT ENHANCEMENTS CONTROL PARAMETERS	CWW3	28
C	EQUIVALENCE (W(490),XFQMDL), (W(491),YFQMDL)	CWW3	29
C	ABSORPTION 500-524	CWW3	30
C	EQUIVALENCE (W(500),AMODEL), (W(501),AFORM), (W(502),AID)	CWW3	31
C	DELTA ABSORPTION 525-549	CWW3	32
C	EQUIVALENCE (W(525),DAMODEL), (W(526),DAFORM), (W(527),DAID)	CWW3	33
C	PRESSURE 550-574	CWW3	34
C	EQUIVALENCE (W(550),PMODEL), (W(551),PFORM), (W(552),PID)	CWW3	35
C	DELTA PRESSURE 575-599	CWW3	36
C	EQUIVALENCE (W(575),DPMODEL), (W(576),DPFORM), (W(577),DPID)	CWW3	37
C	COMMON DECK "B1" INSERTED HERE	CWW3	38
C	INTEGER UMX,UNTBL,UITBL,UFRMTBL,IDSU(10)	CB1	2
C	COMMON/B1/UMX,UNTBL(10),UITBL(10),UFRMTBL(10),UGP(10)	CB1	4
C	EQUIVALENCE (UGP,IDSU)	CB1	5
C	EQUIVALENCE (UPHO,W(103)), (WH,W(104)), (WTH,W(105))	CB1	6
C	EQUIVALENCE (WPH,W(106)), (HO,W(107)), (WGTHO,W(108)), (PHO,W(109))	WGAUSS16	
C	DATA RECOGU/7.0/	WGAUSS17	
C	DATA UMX/1/	WGAUSS18	
C	DATA UNTBL/1,11,8*0/	WUSS2L	2
C	DATA UITBL/1,9*0/	WUSS2L	3
C	DATA UFRMTBL/1,9*0/	WUSS2L	4
C		WUSS2L	5



	8 (RCVRH,W(20)),	CWW2	7
	4 (ONLY,W(21)), (HOP,W(22)), (MAXSTP,W(23)), (PLAT,W(24)), (PLON,W(25))	CWW2	8
	5, (HMAX,W(26)), (RAYFNC,W(29)), (EXTINC,W(33)),	CWW2	9
	6 (HMIN,W(27)), (RGMAX,W(28)),	CWW2	10
	8 (INTYP,W(41)), (MAXERR,W(42)), (ERATIO,W(43)),	CWW2	11
	6 (STEP1,W(44)), (STPMAX,W(45)), (STPMIN,W(46)), (FACTR,W(47)),	CWW2	12
	7 (SKIP,W(71)), (RAYSET,W(72)), (PRTSRP,W(74)), (HITLET,W(75))	CWW2	13
	9, (BINRAY,W(76)), (PAGLN,W(77)), (PLT,W(81)), (PFACTR,W(82)),	CWW2	14
	1 (LLAT,W(83)), (LLON,W(84)), (RLAT,W(85)), (RLON,W(86))	CWW2	15
	2, (TIC,W(87)), (HB,W(88)), (HT,W(89)), (TICV,W(96))	CWW2	16
	REAL MMODEL,MFORM,MID	CWW3	2
C		CWW3	3
C	WIND 100-124	CWW3	4
	EQUIVALENCE (W(100),UMODEL), (W(101),UFORM), (W(102),UID)	CWW3	5
C		CWW3	6
C	DELTA WIND 125-149	CWW3	7
	EQUIVALENCE (W(125),DUMODEL), (W(126),DUFORM), (W(127),DUID)	CWW3	8
C		CWW3	9
C	SOUND SPEED 150-174	CWW3	10
	EQUIVALENCE (W(150),CMODEL), (W(151),CFORM), (W(152),CID)	CWW3	11
	EQUIVALENCE (W(153),REFC)	CWW3	12
C		CWW3	13
C	DELTA SOUND SPEED 175-199	CWW3	14
	EQUIVALENCE (W(175),DCMODEL), (W(176),DCFORM), (W(177),DCID)	CWW3	15
C		CWW3	16
C	TEMPERATURE 200-224	CWW3	17
	EQUIVALENCE (W(200),TMODEL), (W(201),TFORM), (W(202),TID)	CWW3	18
C		CWW3	19
C	DELTA TEMPERATURE 225-249	CWW3	20
	EQUIVALENCE (W(225),DTMODEL), (W(226),DTFORM), (W(227),DTID)	CWW3	21
C		CWW3	22
C	MOLECULAR 250-274	CWW3	23
	EQUIVALENCE (W(250),MMODEL), (W(251),MFORM), (W(252),MID)	CWW3	24
C		CWW3	25
C	RECEIVER HEIGHT 275-299	CWW3	26
	EQUIVALENCE (W(275),RMODEL), (W(276),RFORM), (W(277),RID)	CWW3	27
C		CWW3	28
C	TOPOGRAPHY 300-324	CWW3	29
	EQUIVALENCE (W(300),GMODEL), (W(301),GFORM), (W(302),GID)	CWW3	30
C		CWW3	31
C	DELTA TOPOGRAPHY 325-349	CWW3	32
	EQUIVALENCE (W(325),GUMODEL), (W(326),GUFORM), (W(327),GUID)	CWW3	33
C		CWW3	34
C	UPPER SURFACE TOPOGRAPHY 350-374	CWW3	35
	EQUIVALENCE (W(350),SMODEL), (W(351),SFORM), (W(352),SID)	CWW3	36
C	PLOT ENHANCEMENTS CONTROL PARAMETERS	CWW3	37
C		CWW3	38
	EQUIVALENCE (W(490),XFQMDL), (W(491),YFQMDL)	CWW3	39
C	ABSORPTION 500-524	CWW3	40
	EQUIVALENCE (W(500),AMODEL), (W(501),AFORM), (W(502),AID)	CWW3	41
C		CWW3	42
C	DELTA ABSORPTION 525-549	CWW3	43
	EQUIVALENCE (W(525),DAMODEL), (W(526),DAFORM), (W(527),DAID)	CWW3	44
C		CWW3	45
C	PRESSURE 550-574	CWW3	46

C	EQUIVALENCE (W(550),PMODEL), (W(551),PFORM), (W(552),PID)	CWW3 47
C	DELTA PRESSURE 575-599	CWW3 48
C	EQUIVALENCE (W(575),DPMODEL), (W(576),DPFORM), (W(577),DPID)	CWW3 49
C	COMMON DECK "B2" INSERTED HERE	CWW3 50
C	INTEGER DUMX,DUNTBL,DUITBL,DUFRMTB,IDSU(10)	CWW3 51
	COMMON/B2/DUMX,DUNTBL(10),DUITBL(10),DUFRMTB(10),DUGP(10)	CB2 2
	EQUIVALENCE (DUGP,IDSU)	CB2 4
	DATA RECOGDU/0.0/	CB2 5
	DATA DUMX/1/	CB2 6
	DATA DUNTBL/1,11,8*0/	NPWIND13
	DATA DUITBL/1,9*0/	NINDBL 2
	DATA DUFRMTB/1,9*0/	NINDBL 3
C	ENTRY IPWINDR	NINDBL 4
	IF(RECOGDU .NE. DUMODEL)	NINDBL 5
	1 CALL RERROR('DWINDR ', 'WRNG MODEL', RECOGDU)	NPWIND16
	MODU(3)=6HNPWIND	NPWIND17
	MODU(4)=DUID	NPWIND18
	RETURN	NPWIND19
C	ENTRY PWINDR	NPWIND20
	RETURN	NPWIND21
	END	NPWIND22
		NPWIND23
		NPWIND24
		NPWIND25
		NPWIND26

C	SUBROUTINE GAMRTDM	GAMRTDM8
C	SOUND SPEED MODEL, C**2=GAMMA*R*T/M	GAMRTDM9
C	COMMON DECK "CC" INSERTED HERE	CCC 2
	REAL MODC	CCC 4
C	COMMON/CC/MODC(4), CS, PCST, PCSR, PCSTH, PCSPH	CCC 5
C	COMMON DECK "TT" INSERTED HERE	CTT 2
	REAL MODT	CTT 4
C	COMMON/TT/MODT(4), T, PTT, PTR, PTH, PTPH	CTT 5
C	COMMON DECK "MM" INSERTED HERE	CMM 2
	REAL M, MODM	CMM 4
C	COMMON/MM/MODM(4), M, PMT, PMR, PMTH, PMPH	CMM 5
C	COMMON DECK "CONST" INSERTED HERE	CCONST 2
	COMMON/PCONST/CREG, RGAS, GAMMA	CCONST 4
C	COMMON/MCONST/PI, PIT2, PID2, DEGS, RAD, ALN10	CCONST 5
C	COMMON DECK "WW" INSERTED HERE	CWW 2
	PARAMETER (NWARSZ=1000)	CWW1 3
	COMMON/WW/ID(10), MAXW, W(NWARSZ)	CWW1 4
	REAL MAXSTP, MAXERR, INTYP, LLAT, LLON	CWW2 2
	EQUIVALENCE (EARTH, W(1)), (RAY, W(2)), (XMTRH, W(3)), (TLAT, W(4)),	CWW2 3
	1 (TLON, W(5)), (OW, W(6)), (FBEG, W(7)), (FEND, W(8)), (FSTEP, W(9)),	CWW2 4
	2 (AZ1, W(10)), (AZBEG, W(11)), (AZEND, W(12)), (AZSTEP, W(13)),	CWW2 5
	3 (BETA, W(14)), (ELBEG, W(15)), (ELEND, W(16)), (ELSTEP, W(17)),	CWW2 6
	8 (RCVRH, W(20)),	CWW2 7
	4 (ONLY, W(21)), (HOP, W(22)), (MAXSTP, W(23)), (PLAT, W(24)), (PLON, W(25))	CWW2 8
	5, (HMAX, W(26)), (RAYFNC, W(29)), (EXTINC, W(33)),	CWW2 9

	6 (HMIN,W(27)),(RGMAX,W(28)),	CWW2	10
	8 (INTYP,W(41)),(MAXERR,W(42)),(ERATIO,W(43)),	CWW2	11
	6 (STEP1,W(44)),(STPMAX,W(45)),(STPMIN,W(46)),(FACTR,W(47)),	CWW2	12
	7 (SKIP,W(71)),(RAYSET,W(72)),(PRTSRP,W(74)),(HITLET,W(75))	CWW2	13
	9 ,(BINRAY,W(76)),(PAGLN,W(77)),(PLT,W(81)),(PFACTR,W(82)),	CWW2	14
	1 (LLAT,W(83)),(LLON,W(84)),(RLAT,W(85)),(RLON,W(86))	CWW2	15
	2,(TIC,W(87)),(HB,W(88)),(HT,W(89)),(TICV,W(96))	CWW2	16
	REAL MMODEL,MFORM,MID	CWW3	2
C		CWW3	3
C	WIND 100-124	CWW3	4
	EQUIVALENCE (W(100),UMODEL),(W(101),UFORM),(W(102),UID)	CWW3	5
C		CWW3	6
C	DELTA WIND 125-149	CWW3	7
	EQUIVALENCE (W(125),DUMODEL),(W(126),DUFORM),(W(127),DUID)	CWW3	8
C		CWW3	9
C	SOUND SPEED 150-174	CWW3	10
	EQUIVALENCE (W(150),CMODEL),(W(151),CFORM),(W(152),CID)	CWW3	11
	EQUIVALENCE (W(153),REFC)	CWW3	12
C		CWW3	13
C	DELTA SOUND SPEED 175-199	CWW3	14
	EQUIVALENCE (W(175),DCMODEL),(W(176),DCFORM),(W(177),DCID)	CWW3	15
C		CWW3	16
C	TEMPERATURE 200-224	CWW3	17
	EQUIVALENCE (W(200),TMODEL),(W(201),TFORM),(W(202),TID)	CWW3	18
C		CWW3	19
C	DELTA TEMPERATURE 225-249	CWW3	20
	EQUIVALENCE (W(225),DTMODEL),(W(226),DTFORM),(W(227),DTID)	CWW3	21
C		CWW3	22
C	MOLECULAR 250-274	CWW3	23
	EQUIVALENCE (W(250),MMODEL),(W(251),MFORM),(W(252),MID)	CWW3	24
C		CWW3	25
C	RECEIVER HEIGHT 275-299	CWW3	26
	EQUIVALENCE (W(275),RMODEL),(W(276),RFORM),(W(277),RID)	CWW3	27
C		CWW3	28
C	TOPOGRAPHY 300-324	CWW3	29
	EQUIVALENCE (W(300),GMODEL),(W(301),GFORM),(W(302),GID)	CWW3	30
C		CWW3	31
C	DELTA TOPOGRAPHY 325-349	CWW3	32
	EQUIVALENCE (W(325),GUMODEL),(W(326),GUFORM),(W(327),GUID)	CWW3	33
C		CWW3	34
C	UPPER SURFACE TOPOGRAPHY 350-374	CWW3	35
	EQUIVALENCE (W(350),SMODEL),(W(351),SFORM),(W(352),SID)	CWW3	36
C		CWW3	37
C	PLOT ENHANCEMENTS CONTROL PARAMETERS	CWW3	38
	EQUIVALENCE (W(490),XFQMDL),(W(491),YFQMDL)	CWW3	39
C		CWW3	40
C	ABSORPTION 500-524	CWW3	41
	EQUIVALENCE (W(500),AMODEL),(W(501),AFORM),(W(502),AID)	CWW3	42
C		CWW3	43
C	DELTA ABSORPTION 525-549	CWW3	44
	EQUIVALENCE (W(525),DAMODEL),(W(526),DAFORM),(W(527),DAID)	CWW3	45
C		CWW3	46
C	PRESSURE 550-574	CWW3	47
	EQUIVALENCE (W(550),PMODEL),(W(551),PFORM),(W(552),PID)	CWW3	48
C		CWW3	49
C	DELTA PRESSURE 575-599	CWW3	49

	EQUIVALENCE (W(575),DPMODEL), (W(576),DPFORM), (W(577),DPID)	CWW3 50
C		CWW3 51
C	COMMON DECK "B3" INSERTED HERE	GAMRTD15
C	INTEGER CMX,CNTBL,CITBL,CFRMTBL,IDSC(10)	CB3 2
	COMMON/B3/CMX,CNTBL(10),CITBL(10),CFRMTBL(10),CGP(512)	CB3 4
	EQUIVALENCE (CGP,IDSC),(ANC,CGP(11))	CB3 5
	DATA CMX/1/	CB3 6
	DATA CNTBL/1,11,8*0/	GRTDMBL2
	DATA CITBL/1,9*0/	GRTDMBL3
	DATA CFRMTBL/1,9*0/	GRTDMBL4
	DATA RECOGC/1.0/	GRTDMBL5
C		GAMRTD19
	ENTRY ISPEED	GAMRTD20
C		GAMRTD21
	IF(REFC.GT.0.0) CREF=REFC	GAMRTD22
	IF(RECOGC.NE.CMODEL)	GAMRTD23
1	CALL RERROR('SPEED ','WRNG MODEL',RECOGC)	GAMRTD24
	MODC(1)=7HGAMRTDM	GAMRTD25
	MODC(2)=CID	GAMRTD26
	CALL ITEMP	GAMRTD27
	CALL IMOLWT	GAMRTD28
	CALL IPSPEED	GAMRTD29
C		GAMRTD30
	RETURN	GAMRTD31
C		GAMRTD32
	ENTRY SPEED	GAMRTD33
	CALL TEMP	GAMRTD34
	CALL MOLWT	GAMRTD35
	CS=GAMMA*RGAS*T/M	GAMRTD36
	PCST=CS*(PTT/T - PMT/M)	GAMRTD37
	PCSR=CS*(PTR/T - PMR/M)	GAMRTD38
	PCSTH=CS*(PTTH/T - PMTH/M)	GAMRTD39
	PCSPH=CS*(PTPH/T - PMPH/M)	GAMRTD40
C		GAMRTD41
C		GAMRTD42
	CALL PSPEED	GAMRTD43
	RETURN	GAMRTD44
	END	GAMRTD45
		GAMRTD46
	SUBROUTINE CSTANH	CSTANH10
C	SPEED PROFILE REPRESENTED BY A SEQUENCE OF LINEAR SEGMENTS	CSTANH11
C	SMOOTHLY JOINED BY HYPERBOLIC FUNCTIONS. PARAMETERS ARE INPUT	CSTANH12
C	AS TABULAR DATA WITH SLOPES COMPUTED FROM SPEED DATA.	CSTANH13
C		CSTANH14
	REAL ALC(20),Z(19),B(19),DL(19)	CSTANH15
C	COMMON DECK "RKAM" INSERTED HERE	RKAMCOM2
	REAL KR,KTH,KPH	RKAMCOM4
	COMMON//R,TH,PH,KR,KTH,KPH,RKVAR(14),TPULSE,CSTEP,DRDT(20)	RKAMCOM5
C	COMMON DECK "B3" INSERTED HERE	CB3 2
	INTEGER CMX,CNTBL,CITBL,CFRMTBL,IDSC(10)	CB3 4

	COMMON/B3/CMX,CNTBL(10),CITBL(10),CFRMTBL(10),CGP(512)	CB3	5
	EQUIVALENCE (CGP,IDSC),(ANC,CGP(11))	CB3	6
C	COMMON DECK "CC" INSERTED HERE	CCC	2
	REAL MODC	CCC	4
	COMMON/CC/MODC(4),CS,PCST,PCSR,PCSTH,PCSPH	CCC	5
C	COMMON DECK "CONST" INSERTED HERE	CCONST	2
	COMMON/PCONST/CREF,RGAS,GAMMA	CCONST	4
	COMMON/MCONST/PI,PIT2,PID2,DEGS,RAD,ALN10	CCONST	5
C	COMMON DECK "WW" INSERTED HERE	CWW	2
	PARAMETER (NWARSZ=1000)	CWW1	3
	COMMON/WW/ID(10),MAXW,W(NWARSZ)	CWW1	4
	REAL MAXSTP,MAXERR,INTYP,LLAT,LLON	CWW2	2
	EQUIVALENCE (EARTH,W(1)),(RAY,W(2)),(XMTRH,W(3)),(TLAT,W(4)),	CWW2	3
	1 (TLON,W(5)),(OW,W(6)),(FBEG,W(7)),(FEND,W(8)),(FSTEP,W(9)),	CWW2	4
	2 (AZ1,W(10)),(AZBEG,W(11)),(AZEND,W(12)),(AZSTEP,W(13)),	CWW2	5
	3 (BETA,W(14)),(ELBEG,W(15)),(ELEND,W(16)),(ELSTEP,W(17)),	CWW2	6
	8 (RCVRH,W(20)),	CWW2	7
	4 (ONLY,W(21)),(HOP,W(22)),(MAXSTP,W(23)),(PLAT,W(24)),(PLON,W(25))	CWW2	8
	5,(HMAX,W(26)),(RAYFNC,W(29)),(EXTINC,W(33)),	CWW2	9
	6 (HMIN,W(27)),(RGMAX,W(28)),	CWW2	10
	8 (INTYP,W(41)),(MAXERR,W(42)),(ERATIO,W(43)),	CWW2	11
	6 (STEP1,W(44)),(STPMAX,W(45)),(STPMIN,W(46)),(FACTR,W(47)),	CWW2	12
	7 (SKIP,W(71)),(RAYSET,W(72)),(PRTSRP,W(74)),(HITLET,W(75))	CWW2	13
	9 ,(BINRAY,W(76)),(PAGLN,W(77)),(PLT,W(81)),(PFACTR,W(82)),	CWW2	14
	1 (LLAT,W(83)),(LLON,W(84)),(RLAT,W(85)),(RLON,W(86))	CWW2	15
	2,(TIC,W(87)),(HB,W(88)),(HT,W(89)),(TICV,W(96))	CWW2	16
	REAL MMODEL,MFORM,MID	CWW3	2
C		CWW3	3
C	WIND 100-124	CWW3	4
	EQUIVALENCE (W(100),UMODEL),(W(101),UFORM),(W(102),UID)	CWW3	5
C		CWW3	6
C	DELTA WIND 125-149	CWW3	7
	EQUIVALENCE (W(125),DUMODEL),(W(126),DUFORM),(W(127),DUID)	CWW3	8
C		CWW3	9
C	SOUND SPEED 150-174	CWW3	10
	EQUIVALENCE (W(150),CMODEL),(W(151),CFORM),(W(152),CID)	CWW3	11
	EQUIVALENCE (W(153),REFC)	CWW3	12
C		CWW3	13
C	DELTA SOUND SPEED 175-199	CWW3	14
	EQUIVALENCE (W(175),DCMODEL),(W(176),DCFORM),(W(177),DCID)	CWW3	15
C		CWW3	16
C	TEMPERATURE 200-224	CWW3	17
	EQUIVALENCE (W(200),TMODEL),(W(201),TFORM),(W(202),TID)	CWW3	18
C		CWW3	19
C	DELTA TEMPERATURE 225-249	CWW3	20
	EQUIVALENCE (W(225),DTMODEL),(W(226),DTFORM),(W(227),DTID)	CWW3	21
C		CWW3	22
C	MOLECULAR 250-274	CWW3	23
	EQUIVALENCE (W(250),MMODEL),(W(251),MFORM),(W(252),MID)	CWW3	24
C		CWW3	25
C	RECEIVER HEIGHT 275-299	CWW3	26
	EQUIVALENCE (W(275),RMODEL),(W(276),RFORM),(W(277),RID)	CWW3	27
C		CWW3	28
C	TOPOGRAPHY 300-324	CWW3	29
	EQUIVALENCE (W(300),GMODEL),(W(301),GFORM),(W(302),GID)	CWW3	30

C		CWW3	31
C	DELTA TOPOGRAPHY 325-349	CWW3	32
	EQUIVALENCE (W(325),GUMODEL), (W(326),GUFORM), (W(327),GUID)	CWW3	33
C		CWW3	34
C	UPPER SURFACE TOPOGRAPHY 350-374	CWW3	35
	EQUIVALENCE (W(350),SMODEL), (W(351),SFORM), (W(352),SID)	CWW3	36
C	PLOT ENHANCEMENTS CONTROL PARAMETERS	CWW3	37
C		CWW3	38
	EQUIVALENCE (W(490),XFQMDL), (W(491),YFQMDL)	CWW3	39
C	ABSORPTION 500-524	CWW3	40
	EQUIVALENCE (W(500),AMODEL), (W(501),AFORM), (W(502),AID)	CWW3	41
C		CWW3	42
C	DELTA ABSORPTION 525-549	CWW3	43
	EQUIVALENCE (W(525),DAMODEL), (W(526),DAFORM), (W(527),DAID)	CWW3	44
C		CWW3	45
C	PRESSURE 550-574	CWW3	46
	EQUIVALENCE (W(550),PMODEL), (W(551),PFORM), (W(552),PID)	CWW3	47
C		CWW3	48
C	DELTA PRESSURE 575-599	CWW3	49
	EQUIVALENCE (W(575),DPMODEL), (W(576),DPFORM), (W(577),DPID)	CWW3	50
C		CWW3	51
C		CSTANH21	
	EQUIVALENCE (Z0,CGP(12)), (CS0,CGP(32)), (DL0,CGP(52))	CSTANH22	
	EQUIVALENCE (Z,CGP(13)), (B,CGP(33)), (DL,CGP(53))	CSTANH23	
C		CSTANH24	
	DATA RECOGC,N/2.0,0/	CSTANH25	
	DATA PCST,PCSTH,PCSPH/3*0.0/	CANHBL 2	
	DATA ANC/0.0/	CANHBL 3	
	DATA CMX/2/	CANHBL 4	
	DATA CNTBL/1,11,72,7*0/	CANHBL 5	
	DATA CITBL/1,20,8*0/	CANHBL 6	
	DATA CFRMTBL/1,2,8*0/	CANHBL 7	
C		CSTANH28	
	ENTRY ISPEED	CSTANH29	
C		CSTANH30	
	IF(REFC.GT.0.0) CREF=REFC	CSTANH31	
C		CSTANH32	
	CALL IPSPEED	CSTANH33	
C		CSTANH34	
C	IF HAD PREVIOUS CALL BUT NOTHING THIS TIME, EXIT NOW	CSTANH35	
C	RETAINING PREVIOUS TABULAR DATA COUNT	CSTANH36	
	IF(N.GT.0 .AND. ANC.EQ.0.0) RETURN	CSTANH37	
C		CSTANH38	
	IF(RECOGC .NE. CMODEL)	CSTANH39	
1	CALL RERROR('SPEED ', 'WRNG MODEL', RECOGC)	CSTANH40	
	MODC(1)=6HCSTANH	CSTANH41	
	MODC(2)=CID	CSTANH42	
	N=ANC/3	CSTANH43	
	IF(ANC.NE.3*N.OR.N.LE.0)	CSTANH44	
1	CALL RERROR('CSTANH', 'BAD NUMBER', ANC+2.0)	CSTANH45	
	N=N-2	CSTANH46	
	ANC=0.0	CSTANH47	
C		CSTANH48	
C		CSTANH49	
C	CONVERT 'C' ARRAY INPUT(OVERLAYS 'B' ARRAY) TO 'B' ARRAY	CSTANH50	

C	ZM1=Z0	CSTANH51
	CS0=CS0*CS0	CSTANH52
	CSM1=CS0	CSTANH53
	NP1=N+1	CSTANH54
	DO 10 I=1, NP1	CSTANH55
	ZR=Z(I)	CSTANH56
	ALC(I)=ALCOSH((ZR-Z0) / DL(I))	CSTANH57
	CS=B(I)**2	CSTANH58
	B(I)=(CS-CSM1)/(ZR-ZM1)	CSTANH59
	ZM1=ZR	CSTANH60
10	CSM1=CS	CSTANH61
C		CSTANH62
	RETURN	CSTANH63
C		CSTANH64
	ENTRY SPEED	CSTANH65
C		CSTANH66
	IF(N.LE.0)	CSTANH67
1	CALL RERROR('CSTANH','BAD N VALUE',FLOAT(N))	CSTANH68
C		CSTANH69
	ZR=R-EARTH	CSTANH70
	SUM = 0.	CSTANH71
	PCSR=B(1)	CSTANH72
	DO 1 I = 1, N	CSTANH73
	SAV=0.5*(B(I+1)-B(I))	CSTANH74
	PCSR= PCSR+ SAV * (1.+TANH ((ZR-Z(I)) /DL(I)))	CSTANH75
1	SUM = SUM+DL(I) * SAV *(ALCOSH((ZR-Z(I))/DL(I))-ALC(I))	CSTANH76
	CS = CS0+SUM + 0.5*(B(1) + B(N + 1)) * (ZR-Z0)	CSTANH77
C		CSTANH78
	CALL PSPEED	CSTANH79
	RETURN	CSTANH80
	END	CSTANH81
		CSTANH82

C	SUBROUTINE NPSPEED	NPSPEED8
C	DO-NOTHING SOUND SPEED PERTURBATION MODEL	NPSPEED9
C	COMMON DECK "CC" INSERTED HERE	CCC 2
	REAL MODC	CCC 4
	COMMON/CC/MODC(4), CS, PCST, PCSR, PCSTH, PCSPH	CCC 5
C	COMMON DECK "WW" INSERTED HERE	CWW 2
	PARAMETER (NWARSZ=1000)	CWW1 3
	COMMON/WW/ID(10), MAXW, W(NWARSZ)	CWW1 4
	REAL MAXSTP, MAXERR, INTYP, LLAT, LLON	CWW2 2
	EQUIVALENCE (EARTH, W(1)), (RAY, W(2)), (XMTRH, W(3)), (TLAT, W(4)),	CWW2 3
1	(TLON, W(5)), (OW, W(6)), (FBEG, W(7)), (FEND, W(8)), (FSTEP, W(9)),	CWW2 4
2	(AZ1, W(10)), (AZBEG, W(11)), (AZEND, W(12)), (AZSTEP, W(13)),	CWW2 5
3	(BETA, W(14)), (ELBEG, W(15)), (ELEND, W(16)), (ELSTEP, W(17)),	CWW2 6
8	(RCVRH, W(20)),	CWW2 7
4	(ONLY, W(21)), (HOP, W(22)), (MAXSTP, W(23)), (PLAT, W(24)), (PLON, W(25))	CWW2 8
5,	(HMAX, W(26)), (RAYFNC, W(29)), (EXTINC, W(33)),	CWW2 9
6	(HMIN, W(27)), (RGMAX, W(28)),	CWW2 10
8	(INTYP, W(41)), (MAXERR, W(42)), (ERATIO, W(43)),	CWW2 11

	6 (STEP1,W(44)), (STPMAX,W(45)), (STPMIN,W(46)), (FACTR,W(47)),	CWW2	12
	7 (SKIP,W(71)), (RAYSET,W(72)), (PRTSRP,W(74)), (HITLET,W(75))	CWW2	13
	9 , (BINRAY,W(76)), (PAGLN,W(77)), (PLT,W(81)), (PFACTR,W(82)),	CWW2	14
	1 (LLAT,W(83)), (LLON,W(84)), (RLAT,W(85)), (RLON,W(86))	CWW2	15
	2, (TIC,W(87)), (HB,W(88)), (HT,W(89)), (TICV,W(96))	CWW2	16
	REAL MMODEL,MFORM,MID	CWW3	2
C		CWW3	3
C	WIND 100-124	CWW3	4
	EQUIVALENCE (W(100),UMODEL), (W(101),UFORM), (W(102),UID)	CWW3	5
C		CWW3	6
C	DELTA WIND 125-149	CWW3	7
	EQUIVALENCE (W(125),DUMODEL), (W(126),DUFORM), (W(127),DUID)	CWW3	8
C		CWW3	9
C	SOUND SPEED 150-174	CWW3	10
	EQUIVALENCE (W(150),CMODEL), (W(151),CFORM), (W(152),CID)	CWW3	11
	EQUIVALENCE (W(153),REFC)	CWW3	12
C		CWW3	13
C	DELTA SOUND SPEED 175-199	CWW3	14
	EQUIVALENCE (W(175),DCMODEL), (W(176),DCFORM), (W(177),DCID)	CWW3	15
C		CWW3	16
C	TEMPERATURE 200-224	CWW3	17
	EQUIVALENCE (W(200),TMODEL), (W(201),TFORM), (W(202),TID)	CWW3	18
C		CWW3	19
C	DELTA TEMPERATURE 225-249	CWW3	20
	EQUIVALENCE (W(225),DTMODEL), (W(226),DTFORM), (W(227),DTID)	CWW3	21
C		CWW3	22
C	MOLECULAR 250-274	CWW3	23
	EQUIVALENCE (W(250),MMODEL), (W(251),MFORM), (W(252),MID)	CWW3	24
C		CWW3	25
C	RECEIVER HEIGHT 275-299	CWW3	26
	EQUIVALENCE (W(275),RMODEL), (W(276),RFORM), (W(277),RID)	CWW3	27
C		CWW3	28
C	TOPOGRAPHY 300-324	CWW3	29
	EQUIVALENCE (W(300),GMODEL), (W(301),GFORM), (W(302),GID)	CWW3	30
C		CWW3	31
C	DELTA TOPOGRAPHY 325-349	CWW3	32
	EQUIVALENCE (W(325),GUMODEL), (W(326),GUFORM), (W(327),GUID)	CWW3	33
C		CWW3	34
C	UPPER SURFACE TOPOGRAPHY 350-374	CWW3	35
	EQUIVALENCE (W(350),SMODEL), (W(351),SFORM), (W(352),SID)	CWW3	36
C	PLOT ENHANCEMENTS CONTROL PARAMETERS	CWW3	37
C		CWW3	38
	EQUIVALENCE (W(490),XFQMDL), (W(491),YFQMDL)	CWW3	39
C	ABSORPTION 500-524	CWW3	40
	EQUIVALENCE (W(500),AMODEL), (W(501),AFORM), (W(502),AID)	CWW3	41
C		CWW3	42
C	DELTA ABSORPTION 525-549	CWW3	43
	EQUIVALENCE (W(525),DAMODEL), (W(526),DAFORM), (W(527),DAID)	CWW3	44
C		CWW3	45
C	PRESSURE 550-574	CWW3	46
	EQUIVALENCE (W(550),PMODEL), (W(551),PFORM), (W(552),PID)	CWW3	47
C		CWW3	48
C	DELTA PRESSURE 575-599	CWW3	49
	EQUIVALENCE (W(575),DPMODEL), (W(576),DPFORM), (W(577),DPID)	CWW3	50
C		CWW3	51

C		NPSPEE12
C	COMMON DECK "B2" INSERTED HERE	CB2 2
	INTEGER DUMX,DUNTBL,DUITBL,DUFRMTB,IDSDU(10)	CB2 4
	COMMON/B2/DUMX,DUNTBL(10),DUITBL(10),DUFRMTB(10),DUGP(10)	CB2 5
	EQUIVALENCE (DUGP,IDSDU)	CB2 6
C	DATA DUMX/1/	NPSPEE14
	DATA DUNTBL/1,11,8*0/	NPEEDBL2
	DATA DUITBL/1,9*0/	NPEEDBL3
	DATA DUFRMTB/1,9*0/	NPEEDBL4
C		NPEEDBL5
	DATA RECOGDC/0.0/	NPSPEE17
C		NPSPEE18
	ENTRY IPSPEED	NPSPEE19
	IF(RECOGDC .NE. DCMODEL)	NPSPEE20
1	CALL RERROR('DSPEED ','WRNG MODEL',RECOGDC)	NPSPEE21
	MODC(3)=7HNPSPEED	NPSPEE22
	MODC(4)=DCID	NPSPEE23
	RETURN	NPSPEE24
C		NPSPEE25
	ENTRY PSPEED	NPSPEE26
	RETURN	NPSPEE27
	END	NPSPEE28
		NPSPEE29
	SUBROUTINE CBLOB2	CBLOB2 8
C	SOUND SPEED PERTURBATION MODEL	CBLOB2 9
C	MULTIPLICATIVE PERTURBATION WITH EXPONENTIALLY DECAYING	CBLOB210
C	EFFECT IN ALL THREE DIRECTIONS. GIVE LATITUDE	CBLOB211
C	INSTEAD OF CO-LATITUDE.	CBLOB212
C	COMMON DECK "CONST" INSERTED HERE	CCONST 2
	COMMON/PCONST/CREG,RGAS,GAMMA	CCONST 4
	COMMON/MCONST/PI,PIT2,PID2,DEGS,RAD,ALN10	CCONST 5
C	COMMON DECK "RKAM" INSERTED HERE	RKAMCOM2
	REAL KR,KTH,KPH	RKAMCOM4
	COMMON//R,TH,PH,KR,KTH,KPH,RKVAR(14),TPULSE,CSTEP,DRDT(20)	RKAMCOM5
C	COMMON DECK "B4" INSERTED HERE	CB4 2
	INTEGER DCMX,DCNTBL,DCITBL,DCFRMTB,IDSDC(10)	CB4 4
	COMMON/B4/DCMX,DCNTBL(10),DCITBL(10),DCFRMTB(10),DCGP(10)	CB4 5
	EQUIVALENCE (DCGP,IDSDC)	CB4 6
C		CBLOB216
C	COMMON DECK "CC" INSERTED HERE	CCC 2
	REAL MODC	CCC 4
	COMMON/CC/MODC(4),CS,PCST,PCSR,PCSTH,PCSPH	CCC 5
C	COMMON DECK "WW" INSERTED HERE	CWW 2
	PARAMETER (NWARSZ=1000)	CWW1 3
	COMMON/WW/ID(10),MAXW,W(NWARSZ)	CWW1 4
	REAL MAXSTP,MAXERR,INTYP,LLAT,LLON	CWW2 2
	EQUIVALENCE (EARTH,W(1)),(RAY,W(2)),(XMTRH,W(3)),(TLAT,W(4)),	CWW2 3
1	(TLON,W(5)),(OW,W(6)),(FBEG,W(7)),(FEND,W(8)),(FSTEP,W(9)),	CWW2 4
2	(AZ1,W(10)),(AZBEG,W(11)),(AZEND,W(12)),(AZSTEP,W(13)),	CWW2 5
3	(BETA,W(14)),(ELBEG,W(15)),(ELEND,W(16)),(ELSTEP,W(17)),	CWW2 6

	8 (RCVRH,W(20)),	CWW2	7
	4 (ONLY,W(21)), (HOP,W(22)), (MAXSTP,W(23)), (PLAT,W(24)), (PLON,W(25))	CWW2	8
	5, (HMAX,W(26)), (RAYFNC,W(29)), (EXTINC,W(33)),	CWW2	9
	6 (HMIN,W(27)), (RGMAX,W(28)),	CWW2	10
	8 (INTYP,W(41)), (MAXERR,W(42)), (ERATIO,W(43)),	CWW2	11
	6 (STEP1,W(44)), (STPMAX,W(45)), (STPMIN,W(46)), (FACTR,W(47)),	CWW2	12
	7 (SKIP,W(71)), (RAYSET,W(72)), (PRTSRP,W(74)), (HITLET,W(75))	CWW2	13
	9, (BINRAY,W(76)), (PAGLN,W(77)), (PLT,W(81)), (PFACTR,W(82)),	CWW2	14
	1 (LLAT,W(83)), (LLON,W(84)), (RLAT,W(85)), (RLON,W(86))	CWW2	15
	2, (TIC,W(87)), (HB,W(88)), (HT,W(89)), (TICV,W(96))	CWW2	16
	REAL MMODEL,MFORM,MID	CWW3	2
C		CWW3	3
C	WIND 100-124	CWW3	4
	EQUIVALENCE (W(100),UMODEL), (W(101),UFORM), (W(102),UID)	CWW3	5
C		CWW3	6
C	DELTA WIND 125-149	CWW3	7
	EQUIVALENCE (W(125),DUMODEL), (W(126),DUFORM), (W(127),DUID)	CWW3	8
C		CWW3	9
C	SOUND SPEED 150-174	CWW3	10
	EQUIVALENCE (W(150),CMODEL), (W(151),CFORM), (W(152),CID)	CWW3	11
	EQUIVALENCE (W(153),REFC)	CWW3	12
C		CWW3	13
C	DELTA SOUND SPEED 175-199	CWW3	14
	EQUIVALENCE (W(175),DCMODEL), (W(176),DCFORM), (W(177),DCID)	CWW3	15
C		CWW3	16
C	TEMPERATURE 200-224	CWW3	17
	EQUIVALENCE (W(200),TMODEL), (W(201),TFORM), (W(202),TID)	CWW3	18
C		CWW3	19
C	DELTA TEMPERATURE 225-249	CWW3	20
	EQUIVALENCE (W(225),DTMODEL), (W(226),DTFORM), (W(227),DTID)	CWW3	21
C		CWW3	22
C	MOLECULAR 250-274	CWW3	23
	EQUIVALENCE (W(250),MMODEL), (W(251),MFORM), (W(252),MID)	CWW3	24
C		CWW3	25
C	RECEIVER HEIGHT 275-299	CWW3	26
	EQUIVALENCE (W(275),RMODEL), (W(276),RFORM), (W(277),RID)	CWW3	27
C		CWW3	28
C	TOPOGRAPHY 300-324	CWW3	29
	EQUIVALENCE (W(300),GMODEL), (W(301),GFORM), (W(302),GID)	CWW3	30
C		CWW3	31
C	DELTA TOPOGRAPHY 325-349	CWW3	32
	EQUIVALENCE (W(325),GUMODEL), (W(326),GUFORM), (W(327),GUID)	CWW3	33
C		CWW3	34
C	UPPER SURFACE TOPOGRAPHY 350-374	CWW3	35
	EQUIVALENCE (W(350),SMODEL), (W(351),SFORM), (W(352),SID)	CWW3	36
C		CWW3	37
C	PLOT ENHANCEMENTS CONTROL PARAMETERS	CWW3	38
	EQUIVALENCE (W(490),XFQMDL), (W(491),YFQMDL)	CWW3	39
C		CWW3	40
C	ABSORPTION 500-524	CWW3	41
	EQUIVALENCE (W(500),AMODEL), (W(501),AFORM), (W(502),AID)	CWW3	42
C		CWW3	43
C	DELTA ABSORPTION 525-549	CWW3	44
	EQUIVALENCE (W(525),DAMODEL), (W(526),DAFORM), (W(527),DAID)	CWW3	45
C		CWW3	46
C	PRESSURE 550-574	CWW3	46

C	EQUIVALENCE (W(550),PMODEL), (W(551),PFORM), (W(552),PID)	CWW3 47
C	DELTA PRESSURE 575-599	CWW3 48
C	EQUIVALENCE (W(575),DPMODEL), (W(576),DPFORM), (W(577),DPID)	CWW3 49
C		CWW3 50
C		CWW3 51
	EQUIVALENCE (C0,W(178)), (Z0,W(179)), (CBTH0,W(180))	CBLOB219
	EQUIVALENCE (PH0,W(181)), (WZ,W(182)), (WTH,W(183)), (WPH,W(184))	CBLOB220
	DATA RECOGDC/2.0/	CBLOB221
	DATA DCMX/1/	CBLOB222
	DATA DCNTBL/1,11,8*0/	COB2BL 2
	DATA DCITBL/1,9*0/	COB2BL 3
	DATA DCFRMTB/1,9*0/	COB2BL 4
C	ENTRY IPSPEED	COB2BL 5
	IF(RECOGDC .NE. DCMODEL)	CBLOB225
C	1 CALL RERROR('DSPEED ', 'WRNG MODEL', RECOGDC)	CBLOB226
		CBLOB227
		CBLOB228
	MODC(3)=6HCBLOB2	CBLOB229
	MODC(4)=DCID	CBLOB230
C		CBLOB231
	FWZ=0.0	CBLOB232
	FWTH=0.0	CBLOB233
	FWPH=0.0	CBLOB234
	TH0= PID2-CBTH0	CBLOB235
	IF(WZ.NE.0.0) FWZ=2.0/WZ/WZ	CBLOB236
	IF(WTH.NE.0.0) FWTH=2.0/WTH/WTH	CBLOB237
	IF(WPH.NE.0.0) FWPH=2.0/WPH/WPH	CBLOB238
	RETURN	CBLOB239
C		CBLOB240
	ENTRY PSPEED	CBLOB241
C		CBLOB242
	IF(C0.EQ.0.0) RETURN	CBLOB243
C		CBLOB244
	DZ=R-EARTH-R-Z0	CBLOB245
	DTH=TH-TH0	CBLOB246
	DPH=PH-PH0	CBLOB247
	DEXPO=0.0	CBLOB248
	EXPO=-0.5*(DZ*DZ*FWZ+DTH*DTH*FWTH+DPH*DPH*FWPH)	CBLOB249
	IF(EXPO .GT. -200.0) DEXPO=C0*EXP(EXPO)	CBLOB250
	DEL=1.0+DEXPO	CBLOB251
C		CBLOB252
	PCSR=PCSR*DEL-CS*DEXPO*FWZ*DZ	CBLOB253
	PCSTH=PCSTH*DEL-CS*DEXPO*FWTH*DTH	CBLOB254
	PCSPH=PCSPH*DEL-CS*DEXPO*FWPH*DPH	CBLOB255
	CS=CS*DEL	CBLOB256
	RETURN	CBLOB257
	END	CBLOB258
		CBLOB259
C	SUBROUTINE TLINEAR	TLINEAR8
	LINEAR TEMPERATURE PROFILE	TLINEAR9

C	COMMON DECK "RKAM" INSERTED HERE	RKAMCOM2
	REAL KR, KTH, KPH	RKAMCOM4
	COMMON//R, TH, PH, KR, KTH, KPH, RKVARS(14), TPULSE, CSTEP, DRDT(20)	RKAMCOM5
C	COMMON DECK "MM" INSERTED HERE	CMM
	REAL M, MODM	CMM
	COMMON/MM/MODM(4), M, PMT, PMR, PMTH, PMPH	CMM
C	COMMON DECK "TT" INSERTED HERE	CTT
	REAL MODT	CTT
	COMMON/TT/MODT(4), T, PTT, PTR, PTH, PTPH	CTT
C	COMMON DECK "WW" INSERTED HERE	CWW
	PARAMETER (NWARSZ=1000)	CWW1
	COMMON/WW/ID(10), MAXW, W(NWARSZ)	CWW1
	REAL MAXSTP, MAXERR, INTYP, LLAT, LLON	CWW2
	EQUIVALENCE (EARTH, W(1)), (RAY, W(2)), (XMTRH, W(3)), (TLAT, W(4)),	CWW2
	1 (TLON, W(5)), (OW, W(6)), (FBEG, W(7)), (FEND, W(8)), (FSTEP, W(9)),	CWW2
	2 (AZ1, W(10)), (AZBEG, W(11)), (AZEND, W(12)), (AZSTEP, W(13)),	CWW2
	3 (BETA, W(14)), (ELBEG, W(15)), (ELEND, W(16)), (ELSTEP, W(17)),	CWW2
	8 (RCVRH, W(20)),	CWW2
	4 (ONLY, W(21)), (HOP, W(22)), (MAXSTP, W(23)), (PLAT, W(24)), (PLON, W(25))	CWW2
	5, (HMAX, W(26)), (RAYFNC, W(29)), (EXTINC, W(33)),	CWW2
	6 (HMIN, W(27)), (RGMAX, W(28)),	CWW2
	8 (INTYP, W(41)), (MAXERR, W(42)), (ERATIO, W(43)),	CWW2
	6 (STEP1, W(44)), (STPMAX, W(45)), (STPMIN, W(46)), (FACTR, W(47)),	CWW2
	7 (SKIP, W(71)), (RAYSET, W(72)), (PRTSRP, W(74)), (HITLET, W(75))	CWW2
	9, (BINRAY, W(76)), (PAGLN, W(77)), (PLT, W(81)), (PFACTR, W(82)),	CWW2
	1 (LLAT, W(83)), (LLON, W(84)), (RLAT, W(85)), (RLON, W(86))	CWW2
	2, (TIC, W(87)), (HB, W(88)), (HT, W(89)), (TICV, W(96))	CWW2
	REAL MMODEL, MFORM, MID	CWW3
C		CWW3
C	WIND 100-124	CWW3
	EQUIVALENCE (W(100), UMODEL), (W(101), UFORM), (W(102), UID)	CWW3
C		CWW3
C	DELTA WIND 125-149	CWW3
	EQUIVALENCE (W(125), DUMODEL), (W(126), DUFORM), (W(127), DUID)	CWW3
C		CWW3
C	SOUND SPEED 150-174	CWW3
	EQUIVALENCE (W(150), CMODEL), (W(151), CFORM), (W(152), CID)	CWW3
	EQUIVALENCE (W(153), REFC)	CWW3
C		CWW3
C	DELTA SOUND SPEED 175-199	CWW3
	EQUIVALENCE (W(175), DCMODEL), (W(176), DCFORM), (W(177), DCID)	CWW3
C		CWW3
C	TEMPERATURE 200-224	CWW3
	EQUIVALENCE (W(200), TMODEL), (W(201), TFORM), (W(202), TID)	CWW3
C		CWW3
C	DELTA TEMPERATURE 225-249	CWW3
	EQUIVALENCE (W(225), DTMODEL), (W(226), DTFORM), (W(227), DTID)	CWW3
C		CWW3
C	MOLECULAR 250-274	CWW3
	EQUIVALENCE (W(250), MMODEL), (W(251), MFORM), (W(252), MID)	CWW3
C		CWW3
C	RECEIVER HEIGHT 275-299	CWW3
	EQUIVALENCE (W(275), RMODEL), (W(276), RFORM), (W(277), RID)	CWW3
C		CWW3
C	TOPOGRAPHY 300-324	CWW3

C	EQUIVALENCE (W(300),GMODEL), (W(301),GFORM), (W(302),GID)	CWW3 30
C	DELTA TOPOGRAPHY 325-349	CWW3 31
C	EQUIVALENCE (W(325),GUMODEL), (W(326),GUFORM), (W(327),GUID)	CWW3 32
C	UPPER SURFACE TOPOGRAPHY 350-374	CWW3 33
C	EQUIVALENCE (W(350),SMODEL), (W(351),SFORM), (W(352),SID)	CWW3 34
C	PLOT ENHANCEMENTS CONTROL PARAMETERS	CWW3 35
C	EQUIVALENCE (W(490),XFQMDL), (W(491),YFQMDL)	CWW3 36
C	ABSORPTION 500-524	CWW3 37
C	EQUIVALENCE (W(500),AMODEL), (W(501),AFORM), (W(502),AID)	CWW3 38
C	DELTA ABSORPTION 525-549	CWW3 39
C	EQUIVALENCE (W(525),DAMODEL), (W(526),DAFORM), (W(527),DAID)	CWW3 40
C	PRESSURE 550-574	CWW3 41
C	EQUIVALENCE (W(550),PMODEL), (W(551),PFORM), (W(552),PID)	CWW3 42
C	DELTA PRESSURE 575-599	CWW3 43
C	EQUIVALENCE (W(575),DPMODEL), (W(576),DPFORM), (W(577),DPID)	CWW3 44
C	EQUIVALENCE (TGND, W(203)), (A, W(204))	CWW3 45
C	COMMON DECK "B5" INSERTED HERE	CWW3 46
	INTEGER TMX,TNTBL,TITBL,TFRMTBL,IDST(10)	CWW3 47
	COMMON/B5/TMX,TNTBL(10),TITBL(10),TFRMTBL(10),TGP(262)	CWW3 48
	EQUIVALENCE (TGP,IDST), (ANT,TGP(11))	CWW3 49
	DATA RECOGT/1.0/	CWW3 50
	DATA ANT/0.0/	CWW3 51
	DATA TMX/1/	TLINEA14
	DATA TNTBL/1,11,8*0/	CB5 2
	DATA TITBL/1,9*0/	CB5 4
	DATA TFRMTBL/1,9*0/	CB5 5
	ENTRY ITEMP	CB5 6
C	IF(RECOGT .NE. TMODEL)	TLINEA16
C	1 CALL RERROR('TEMP ', 'WRNG MODEL', RECOGT)	TNEARBL2
	MODT(1)=7HTLINEAR	TNEARBL3
	MODT(2)=TID	TNEARBL4
	CALL IPTEMP	TNEARBL5
C	RETURN	TNEARBL6
C	ENTRY TEMP	TLINEA19
	H = R - EARTH	TLINEA20
	T = TGND + A * H	TLINEA21
	CALL CLEAR(PTT,4)	TLINEA22
	PTR=A	TLINEA23
C	CALL PTEMP	TLINEA24
	RETURN	TLINEA25
	END	TLINEA26
		TLINEA27
		TLINEA28
		TLINEA29
		TLINEA30
		TLINEA31
		TLINEA32
		TLINEA33
		TLINEA34
		TLINEA35
		TLINEA36
		TLINEA37
		TLINEA38

	SUBROUTINE TTANH5	TTANH5 9
C	TEMPERATURE PROFILE REPRESENTED BY A SEQUENCE OF LINEAR SEGMENTS	TTANH510
C	SMOOTHLY JOINED BY HYPERBOLIC FUNCTIONS. PARAMETERS ARE INPUT	TTANH511
C	AS TABULAR DATA WITH SLOPES COMPUTED FROM TEMPERATURE DATA.	TTANH512
C	REFERENCE TEMPERATURE TO IS READ FROM TABULAR DATA.	TTANH513
	DIMENSION C(20), TM(19), Z(19), DL(19)	TTANH514
C	COMMON DECK "RKAM" INSERTED HERE	RKAMCOM2
	REAL KR, KTH, KPH	RKAMCOM4
	COMMON//R, TH, PH, KR, KTH, KPH, RKVARS(14), TPULSE, CSTEP, DRDT(20)	RKAMCOM5
C	COMMON DECK "TT" INSERTED HERE	CTT 2
	REAL MODT	CTT 4
	COMMON/TT/MODT(4), T, PTT, PTR, PTH, PTPH	CTT 5
C	COMMON DECK "WW" INSERTED HERE	CWW 2
	PARAMETER (NWARSZ=1000)	CWW1 3
	COMMON/WW/ID(10), MAXW, W(NWARSZ)	CWW1 4
	REAL MAXSTP, MAXERR, INTYP, LLAT, LLON	CWW2 2
	EQUIVALENCE (EARTH, W(1)), (RAY, W(2)), (XMTRH, W(3)), (TLAT, W(4)),	CWW2 3
	1 (TLON, W(5)), (OW, W(6)), (FBEG, W(7)), (FEND, W(8)), (FSTEP, W(9)),	CWW2 4
	2 (AZ1, W(10)), (AZBEG, W(11)), (AZEND, W(12)), (AZSTEP, W(13)),	CWW2 5
	3 (BETA, W(14)), (ELBEG, W(15)), (ELEND, W(16)), (ELSTEP, W(17)),	CWW2 6
	8 (RCVRH, W(20)),	CWW2 7
	4 (ONLY, W(21)), (HOP, W(22)), (MAXSTP, W(23)), (PLAT, W(24)), (PLON, W(25))	CWW2 8
	5, (HMAX, W(26)), (RAYFNC, W(29)), (EXTINC, W(33)),	CWW2 9
	6 (HMIN, W(27)), (RGMAX, W(28)),	CWW2 10
	8 (INTYP, W(41)), (MAXERR, W(42)), (ERATIO, W(43)),	CWW2 11
	6 (STEP1, W(44)), (STPMAX, W(45)), (STPMIN, W(46)), (FACTR, W(47)),	CWW2 12
	7 (SKIP, W(71)), (RAYSET, W(72)), (PRTSRP, W(74)), (HITLET, W(75))	CWW2 13
	9, (BINRAY, W(76)), (PAGLN, W(77)), (PLT, W(81)), (PFACTR, W(82)),	CWW2 14
	1 (LLAT, W(83)), (LLON, W(84)), (RLAT, W(85)), (RLON, W(86))	CWW2 15
	2, (TIC, W(87)), (HB, W(88)), (HT, W(89)), (TICV, W(96))	CWW2 16
	REAL MMODEL, MFORM, MID	CWW3 2
C		CWW3 3
C	WIND 100-124	CWW3 4
	EQUIVALENCE (W(100), UMODEL), (W(101), UFORM), (W(102), UID)	CWW3 5
C		CWW3 6
C	DELTA WIND 125-149	CWW3 7
	EQUIVALENCE (W(125), DUMODEL), (W(126), DUFORM), (W(127), DUID)	CWW3 8
C		CWW3 9
C	SOUND SPEED 150-174	CWW3 10
	EQUIVALENCE (W(150), CMODEL), (W(151), CFORM), (W(152), CID)	CWW3 11
	EQUIVALENCE (W(153), REFC)	CWW3 12
C		CWW3 13
C	DELTA SOUND SPEED 175-199	CWW3 14
	EQUIVALENCE (W(175), DCMODEL), (W(176), DCFORM), (W(177), DCID)	CWW3 15
C		CWW3 16
C	TEMPERATURE 200-224	CWW3 17
	EQUIVALENCE (W(200), TMODEL), (W(201), TFORM), (W(202), TID)	CWW3 18
C		CWW3 19
C	DELTA TEMPERATURE 225-249	CWW3 20
	EQUIVALENCE (W(225), DTMODEL), (W(226), DTFORM), (W(227), DTID)	CWW3 21
C		CWW3 22
C	MOLECULAR 250-274	CWW3 23

C	EQUIVALENCE (W(250),MMODEL), (W(251),MFORM), (W(252),MID)	CWW3	24
C	RECEIVER HEIGHT 275-299	CWW3	25
C	EQUIVALENCE (W(275),RMODEL), (W(276),RFORM), (W(277),RID)	CWW3	26
C	TOPOGRAPHY 300-324	CWW3	27
C	EQUIVALENCE (W(300),GMODEL), (W(301),GFORM), (W(302),GID)	CWW3	28
C	DELTA TOPOGRAPHY 325-349	CWW3	29
C	EQUIVALENCE (W(325),GUMODEL), (W(326),GUFORM), (W(327),GUID)	CWW3	30
C	UPPER SURFACE TOPOGRAPHY 350-374	CWW3	31
C	EQUIVALENCE (W(350),SMODEL), (W(351),SFORM), (W(352),SID)	CWW3	32
C	PLOT ENHANCEMENTS CONTROL PARAMETERS	CWW3	33
C	EQUIVALENCE (W(490),XFQMDL), (W(491),YFQMDL)	CWW3	34
C	ABSORPTION 500-524	CWW3	35
C	EQUIVALENCE (W(500),AMODEL), (W(501),AFORM), (W(502),AID)	CWW3	36
C	DELTA ABSORPTION 525-549	CWW3	37
C	EQUIVALENCE (W(525),DAMODEL), (W(526),DAFORM), (W(527),DAID)	CWW3	38
C	PRESSURE 550-574	CWW3	39
C	EQUIVALENCE (W(550),PMODEL), (W(551),PFORM), (W(552),PID)	CWW3	40
C	DELTA PRESSURE 575-599	CWW3	41
C	EQUIVALENCE (W(575),DPMODEL), (W(576),DPFORM), (W(577),DPID)	CWW3	42
C	COMMON DECK "B5" INSERTED HERE	CWW3	43
C	INTEGER TMX,TNTBL,TITBL,TFRMTBL,IDST(10)	CB5	44
C	COMMON/B5/TMX,TNTBL(10),TITBL(10),TFRMTBL(10),TGP(262)	CB5	45
C	EQUIVALENCE (TGP,IDST), (ANT,TGP(11))	CB5	46
C	EQUIVALENCE (Z0,TGP(12)), (TM,TGP(33))	TTANH519	47
C	EQUIVALENCE (Z,TGP(13)), (C,TGP(32)), (DL,TGP(53))	TTANH520	48
C	DATA RECOGT,N/7.0,0/	TTANH521	49
C	DATA ANT/0.0/	TTANH522	50
C	DATA TMX/2/	TNH5BL 2	51
C	DATA TNTBL/1,11,72,7*0/	TNH5BL 3	52
C	DATA TITBL/1,20,8*0/	TNH5BL 4	53
C	DATA TFRMTBL/1,2,8*0/	TNH5BL 5	54
C	COSH (X) = (EXP (X) + 1. / (EXP (X))) / 2.	TNH5BL 6	55
C	ENTRY ITEMP	TTANH525	56
C	CALL IPTEMP	TTANH526	57
C	IF HAD PREVIOUS CALL BUT NOTHING THIS TIME, EXIT NOW	TTANH527	58
C	RETAINING PREVIOUS TABULAR DATA COUNT	TTANH528	59
C	IF(N.GT.0 .AND. ANT.EQ.0.0) RETURN	TTANH529	60
C	IF(RECOGT .NE. TMODEL)	TTANH530	61
C	1 CALL RERROR('TEMP ', 'WRNG MODEL', RECOGT)	TTANH531	62
		TTANH532	63
		TTANH533	64
		TTANH534	65
		TTANH535	66
		TTANH536	67
		TTANH537	68
		TTANH538	69



C	BETWEEN POINTS TO INSURE A CONTINUOUS TEMPERATURE GRADIENT	TTABLE10
	DIMENSION HPC(250),FN2C(250),ALPHA(250),TTBETA(250),GAMM(250),	TTABLE11
1	DELTA(250),SLOPE(250),MAT(4,5)	TTABLE12
	REAL MAT	TTABLE13
C	COMMON DECK "CONST" INSERTED HERE	CCONST 2
	COMMON/PCONST/CREF,RGAS,GAMMA	CCONST 4
	COMMON/MCONST/PI,PIT2,PID2,DEGS,RAD,ALN10	CCONST 5
C	COMMON DECK "RKAM" INSERTED HERE	RKAMCOM2
	REAL KR,KTH,KPH	RKAMCOM4
	COMMON//R,TH,PH,KR,KTH,KPH,RKVAR(14),TPULSE,CSTEP,DRDT(20)	RKAMCOM5
C	COMMON DECK "TT" INSERTED HERE	CTT 2
	REAL MODT	CTT 4
	COMMON/TT/MODT(4),T,PTT,PTR,PPTH,PTPH	CTT 5
C	COMMON DECK "WW" INSERTED HERE	CWW 2
	PARAMETER (NWARSZ=1000)	CWW1 3
	COMMON/WW/ID(10),MAXW,W(NWARSZ)	CWW1 4
	REAL MAXSTP,MAXERR,INTYP,LLAT,LLON	CWW2 2
	EQUIVALENCE (EARTH,W(1)),(RAY,W(2)),(XMTRH,W(3)),(TLAT,W(4)),	CWW2 3
1	(TLON,W(5)),(OW,W(6)),(FBEG,W(7)),(FEND,W(8)),(FSTEP,W(9)),	CWW2 4
2	(AZ1,W(10)),(AZBEG,W(11)),(AZEND,W(12)),(AZSTEP,W(13)),	CWW2 5
3	(BETA,W(14)),(ELBEG,W(15)),(EEND,W(16)),(ELSTEP,W(17)),	CWW2 6
8	(RCVRH,W(20)),	CWW2 7
4	(ONLY,W(21)),(HOP,W(22)),(MAXSTP,W(23)),(PLAT,W(24)),(PLON,W(25))	CWW2 8
5,	(HMAX,W(26)),(RAYFNC,W(29)),(EXTINC,W(33)),	CWW2 9
6	(HMIN,W(27)),(RGMAX,W(28)),	CWW2 10
8	(INTYP,W(41)),(MAXERR,W(42)),(ERATIO,W(43)),	CWW2 11
6	(STEP1,W(44)),(STPMAX,W(45)),(STPMIN,W(46)),(FACTR,W(47)),	CWW2 12
7	(SKIP,W(71)),(RAYSET,W(72)),(PRTSRP,W(74)),(HITLET,W(75))	CWW2 13
9	,(BINRAY,W(76)),(PAGLN,W(77)),(PLT,W(81)),(PFACTR,W(82)),	CWW2 14
1	(LLAT,W(83)),(LLON,W(84)),(RLAT,W(85)),(RLON,W(86))	CWW2 15
2,	(TIC,W(87)),(HB,W(88)),(HT,W(89)),(TICV,W(96))	CWW2 16
	REAL MMODEL,MFORM,MID	CWW3 2
C		CWW3 3
C	WIND 100-124	CWW3 4
	EQUIVALENCE (W(100),UMODEL),(W(101),UFORM),(W(102),UID)	CWW3 5
C		CWW3 6
C	DELTA WIND 125-149	CWW3 7
	EQUIVALENCE (W(125),DUMODEL),(W(126),DUFORM),(W(127),DUID)	CWW3 8
C		CWW3 9
C	SOUND SPEED 150-174	CWW3 10
	EQUIVALENCE (W(150),CMODEL),(W(151),CFORM),(W(152),CID)	CWW3 11
	EQUIVALENCE (W(153),REFC)	CWW3 12
C		CWW3 13
C	DELTA SOUND SPEED 175-199	CWW3 14
	EQUIVALENCE (W(175),DCMODEL),(W(176),DCFORM),(W(177),DCID)	CWW3 15
C		CWW3 16
C	TEMPERATURE 200-224	CWW3 17
	EQUIVALENCE (W(200),TMODEL),(W(201),TFORM),(W(202),TID)	CWW3 18
C		CWW3 19
C	DELTA TEMPERATURE 225-249	CWW3 20
	EQUIVALENCE (W(225),DTMODEL),(W(226),DTFORM),(W(227),DTID)	CWW3 21
C		CWW3 22
C	MOLECULAR 250-274	CWW3 23
	EQUIVALENCE (W(250),MMODEL),(W(251),MFORM),(W(252),MID)	CWW3 24
C		CWW3 25

C	RECEIVER HEIGHT 275-299	CWW3 26
	EQUIVALENCE (W(275),RMODEL), (W(276),RFORM), (W(277),RID)	CWW3 27
C		CWW3 28
C	TOPOGRAPHY 300-324	CWW3 29
	EQUIVALENCE (W(300),GMODEL), (W(301),GFORM), (W(302),GID)	CWW3 30
C		CWW3 31
C	DELTA TOPOGRAPHY 325-349	CWW3 32
	EQUIVALENCE (W(325),GUMODEL), (W(326),GUFORM), (W(327),GUID)	CWW3 33
C		CWW3 34
C	UPPER SURFACE TOPOGRAPHY 350-374	CWW3 35
	EQUIVALENCE (W(350),SMODEL), (W(351),SFORM), (W(352),SID)	CWW3 36
C	PLOT ENHANCEMENTS CONTROL PARAMETERS	CWW3 37
C		CWW3 38
	EQUIVALENCE (W(490),XFQMDL), (W(491),YFQMDL)	CWW3 39
C	ABSORPTION 500-524	CWW3 40
	EQUIVALENCE (W(500),AMODEL), (W(501),AFORM), (W(502),AID)	CWW3 41
C		CWW3 42
C	DELTA ABSORPTION 525-549	CWW3 43
	EQUIVALENCE (W(525),DAMODEL), (W(526),DAFORM), (W(527),DAID)	CWW3 44
C		CWW3 45
C	PRESSURE 550-574	CWW3 46
	EQUIVALENCE (W(550),PMODEL), (W(551),PFORM), (W(552),PID)	CWW3 47
C		CWW3 48
C	DELTA PRESSURE 575-599	CWW3 49
	EQUIVALENCE (W(575),DPMODEL), (W(576),DPFORM), (W(577),DPID)	CWW3 50
C		CWW3 51
C	COMMON DECK "B5" INSERTED HERE	CB5 2
	INTEGER TMX,TNTBL,TITBL,TFRMTBL,IDST(10)	CB5 4
	COMMON/B5/TMX,TNTBL(10),TITBL(10),TFRMTBL(10),TGP(262)	CB5 5
	EQUIVALENCE (TGP,IDST), (ANT,TGP(11))	CB5 6
	EQUIVALENCE (AN,TGP(11)), (HPC,TGP(12)), (FN2C,TGP(262))	TTABLE19
C		TTABLE20
	DATA RECOGT,NOC/6.0,0/	TTABLE21
	DATA ANT/0.0/	TTLEBL 2
	DATA TMX/2/	TTLEBL 3
	DATA TNTBL/1,11,512,7*0/	TTLEBL 4
	DATA TITBL/1,250,8*0/	TTLEBL 5
	DATA TFRMTBL/1,2,8*0/	TTLEBL 6
C		TTABLE24
	ENTRY ITEMP	TTABLE25
C		TTABLE26
C		TTABLE27
	CALL IPTEMP	TTABLE28
C		TTABLE29
C	IF HAD PREVIOUS CALL BUT NOTHING THIS TIME, EXIT NOW	TTABLE30
C	RETAINING PREVIOUS TABULAR DATA COUNT	TTABLE31
	IF(NOC.GT.0 .AND. ANT.LE.0.0) RETURN	TTABLE32
C		TTABLE33
	IF(RECOGT.NE.TMODEL)	TTABLE34
1	CALL RERROR('TEMP ', 'WRNG MODEL',RECOGT)	TTABLE35
C		TTABLE36
	NOC=ANT/2	TTABLE37
	IF(ANT.NE.2*NOC .OR. NOC.LE.1)	TTABLE38
1	CALL RERROR('TTABLE', 'BAD NUMBER',ANT)	TTABLE39
	ANT=0.0	TTABLE40

C	MODT(1)=6HTTABLE	TTABLE41
	MODT(2)=TID	TTABLE42
C		TTABLE43
C		TTABLE44
	SLOPE(1)=(FN2C(2)-FN2C(1))/(HPC(2)-HPC(1))	TTABLE45
	SLOPE(NOC)=0.	TTABLE46
	NMAX=1	TTABLE47
	DO 6 I=2,NOC	TTABLE48
	IF (FN2C(I).GT.FN2C(NMAX)) NMAX=I	TTABLE49
	IF (I.EQ.NOC) GO TO 4	TTABLE50
	DO 3 J=1,3	TTABLE51
	M=I+J-2	TTABLE52
	MAT(J,1)=1.	TTABLE53
	MAT(J,2)=HPC(M)	TTABLE54
	MAT(J,3)=HPC(M)**2	TTABLE55
3	MAT(J,4)=FN2C(M)	TTABLE56
	CALL GAUSEL (MAT,4,3,4,NRANK)	TTABLE57
	IF (NRANK.LT.3) GO TO 60	TTABLE58
	SLOPE(I)=MAT(2,4)+2.*MAT(3,4)*HPC(I)	TTABLE59
4	DO 5 J=1,2	TTABLE60
	M=I+J-2	TTABLE61
	MAT(J,1)=1.	TTABLE62
	MAT(J,2)=HPC(M)	TTABLE63
	MAT(J,3)=HPC(M)**2	TTABLE64
	MAT(J,4)=HPC(M)**3	TTABLE65
	MAT(J,5)=FN2C(M)	TTABLE66
	L=J+2	TTABLE67
	MAT(L,1)=0.	TTABLE68
	MAT(L,2)=1.	TTABLE69
	MAT(L,3)=2.*HPC(M)	TTABLE70
	MAT(L,4)=3.*HPC(M)**2	TTABLE71
5	MAT(L,5)=SLOPE(M)	TTABLE72
	CALL GAUSEL (MAT,4,4,5,NRANK)	TTABLE73
	IF (NRANK.LT.4) GO TO 60	TTABLE74
	ALPHA(I)=MAT(1,5)	TTABLE75
	TTBETA(I)=MAT(2,5)	TTABLE76
	GAMM(I)=MAT(3,5)	TTABLE77
6	DELTA(I)=MAT(4,5)	TTABLE78
	HMAX=HPC(NMAX)	TTABLE79
	NH=2	TTABLE80
C		TTABLE81
	RETURN	TTABLE82
C		TTABLE83
	60 PRINT 6000, I,HPC(I)	TTABLE84
6000	FORMAT(' THE',I4,'TH POINT IN THE TEMPERATURE PROFILE HAS'	TTABLE85
	1,' THE HEIGHT',F8.2,' KM, WHICH IS THE SAME AS ANOTHER POINT.')	TTABLE86
	CALL EXIT	TTABLE87
C		TTABLE88
	ENTRY TEMP	TTABLE89
C		TTABLE90
C		TTABLE91
	IF(NOC.LE.0)	TTABLE92
1	CALL RERROR('TTABLE','BAD N VALUE',FLOAT(NOC))	TTABLE93
C		TTABLE94
		TTABLE95

H=R-EARTH	TTABLE96
PTT=0.0	TTABLE97
PTR=0.0	TTABLE98
PPTH=0.0	TTABLE99
PTPH=0.0	TTABL100
IF (H.GE.HPC(1)) GO TO 12	TTABL101
11 NH=2	TTABL102
T=FN2C(1)+SLOPE(1)*(H-HPC(1))	TTABL103
PTR=SLOPE(1)	TTABL104
RETURN	TTABL105
12 IF (H.GE.HPC(NOC)) GO TO 18	TTABL106
NSTEP=1	TTABL107
IF (H.LT.HPC(NH-1)) NSTEP=-1	TTABL108
15 IF (HPC(NH-1).LE.H.AND.H.LT.HPC(NH)) GO TO 16	TTABL109
NH=NH+NSTEP	TTABL110
GO TO 15	TTABL111
16 T=(ALPHA(NH)+H*(TTBETA(NH)+H*(GAMM(NH)+H*DELTA(NH))))	TTABL112
PTR=(TTBETA(NH)+H*(2.*GAMM(NH)+H*3.*DELTA(NH)))	TTABL113
RETURN	TTABL114
18 T=FN2C(NOC)	TTABL115
C	TTABL116
CALL PTEMP	TTABL117
RETURN	TTABL118
END	TTABL119

SUBROUTINE NTEMP	NTEMP	9
C DO-NOTHING TEMPERATURE MODEL	NTEMP	10
C COMMON DECK "TT" INSERTED HERE	CTT	2
REAL MODT	CTT	4
COMMON/TT/MODT(4), T,PTT,PTR,PPTH,PTPH	CTT	5
C COMMON DECK "WW" INSERTED HERE	CWW	2
PARAMETER (NWARSZ=1000)	CWW1	3
COMMON/WW/ID(10),MAXW,W(NWARSZ)	CWW1	4
REAL MAXSTP,MAXERR,INTYP,LLAT,LLON	CWW2	2
EQUIVALENCE (EARTH,W(1)),(RAY,W(2)),(XMTRH,W(3)),(TLAT,W(4)),	CWW2	3
1 (TLON,W(5)),(OW,W(6)),(FBEG,W(7)),(FEND,W(8)),(FSTEP,W(9)),	CWW2	4
2 (AZ1,W(10)),(AZBEG,W(11)),(AZEND,W(12)),(AZSTEP,W(13)),	CWW2	5
3 (BETA,W(14)),(ELBEG,W(15)),(ELEND,W(16)),(ELSTEP,W(17)),	CWW2	6
8 (RCVRH,W(20)),	CWW2	7
4 (ONLY,W(21)),(HOP,W(22)),(MAXSTP,W(23)),(PLAT,W(24)),(PLON,W(25))	CWW2	8
5,(HMAX,W(26)),(RAYFNC,W(29)),(EXTINC,W(33)),	CWW2	9
6 (HMIN,W(27)),(RGMX,W(28)),	CWW2	10
8 (INTYP,W(41)),(MAXERR,W(42)),(ERATIO,W(43)),	CWW2	11
6 (STEP1,W(44)),(STPMAX,W(45)),(STPMIN,W(46)),(FACTR,W(47)),	CWW2	12
7 (SKIP,W(71)),(RAYSET,W(72)),(PRTSRP,W(74)),(HITLET,W(75))	CWW2	13
9 ,(BINRAY,W(76)),(PAGLN,W(77)),(PLT,W(81)),(PFACTR,W(82)),	CWW2	14
1 (LLAT,W(83)),(LLON,W(84)),(RLAT,W(85)),(RLON,W(86))	CWW2	15
2,(TIC,W(87)),(HB,W(88)),(HT,W(89)),(TICV,W(96))	CWW2	16
REAL MMODEL,MFORM,MID	CWW3	2
C	CWW3	3
C WIND 100-124	CWW3	4

C	EQUIVALENCE (W(100),UMODEL), (W(101),UFORM), (W(102),UID)	CWW3	5
C	DELTA WIND 125-149	CWW3	6
C	EQUIVALENCE (W(125),DUMODEL), (W(126),DUFORM), (W(127),DUID)	CWW3	7
C	SOUND SPEED 150-174	CWW3	8
C	EQUIVALENCE (W(150),CMODEL), (W(151),CFORM), (W(152),CID)	CWW3	9
C	EQUIVALENCE (W(153),REFC)	CWW3	10
C	DELTA SOUND SPEED 175-199	CWW3	11
C	EQUIVALENCE (W(175),DCMODEL), (W(176),DCFORM), (W(177),DCID)	CWW3	12
C	TEMPERATURE 200-224	CWW3	13
C	EQUIVALENCE (W(200),TMODEL), (W(201),TFORM), (W(202),TID)	CWW3	14
C	DELTA TEMPERATURE 225-249	CWW3	15
C	EQUIVALENCE (W(225),DTMODEL), (W(226),DTFORM), (W(227),DTID)	CWW3	16
C	MOLECULAR 250-274	CWW3	17
C	EQUIVALENCE (W(250),MMODEL), (W(251),MFORM), (W(252),MID)	CWW3	18
C	RECEIVER HEIGHT 275-299	CWW3	19
C	EQUIVALENCE (W(275),RMODEL), (W(276),RFORM), (W(277),RID)	CWW3	20
C	TOPOGRAPHY 300-324	CWW3	21
C	EQUIVALENCE (W(300),GMODEL), (W(301),GFORM), (W(302),GID)	CWW3	22
C	DELTA TOPOGRAPHY 325-349	CWW3	23
C	EQUIVALENCE (W(325),GUMODEL), (W(326),GUFORM), (W(327),GUID)	CWW3	24
C	UPPER SURFACE TOPOGRAPHY 350-374	CWW3	25
C	EQUIVALENCE (W(350),SMODEL), (W(351),SFORM), (W(352),SID)	CWW3	26
C	PLOT ENHANCEMENTS CONTROL PARAMETERS	CWW3	27
C	EQUIVALENCE (W(490),XFQMDL), (W(491),YFQMDL)	CWW3	28
C	ABSORPTION 500-524	CWW3	29
C	EQUIVALENCE (W(500),AMODEL), (W(501),AFORM), (W(502),AID)	CWW3	30
C	DELTA ABSORPTION 525-549	CWW3	31
C	EQUIVALENCE (W(525),DAMODEL), (W(526),DAFORM), (W(527),DAID)	CWW3	32
C	PRESSURE 550-574	CWW3	33
C	EQUIVALENCE (W(550),PMODEL), (W(551),PFORM), (W(552),PID)	CWW3	34
C	DELTA PRESSURE 575-599	CWW3	35
C	EQUIVALENCE (W(575),DPMODEL), (W(576),DPFORM), (W(577),DPID)	CWW3	36
C	COMMON DECK "B5" INSERTED HERE	CWW3	37
C	INTEGER TMX,TNTBL,TITBL,TFRMTBL,IDST(10)	CB5	2
C	COMMON/B5/TMX,TNTBL(10),TITBL(10),TFRMTBL(10),TGP(262)	CB5	4
C	EQUIVALENCE (TGP,IDST), (ANT,TGP(11))	CB5	5
C	DATA RECOGT/0.0/	CB5	6
	DATA TMX/1/	NTEMP	14
	DATA TNTBL/1,11,8*0/	NTEMP	15
		NMPBL	2
		NMPBL	3

	DATA TITBL/1,9*0/	NMPBL 4
	DATA TFRMTBL/1,9*0/	NMPBL 5
C	ENTRY ITEMP	NTEMP 18
	IF(RECOGT .NE. TMODEL)	NTEMP 19
1	CALL RERROR('TEMP ', 'WRNG MODEL', RECOGT)	NTEMP 20
C		NTEMP 21
	MODT(1)=5HNTEMP	NTEMP 22
	MODT(2)=DTID	NTEMP 23
	RETURN	NTEMP 24
C		NTEMP 25
	ENTRY TEMP	NTEMP 26
	RETURN	NTEMP 27
	END	NTEMP 28
		NTEMP 29

	SUBROUTINE TBLOB2	TBLOB2 8
C	TEMPERATURE PERTURBATION MODEL	TBLOB2 9
C	MULTIPLICATIVE PERTURBATION WITH EXPONENTIALLY DECAYING	TBLOB210
C	EFFECT IN ALL THREE DIRECTIONS. GIVE LATITUDE	TBLOB211
C	INSTEAD OF CO-LATITUDE.	TBLOB212
C	COMMON DECK "CONST" INSERTED HERE	CCONST 2
	COMMON/PCONST/CREF, RGAS, GAMMA	CCONST 4
	COMMON/MCONST/PI, PIT2, PID2, DEGS, RAD, ALN10	CCONST 5
C	COMMON DECK "RKAM" INSERTED HERE	RKAMCOM2
	REAL KR, KTH, KPH	RKAMCOM4
	COMMON//R, TH, PH, KR, KTH, KPH, RKVARS(14), TPULSE, CSTEP, DRDT(20)	RKAMCOM5
C	COMMON DECK "B6" INSERTED HERE	CB6 2
	INTEGER DTMX, DTNTBL, DTITBL, DTFRMTB, IDSDT(10)	CB6 4
	COMMON/B6/DTMX, DTNTBL(10), DTITBL(10), DTFRMTB(10), DTGP(10)	CB6 5
	EQUIVALENCE (DTGP, IDSDT)	CB6 6
C		TBLOB216
C	COMMON DECK "TT" INSERTED HERE	CTT 2
	REAL MODT	CTT 4
	COMMON/TT/MODT(4), T, PTT, PTR, PTH, PTPH	CTT 5
C	COMMON DECK "WW" INSERTED HERE	CWW 2
	PARAMETER (NWARSZ=1000)	CWW1 3
	COMMON/WW/ID(10), MAXW, W(NWARSZ)	CWW1 4
	REAL MAXSTP, MAXERR, INTYP, LLAT, LLON	CWW2 2
	EQUIVALENCE (EARTH, W(1)), (RAY, W(2)), (XMTRH, W(3)), (TLAT, W(4)),	CWW2 3
1	(TLON, W(5)), (OW, W(6)), (FBEG, W(7)), (FEND, W(8)), (FSTEP, W(9)),	CWW2 4
2	(AZ1, W(10)), (AZBEG, W(11)), (AZEND, W(12)), (AZSTEP, W(13)),	CWW2 5
3	(BETA, W(14)), (ELBEG, W(15)), (ELEND, W(16)), (ELSTEP, W(17)),	CWW2 6
8	(RCVRH, W(20)),	CWW2 7
4	(ONLY, W(21)), (HOP, W(22)), (MAXSTP, W(23)), (PLAT, W(24)), (PLON, W(25))	CWW2 8
5,	(HMAX, W(26)), (RAYFNC, W(29)), (EXTINC, W(33)),	CWW2 9
6	(HMIN, W(27)), (RGMAX, W(28)),	CWW2 10
8	(INTYP, W(41)), (MAXERR, W(42)), (ERATIO, W(43)),	CWW2 11
6	(STEP1, W(44)), (STPMAX, W(45)), (STPMIN, W(46)), (FACTR, W(47)),	CWW2 12
7	(SKIP, W(71)), (RAYSET, W(72)), (PRTSRP, W(74)), (HITLET, W(75))	CWW2 13
9	, (BINRAY, W(76)), (PAGLN, W(77)), (PLT, W(81)), (PFACTR, W(82)),	CWW2 14
1	(LLAT, W(83)), (LLON, W(84)), (RLAT, W(85)), (RLON, W(86))	CWW2 15

	2, (TIC,W(87)), (HB,W(88)), (HT,W(89)), (TICV,W(96))	CWW2	16
	REAL MMODEL,MFORM,MID	CWW3	2
C		CWW3	3
C	WIND 100-124	CWW3	4
	EQUIVALENCE (W(100),UMODEL), (W(101),UFORM), (W(102),UID)	CWW3	5
C		CWW3	6
C	DELTA WIND 125-149	CWW3	7
	EQUIVALENCE (W(125),DUMODEL), (W(126),DUFORM), (W(127),DUID)	CWW3	8
C		CWW3	9
C	SOUND SPEED 150-174	CWW3	10
	EQUIVALENCE (W(150),CMODEL), (W(151),CFORM), (W(152),CID)	CWW3	11
	EQUIVALENCE (W(153),REFC)	CWW3	12
C		CWW3	13
C	DELTA SOUND SPEED 175-199	CWW3	14
	EQUIVALENCE (W(175),DCMODEL), (W(176),DCFORM), (W(177),DCID)	CWW3	15
C		CWW3	16
C	TEMPERATURE 200-224	CWW3	17
	EQUIVALENCE (W(200),TMODEL), (W(201),TFORM), (W(202),TID)	CWW3	18
C		CWW3	19
C	DELTA TEMPERATURE 225-249	CWW3	20
	EQUIVALENCE (W(225),DTMODEL), (W(226),DTFORM), (W(227),DTID)	CWW3	21
C		CWW3	22
C	MOLECULAR 250-274	CWW3	23
	EQUIVALENCE (W(250),MMODEL), (W(251),MFORM), (W(252),MID)	CWW3	24
C		CWW3	25
C	RECEIVER HEIGHT 275-299	CWW3	26
	EQUIVALENCE (W(275),RMODEL), (W(276),RFORM), (W(277),RID)	CWW3	27
C		CWW3	28
C	TOPOGRAPHY 300-324	CWW3	29
	EQUIVALENCE (W(300),GMODEL), (W(301),GFORM), (W(302),GID)	CWW3	30
C		CWW3	31
C	DELTA TOPOGRAPHY 325-349	CWW3	32
	EQUIVALENCE (W(325),GUMODEL), (W(326),GUFORM), (W(327),GUID)	CWW3	33
C		CWW3	34
C	UPPER SURFACE TOPOGRAPHY 350-374	CWW3	35
	EQUIVALENCE (W(350),SMODEL), (W(351),SFORM), (W(352),SID)	CWW3	36
C		CWW3	37
C	PLOT ENHANCEMENTS CONTROL PARAMETERS	CWW3	38
	EQUIVALENCE (W(490),XFQMDL), (W(491),YFQMDL)	CWW3	39
C	ABSORPTION 500-524	CWW3	40
	EQUIVALENCE (W(500),AMODEL), (W(501),AFORM), (W(502),AID)	CWW3	41
C		CWW3	42
C	DELTA ABSORPTION 525-549	CWW3	43
	EQUIVALENCE (W(525),DAMODEL), (W(526),DAFORM), (W(527),DAID)	CWW3	44
C		CWW3	45
C	PRESSURE 550-574	CWW3	46
	EQUIVALENCE (W(550),PMODEL), (W(551),PFORM), (W(552),PID)	CWW3	47
C		CWW3	48
C	DELTA PRESSURE 575-599	CWW3	49
	EQUIVALENCE (W(575),DPMODEL), (W(576),DPFORM), (W(577),DPID)	CWW3	50
C		CWW3	51
C		TBLOB219	
	EQUIVALENCE (CO,W(228)), (ZO,W(229)), (TBTHO,W(230))	TBLOB220	
	EQUIVALENCE (PHO,W(231)), (WZ,W(232)), (WTH,W(233)), (WPH,W(234))	TBLOB221	
C		TBLOB222	

	DATA RECOGDT/2.0/	TBLOB223
	DATA DTMX/1/	TOB2BL 2
	DATA DTNTBL/1,11,8*0/	TOB2BL 3
	DATA DTITBL/1,9*0/	TOB2BL 4
	DATA DTFRMTB/1,9*0/	TOB2BL 5
C	ENTRY IPTEMP	TBLOB226
	IF(RECOGDT .NE. DTMODEL)	TBLOB227
	1 CALL RERROR('DTEMP ', 'WRNG MODEL', RECOGDT)	TBLOB228
C		TBLOB229
C		TBLOB230
	MODT(3)=6HTBLOB2	TBLOB231
	MODT(4)=DTID	TBLOB232
C		TBLOB233
	FWZ=0.0	TBLOB234
	FWTH=0.0	TBLOB235
	FwPH=0.0	TBLOB236
	TH0= PID2-TBTH0	TBLOB237
	IF(WZ.NE.0.0) FWZ=2.0/WZ/WZ	TBLOB238
	IF(WTH.NE.0.0) FWTH=2.0/WTH/WTH	TBLOB239
	IF(WPH.NE.0.0) FwPH=2.0/WPH/WPH	TBLOB240
	RETURN	TBLOB241
C		TBLOB242
	ENTRY PTEMP	TBLOB243
C		TBLOB244
	IF(CO.EQ.0.0) RETURN	TBLOB245
C		TBLOB246
	DZ=R-EARTH-R-Z0	TBLOB247
	DTH=TH-TH0	TBLOB248
	DPH=PH-PH0	TBLOB249
	DEXPO=0.0	TBLOB250
	EXPO=-0.5*(DZ*DZ*FWZ+DTH*DTH*FWTH+DPH*DPH*FWPH)	TBLOB251
	IF(EXPO .GT. -200.0) DEXPO=CO*EXP(EXPO)	TBLOB252
	DEL=1.0+DEXPO	TBLOB253
C		TBLOB254
	PTR=PTR*DEL-T*DEXPO*FWZ*DZ	TBLOB255
	PPTH=PPTH*DEL-T*DEXPO*FWTH*DTH	TBLOB256
	PTPH=PTPH*DEL-T*DEXPO*FWPH*DPH	TBLOB257
	T=T*DEL	TBLOB258
	RETURN	TBLOB259
	END	TBLOB260
		TBLOB261

	SUBROUTINE NPTEMP	NPTEMP 8
C	DO-NOTHING TEMPERATURE PERTURBATION MODEL	NPTEMP 9
C	COMMON DECK "TT" INSERTED HERE	CTT 2
	REAL MODT	CTT 4
	COMMON/TT/MODT(4), T, PTT, PTR, PPTH, PTPH	CTT 5
C	COMMON DECK "WW" INSERTED HERE	CWW 2
	PARAMETER (NWARSZ=1000)	CWW1 3
	COMMON/WW/ID(10), MAXW, W(NWARSZ)	CWW1 4
	REAL MAXSTP, MAXERR, INTYP, LLAT, LLON	CWW2 2

	EQUIVALENCE (EARTH, W(1)), (RAY, W(2)), (XMTRH, W(3)), (TLAT, W(4)),	CWW2	3
1	(TLON, W(5)), (OW, W(6)), (FBEG, W(7)), (FEND, W(8)), (FSTEP, W(9)),	CWW2	4
2	(AZ1, W(10)), (AZBEG, W(11)), (AZEND, W(12)), (AZSTEP, W(13)),	CWW2	5
3	(BETA, W(14)), (ELBEG, W(15)), (ELEND, W(16)), (ELSTEP, W(17)),	CWW2	6
8	(RCVRH, W(20)),	CWW2	7
4	(ONLY, W(21)), (HOP, W(22)), (MAXSTP, W(23)), (PLAT, W(24)), (PLON, W(25))	CWW2	8
5,	(HMAX, W(26)), (RAYFNC, W(29)), (EXTINC, W(33)),	CWW2	9
6	(HMIN, W(27)), (RGMAX, W(28)),	CWW2	10
8	(INTYP, W(41)), (MAXERR, W(42)), (ERATIO, W(43)),	CWW2	11
6	(STEP1, W(44)), (STPMAX, W(45)), (STPMIN, W(46)), (FACTR, W(47)),	CWW2	12
7	(SKIP, W(71)), (RAYSET, W(72)), (PRTSRP, W(74)), (HITLET, W(75))	CWW2	13
9	, (BINRAY, W(76)), (PAGLN, W(77)), (PLT, W(81)), (PFACTR, W(82)),	CWW2	14
1	(LLAT, W(83)), (LLON, W(84)), (RLAT, W(85)), (RLON, W(86))	CWW2	15
2,	(TIC, W(87)), (HB, W(88)), (HT, W(89)), (TICV, W(96))	CWW2	16
	REAL MMODEL, MFORM, MID	CWW3	2
C		CWW3	3
C	WIND 100-124	CWW3	4
	EQUIVALENCE (W(100), UMODEL), (W(101), UFORM), (W(102), UID)	CWW3	5
C		CWW3	6
C	DELTA WIND 125-149	CWW3	7
	EQUIVALENCE (W(125), DUMODEL), (W(126), DUFORM), (W(127), DUID)	CWW3	8
C		CWW3	9
C	SOUND SPEED 150-174	CWW3	10
	EQUIVALENCE (W(150), CMODEL), (W(151), CFORM), (W(152), CID)	CWW3	11
	EQUIVALENCE (W(153), REFC)	CWW3	12
C		CWW3	13
C	DELTA SOUND SPEED 175-199	CWW3	14
	EQUIVALENCE (W(175), DCMODEL), (W(176), DCFORM), (W(177), DCID)	CWW3	15
C		CWW3	16
C	TEMPERATURE 200-224	CWW3	17
	EQUIVALENCE (W(200), TMODEL), (W(201), TFORM), (W(202), TID)	CWW3	18
C		CWW3	19
C	DELTA TEMPERATURE 225-249	CWW3	20
	EQUIVALENCE (W(225), DTMODEL), (W(226), DTFORM), (W(227), DTID)	CWW3	21
C		CWW3	22
C	MOLECULAR 250-274	CWW3	23
	EQUIVALENCE (W(250), MMODEL), (W(251), MFORM), (W(252), MID)	CWW3	24
C		CWW3	25
C	RECEIVER HEIGHT 275-299	CWW3	26
	EQUIVALENCE (W(275), RMODEL), (W(276), RFORM), (W(277), RID)	CWW3	27
C		CWW3	28
C	TOPOGRAPHY 300-324	CWW3	29
	EQUIVALENCE (W(300), GMODEL), (W(301), GFORM), (W(302), GID)	CWW3	30
C		CWW3	31
C	DELTA TOPOGRAPHY 325-349	CWW3	32
	EQUIVALENCE (W(325), GUMODEL), (W(326), GUFORM), (W(327), GUID)	CWW3	33
C		CWW3	34
C	UPPER SURFACE TOPOGRAPHY 350-374	CWW3	35
	EQUIVALENCE (W(350), SMODEL), (W(351), SFORM), (W(352), SID)	CWW3	36
C		CWW3	37
C	PLOT ENHANCEMENTS CONTROL PARAMETERS	CWW3	38
	EQUIVALENCE (W(490), XFQMDL), (W(491), YFQMDL)	CWW3	39
C	ABSORPTION 500-524	CWW3	40
	EQUIVALENCE (W(500), AMODEL), (W(501), AFORM), (W(502), AID)	CWW3	41
C		CWW3	42

C	DELTA ABSORPTION	525-549	CWW3	43
	EQUIVALENCE	(W(525), DAMODEL), (W(526), DAFORM), (W(527), DAID)	CWW3	44
C			CWW3	45
C	PRESSURE	550-574	CWW3	46
	EQUIVALENCE	(W(550), PMODEL), (W(551), PFORM), (W(552), PID)	CWW3	47
C			CWW3	48
C	DELTA PRESSURE	575-599	CWW3	49
	EQUIVALENCE	(W(575), DPMODEL), (W(576), DPFORM), (W(577), DPID)	CWW3	50
C			CWW3	51
C	COMMON DECK "B6" INSERTED HERE		NPTEMP12	
	INTEGER	DTMX, DTNTBL, DTITBL, DTFRMTB, IDS DT(10)	CB6	2
	COMMON/B6/DTMX, DTNTBL(10), DTITBL(10), DTFRMTB(10), DTGP(10)		CB6	4
	EQUIVALENCE	(DTGP, IDS DT)	CB6	5
C			CB6	6
	DATA	DTMX/1/	NPTEMP14	
	DATA	DTNTBL/1,11,8*0/	NEMPBL	2
	DATA	DTITBL/1,9*0/	NEMPBL	3
	DATA	DTFRMTB/1,9*0/	NEMPBL	4
C			NEMPBL	5
	DATA	RECOGDT/0.0/	NPTEMP17	
C			NPTEMP18	
	ENTRY	IPTEMP	NPTEMP19	
	IF	(RECOGDT .NE. DTMODEL)	NPTEMP20	
1	CALL	RERROR('DTEMP ', 'WRNG MODEL', RECOGDT)	NPTEMP21	
C			NPTEMP22	
	MODT	(3)=6HNPTEMP	NPTEMP23	
	MODT	(4)=DTID	NPTEMP24	
	RETURN		NPTEMP25	
C			NPTEMP26	
	ENTRY	PTEMP	NPTEMP27	
	RETURN		NPTEMP28	
	END		NPTEMP29	
			NPTEMP30	
	SUBROUTINE	MCONST	MCONST	8
C	CONSTANT	MOLECULAR WEIGHT MODEL	MCONST	9
C	COMMON	DECK "WW" INSERTED HERE	CWW	2
	PARAMETER	(NWARSZ=1000)	CWW1	3
	COMMON/WW/ID	(10), MAXW, W(NWARSZ)	CWW1	4
	REAL	MAXSTP, MAXERR, INTYP, LLAT, LLON	CWW2	2
	EQUIVALENCE	(EARTH, W(1)), (RAY, W(2)), (XMTRH, W(3)), (TLAT, W(4)),	CWW2	3
1	(TLON, W(5)), (OW, W(6)), (FBEG, W(7)), (FEND, W(8)), (FSTEP, W(9)),		CWW2	4
2	(AZ1, W(10)), (AZBEG, W(11)), (AZEND, W(12)), (AZSTEP, W(13)),		CWW2	5
3	(BETA, W(14)), (ELBEG, W(15)), (ELEND, W(16)), (ELSTEP, W(17)),		CWW2	6
8	(RCVRH, W(20)),		CWW2	7
4	(ONLY, W(21)), (HOP, W(22)), (MAXSTP, W(23)), (PLAT, W(24)), (PLON, W(25))		CWW2	8
5,	(HMAX, W(26)), (RAYFNC, W(29)), (EXTINC, W(33)),		CWW2	9
6	(HMIN, W(27)), (RGMAX, W(28)),		CWW2	10
8	(INTYP, W(41)), (MAXERR, W(42)), (ERATIO, W(43)),		CWW2	11
6	(STEP1, W(44)), (STPMAX, W(45)), (STPMIN, W(46)), (FACTR, W(47)),		CWW2	12
7	(SKIP, W(71)), (RAYSET, W(72)), (PRTSRP, W(74)), (HITLET, W(75))		CWW2	13

	9 , (BINRAY,W(76)) , (PAGLN,W(77)) , (PLT,W(81)) , (PFACTR,W(82)) ,	CWW2	14
	1 (LLAT,W(83)) , (LLON,W(84)) , (RLAT,W(85)) , (RLON,W(86))	CWW2	15
	2, (TIC,W(87)) , (HB,W(88)) , (HT,W(89)) , (TICV,W(96))	CWW2	16
	REAL MMODEL,MFORM,MID	CWW3	2
C		CWW3	3
C	WIND 100-124	CWW3	4
	EQUIVALENCE (W(100),UMODEL) , (W(101),UFORM) , (W(102),UID)	CWW3	5
C		CWW3	6
C	DELTA WIND 125-149	CWW3	7
	EQUIVALENCE (W(125),DUMODEL) , (W(126),DIFORM) , (W(127),DUID)	CWW3	8
C		CWW3	9
C	SOUND SPEED 150-174	CWW3	10
	EQUIVALENCE (W(150),CMODEL) , (W(151),CFORM) , (W(152),CID)	CWW3	11
	EQUIVALENCE (W(153),REFC)	CWW3	12
C		CWW3	13
C	DELTA SOUND SPEED 175-199	CWW3	14
	EQUIVALENCE (W(175),DCMODEL) , (W(176),DCFORM) , (W(177),DCID)	CWW3	15
C		CWW3	16
C	TEMPERATURE 200-224	CWW3	17
	EQUIVALENCE (W(200),TMODEL) , (W(201),TFORM) , (W(202),TID)	CWW3	18
C		CWW3	19
C	DELTA TEMPERATURE 225-249	CWW3	20
	EQUIVALENCE (W(225),DTMODEL) , (W(226),DTFORM) , (W(227),DTID)	CWW3	21
C		CWW3	22
C	MOLECULAR 250-274	CWW3	23
	EQUIVALENCE (W(250),MMODEL) , (W(251),MFORM) , (W(252),MID)	CWW3	24
C		CWW3	25
C	RECEIVER HEIGHT 275-299	CWW3	26
	EQUIVALENCE (W(275),RMODEL) , (W(276),RFORM) , (W(277),RID)	CWW3	27
C		CWW3	28
C	TOPOGRAPHY 300-324	CWW3	29
	EQUIVALENCE (W(300),GMODEL) , (W(301),GFORM) , (W(302),GID)	CWW3	30
C		CWW3	31
C	DELTA TOPOGRAPHY 325-349	CWW3	32
	EQUIVALENCE (W(325),GUMODEL) , (W(326),GIFORM) , (W(327),GUID)	CWW3	33
C		CWW3	34
C	UPPER SURFACE TOPOGRAPHY 350-374	CWW3	35
	EQUIVALENCE (W(350),SMODEL) , (W(351),SFORM) , (W(352),SID)	CWW3	36
C		CWW3	37
C	PLOT ENHANCEMENTS CONTROL PARAMETERS	CWW3	38
	EQUIVALENCE (W(490),XFQMDL) , (W(491),YFQMDL)	CWW3	39
C	ABSORPTION 500-524	CWW3	40
	EQUIVALENCE (W(500),AMODEL) , (W(501),AFORM) , (W(502),AID)	CWW3	41
C		CWW3	42
C	DELTA ABSORPTION 525-549	CWW3	43
	EQUIVALENCE (W(525),DAMODEL) , (W(526),DAFORM) , (W(527),DAID)	CWW3	44
C		CWW3	45
C	PRESSURE 550-574	CWW3	46
	EQUIVALENCE (W(550),PMODEL) , (W(551),PFORM) , (W(552),PID)	CWW3	47
C		CWW3	48
C	DELTA PRESSURE 575-599	CWW3	49
	EQUIVALENCE (W(575),DPMODEL) , (W(576),DPFORM) , (W(577),DPID)	CWW3	50
C		CWW3	51
C	COMMON DECK "MM" INSERTED HERE	CMM	2
	REAL M,MODM	CMM	4

	COMMON/MM/MODM(4),M,PMT,PMR,PMTH,MPH	CMM	5
	REAL MLCNST	MCONST12	
	EQUIVALENCE (W(253),MLCNST)	MCONST13	
C	COMMON DECK "B7" INSERTED HERE	CB7	2
	INTEGER MMX,MNTBL,MITBL,MFRMTBL,IDS(10)	CB7	4
	REAL MGP	CB7	5
	COMMON/B7/MMX,MNTBL(10),MITBL(10),MFRMTBL(10),MGP(10)	CB7	6
	EQUIVALENCE (MGP,IDS)	CB7	7
	DATA RECOGM/1.0/	MCONST15	
	DATA MMX/1/	MNSTBL	2
	DATA MNTBL/1,11,8*0/	MNSTBL	3
	DATA MITBL/1,9*0/	MNSTBL	4
	DATA MFRMTBL/1,9*0/	MNSTBL	5
C	ENTRY IMOLWT	MCONST18	
C		MCONST19	
	IF(RECOGM .NE. MMODEL)	MCONST20	
C	1 CALL RERROR('IMOLWT ','WRNG MODEL',RECOGM)	MCONST21	
		MCONST22	
C	MODM(1)=6HMCONST	MCONST23	
	MODM(2)=MID	MCONST24	
C		MCONST25	
	RETURN	MCONST26	
C		MCONST27	
	ENTRY MOLWT	MCONST28	
	M=MLCNST	MCONST29	
	CALL CLEAR(PMT,4)	MCONST30	
	END	MCONST31	
		MCONST32	

	SUBROUTINE GHORIZ	GHORIZ	8
C	TERRAIN MODEL USING FIXED OFFSET TO EARTH'S SURFACE	GHORIZ	9
C	COMMON DECK "GG" INSERTED HERE	CGG	2
	REAL MODG	CGG	4
	COMMON/GG/MODG(4)	CGG	5
	COMMON/GG/G,PGR,PGRR,PGRTH,PGRPH	CGG	6
	COMMON/GG/PGTH,PGPH,PGTHTH,PGPHPH,PGTHPH,GSELECT,GTIME	CGG	7
C	COMMON DECK "WW" INSERTED HERE	CWW	2
	PARAMETER (NWARSZ=1000)	CWW1	3
	COMMON/WW/ID(10),MAXW,W(NWARSZ)	CWW1	4
	REAL MAXSTP,MAXERR,INTYP,LLAT,LLON	CWW2	2
	EQUIVALENCE (EARTH,W(1)),(RAY,W(2)),(XMTRH,W(3)),(TLAT,W(4)),	CWW2	3
	1 (TLON,W(5)),(OW,W(6)),(FBEG,W(7)),(FEND,W(8)),(FSTEP,W(9)),	CWW2	4
	2 (AZ1,W(10)),(AZBEG,W(11)),(AZEND,W(12)),(AZSTEP,W(13)),	CWW2	5
	3 (BETA,W(14)),(ELBEG,W(15)),(ELEND,W(16)),(ELSTEP,W(17)),	CWW2	6
	8 (RCVRH,W(20)),	CWW2	7
	4 (ONLY,W(21)),(HOP,W(22)),(MAXSTP,W(23)),(PLAT,W(24)),(PLON,W(25))	CWW2	8
	5,(HMAX,W(26)),(RAYFNC,W(29)),(EXTINC,W(33)),	CWW2	9
	6 (HMIN,W(27)),(RGMX,W(28)),	CWW2	10
	8 (INTYP,W(41)),(MAXERR,W(42)),(ERATIO,W(43)),	CWW2	11
	6 (STEP1,W(44)),(STPMAX,W(45)),(STPMIN,W(46)),(FACTR,W(47)),	CWW2	12
	7 (SKIP,W(71)),(RAYSET,W(72)),(PRTSRP,W(74)),(HITLET,W(75))	CWW2	13

9	, (BINRAY, W(76)), (PAGLN, W(77)), (PLT, W(81)), (PFACTR, W(82)),	CWW2	14
1	(LLAT, W(83)), (LLON, W(84)), (RLAT, W(85)), (RLON, W(86))	CWW2	15
2	, (TIC, W(87)), (HB, W(88)), (HT, W(89)), (TICV, W(96))	CWW2	16
	REAL MMODEL, MFORM, MID	CWW3	2
C		CWW3	3
C	WIND 100-124	CWW3	4
	EQUIVALENCE (W(100), UMODEL), (W(101), UFORM), (W(102), UID)	CWW3	5
C		CWW3	6
C	DELTA WIND 125-149	CWW3	7
	EQUIVALENCE (W(125), DUMODEL), (W(126), DUFORM), (W(127), DUID)	CWW3	8
C		CWW3	9
C	SOUND SPEED 150-174	CWW3	10
	EQUIVALENCE (W(150), CMODEL), (W(151), CFORM), (W(152), CID)	CWW3	11
	EQUIVALENCE (W(153), REFC)	CWW3	12
C		CWW3	13
C	DELTA SOUND SPEED 175-199	CWW3	14
	EQUIVALENCE (W(175), DCMODEL), (W(176), DCFORM), (W(177), DCID)	CWW3	15
C		CWW3	16
C	TEMPERATURE 200-224	CWW3	17
	EQUIVALENCE (W(200), TMODEL), (W(201), TFORM), (W(202), TID)	CWW3	18
C		CWW3	19
C	DELTA TEMPERATURE 225-249	CWW3	20
	EQUIVALENCE (W(225), DTMODEL), (W(226), DTFORM), (W(227), DTID)	CWW3	21
C		CWW3	22
C	MOLECULAR 250-274	CWW3	23
	EQUIVALENCE (W(250), MMODEL), (W(251), MFORM), (W(252), MID)	CWW3	24
C		CWW3	25
C	RECEIVER HEIGHT 275-299	CWW3	26
	EQUIVALENCE (W(275), RMODEL), (W(276), RFORM), (W(277), RID)	CWW3	27
C		CWW3	28
C	TOPOGRAPHY 300-324	CWW3	29
	EQUIVALENCE (W(300), GMODEL), (W(301), GFORM), (W(302), GID)	CWW3	30
C		CWW3	31
C	DELTA TOPOGRAPHY 325-349	CWW3	32
	EQUIVALENCE (W(325), GUMODEL), (W(326), GUFORM), (W(327), GUID)	CWW3	33
C		CWW3	34
C	UPPER SURFACE TOPOGRAPHY 350-374	CWW3	35
	EQUIVALENCE (W(350), SMODEL), (W(351), SFORM), (W(352), SID)	CWW3	36
C	PLOT ENHANCEMENTS CONTROL PARAMETERS	CWW3	37
C		CWW3	38
	EQUIVALENCE (W(490), XFQMDL), (W(491), YFQMDL)	CWW3	39
C	ABSORPTION 500-524	CWW3	40
	EQUIVALENCE (W(500), AMODEL), (W(501), AFORM), (W(502), AID)	CWW3	41
C		CWW3	42
C	DELTA ABSORPTION 525-549	CWW3	43
	EQUIVALENCE (W(525), DAMODEL), (W(526), DAFORM), (W(527), DAID)	CWW3	44
C		CWW3	45
C	PRESSURE 550-574	CWW3	46
	EQUIVALENCE (W(550), PMODEL), (W(551), PFORM), (W(552), PID)	CWW3	47
C		CWW3	48
C	DELTA PRESSURE 575-599	CWW3	49
	EQUIVALENCE (W(575), DPMODEL), (W(576), DPFORM), (W(577), DPID)	CWW3	50
C		CWW3	51
C	COMMON DECK "RKAM" INSERTED HERE	RKAMCOM2	
	REAL KR, KTH, KPH	RKAMCOM4	

C	COMMON//R, TH, PH, KR, KTH, KPH, RKVARS (14), TPULSE, CSTEP, DRDT (20)	RKAMCOM5
	EQUIVALENCE (W(303), Z0)	GHORIZ13
C		GHORIZ14
C	COMMON DECK "B9" INSERTED HERE	GHORIZ15
	INTEGER GMX, GNTBL, GITBL, GFRMTBL, IDSG (10)	CB8 2
	COMMON/B9/GMX, GNTBL (10), GITBL (10), GFRMTBL (10), GGP (113)	CB8 4
	EQUIVALENCE (GGP, IDSG), (ANG, GGP (11))	CB8 5
C		CB8 6
	DATA RECOGG/1.0/	GHORIZ17
C		GHORIZ18
	DATA GMX/1/	GHORIZ19
	DATA GNTBL/1, 11, 8*0/	GRIZBL 2
	DATA GITBL/1, 9*0/	GRIZBL 3
	DATA GFRMTBL/1, 9*0/	GRIZBL 4
C		GRIZBL 5
	ENTRY ITOPOG	GHORIZ22
	IF (RECOGG .NE. GMODEL)	GHORIZ23
1	CALL RERROR ('GHORIZ ', 'WRNG MODEL', RECOGG)	GHORIZ24
	MODG (1) = 6HGHORIZ	GHORIZ25
	MODG (2) = GID	GHORIZ26
	RETURN	GHORIZ27
	ENTRY TOPOG	GHORIZ28
	G=R-W (1) -Z0	GHORIZ29
	PGR=1.0	GHORIZ30
	CALL CLEAR (PGRR, 8)	GHORIZ31
	END	GHORIZ32
		GHORIZ33
	SUBROUTINE GLORENZ	GLORENZ8
C	TERRAIN MODEL USING LORENZIAN SHAPED HORIZONTAL SURFACE LOCATED A	GLORENZ9
C	ARBITRARY GEOGRAPHICAL LOCATION.	GLORENZ10
C		GLORENZ11
C	COMMON DECK "CONST" INSERTED HERE	CCONST 2
	COMMON/PCONST/CREF, RGAS, GAMMA	CCONST 4
	COMMON/MCONST/PI, PIT2, PID2, DEGS, RAD, ALN10	CCONST 5
C	COMMON DECK "B9" INSERTED HERE	CB8 2
	INTEGER GMX, GNTBL, GITBL, GFRMTBL, IDSG (10)	CB8 4
	COMMON/B9/GMX, GNTBL (10), GITBL (10), GFRMTBL (10), GGP (113)	CB8 5
	EQUIVALENCE (GGP, IDSG), (ANG, GGP (11))	CB8 6
C	COMMON DECK "RKAM" INSERTED HERE	RKAMCOM2
	REAL KR, KTH, KPH	RKAMCOM4
	COMMON//R, TH, PH, KR, KTH, KPH, RKVARS (14), TPULSE, CSTEP, DRDT (20)	RKAMCOM5
C	COMMON DECK "GG" INSERTED HERE	CGG 2
	REAL MODG	CGG 4
	COMMON/GG/MODG (4)	CGG 5
	COMMON/GG/G, PGR, PGRR, PGRTH, PGRPH	CGG 6
	COMMON/GG/PGTH, PGPH, PGTHTH, PGPHPH, PGTHPH, GSELECT, GTIME	CGG 7
C	COMMON DECK "B10" INSERTED HERE	CB9 2
	INTEGER DGMX, DGNTBL, DGITBL, DGFRMTB, IDSDG (10)	CB9 4
	COMMON/B10/DGMX, DGNTBL (10), DGITBL (10), DGFRMTB (10), DGGP (10)	CB9 5
	EQUIVALENCE (DGGP, IDSDG)	CB9 6

C	COMMON DECK "WW" INSERTED HERE	CWW	2
	PARAMETER (NWAR SZ=1000)	CWW1	3
	COMMON/WW/ID(10),MAXW,W(NWAR SZ)	CWW1	4
	REAL MAXSTP,MAXERR,INTYP,LLAT,LLON	CWW2	2
	EQUIVALENCE (EARTH R,W(1)),(RAY,W(2)),(XMTRH,W(3)),(TLAT,W(4)),	CWW2	3
	1 (TLON,W(5)),(OW,W(6)),(FBEG,W(7)),(FEND,W(8)),(FSTEP,W(9)),	CWW2	4
	2 (AZ1,W(10)),(AZBEG,W(11)),(AZEND,W(12)),(AZSTEP,W(13)),	CWW2	5
	3 (BETA,W(14)),(ELBEG,W(15)),(ELEND,W(16)),(ELSTEP,W(17)),	CWW2	6
	8 (RCVRH,W(20)),	CWW2	7
	4 (ONLY,W(21)),(HOP,W(22)),(MAXSTP,W(23)),(PLAT,W(24)),(PLON,W(25))	CWW2	8
	5,(HMAX,W(26)),(RAYFNC,W(29)),(EXTINC,W(33)),	CWW2	9
	6 (HMIN,W(27)),(RGMAX,W(28)),	CWW2	10
	8 (INTYP,W(41)),(MAXERR,W(42)),(ERATIO,W(43)),	CWW2	11
	6 (STEP1,W(44)),(STPMAX,W(45)),(STPMIN,W(46)),(FACTR,W(47)),	CWW2	12
	7 (SKIP,W(71)),(RAYSET,W(72)),(PRTSRP,W(74)),(HITLET,W(75))	CWW2	13
	9 ,(BINRAY,W(76)),(PAGLN,W(77)),(PLT,W(81)),(PFACTR,W(82)),	CWW2	14
	1 (LLAT,W(83)),(LLON,W(84)),(RLAT,W(85)),(RLON,W(86))	CWW2	15
	2,(TIC,W(87)),(HB,W(88)),(HT,W(89)),(TICV,W(96))	CWW2	16
	REAL MMODEL,MFORM,MID	CWW3	2
C		CWW3	3
C	WIND 100-124	CWW3	4
	EQUIVALENCE (W(100),UMODEL),(W(101),UFORM),(W(102),UID)	CWW3	5
C		CWW3	6
C	DELTA WIND 125-149	CWW3	7
	EQUIVALENCE (W(125),DUMODEL),(W(126),DUFORM),(W(127),DUID)	CWW3	8
C		CWW3	9
C	SOUND SPEED 150-174	CWW3	10
	EQUIVALENCE (W(150),CMODEL),(W(151),CFORM),(W(152),CID)	CWW3	11
	EQUIVALENCE (W(153),REFC)	CWW3	12
C		CWW3	13
C	DELTA SOUND SPEED 175-199	CWW3	14
	EQUIVALENCE (W(175),DCMODEL),(W(176),DCFORM),(W(177),DCID)	CWW3	15
C		CWW3	16
C	TEMPERATURE 200-224	CWW3	17
	EQUIVALENCE (W(200),TMODEL),(W(201),TFORM),(W(202),TID)	CWW3	18
C		CWW3	19
C	DELTA TEMPERATURE 225-249	CWW3	20
	EQUIVALENCE (W(225),DTMODEL),(W(226),DTFORM),(W(227),DTID)	CWW3	21
C		CWW3	22
C	MOLECULAR 250-274	CWW3	23
	EQUIVALENCE (W(250),MMODEL),(W(251),MFORM),(W(252),MID)	CWW3	24
C		CWW3	25
C	RECEIVER HEIGHT 275-299	CWW3	26
	EQUIVALENCE (W(275),RMODEL),(W(276),RFORM),(W(277),RID)	CWW3	27
C		CWW3	28
C	TOPOGRAPHY 300-324	CWW3	29
	EQUIVALENCE (W(300),GMODEL),(W(301),GFORM),(W(302),GID)	CWW3	30
C		CWW3	31
C	DELTA TOPOGRAPHY 325-349	CWW3	32
	EQUIVALENCE (W(325),GUMODEL),(W(326),GUFORM),(W(327),GUID)	CWW3	33
C		CWW3	34
C	UPPER SURFACE TOPOGRAPHY 350-374	CWW3	35
	EQUIVALENCE (W(350),SMODEL),(W(351),SFORM),(W(352),SID)	CWW3	36
C		CWW3	37
C	PLOT ENHANCEMENTS CONTROL PARAMETERS	CWW3	38

C	EQUIVALENCE (W(490),XFQMDL), (W(491),YFQMDL)	CWW3 39
	ABSORPTION 500-524	CWW3 40
C	EQUIVALENCE (W(500),AMODEL), (W(501),AFORM), (W(502),AID)	CWW3 41
C	DELTA ABSORPTION 525-549	CWW3 42
C	EQUIVALENCE (W(525),DAMODEL), (W(526),DAFORM), (W(527),DAID)	CWW3 43
C	PRESSURE 550-574	CWW3 44
C	EQUIVALENCE (W(550),PMODEL), (W(551),PFORM), (W(552),PID)	CWW3 45
C	DELTA PRESSURE 575-599	CWW3 46
C	EQUIVALENCE (W(575),DPMODEL), (W(576),DPFORM), (W(577),DPID)	CWW3 47
C	EQUIVALENCE (GCZAMP,W(303))	CWW3 48
	EQUIVALENCE (GCLAMZ,W(304)) , (GCTHDL,W(305))	CWW3 49
	EQUIVALENCE (GCBASE,W(306))	CWW3 50
C	DATA RECOGG/4.0/	CWW3 51
	DATA GMX/1/	GLOREN18
	DATA GNTBL/1,11,8*0/	GLOREN19
	DATA GITBL/1,9*0/	GLOREN20
	DATA GFRMTBL/1,9*0/	GLOREN21
C	ENTRY ITOPOG	GLOREN22
C	IF(RECOGG .NE. GMODEL)	GRENZBL2
1	CALL RERROR('GROUND ', 'WRNG MODEL', RECOGG)	GRENZBL3
	MODG(1)=7HGLorenz	GRENZBL4
	MODG(2)=GID	GRENZBL5
C	GCTH0=PID2-GCLAMZ	GLOREN25
	GCINV=1.0/GCTHDL	GLOREN26
	CALL IPTOPOG	GLOREN27
	RETURN	GLOREN28
C	ENTRY TOPOG	GLOREN29
C	CALL CLEAR(PGRTH,7)	GLOREN30
C	ETA=(TH-GCTH0)*GCINV	GLOREN31
	ETA2=ETA*ETA	GLOREN32
	GBINOM=1.0/(1.0 + ETA2)	GLOREN33
	Z=GCZAMP*GBINOM	GLOREN34
	G=R-EARTH-R-Z-GCBASE	GLOREN35
C	PGR=1.0	GLOREN36
	GBINOMB=GBINOM*GCINV	GLOREN37
	PGTH=2.0*Z*ETA*GBINOMB	GLOREN38
	PGTHTH=2.0*Z*GBINOMB*GBINOMB*(1.0-3.0*ETA2)	GLOREN39
C	RETURN	GLOREN40
	END	GLOREN41
		GLOREN42
		GLOREN43
		GLOREN44
		GLOREN45
		GLOREN46
		GLOREN47
		GLOREN48
		GLOREN49
		GLOREN50
		GLOREN51
		GLOREN52
		GLOREN53
		GLOREN54
		GLOREN55

	SUBROUTINE GTANH	GTANH 8
C	TERRAIN PROFILE REPRESENTED BY A SEQUENCE OF LINEAR SEGMENTS	GTANH 9
C	SMOOTHLY JOINED BY HYPERBOLIC FUNCTIONS. PARAMETERS ARE INPUT	GTANH 10
C	AS TABULAR DATA WITH SLOPES COMPUTED FROM TERRAIN DATA.	GTANH 11
C	COMMON DECK "CONST" INSERTED HERE	CCONST 2
	COMMON/PCONST/CREF, RGAS, GAMMA	CCONST 4
	COMMON/MCONST/PI, PIT2, PID2, DEGS, RAD, ALN10	CCONST 5
C	TERRAIN MODEL	GTANH 13
	REAL C(49), LAM0, LMI, LMIM1, LM(49), DL(49), ALC(50)	GTANH 14
C	COMMON DECK "RKAM" INSERTED HERE	RKAMCOM2
	REAL KR, KTH, KPH	RKAMCOM4
	COMMON//R, TH, PH, KR, KTH, KPH, RKVARS(14), TPULSE, CSTEP, DRDT(20)	RKAMCOM5
C	COMMON DECK "GG" INSERTED HERE	CGG 2
	REAL MODG	CGG 4
	COMMON/GG/MODG(4)	CGG 5
	COMMON/GG/G, PGR, PGRR, PGRTH, PGRPH	CGG 6
	COMMON/GG/PGTH, PGPH, PGTHTH, PGPHPH, PGTHPH, GSELECT, GTIME	CGG 7
C	COMMON DECK "B9" INSERTED HERE	CB8 2
	INTEGER GMX, GNTBL, GITBL, GFRMTBL, IDSG(10)	CB8 4
	COMMON/B9/GMX, GNTBL(10), GITBL(10), GFRMTBL(10), GGP(113)	CB8 5
	EQUIVALENCE (GGP, IDSG), (ANG, GGP(11))	CB8 6
C	COMMON DECK "WW" INSERTED HERE	CWW 2
	PARAMETER (NWARSZ=1000)	CWW1 3
	COMMON/WW/ID(10), MAXW, W(NWARSZ)	CWW1 4
	REAL MAXSTP, MAXERR, INTYP, LLAT, LLON	CWW2 2
	EQUIVALENCE (EARTH, W(1)), (RAY, W(2)), (XMTRH, W(3)), (TLAT, W(4)),	CWW2 3
	1 (TLON, W(5)), (OW, W(6)), (FBEG, W(7)), (FEND, W(8)), (FSTEP, W(9)),	CWW2 4
	2 (AZ1, W(10)), (AZBEG, W(11)), (AZEND, W(12)), (AZSTEP, W(13)),	CWW2 5
	3 (BETA, W(14)), (ELBEG, W(15)), (ELEND, W(16)), (ELSTEP, W(17)),	CWW2 6
	8 (RCVRH, W(20)),	CWW2 7
	4 (ONLY, W(21)), (HOP, W(22)), (MAXSTP, W(23)), (PLAT, W(24)), (PLON, W(25))	CWW2 8
	5, (HMAX, W(26)), (RAYFNC, W(29)), (EXTINC, W(33)),	CWW2 9
	6 (HMIN, W(27)), (RGMAX, W(28)),	CWW2 10
	8 (INTYP, W(41)), (MAXERR, W(42)), (ERATIO, W(43)),	CWW2 11
	6 (STEP1, W(44)), (STPMAX, W(45)), (STPMIN, W(46)), (FACTR, W(47)),	CWW2 12
	7 (SKIP, W(71)), (RAYSET, W(72)), (PRTSRP, W(74)), (HITLET, W(75))	CWW2 13
	9, (BINRAY, W(76)), (PAGLN, W(77)), (PLT, W(81)), (PFACTR, W(82)),	CWW2 14
	1 (LLAT, W(83)), (LLON, W(84)), (RLAT, W(85)), (RLON, W(86))	CWW2 15
	2, (TIC, W(87)), (HB, W(88)), (HT, W(89)), (TICV, W(96))	CWW2 16
	REAL MMODEL, MFORM, MID	CWW3 2
C		CWW3 3
C	WIND 100-124	CWW3 4
	EQUIVALENCE (W(100), UMODEL), (W(101), UFORM), (W(102), UID)	CWW3 5
C		CWW3 6
C	DELTA WIND 125-149	CWW3 7
	EQUIVALENCE (W(125), DUMODEL), (W(126), DUFORM), (W(127), DUID)	CWW3 8
C		CWW3 9
C	SOUND SPEED 150-174	CWW3 10
	EQUIVALENCE (W(150), CMODEL), (W(151), CFORM), (W(152), CID)	CWW3 11
	EQUIVALENCE (W(153), REFC)	CWW3 12
C		CWW3 13
C	DELTA SOUND SPEED 175-199	CWW3 14

C	EQUIVALENCE (W(175),DCMODEL), (W(176),DCFORM), (W(177),DCID)	CWW3	15
C	TEMPERATURE 200-224	CWW3	16
C	EQUIVALENCE (W(200),TMODEL), (W(201),TFORM), (W(202),TID)	CWW3	17
C		CWW3	18
C	DELTA TEMPERATURE 225-249	CWW3	19
C	EQUIVALENCE (W(225),DTMODEL), (W(226),DTFORM), (W(227),DTID)	CWW3	20
C		CWW3	21
C	MOLECULAR 250-274	CWW3	22
C	EQUIVALENCE (W(250),MMODEL), (W(251),MFORM), (W(252),MID)	CWW3	23
C		CWW3	24
C	RECEIVER HEIGHT 275-299	CWW3	25
C	EQUIVALENCE (W(275),RMODEL), (W(276),RFORM), (W(277),RID)	CWW3	26
C		CWW3	27
C	TOPOGRAPHY 300-324	CWW3	28
C	EQUIVALENCE (W(300),GMODEL), (W(301),GFORM), (W(302),GID)	CWW3	29
C		CWW3	30
C	DELTA TOPOGRAPHY 325-349	CWW3	31
C	EQUIVALENCE (W(325),GUMODEL), (W(326),GUFORM), (W(327),GUID)	CWW3	32
C		CWW3	33
C	UPPER SURFACE TOPOGRAPHY 350-374	CWW3	34
C	EQUIVALENCE (W(350),SMODEL), (W(351),SFORM), (W(352),SID)	CWW3	35
C	PLOT ENHANCEMENTS CONTROL PARAMETERS	CWW3	36
C		CWW3	37
C	EQUIVALENCE (W(490),XFQMDL), (W(491),YFQMDL)	CWW3	38
C	ABSORPTION 500-524	CWW3	39
C	EQUIVALENCE (W(500),AMODEL), (W(501),AFORM), (W(502),AID)	CWW3	40
C		CWW3	41
C	DELTA ABSORPTION 525-549	CWW3	42
C	EQUIVALENCE (W(525),DAMODEL), (W(526),DAFORM), (W(527),DAID)	CWW3	43
C		CWW3	44
C	PRESSURE 550-574	CWW3	45
C	EQUIVALENCE (W(550),PMODEL), (W(551),PFORM), (W(552),PID)	CWW3	46
C		CWW3	47
C	DELTA PRESSURE 575-599	CWW3	48
C	EQUIVALENCE (W(575),DPMODEL), (W(576),DPFORM), (W(577),DPID)	CWW3	49
C		CWW3	50
C	EQUIVALENCE (LAMO,GGP(12)), (ZO,GGP(62)), (DLO,GGP(112))	CWW3	51
C	EQUIVALENCE (LM,GGP(13)), (C,GGP(63)), (DL,GGP(113))	GTANH	19
C		GTANH	20
C	DATA RECOGG/3.0/	GTANH	21
C	DATA ANG/0.0/	GTANH	22
C	DATA GMX/2/	GNHBL	2
C	DATA GNTBL/1,11,162,7*0/	GNHBL	3
C	DATA GITBL/1,50,8*0/	GNHBL	4
C	DATA GFRMTBL/1,2,8*0/	GNHBL	5
C		GNHBL	6
C	ENTRY ITOPOG	GTANH	25
C		GTANH	26
C	CALL IPTOPOG	GTANH	27
C		GTANH	28
C	IF HAD PREVIOUS CALL BUT NOTHING THIS TIME, EXIT NOW	GTANH	29
C	RETAINING PREVIOUS TABULAR DATA COUNT	GTANH	30
C	IF(N.GT.0 .AND. ANG.EQ.0.0) RETURN	GTANH	31
C		GTANH	32
C		GTANH	33

	IF(RECOGG .NE. GMODEL)	GTANH 34
	1 CALL RERROR('TOPO ', 'WRNG MODEL', RECOGG)	GTANH 35
	MODG(1)=5HG TANH	GTANH 36
	MODG(2)=GID	GTANH 37
	N=ANG/3	GTANH 38
	IF(ANG.NE.3*N.OR.N.LE.0)	GTANH 39
	1 CALL RERROR('GTANH', 'BAD NUMBER', ANG+2.0)	GTANH 40
	N=N-2	GTANH 41
	ANG=0.0	GTANH 42
C		GTANH 43
C		GTANH 44
C	CONVERT 'Z' ARRAY INPUT(OVERLAYS 'C' ARRAY) TO 'C' ARRAY	GTANH 45
		GTANH 46
	ZM1=Z0	GTANH 47
	LAM0=PID2-LAM0	GTANH 48
	LMIM1=LAM0	GTANH 49
	NP1=N+1	GTANH 50
	DO 10 I=1, NP1	GTANH 51
	Z=C(I)	GTANH 52
	LMI=PID2-LM(I)	GTANH 53
	LM(I)=LMI	GTANH 54
	ALC(I)=ALCOSH((LMI-LAM0) / DL(I))	GTANH 55
	C(I)=(Z-ZM1)/(LMI-LMIM1)	GTANH 56
	ZM1=Z	GTANH 57
10	LMIM1=LMI	GTANH 58
C		GTANH 59
	RETURN	GTANH 60
C		GTANH 61
	ENTRY TOPOG	GTANH 62
C		GTANH 63
	IF(N.LE.0)	GTANH 64
C	1 CALL RERROR('GTANH', 'BAD N VALUE', FLOAT(N))	GTANH 65
		GTANH 66
	SUM = 0.	GTANH 67
	DO 1 I = 1, N	GTANH 68
1	SUM = SUM + DL(I) * (C(I + 1) - C(I)) / 2. * (ALCOSH(((TH-LM	GTANH 69
	1(I)) / DL(I))) - ALC(I))	GTANH 70
	Z = Z0 - SUM + (C(1) + C(N + 1)) * (TH-LAM0) / 2.	GTANH 71
	G=R-EARTH-R-Z	GTANH 72
	PGR=1.0	GTANH 73
C		GTANH 74
	PGTH = C(1)	GTANH 75
	DO 2 I = 1, N	GTANH 76
2	PGTH= PGTH+ (C(I + 1) - C(I)) / 2. * (1. + TANH ((LM(I)- TH) /DL	GTANH 77
	1 (I)))	GTANH 78
	PGTH=-PGTH	GTANH 79
	PGTHTH=0.0	GTANH 80
	DO 3 I=1,N	GTANH 81
3	PGTHTH=PGTHTH+	GTANH 82
	1 (C(I+1)-C(I))/2.*(1.0-TANH((LM(I)-TH)/DL(I))**2)/DL(I)	GTANH 83
C		GTANH 84
	CALL PTOPOG	GTANH 85
	RETURN	GTANH 86
	END	GTANH 87

	SUBROUTINE NPTErr	NPTErr 8
C	DO-NOTHING TERRAIN PERTURBATION MODEL	NPTErr 9
C	COMMON DECK "GG" INSERTED HERE	CGG 2
	REAL MODG	CGG 4
	COMMON/GG/MODG(4)	CGG 5
	COMMON/GG/G, PGR, PGRR, PGRTH, PGRPH	CGG 6
	COMMON/GG/PGTH, PGP, PGTHTH, PGP, PGTHPH, PGTHPH, GSELECT, GTIME	CGG 7
C		NPTErr11
C	COMMON DECK "B10" INSERTED HERE	CB9 2
	INTEGER DGMX, DGNTBL, DGITBL, DGFRMTB, IDSDG(10)	CB9 4
	COMMON/B10/DGMX, DGNTBL(10), DGITBL(10), DGFRMTB(10), DGGP(10)	CB9 5
	EQUIVALENCE (DGGP, IDSDG)	CB9 6
C		NPTErr13
	DATA DGMX/1/	NERRBL 2
	DATA DGNTBL/1, 11, 8*0/	NERRBL 3
	DATA DGITBL/1, 9*0/	NERRBL 4
	DATA DGFRMTB/1, 9*0/	NERRBL 5
C		NPTErr16
	ENTRY IPTOPOG	NPTErr17
C		NPTErr18
	MODG(3)=6HNPTErr	NPTErr19
	ENTRY PTOPOG	NPTErr20
	END	NPTErr21

	SUBROUTINE MUARDC	MUARDC 8
C	ARDC BACKGROUND ABSORPTION FORMULA	MUARDC 9
C		MUARDC10
C	COMMON DECK "WW" INSERTED HERE	CWW 2
	PARAMETER (NWARSZ=1000)	CWW1 3
	COMMON/WW/ID(10), MAXW, W(NWARSZ)	CWW1 4
	REAL MAXSTP, MAXERR, INTYP, LLAT, LLON	CWW2 2
	EQUIVALENCE (EARTH, W(1)), (RAY, W(2)), (XMTRH, W(3)), (TLAT, W(4)),	CWW2 3
	1 (TLON, W(5)), (OW, W(6)), (FBEG, W(7)), (FEND, W(8)), (FSTEP, W(9)),	CWW2 4
	2 (AZ1, W(10)), (AZBEG, W(11)), (AZEND, W(12)), (AZSTEP, W(13)),	CWW2 5
	3 (BETA, W(14)), (ELBEG, W(15)), (ELEND, W(16)), (ELSTEP, W(17)),	CWW2 6
	8 (RCVRH, W(20)),	CWW2 7
	4 (ONLY, W(21)), (HOP, W(22)), (MAXSTP, W(23)), (PLAT, W(24)), (PLON, W(25))	CWW2 8
	5, (HMAX, W(26)), (RAYFNC, W(29)), (EXTINC, W(33)),	CWW2 9
	6 (HMIN, W(27)), (RGMAX, W(28)),	CWW2 10
	8 (INTYP, W(41)), (MAXERR, W(42)), (ERATIO, W(43)),	CWW2 11
	6 (STEP1, W(44)), (STPMAX, W(45)), (STPMIN, W(46)), (FACTR, W(47)),	CWW2 12
	7 (SKIP, W(71)), (RAYSET, W(72)), (PRTSRP, W(74)), (HITLET, W(75))	CWW2 13
	9, (BINRAY, W(76)), (PAGLN, W(77)), (PLT, W(81)), (PFACTR, W(82)),	CWW2 14
	1 (LLAT, W(83)), (LLON, W(84)), (RLAT, W(85)), (RLON, W(86))	CWW2 15
	2, (TIC, W(87)), (HB, W(88)), (HT, W(89)), (TICV, W(96))	CWW2 16
	REAL MMODEL, MFORM, MID	CWW3 2
C		CWW3 3

C	WIND	100-124		CWW3	4
	EQUIVALENCE	(W(100), UMODEL), (W(101), UFORM), (W(102), UID)		CWW3	5
C	DELTA WIND	125-149		CWW3	6
	EQUIVALENCE	(W(125), DUMODEL), (W(126), DUFORM), (W(127), DUID)		CWW3	7
C	SOUND SPEED	150-174		CWW3	8
	EQUIVALENCE	(W(150), CMODEL), (W(151), CFORM), (W(152), CID)		CWW3	9
	EQUIVALENCE	(W(153), REFC)		CWW3	10
C	DELTA SOUND SPEED	175-199		CWW3	11
	EQUIVALENCE	(W(175), DCMODEL), (W(176), DCFORM), (W(177), DCID)		CWW3	12
C	TEMPERATURE	200-224		CWW3	13
	EQUIVALENCE	(W(200), TMODEL), (W(201), TFORM), (W(202), TID)		CWW3	14
C	DELTA TEMPERATURE	225-249		CWW3	15
	EQUIVALENCE	(W(225), DTMODEL), (W(226), DTFORM), (W(227), DTID)		CWW3	16
C	MOLECULAR	250-274		CWW3	17
	EQUIVALENCE	(W(250), MMODEL), (W(251), MFORM), (W(252), MID)		CWW3	18
C	RECEIVER HEIGHT	275-299		CWW3	19
	EQUIVALENCE	(W(275), RMODEL), (W(276), RFORM), (W(277), RID)		CWW3	20
C	TOPOGRAPHY	300-324		CWW3	21
	EQUIVALENCE	(W(300), GMODEL), (W(301), GFORM), (W(302), GID)		CWW3	22
C	DELTA TOPOGRAPHY	325-349		CWW3	23
	EQUIVALENCE	(W(325), GUMODEL), (W(326), GUFORM), (W(327), GUID)		CWW3	24
C	UPPER SURFACE TOPOGRAPHY	350-374		CWW3	25
	EQUIVALENCE	(W(350), SMODEL), (W(351), SFORM), (W(352), SID)		CWW3	26
C	PLOT ENHANCEMENTS CONTROL PARAMETERS			CWW3	27
	EQUIVALENCE	(W(490), XFQMDL), (W(491), YFQMDL)		CWW3	28
C	ABSORPTION	500-524		CWW3	29
	EQUIVALENCE	(W(500), AMODEL), (W(501), AFORM), (W(502), AID)		CWW3	30
C	DELTA ABSORPTION	525-549		CWW3	31
	EQUIVALENCE	(W(525), DAMODEL), (W(526), DAFORM), (W(527), DAID)		CWW3	32
C	PRESSURE	550-574		CWW3	33
	EQUIVALENCE	(W(550), PMODEL), (W(551), PFORM), (W(552), PID)		CWW3	34
C	DELTA PRESSURE	575-599		CWW3	35
	EQUIVALENCE	(W(575), DPMODEL), (W(576), DPFORM), (W(577), DPID)		CWW3	36
C				CWW3	37
	EQUIVALENCE	(W(503), BETAV), (W(504), SUTH), (W(505), PRNDTL)		CWW3	38
C	COMMON DECK "RINREAL" INSERTED HERE			CWW3	39
	LOGICAL SPACE			CWW3	40
	REAL LPOLAR, LPOLRI, KPHK, KPHKI, KAY2, KAY2I			CWW3	41
	CHARACTER DISPM*6			CWW3	42
				CWW3	43
				CWW3	44
				CWW3	45
				CWW3	46
				CWW3	47
				CWW3	48
				CWW3	49
				CWW3	50
				CWW3	51
				MUARDC12	
				MUARDC13	
				MUARDC14	
				CRINREA2	
				CRINREA4	
				CRINREA5	
				CRINREA6	

	COMMON/RINPL/DISPM	CRINREA7
	COMMON /RIN/ MODRIN(8) ,RAYNAME(2,3) ,TYPE(3) ,SPACE	CRINREA8
	COMMON/RIN/OMEGMIN,OMEGMAX,KAY2,KAY2I,	CRINREA9
	1 H,HI,PHT,PHTI,PHR,PHRI,PHTH,PHTHI,PHPH,PHPHI	CRINRE10
	2, PHOW,PHOWI,PHKR,PHKRI,PHKTH,PHKTI, PHKPH,PHKPI	CRINRE11
	3 ,KPHK,KPHKI,POLAR,POLARI,LPOLAR,LPOLRI,SGN	CRINRE12
C	COMMON DECK "CONST" INSERTED HERE	CCONST 2
	COMMON/PCONST/CREG,RGAS,GAMMA	CCONST 4
	COMMON/MCONST/PI,PIT2,PID2,DEGS,RAD,ALN10	CCONST 5
C	COMMON DECK "TT" INSERTED HERE	CTT 2
	REAL MODT	CTT 4
	COMMON/TT/MODT(4) , T,PTT,PTR,PPTH,PTPH	CTT 5
C	COMMON DECK "AA" INSERTED HERE	CAA 2
	REAL MODA	CAA 4
	REAL MU,MUPT,MUPR,MUPH,MUPPH	CAA 5
	REAL KAP,KAPPT,KAPPR,KAPPTH,KAPPPH	CAA 6
	COMMON/AA/MODA(4) ,MU,MUPT,MUPR,MUPH,MUPPH	CAA 7
	COMMON/AA/KAP,KAPPT,KAPPR,KAPPTH,KAPPPH	CAA 8
C		MUARDC19
C	COMMON DECK "MM" INSERTED HERE	CMM 2
	REAL M,MODM	CMM 4
	COMMON/MM/MODM(4) ,M,PMT,PMR,PMTH,PMPH	CMM 5
C		MUARDC21
C	COMMON DECK "CB17" INSERTED HERE	CB17 2
	INTEGER VMX,VNTBL,VITBL,VFRMTBL,IDSV(10)	CB17 4
	COMMON/B17/VMX,VNTBL(10),VITBL(10),VFRMTBL(10),VGP(53)	CB17 5
	EQUIVALENCE (VGP,IDSV),(ANV,VGP(11))	CB17 6
C		MUARDC23
	DATA VMX/1/	MRDCBL 2
	DATA VNTBL/1,11,8*0/	MRDCBL 3
	DATA VITBL/1,9*0/	MRDCBL 4
	DATA VFRMTBL/1,9*0/	MRDCBL 5
	DATA RECOGA/1.0/	MUARDC26
C		MUARDC27
	ENTRY IABSRP	MUARDC28
	IF(RECOGA .NE. AMODEL)	MUARDC29
	1 CALL RERROR('ABSRP ','WRNG MODEL',RECOGA)	MUARDC30
	MODA(1)=6HMUARDC	MUARDC31
	MODA(2)=AID	MUARDC32
C	SET ALL VICOSITY/CONDUCTIVITY VALUES TO ZERO	MUARDC33
C	INITIALLY	MUARDC34
	CALL CLEAR(MU,10)	MUARDC35
	CALL IPABSRP	MUARDC36
	RETURN	MUARDC37
C		MUARDC38
	ENTRY ABSRP	MUARDC39
	MU=BETAV*T**1.5/(SUTH+T)	MUARDC40
	KAP=GAMMA*RGAS*MU/((GAMMA-1.0)*M*PRNDTL)	MUARDC41
	CALL PABSRP	MUARDC42
	END	MUARDC43

	SUBROUTINE NPABSR	NPABSR 8
C	DO-NOTHING ABSORPTION PERTURBATION MODEL	NPABSR 9
C	COMMON DECK "WW" INSERTED HERE	CWW 2
	PARAMETER (NWARSZ=1000)	CWW1 3
	COMMON/WW/ID(10),MAXW,W(NWARSZ)	CWW1 4
	REAL MAXSTP,MAXERR,INTYP,LLAT,LLON	CWW2 2
	EQUIVALENCE (EARTH, W(1)), (RAY, W(2)), (XMTRH, W(3)), (TLAT, W(4)),	CWW2 3
	1 (TLON, W(5)), (OW, W(6)), (FBEG, W(7)), (FEND, W(8)), (FSTEP, W(9)),	CWW2 4
	2 (AZ1, W(10)), (AZBEG, W(11)), (AZEND, W(12)), (AZSTEP, W(13)),	CWW2 5
	3 (BETA, W(14)), (ELBEG, W(15)), (ELEND, W(16)), (ELSTEP, W(17)),	CWW2 6
	8 (RCVRH, W(20)),	CWW2 7
	4 (ONLY, W(21)), (HOP, W(22)), (MAXSTP, W(23)), (PLAT, W(24)), (PLON, W(25))	CWW2 8
	5, (HMAX, W(26)), (RAYFNC, W(29)), (EXTINC, W(33)),	CWW2 9
	6 (HMIN, W(27)), (RGMAX, W(28)),	CWW2 10
	8 (INTYP, W(41)), (MAXERR, W(42)), (ERATIO, W(43)),	CWW2 11
	6 (STEP1, W(44)), (STPMAX, W(45)), (STPMIN, W(46)), (FACTR, W(47)),	CWW2 12
	7 (SKIP, W(71)), (RAYSET, W(72)), (PRTSRP, W(74)), (HITLET, W(75))	CWW2 13
	9, (BINRAY, W(76)), (PAGLN, W(77)), (PLT, W(81)), (PFACTR, W(82)),	CWW2 14
	1 (LLAT, W(83)), (LLON, W(84)), (RLAT, W(85)), (RLON, W(86))	CWW2 15
	2, (TIC, W(87)), (HB, W(88)), (HT, W(89)), (TICV, W(96))	CWW2 16
	REAL MMODEL, MFORM, MID	CWW3 2
C		CWW3 3
C	WIND 100-124	CWW3 4
	EQUIVALENCE (W(100), UMODEL), (W(101), UFORM), (W(102), UID)	CWW3 5
C		CWW3 6
C	DELTA WIND 125-149	CWW3 7
	EQUIVALENCE (W(125), DUMODEL), (W(126), DUFORM), (W(127), DUID)	CWW3 8
C		CWW3 9
C	SOUND SPEED 150-174	CWW3 10
	EQUIVALENCE (W(150), CMODEL), (W(151), CFORM), (W(152), CID)	CWW3 11
	EQUIVALENCE (W(153), REFC)	CWW3 12
C		CWW3 13
C	DELTA SOUND SPEED 175-199	CWW3 14
	EQUIVALENCE (W(175), DCMODEL), (W(176), DCFORM), (W(177), DCID)	CWW3 15
C		CWW3 16
C	TEMPERATURE 200-224	CWW3 17
	EQUIVALENCE (W(200), TMODEL), (W(201), TFORM), (W(202), TID)	CWW3 18
C		CWW3 19
C	DELTA TEMPERATURE 225-249	CWW3 20
	EQUIVALENCE (W(225), DTMODEL), (W(226), DTFORM), (W(227), DTID)	CWW3 21
C		CWW3 22
C	MOLECULAR 250-274	CWW3 23
	EQUIVALENCE (W(250), MMODEL), (W(251), MFORM), (W(252), MID)	CWW3 24
C		CWW3 25
C	RECEIVER HEIGHT 275-299	CWW3 26
	EQUIVALENCE (W(275), RMODEL), (W(276), RFORM), (W(277), RID)	CWW3 27
C		CWW3 28
C	TOPOGRAPHY 300-324	CWW3 29
	EQUIVALENCE (W(300), GMODEL), (W(301), GFORM), (W(302), GID)	CWW3 30
C		CWW3 31
C	DELTA TOPOGRAPHY 325-349	CWW3 32
	EQUIVALENCE (W(325), GUMODEL), (W(326), GUFORM), (W(327), GUID)	CWW3 33
C		CWW3 34
C	UPPER SURFACE TOPOGRAPHY 350-374	CWW3 35
	EQUIVALENCE (W(350), SMODEL), (W(351), SFORM), (W(352), SID)	CWW3 36

C	PLOT ENHANCEMENTS CONTROL PARAMETERS	CWW3	37
C		CWW3	38
	EQUIVALENCE (W(490),XFQMDL), (W(491),YFQMDL)	CWW3	39
C	ABSORPTION 500-524	CWW3	40
	EQUIVALENCE (W(500),AMODEL), (W(501),AFORM), (W(502),AID)	CWW3	41
C		CWW3	42
C	DELTA ABSORPTION 525-549	CWW3	43
	EQUIVALENCE (W(525),DAMODEL), (W(526),DAFORM), (W(527),DAID)	CWW3	44
C		CWW3	45
C	PRESSURE 550-574	CWW3	46
	EQUIVALENCE (W(550),PMODEL), (W(551),PFORM), (W(552),PID)	CWW3	47
C		CWW3	48
C	DELTA PRESSURE 575-599	CWW3	49
	EQUIVALENCE (W(575),DPMODEL), (W(576),DPFORM), (W(577),DPID)	CWW3	50
C		CWW3	51
C	COMMON DECK "AA" INSERTED HERE	CAA	2
	REAL MODA	CAA	4
	REAL MU, MUPT, MUPR, MUPTH, MUPPH	CAA	5
	REAL KAP, KAPPT, KAPPR, KAPPTH, KAPPPH	CAA	6
	COMMON/AA/MODA(4), MU, MUPT, MUPR, MUPTH, MUPPH	CAA	7
	COMMON/AA/KAP, KAPPT, KAPPR, KAPPTH, KAPPPH	CAA	8
C		NPABSR12	
C	COMMON DECK "CB18" INSERTED HERE	CB18	2
	INTEGER DVMX, DVNTBL, DVITBL, DVFRMTB, IDSDV(10)	CB18	4
	COMMON/B18/DVMX, DVNTBL(10), DVITBL(10), DVFRMTB(10), DVGP(11)	CB18	5
	EQUIVALENCE (DVGP, IDSDV), (ANDV, DVGP(11))	CB18	6
C		NPABSR14	
	DATA DVMX/1/	NBSRBL	2
	DATA DVNTBL/1,11,8*0/	NBSRBL	3
	DATA DVITBL/1,9*0/	NBSRBL	4
	DATA DVFRMTB/1,9*0/	NBSRBL	5
C		NPABSR17	
	DATA RECOGDA/0.0/	NPABSR18	
C		NPABSR19	
	ENTRY IPABSRP	NPABSR20	
	IF(RECOGDA .NE. DAMODEL)	NPABSR21	
1	CALL ERROR('DABSRP ', 'WRNG MODEL', RECOGDA)	NPABSR22	
	MODA(3)=6HNPABSR	NPABSR23	
	MODA(4)=DAID	NPABSR24	
	RETURN	NPABSR25	
C		NPABSR26	
	ENTRY PABSRP	NPABSR27	
	RETURN	NPABSR28	
	END	NPABSR29	
	SUBROUTINE PEXP	PEXP	8
C		PEXP	9
C	SCALE HEIGHT PRESSURE MODEL	PEXP	10
C		PEXP	11
C	COMMON DECK "WW" INSERTED HERE	CWW	2
	PARAMETER (NWAR SZ=1000)	CWW1	3

	COMMON/WW/ID(10),MAXW,W(NWARSZ)		
	REAL MAXSTP,MAXERR,INTYP,LLAT,LLON	CWW1	4
	EQUIVALENCE (EARTH, W(1)), (RAY, W(2)), (XMTRH, W(3)), (TLAT, W(4)),	CWW2	2
1	(TLON, W(5)), (OW, W(6)), (FBEG, W(7)), (FEND, W(8)), (FSTEP, W(9)),	CWW2	3
2	(AZ1, W(10)), (AZBEG, W(11)), (AZEND, W(12)), (AZSTEP, W(13)),	CWW2	4
3	(BETA, W(14)), (ELBEG, W(15)), (ELEND, W(16)), (ELSTEP, W(17)),	CWW2	5
8	(RCVRH, W(20)),	CWW2	6
4	(ONLY, W(21)), (HOP, W(22)), (MAXSTP, W(23)), (PLAT, W(24)), (PLON, W(25))	CWW2	7
5	, (HMAX, W(26)), (RAYFNC, W(29)), (EXTINC, W(33)),	CWW2	8
6	(HMIN, W(27)), (RGMAX, W(28)),	CWW2	9
8	(INTYP, W(41)), (MAXERR, W(42)), (ERATIO, W(43)),	CWW2	10
6	(STEP1, W(44)), (STPMAX, W(45)), (STPMIN, W(46)), (FACTR, W(47)),	CWW2	11
7	(SKIP, W(71)), (RAYSET, W(72)), (PRTSRP, W(74)), (HITLET, W(75))	CWW2	12
9	, (BINRAY, W(76)), (PAGLN, W(77)), (PLT, W(81)), (PFACTR, W(82)),	CWW2	13
1	(LLAT, W(83)), (LLON, W(84)), (RLAT, W(85)), (RLON, W(86))	CWW2	14
2	, (TIC, W(87)), (HB, W(88)), (HT, W(89)), (TICV, W(96))	CWW2	15
	REAL MMODEL, MFORM, MID	CWW2	16
C		CWW3	2
C	WIND 100-124	CWW3	3
	EQUIVALENCE (W(100), UMODEL), (W(101), UFORM), (W(102), UID)	CWW3	4
C		CWW3	5
C	DELTA WIND 125-149	CWW3	6
	EQUIVALENCE (W(125), DUMODEL), (W(126), DUFORM), (W(127), DUID)	CWW3	7
C		CWW3	8
C	SOUND SPEED 150-174	CWW3	9
	EQUIVALENCE (W(150), CMODEL), (W(151), CFORM), (W(152), CID)	CWW3	10
	EQUIVALENCE (W(153), REFC)	CWW3	11
C		CWW3	12
C	DELTA SOUND SPEED 175-199	CWW3	13
	EQUIVALENCE (W(175), DCMODEL), (W(176), DCFORM), (W(177), DCID)	CWW3	14
C		CWW3	15
C	TEMPERATURE 200-224	CWW3	16
	EQUIVALENCE (W(200), TMODEL), (W(201), TFORM), (W(202), TID)	CWW3	17
C		CWW3	18
C	DELTA TEMPERATURE 225-249	CWW3	19
	EQUIVALENCE (W(225), DTMODEL), (W(226), DTFORM), (W(227), DTID)	CWW3	20
C		CWW3	21
C	MOLECULAR 250-274	CWW3	22
	EQUIVALENCE (W(250), MMODEL), (W(251), MFORM), (W(252), MID)	CWW3	23
C		CWW3	24
C	RECEIVER HEIGHT 275-299	CWW3	25
	EQUIVALENCE (W(275), RMODEL), (W(276), RFORM), (W(277), RID)	CWW3	26
C		CWW3	27
C	TOPOGRAPHY 300-324	CWW3	28
	EQUIVALENCE (W(300), GMODEL), (W(301), GFORM), (W(302), GID)	CWW3	29
C		CWW3	30
C	DELTA TOPOGRAPHY 325-349	CWW3	31
	EQUIVALENCE (W(325), GUMODEL), (W(326), GUFORM), (W(327), GUID)	CWW3	32
C		CWW3	33
C	UPPER SURFACE TOPOGRAPHY 350-374	CWW3	34
	EQUIVALENCE (W(350), SMODEL), (W(351), SFORM), (W(352), SID)	CWW3	35
C		CWW3	36
C	PLOT ENHANCEMENTS CONTROL PARAMETERS	CWW3	37
		CWW3	38
	EQUIVALENCE (W(490), XFQMDL), (W(491), YFQMDL)	CWW3	39
C	ABSORPTION 500-524	CWW3	40

	EQUIVALENCE (W(500),AMODEL), (W(501),AFORM), (W(502),AID)	CWW3	41
C		CWW3	42
C	DELTA ABSORPTION           525-549	CWW3	43
	EQUIVALENCE (W(525),DAMODEL), (W(526),DAFORM), (W(527),DAID)	CWW3	44
C		CWW3	45
C	PRESSURE                   550-574	CWW3	46
	EQUIVALENCE (W(550),PMODEL), (W(551),PFORM), (W(552),PID)	CWW3	47
C		CWW3	48
C	DELTA PRESSURE            575-599	CWW3	49
	EQUIVALENCE (W(575),DPMODEL), (W(576),DPFORM), (W(577),DPID)	CWW3	50
C		CWW3	51
C	COMMON DECK "RKAM" INSERTED HERE	RKAMCOM2	
	REAL KR, KTH, KPH	RKAMCOM4	
	COMMON//R, TH, PH, KR, KTH, KPH, RKVARS(14), TPULSE, CSTEP, DRDT(20)	RKAMCOM5	
C	COMMON DECK "CONST" INSERTED HERE	CCONST	2
	COMMON/PCONST/CREF, RGAS, GAMMA	CCONST	4
	COMMON/MCONST/PI, PIT2, PID2, DEGS, RAD, ALN10	CCONST	5
C	COMMON DECK "PP" INSERTED HERE	CPP	2
	REAL MODP	CPP	4
	COMMON/PP/MODP(4), P, PPT, PPR, PPTH, PPPH	CPP	5
C	COMMON DECK "TT" INSERTED HERE	CTT	2
	REAL MODT	CTT	4
	COMMON/TT/MODT(4), T, PTT, PTR, PTH, PTPH	CTT	5
C	COMMON DECK "MM" INSERTED HERE	CMM	2
	REAL M, MODM	CMM	4
	COMMON/MM/MODM(4), M, PMT, PMR, PMTH, PMPH	CMM	5
C		PEXP	18
	EQUIVALENCE (W(553),P0), (W(554),HSCALE)	PEXP	19
C		PEXP	20
C	COMMON DECK "CB19" INSERTED HERE	CB19	2
	INTEGER PRMX, PRNTBL, PRITBL, PRFRMTB, IDSPR(10)	CB19	4
	COMMON/B19/PRMX, PRNTBL(10), PRITBL(10), PRFRMTB(10), PRGP(11)	CB19	5
	EQUIVALENCE (PRGP, IDSPR), (ANP, PRGP(11))	CB19	6
C		PEXP	22
	DATA PRMX/1/	PPBL	2
	DATA PRNTBL/1,11,8*0/	PPBL	3
	DATA PRITBL/1,9*0/	PPBL	4
	DATA PRFRMTB/1,9*0/	PPBL	5
	DATA RECOGP/1.0/	PEXP	25
C		PEXP	26
	ENTRY IPRES	PEXP	27
	IF(RECOGP .NE. PMODEL)	PEXP	28
1	CALL RERROR('PRESUR ', 'WRNG MODEL', RECOGP)	PEXP	29
	MODP(1)=4HPEXP	PEXP	30
	MODP(2)=PID	PEXP	31
	CALL IPPRES	PEXP	32
	RETURN	PEXP	33
C		PEXP	34
	ENTRY PRES	PEXP	35
	Z=R-EARTH	PEXP	36
	EX=-Z/HSCALE	PEXP	37
	P=P0*EXP(EX)	PEXP	38
	PPT=0.0	PEXP	39
	PPR=P*EX/Z	PEXP	40
	PPTH=0.0	PEXP	41

PPPH=0.0  
 CALL PPRES  
 RETURN  
 END

PEXP 42  
 PEXP 43  
 PEXP 44  
 PEXP 45

	SUBROUTINE NPPRES	NPPRES 8
C	DO-NOTHING PRESSURE PERTURBATION MODEL	NPPRES 9
C	COMMON DECK "WW" INSERTED HERE	CWW 2
	PARAMETER (NWARSZ=1000)	CWW1 3
	COMMON/WW/ID(10),MAXW,W(NWARSZ)	CWW1 4
	REAL MAXSTP,MAXERR,INTYP,LLAT,LLON	CWW2 2
	EQUIVALENCE (EARTH, W(1)), (RAY, W(2)), (XMTRH, W(3)), (TLAT, W(4)),	CWW2 3
	1 (TLON, W(5)), (OW, W(6)), (FBEG, W(7)), (FEND, W(8)), (FSTEP, W(9)),	CWW2 4
	2 (AZ1, W(10)), (AZBEG, W(11)), (AZEND, W(12)), (AZSTEP, W(13)),	CWW2 5
	3 (BETA, W(14)), (ELBEG, W(15)), (ELEND, W(16)), (ELSTEP, W(17)),	CWW2 6
	8 (RCVRH, W(20)),	CWW2 7
	4 (ONLY, W(21)), (HOP, W(22)), (MAXSTP, W(23)), (PLAT, W(24)), (PLON, W(25))	CWW2 8
	5, (HMAX, W(26)), (RAYFNC, W(29)), (EXTINC, W(33)),	CWW2 9
	6 (HMIN, W(27)), (RGMAX, W(28)),	CWW2 10
	8 (INTYP, W(41)), (MAXERR, W(42)), (ERATIO, W(43)),	CWW2 11
	6 (STEP1, W(44)), (STPMAX, W(45)), (STPMIN, W(46)), (FACTR, W(47)),	CWW2 12
	7 (SKIP, W(71)), (RAYSET, W(72)), (PRTSRP, W(74)), (HITLET, W(75))	CWW2 13
	9, (BINRAY, W(76)), (PAGLN, W(77)), (PLT, W(81)), (PFACTR, W(82)),	CWW2 14
	1 (LLAT, W(83)), (LLON, W(84)), (RLAT, W(85)), (RLON, W(86))	CWW2 15
	2, (TIC, W(87)), (HB, W(88)), (HT, W(89)), (TICV, W(96))	CWW2 16
	REAL MMODEL, MFORM, MID	CWW3 2
C		CWW3 3
C	WIND 100-124	CWW3 4
	EQUIVALENCE (W(100), UMODEL), (W(101), UFORM), (W(102), UID)	CWW3 5
C		CWW3 6
C	DELTA WIND 125-149	CWW3 7
	EQUIVALENCE (W(125), DUMODEL), (W(126), DUFORM), (W(127), DUID)	CWW3 8
C		CWW3 9
C	SOUND SPEED 150-174	CWW3 10
	EQUIVALENCE (W(150), CMODEL), (W(151), CFORM), (W(152), CID)	CWW3 11
	EQUIVALENCE (W(153), REFC)	CWW3 12
C		CWW3 13
C	DELTA SOUND SPEED 175-199	CWW3 14
	EQUIVALENCE (W(175), DCMODEL), (W(176), DCFORM), (W(177), DCID)	CWW3 15
C		CWW3 16
C	TEMPERATURE 200-224	CWW3 17
	EQUIVALENCE (W(200), TMODEL), (W(201), TFORM), (W(202), TID)	CWW3 18
C		CWW3 19
C	DELTA TEMPERATURE 225-249	CWW3 20
	EQUIVALENCE (W(225), DTMODEL), (W(226), DTFORM), (W(227), DTID)	CWW3 21
C		CWW3 22
C	MOLECULAR 250-274	CWW3 23
	EQUIVALENCE (W(250), MMODEL), (W(251), MFORM), (W(252), MID)	CWW3 24
C		CWW3 25
C	RECEIVER HEIGHT 275-299	CWW3 26
	EQUIVALENCE (W(275), RMODEL), (W(276), RFORM), (W(277), RID)	CWW3 27

C		CWW3	28
C	TOPOGRAPHY 300-324	CWW3	29
	EQUIVALENCE (W(300),GMODEL),(W(301),GFORM),(W(302),GID)	CWW3	30
C		CWW3	31
C	DELTA TOPOGRAPHY 325-349	CWW3	32
	EQUIVALENCE (W(325),GUMODEL),(W(326),GUFORM),(W(327),GUID)	CWW3	33
C		CWW3	34
C	UPPER SURFACE TOPOGRAPHY 350-374	CWW3	35
	EQUIVALENCE (W(350),SMODEL),(W(351),SFORM),(W(352),SID)	CWW3	36
C	PLOT ENHANCEMENTS CONTROL PARAMETERS	CWW3	37
C		CWW3	38
	EQUIVALENCE (W(490),XFQMDL),(W(491),YFQMDL)	CWW3	39
C	ABSORPTION 500-524	CWW3	40
	EQUIVALENCE (W(500),AMODEL),(W(501),AFORM),(W(502),AID)	CWW3	41
C		CWW3	42
C	DELTA ABSORPTION 525-549	CWW3	43
	EQUIVALENCE (W(525),DAMODEL),(W(526),DAFORM),(W(527),DAID)	CWW3	44
C		CWW3	45
C	PRESSURE 550-574	CWW3	46
	EQUIVALENCE (W(550),PMODEL),(W(551),PFORM),(W(552),PID)	CWW3	47
C		CWW3	48
C	DELTA PRESSURE 575-599	CWW3	49
	EQUIVALENCE (W(575),DPMODEL),(W(576),DPFORM),(W(577),DPID)	CWW3	50
C		CWW3	51
C	COMMON DECK "PP" INSERTED HERE	CPP	2
	REAL MODP	CPP	4
	COMMON/PP/MODP(4),P,PPT,PPR,PPTH,PPPH	CPP	5
C		NPPRES12	
C	COMMON DECK "CB20" INSERTED HERE	CB20	2
	INTEGER DPMX,DPNTBL,DPITBL,DPFRMTB,IDSDP(10)	CB20	4
	COMMON/B20/DPMX,DPNTBL(10),DPITBL(10),DPFRMTB(10),DPGP(11)	CB20	5
	EQUIVALENCE (DPGP,IDSDP),(ANDP,DPGP(11))	CB20	6
C		NPPRES14	
	DATA DPMX/1/	NRESBL	2
	DATA DPNTBL/1,11,8*0/	NRESBL	3
	DATA DPITBL/1,9*0/	NRESBL	4
	DATA DPFRMTB/1,9*0/	NRESBL	5
C		NPPRES17	
	DATA RECOGDP/0.0/	NPPRES18	
C		NPPRES19	
	ENTRY IPPRES	NPPRES20	
	IF(RECOGDP.NE.DPMODEL)	NPPRES21	
1	CALL RERROR('DPPRES ','WRNG MODEL',RECOGDP)	NPPRES22	
	MODP(3)=6HNPPRES	NPPRES23	
	MODP(4)=DPID	NPPRES24	
	RETURN	NPPRES25	
C		NPPRES26	
	ENTRY PPRES	NPPRES27	
	RETURN	NPPRES28	
	END	NPPRES29	

	SUBROUTINE RHORIZ	RHORIZ 8
C	RECEIVER MODEL USING FIXED OFFSET TO EARTH'S SURFACE.	RHORIZ 9
C	COMMON DECK "RR" INSERTED HERE	CRR 2
	REAL MODREC	CRR 4
	COMMON/RR/ MODREC(4)	CRR 5
	COMMON/RR/F, PFR, PFRR, PFRTH, PFRPH	CRR 6
	COMMON/RR/PFTH, PFPH, PFTHTH, PFPHPH, PFTHPH, FSELECT, FTIME	CRR 7
C	COMMON DECK "WW" INSERTED HERE	CWW 2
	PARAMETER (NWARSZ=1000)	CWW1 3
	COMMON/WW/ID(10), MAXW, W(NWARSZ)	CWW1 4
	REAL MAXSTP, MAXERR, INTYP, LLAT, LLON	CWW2 2
	EQUIVALENCE (EARTH, W(1)), (RAY, W(2)), (XMTRH, W(3)), (TLAT, W(4)),	CWW2 3
	1 (TLON, W(5)), (OW, W(6)), (FBEG, W(7)), (FEND, W(8)), (FSTEP, W(9)),	CWW2 4
	2 (AZ1, W(10)), (AZBEG, W(11)), (AZEND, W(12)), (AZSTEP, W(13)),	CWW2 5
	3 (BETA, W(14)), (ELBEG, W(15)), (ELEND, W(16)), (ELSTEP, W(17)),	CWW2 6
	8 (RCVRH, W(20)),	CWW2 7
	4 (ONLY, W(21)), (HOP, W(22)), (MAXSTP, W(23)), (PLAT, W(24)), (PLON, W(25))	CWW2 8
	5, (HMAX, W(26)), (RAYFNC, W(29)), (EXTINC, W(33)),	CWW2 9
	6 (HMIN, W(27)), (RGMAX, W(28)),	CWW2 10
	8 (INTYP, W(41)), (MAXERR, W(42)), (ERATIO, W(43)),	CWW2 11
	6 (STEP1, W(44)), (STPMAX, W(45)), (STPMIN, W(46)), (FACTR, W(47)),	CWW2 12
	7 (SKIP, W(71)), (RAYSET, W(72)), (PRTSRP, W(74)), (HITLET, W(75))	CWW2 13
	9, (BINRAY, W(76)), (PAGLN, W(77)), (PLT, W(81)), (PFACTR, W(82)),	CWW2 14
	1 (LLAT, W(83)), (LLON, W(84)), (RLAT, W(85)), (RLON, W(86))	CWW2 15
	2, (TIC, W(87)), (HB, W(88)), (HT, W(89)), (TICV, W(96))	CWW2 16
	REAL MMODEL, MFORM, MID	CWW3 2
C		CWW3 3
C	WIND 100-124	CWW3 4
	EQUIVALENCE (W(100), UMODEL), (W(101), UFORM), (W(102), UID)	CWW3 5
C		CWW3 6
C	DELTA WIND 125-149	CWW3 7
	EQUIVALENCE (W(125), DUMODEL), (W(126), DUFORM), (W(127), DUID)	CWW3 8
C		CWW3 9
C	SOUND SPEED 150-174	CWW3 10
	EQUIVALENCE (W(150), CMODEL), (W(151), CFORM), (W(152), CID)	CWW3 11
	EQUIVALENCE (W(153), REFC)	CWW3 12
C		CWW3 13
C	DELTA SOUND SPEED 175-199	CWW3 14
	EQUIVALENCE (W(175), DCMODEL), (W(176), DCFORM), (W(177), DCID)	CWW3 15
C		CWW3 16
C	TEMPERATURE 200-224	CWW3 17
	EQUIVALENCE (W(200), TMODEL), (W(201), TFORM), (W(202), TID)	CWW3 18
C		CWW3 19
C	DELTA TEMPERATURE 225-249	CWW3 20
	EQUIVALENCE (W(225), DTMODEL), (W(226), DTFORM), (W(227), DTID)	CWW3 21
C		CWW3 22
C	MOLECULAR 250-274	CWW3 23
	EQUIVALENCE (W(250), MMODEL), (W(251), MFORM), (W(252), MID)	CWW3 24
C		CWW3 25
C	RECEIVER HEIGHT 275-299	CWW3 26
	EQUIVALENCE (W(275), RMODEL), (W(276), RFORM), (W(277), RID)	CWW3 27
C		CWW3 28
C	TOPOGRAPHY 300-324	CWW3 29
	EQUIVALENCE (W(300), GMODEL), (W(301), GFORM), (W(302), GID)	CWW3 30
C		CWW3 31

C	DELTA TOPOGRAPHY 325-349	CWW3 32
	EQUIVALENCE (W(325),GUMODEL),(W(326),GUFORM),(W(327),GUID)	CWW3 33
C		CWW3 34
C	UPPER SURFACE TOPOGRAPHY 350-374	CWW3 35
	EQUIVALENCE (W(350),SMODEL),(W(351),SFORM),(W(352),SID)	CWW3 36
C	PLOT ENHANCEMENTS CONTROL PARAMETERS	CWW3 37
C		CWW3 38
	EQUIVALENCE (W(490),XFQMDL),(W(491),YFQMDL)	CWW3 39
C	ABSORPTION 500-524	CWW3 40
	EQUIVALENCE (W(500),AMODEL),(W(501),AFORM),(W(502),AID)	CWW3 41
C		CWW3 42
C	DELTA ABSORPTION 525-549	CWW3 43
	EQUIVALENCE (W(525),DAMODEL),(W(526),DAFORM),(W(527),DAID)	CWW3 44
C		CWW3 45
C	PRESSURE 550-574	CWW3 46
	EQUIVALENCE (W(550),PMODEL),(W(551),PFORM),(W(552),PID)	CWW3 47
C		CWW3 48
C	DELTA PRESSURE 575-599	CWW3 49
	EQUIVALENCE (W(575),DPMODEL),(W(576),DPFORM),(W(577),DPID)	CWW3 50
C		CWW3 51
C	COMMON DECK "RKAM" INSERTED HERE	RKAMCOM2
	REAL KR,KTH,KPH	RKAMCOM4
	COMMON//R,TH,PH,KR,KTH,KPH,RKVAR(14),TPULSE,CSTEP,DRDT(20)	RKAMCOM5
C		RHORIZ13
C	COMMON DECK "B8" INSERTED HERE	CB10 2
	INTEGER RMX,RNTBL,RITBL,RFRMTBL,IDSR(10)	CB10 4
	COMMON/B8/RMX,RNTBL(10),RITBL(10),RFRMTBL(10),RGP(10)	CB10 5
	EQUIVALENCE (RGP,IDSR)	CB10 6
C		RHORIZ15
	DATA RECORR/1.0/	RHORIZ16
	DATA RMX/1/	RRIZBL 2
	DATA RNTBL/1,11,8*0/	RRIZBL 3
	DATA RITBL/1,9*0/	RRIZBL 4
	DATA RFRMTBL/1,9*0/	RRIZBL 5
C		RHORIZ19
	ENTRY IRECVR	RHORIZ20
C		RHORIZ21
	IF(RECORR.NE.RMODEL)	RHORIZ22
1	CALL RERROR('RECEIVR','WRNG MODEL',RECORR)	RHORIZ23
C		RHORIZ24
	MODREC(1)=6HRHORIZ	RHORIZ25
	MODREC(2)=RID	RHORIZ26
	RETURN	RHORIZ27
	ENTRY RECEIVER	RHORIZ28
	F=R-W(1)-W(20)	RHORIZ29
	PFR=1.0	RHORIZ30
	CALL CLEAR(PFRR,8)	RHORIZ31
	END	RHORIZ32
C		
	SUBROUTINE RTERR	RTERR 8
C	RECEIVER MODEL USING FIXED OFFSET TO TERRAIN HEIGHT	RTERR 9

C	COMMON DECK "RKAM" INSERTED HERE	RKAMCOM2
	REAL KR, KTH, KPH	RKAMCOM4
	COMMON /R, TH, PH, KR, KTH, KPH, RKVARS(14), TPULSE, CSTEP, DRDT(20)	RKAMCOM5
C	COMMON DECK "WW" INSERTED HERE	CWW 2
	PARAMETER (NWARSZ=1000)	CWW1 3
	COMMON /WW /ID(10), MAXW, W(NWARSZ)	CWW1 4
	REAL MAXSTP, MAXERR, INTYP, LLAT, LLON	CWW2 2
	EQUIVALENCE (EARTH, W(1)), (RAY, W(2)), (XMTRH, W(3)), (TLAT, W(4)),	CWW2 3
	1 (TLON, W(5)), (OW, W(6)), (FBEG, W(7)), (FEND, W(8)), (FSTEP, W(9)),	CWW2 4
	2 (AZ1, W(10)), (AZBEG, W(11)), (AZEND, W(12)), (AZSTEP, W(13)),	CWW2 5
	3 (BETA, W(14)), (ELBEG, W(15)), (ELEND, W(16)), (ELSTEP, W(17)),	CWW2 6
	8 (RCVRH, W(20)),	CWW2 7
	4 (ONLY, W(21)), (HOP, W(22)), (MAXSTP, W(23)), (PLAT, W(24)), (PLON, W(25))	CWW2 8
	5, (HMAX, W(26)), (RAYFNC, W(29)), (EXTINC, W(33)),	CWW2 9
	6 (HMIN, W(27)), (RGMX, W(28)),	CWW2 10
	8 (INTYP, W(41)), (MAXERR, W(42)), (ERATIO, W(43)),	CWW2 11
	6 (STEP1, W(44)), (STPMAX, W(45)), (STPMIN, W(46)), (FACTR, W(47)),	CWW2 12
	7 (SKIP, W(71)), (RAYSET, W(72)), (PRTSRP, W(74)), (HITLET, W(75))	CWW2 13
	9, (BINRAY, W(76)), (PAGLN, W(77)), (PLT, W(81)), (PFACTR, W(82)),	CWW2 14
	1 (LLAT, W(83)), (LLON, W(84)), (RLAT, W(85)), (RLON, W(86))	CWW2 15
	2, (TIC, W(87)), (HB, W(88)), (HT, W(89)), (TICV, W(96))	CWW2 16
	REAL MMODEL, MFORM, MID	CWW3 2
C		CWW3 3
C	WIND 100-124	CWW3 4
	EQUIVALENCE (W(100), UMODEL), (W(101), UFORM), (W(102), UID)	CWW3 5
C		CWW3 6
C	DELTA WIND 125-149	CWW3 7
	EQUIVALENCE (W(125), DUMODEL), (W(126), DUFORM), (W(127), DUID)	CWW3 8
C		CWW3 9
C	SOUND SPEED 150-174	CWW3 10
	EQUIVALENCE (W(150), CMODEL), (W(151), CFORM), (W(152), CID)	CWW3 11
	EQUIVALENCE (W(153), REFC)	CWW3 12
C		CWW3 13
C	DELTA SOUND SPEED 175-199	CWW3 14
	EQUIVALENCE (W(175), DCMODEL), (W(176), DCFORM), (W(177), DCID)	CWW3 15
C		CWW3 16
C	TEMPERATURE 200-224	CWW3 17
	EQUIVALENCE (W(200), TMODEL), (W(201), TFORM), (W(202), TID)	CWW3 18
C		CWW3 19
C	DELTA TEMPERATURE 225-249	CWW3 20
	EQUIVALENCE (W(225), DTMODEL), (W(226), DTFORM), (W(227), DTID)	CWW3 21
C		CWW3 22
C	MOLECULAR 250-274	CWW3 23
	EQUIVALENCE (W(250), MMODEL), (W(251), MFORM), (W(252), MID)	CWW3 24
C		CWW3 25
C	RECEIVER HEIGHT 275-299	CWW3 26
	EQUIVALENCE (W(275), RMODEL), (W(276), RFORM), (W(277), RID)	CWW3 27
C		CWW3 28
C	TOPOGRAPHY 300-324	CWW3 29
	EQUIVALENCE (W(300), GMODEL), (W(301), GFORM), (W(302), GID)	CWW3 30
C		CWW3 31
C	DELTA TOPOGRAPHY 325-349	CWW3 32
	EQUIVALENCE (W(325), GUMODEL), (W(326), GUFORM), (W(327), GUID)	CWW3 33
C		CWW3 34
C	UPPER SURFACE TOPOGRAPHY 350-374	CWW3 35

C	EQUIVALENCE (W(350),SMODEL), (W(351),SFORM), (W(352),SID)	CWW3	36
C	PLOT ENHANCEMENTS CONTROL PARAMETERS	CWW3	37
C		CWW3	38
C	EQUIVALENCE (W(490),XFQMDL), (W(491),YFQMDL)	CWW3	39
C	ABSORPTION 500-524	CWW3	40
C	EQUIVALENCE (W(500),AMODEL), (W(501),AFORM), (W(502),AID)	CWW3	41
C		CWW3	42
C	DELTA ABSORPTION 525-549	CWW3	43
C	EQUIVALENCE (W(525),DAMODEL), (W(526),DAFORM), (W(527),DAID)	CWW3	44
C		CWW3	45
C	PRESSURE 550-574	CWW3	46
C	EQUIVALENCE (W(550),PMODEL), (W(551),PFORM), (W(552),PID)	CWW3	47
C		CWW3	48
C	DELTA PRESSURE 575-599	CWW3	49
C	EQUIVALENCE (W(575),DPMODEL), (W(576),DPFORM), (W(577),DPID)	CWW3	50
C		CWW3	51
C	COMMON DECK "RR" INSERTED HERE	CRR	2
	REAL MODREC	CRR	4
	COMMON/RR/ MODREC(4)	CRR	5
	COMMON/RR/F, PFR, PFRR, PFRTH, PFRPH	CRR	6
	COMMON/RR/PFTH, PFPH, PFTHTH, PFPHPH, PFTHPH, FSELECT, FTIME	CRR	7
C	COMMON DECK "GG" INSERTED HERE	CGG	2
	REAL MODG	CGG	4
	COMMON/GG/MODG(4)	CGG	5
	COMMON/GG/G, PGR, PGRR, PGRTH, PGRPH	CGG	6
	COMMON/GG/PGTH, PGPH, PGTHTH, PGPHPH, PGTHPH, GSELECT, GTIME	CGG	7
C		RTERR	14
C	COMMON DECK "B8" INSERTED HERE	CB10	2
	INTEGER RMX, RNTBL, RITBL, RFRMTBL, IDSR(10)	CB10	4
	COMMON/B8/RMX, RNTBL(10), RITBL(10), RFRMTBL(10), RGP(10)	CB10	5
	EQUIVALENCE (RGP, IDSR)	CB10	6
C		RTERR	16
	DATA RMX/1/	RRBL	2
	DATA RNTBL/1,11,8*0/	RRBL	3
	DATA RITBL/1,9*0/	RRBL	4
	DATA RFRMTBL/1,9*0/	RRBL	5
C		RTERR	19
	DATA RECORR/2.0/	RTERR	20
C		RTERR	21
	ENTRY IRECVR	RTERR	22
C		RTERR	23
	IF(RECORR .NE. RMODEL)	RTERR	24
	1 CALL RERROR('RECEIVR', 'WRNG MODEL', RECORR)	RTERR	25
	MODREC(1)=5HRTErr	RTERR	26
	MODREC(2)=RID	RTERR	27
	RETURN	RTERR	28
C		RTERR	29
	ENTRY RECEVER	RTERR	30
C	GET CURRENT TERRAIN HEIGHT(MUST USE GET1 TO AVOID RECURSION	RTERR	31
C	SINCE WE ARE PROBABLY BEING CALLED BY GET RIGHT NOW)	RTERR	32
	F=GET1(G)-W(20)	RTERR	33
	CALL RMOVE(PFR, PGR, 9)	RTERR	34
	END	RTERR	35

	SUBROUTINE RVERT	RVERT 8
C	VERTICAL(CONICAL) RECEIVER SURFACE AT A FIXED RADIUS FROM	RVERT 9
C	A SPECIFIED ORIGIN.	RVERT 10
C		RVERT 11
C	COMMON DECK "RKAM" INSERTED HERE	RKAMCOM2
	REAL KR, KTH, KPH	RKAMCOM4
	COMMON//R, TH, PH, KR, KTH, KPH, RKVARS(14), TPULSE, CSTEP, DRDT(20)	RKAMCOM5
C	COMMON DECK "RR" INSERTED HERE	CRR 2
	REAL MODREC	CRR 4
	COMMON/RR/ MODREC(4)	CRR 5
	COMMON/RR/F, PFR, PFRR, PFRTH, PFRPH	CRR 6
	COMMON/RR/PFTH, PFPH, PFTHTH, PFPHPH, PFTHPH, FSELECT, FTIME	CRR 7
C	COMMON DECK "B8" INSERTED HERE	CB10 2
	INTEGER RMX, RNTBL, RITBL, RFRMTBL, IDSR(10)	CB10 4
	COMMON/B8/RMX, RNTBL(10), RITBL(10), RFRMTBL(10), RGP(10)	CB10 5
	EQUIVALENCE (RGP, IDSR)	CB10 6
C	COMMON DECK "GAMANG" INSERTED HERE	CGAMANG2
	COMMON/SPHGAM/SINLMO, COSLMO, GPHO, COSPHD, SINTH, COSTH	CGAMANG4
	COMMON/SPHGAM/GAMFUN, PGMTH, PGMPH, PGMTHTH, PGMPPH, PGMTHPH	CGAMANG5
C	COMMON DECK "WW" INSERTED HERE	CWW 2
	PARAMETER (NWARSZ=1000)	CWW1 3
	COMMON/WW/ID(10), MAXW, W(NWARSZ)	CWW1 4
	REAL MAXSTP, MAXERR, INTYP, LLAT, LLON	CWW2 2
	EQUIVALENCE (EARTH, W(1)), (RAY, W(2)), (XMTRH, W(3)), (TLAT, W(4)),	CWW2 3
	1 (TLON, W(5)), (OW, W(6)), (FBEG, W(7)), (FEND, W(8)), (FSTEP, W(9)),	CWW2 4
	2 (AZ1, W(10)), (AZBEG, W(11)), (AZEND, W(12)), (AZSTEP, W(13)),	CWW2 5
	3 (BETA, W(14)), (ELBEG, W(15)), (ELEND, W(16)), (ELSTEP, W(17)),	CWW2 6
	8 (RCVRH, W(20)),	CWW2 7
	4 (ONLY, W(21)), (HOP, W(22)), (MAXSTP, W(23)), (PLAT, W(24)), (PLON, W(25))	CWW2 8
	5, (HMAX, W(26)), (RAYFNC, W(29)), (EXTINC, W(33)),	CWW2 9
	6 (HMIN, W(27)), (RGMAX, W(28)),	CWW2 10
	8 (INTYP, W(41)), (MAXERR, W(42)), (ERATIO, W(43)),	CWW2 11
	6 (STEP1, W(44)), (STPMAX, W(45)), (STPMIN, W(46)), (FACTR, W(47)),	CWW2 12
	7 (SKIP, W(71)), (RAYSET, W(72)), (PRTSRP, W(74)), (HITLET, W(75))	CWW2 13
	9, (BINRAY, W(76)), (PAGLN, W(77)), (PLT, W(81)), (PFACTR, W(82)),	CWW2 14
	1 (LLAT, W(83)), (LLON, W(84)), (RLAT, W(85)), (RLON, W(86))	CWW2 15
	2, (TIC, W(87)), (HB, W(88)), (HT, W(89)), (TICV, W(96))	CWW2 16
	REAL MMODEL, MFORM, MID	CWW3 2
C		CWW3 3
C	WIND 100-124	CWW3 4
	EQUIVALENCE (W(100), UMODEL), (W(101), UFORM), (W(102), UID)	CWW3 5
C		CWW3 6
C	DELTA WIND 125-149	CWW3 7
	EQUIVALENCE (W(125), DUMODEL), (W(126), DUFORM), (W(127), DUID)	CWW3 8
C		CWW3 9
C	SOUND SPEED 150-174	CWW3 10
	EQUIVALENCE (W(150), CMODEL), (W(151), CFORM), (W(152), CID)	CWW3 11
	EQUIVALENCE (W(153), REFC)	CWW3 12
C		CWW3 13
C	DELTA SOUND SPEED 175-199	CWW3 14
	EQUIVALENCE (W(175), DCMODEL), (W(176), DCFORM), (W(177), DCID)	CWW3 15
C		CWW3 16

C	TEMPERATURE	200-224	CWW3	17
	EQUIVALENCE	(W(200),TMODEL),(W(201),TFORM),(W(202),TID)	CWW3	18
C			CWW3	19
C	DELTA TEMPERATURE	225-249	CWW3	20
	EQUIVALENCE	(W(225),DTMODEL),(W(226),DTFORM),(W(227),DTID)	CWW3	21
C			CWW3	22
C	MOLECULAR	250-274	CWW3	23
	EQUIVALENCE	(W(250),MMODEL),(W(251),MFORM),(W(252),MID)	CWW3	24
C			CWW3	25
C	RECEIVER HEIGHT	275-299	CWW3	26
	EQUIVALENCE	(W(275),RMODEL),(W(276),RFORM),(W(277),RID)	CWW3	27
C			CWW3	28
C	TOPOGRAPHY	300-324	CWW3	29
	EQUIVALENCE	(W(300),GMODEL),(W(301),GFORM),(W(302),GID)	CWW3	30
C			CWW3	31
C	DELTA TOPOGRAPHY	325-349	CWW3	32
	EQUIVALENCE	(W(325),GUMODEL),(W(326),GUFORM),(W(327),GUID)	CWW3	33
C			CWW3	34
C	UPPER SURFACE TOPOGRAPHY	350-374	CWW3	35
	EQUIVALENCE	(W(350),SMODEL),(W(351),SFORM),(W(352),SID)	CWW3	36
C		PLOT ENHANCEMENTS CONTROL PARAMETERS	CWW3	37
C			CWW3	38
	EQUIVALENCE	(W(490),XFQMDL),(W(491),YFQMDL)	CWW3	39
C	ABSORPTION	500-524	CWW3	40
	EQUIVALENCE	(W(500),AMODEL),(W(501),AFORM),(W(502),AID)	CWW3	41
C			CWW3	42
C	DELTA ABSORPTION	525-549	CWW3	43
	EQUIVALENCE	(W(525),DAMODEL),(W(526),DAFORM),(W(527),DAID)	CWW3	44
C			CWW3	45
C	PRESSURE	550-574	CWW3	46
	EQUIVALENCE	(W(550),PMODEL),(W(551),PFORM),(W(552),PID)	CWW3	47
C			CWW3	48
C	DELTA PRESSURE	575-599	CWW3	49
	EQUIVALENCE	(W(575),DPMODEL),(W(576),DPFORM),(W(577),DPID)	CWW3	50
C			CWW3	51
	EQUIVALENCE	(RVALPH0,W(278)),(RVLAMZ,W(279)),(RVPH0,W(280))	RVERT	17
C			RVERT	18
	DATA RMX/1/		RRTBL	2
	DATA RNTBL/1,11,8*0/		RRTBL	3
	DATA RITBL/1,9*0/		RRTBL	4
	DATA RFRMTBL/1,9*0/		RRTBL	5
	DATA RECORR/ <del>±-0</del> /		RVERT	21
	3.0		RVERT	22
C			RVERT	23
C	ENTRY IRECVR		RVERT	24
C			RVERT	25
	IF(RECORR.NE.RMODEL)		RVERT	26
1	CALL RERROR(7HRECEIVR,10HWRNG MODEL,RECORR)		RVERT	27
	MODREC(1)=7HRVERT		RVERT	28
	MODREC(2)=RID		RVERT	29
C			RVERT	30
	SINLMZ=SIN(RVLAMZ)		RVERT	31
	COSLMZ=COS(RVLAMZ)		RVERT	32
	COSALP=COS(RVALPH0)		RVERT	33
C			RVERT	34

C	RETURN	RVERT 35
C	ENTRY RECEIVER	RVERT 36
C	SINLMO=SINLMZ	RVERT 37
C	COSLMO=COSLMZ	RVERT 38
C	GPHO=RVPHO	RVERT 39
C	CALL GAMANG(TH,PH)	RVERT 40
C	F=GAMFUN-COSALP	RVERT 41
C	PFR=0.0	RVERT 42
C	CALL RMOVE(PFTH,PGMTH,5)	RVERT 43
C	RETURN	RVERT 44
C	END	RVERT 45
		RVERT 46
		RVERT 47
		RVERT 48
		RVERT 49
		RVERT 50

C	SUBROUTINE SMPANN	SMPANN 9
C	ANNOTATION MODEL FOR MINIMUM GRAPHICS SUPPORT	SMPANN10
C	CHARACTER*(*) S,C	SMPANN11
C	INITIALIZES PLOT IN DRAFT MODE(DOES NOT REQUIRE DISSPLA)	SMPANN12
C	COMMON DECK "WWR" INSERTED HERE	SMPANN13
C	PARAMETER (NWARSZ=1000)	SMPANN14
C	COMMON/WW/ID(10),MAXW,W(NWARSZ)	SMPANN15
C	REAL MAXSTP,MAXERR,INTYP,LLAT,LLON	CWWR 2
C	EQUIVALENCE (EARTH,W(1)),(RAY,W(2)),(XMTRH,W(3)),(TLAT,W(4)),	CWW1 3
C	1 (TLON,W(5)),(OW,W(6)),(FBEG,W(7)),(FEND,W(8)),(FSTEP,W(9)),	CWW1 4
C	2 (AZ1,W(10)),(AZBEG,W(11)),(AZEND,W(12)),(AZSTEP,W(13)),	CWW2 2
C	3 (BETA,W(14)),(ELBEG,W(15)),(ELEND,W(16)),(ELSTEP,W(17)),	CWW2 3
C	8 (RCVRH,W(20)),	CWW2 4
C	4 (ONLY,W(21)),(HOP,W(22)),(MAXSTP,W(23)),(PLAT,W(24)),(PLON,W(25))	CWW2 5
C	5,(HMAX,W(26)),(RAYFNC,W(29)),(EXTINC,W(33)),	CWW2 6
C	6 (HMIN,W(27)),(RGMAT,W(28)),	CWW2 7
C	8 (INTYP,W(41)),(MAXERR,W(42)),(ERATIO,W(43)),	CWW2 8
C	6 (STEP1,W(44)),(STPMAX,W(45)),(STPMIN,W(46)),(FACTR,W(47)),	CWW2 9
C	7 (SKIP,W(71)),(RAYSET,W(72)),(PRTSRP,W(74)),(HITLET,W(75))	CWW2 10
C	9 ,(BINRAY,W(76)),(PAGLN,W(77)),(PLT,W(81)),(PFACTR,W(82)),	CWW2 11
C	1 (LLAT,W(83)),(LLON,W(84)),(RLAT,W(85)),(RLON,W(86))	CWW2 12
C	2,(TIC,W(87)),(HB,W(88)),(HT,W(89)),(TICV,W(96))	CWW2 13
C	COMMON DECK "ANNOT" INSERTED HERE	CWW2 14
C	CHARACTER*10 ANOTES,HNOTES	CWW2 15
C	COMMON/ANNCTL/LENA(4),LENHA(3)	CWW2 16
C	COMMON/ANNCTC/ANOTES(2,4),HNOTES(4,3)	ANNOT 2
C	DATA LENA,ANOTES	ANNOT 4
C	1 /2*1,2*2,'DEPTH (M)',',','DEPTH (KM)',',',	ANNOT 5
C	2 'HEIGHT (M)',',','HEIGHT (KM)',',')/'	ANNOT 6
		SMPANN18
		SANNBL 2
		SANNBL 3
		SANNBL 4
		SANNBL 5

	DATA LENHA,HNOTES	SANNBL 6
	1 /3,2,3, 'RANGE AT S','EA LEVEL (' , 'KM) ', ' '	SANNBL 7
	2 , 'RANGE (DEG', ' ) ', 2* ' '	SANNBL 8
	3 , 'CROSS RANG', 'E AT SEA L', 'EVEL (KM) ', ' ' /	SANNBL 9
C	ENTRY SETANN	SMPANN21
C	RETURN	SMPANN22
C	ENTRY ANNFIL(S,C)	SMPANN23
	CALL SFILTR(S,C,'#!')	SMPANN24
	END	SMPANN25
		SMPANN26
		SMPANN27
		SMPANN28
	SUBROUTINE FULANN	FULANN 9
C	ANNOTATION MODEL SUITED FOR PUBLICATION QUALITY LETTERING	FULANN10
C	CHARACTER*(*) S,C	FULANN11
C	INITIALIZES PLOT IN PUBLICATION-QUALITY MODE(REQUIRES DISSPLA)	FULANN12
C	COMMON DECK "WWR" INSERTED HERE	FULANN13
C	PARAMETER (NWARSZ=1000)	FULANN14
C	COMMON/WW/ID(10),MAXW,W(NWARSZ)	FULANN15
	REAL MAXSTP,MAXERR,INTYP,LLAT,LLON	CWWR 2
	EQUIVALENCE (EARTH, W(1)), (RAY, W(2)), (XMTRH, W(3)), (TLAT, W(4)),	CWW1 3
	1 (TLON, W(5)), (OW, W(6)), (FBEG, W(7)), (FEND, W(8)), (FSTEP, W(9)),	CWW1 4
	2 (AZ1, W(10)), (AZBEG, W(11)), (AZEND, W(12)), (AZSTEP, W(13)),	CWW2 2
	3 (BETA, W(14)), (ELBEG, W(15)), (ELEND, W(16)), (ELSTEP, W(17)),	CWW2 3
	8 (RCVRH, W(20)),	CWW2 4
	4 (ONLY, W(21)), (HOP, W(22)), (MAXSTP, W(23)), (PLAT, W(24)), (PLON, W(25))	CWW2 5
	5, (HMAX, W(26)), (RAYFNC, W(29)), (EXTINC, W(33)),	CWW2 6
	6 (HMIN, W(27)), (RGMAX, W(28)),	CWW2 7
	8 (INTYP, W(41)), (MAXERR, W(42)), (ERATIO, W(43)),	CWW2 8
	6 (STEP1, W(44)), (STPMAX, W(45)), (STPMIN, W(46)), (FACTR, W(47)),	CWW2 9
	7 (SKIP, W(71)), (RAYSET, W(72)), (PRTSRP, W(74)), (HITLET, W(75))	CWW2 10
	9 , (BINRAY, W(76)), (PAGLN, W(77)), (PLT, W(81)), (PFACTR, W(82)),	CWW2 11
	1 (LLAT, W(83)), (LLON, W(84)), (RLAT, W(85)), (RLON, W(86))	CWW2 12
	2, (TIC, W(87)), (HB, W(88)), (HT, W(89)), (TICV, W(96))	CWW2 13
C	COMMON DECK "ANNOT" INSERTED HERE	CWW2 14
	CHARACTER*10 ANOTES,HNOTES	CWW2 15
	COMMON/ANNCTL/LENA(4),LENHA(3)	CWW2 16
	COMMON/ANNCTC/ANOTES(2,4),HNOTES(4,3)	ANNOT 2
C	DATA LENA,ANOTES	ANNOT 4
	1 /4*2, 'DEPTH (#M', ' ) ', 'DEPTH (#KM', '! ) ',	ANNOT 5
	2 'HEIGHT (#M', '! ) ', 'HEIGHT (#K', 'M! ) ' /	ANNOT 6
	DATA LENHA,HNOTES	FULANN18
	1 /3,2,4, 'RANGE AT S','EA LEVEL (' , '#KM! ) ', ' '	FANNBL 2
	2 , 'RANGE (#DE', 'G! ) ', 2* ' '	FANNBL 3
	3 , 'CROSS RANG', 'E AT SEA L', 'EVEL (#KM! , ' ) ' /	FANNBL 4
	ENTRY SETANN	FANNBL 5
		FANNBL 6
		FANNBL 7
		FANNBL 8
		FULANN21



## DDSPLA -- Programs for reading Graphics Output File (Tape File 6)

	PROGRAM DDSPLA(TAPE5,INPUT,OUTPUT,TAPE9)	DDSPLA 3
	COMMON/DD/IN, IOR, IT, IS, IC, ICC, IX, IY	DDSPLA 4
	COMMON/SUPNEG/IDEL, NMBS	DDSPLA 5
C	PARAMETER (LIMPTS=700)	DDSPLA 6
	REAL XV(LIMPTS), YV(LIMPTS)	DDSPLA 7
	INTEGER A(4), C(4), E(4)	DDSPLA 8
	LOGICAL COMPCL	DDSPLA 9
	CHARACTER LINE*72, TEXT*80, S*10	DDSPLA10
	EQUIVALENCE (IX, XXX), (IY, YYY)	DDSPLA11
	DATA COMPCL/.TRUE./	DDSPLA12
	DATA KNT/0/	DDSPLA13
C	REWIND 5	DDSPLA14
10	READ(5, END=100, ERR=100) IT, IX, IY	DDSPLA15
C	IF(IT.GT.29) PRINT *, IT, IX, IY, XXX, YYY	DDSPLA16
	IF(IT.GT.20) THEN	DDSPLA17
	IF(COMPCL) THEN	DDSPLA18
	WRITE(LINE, ' (A, 3(I4, 1X), 2G13.6) ')	DDSPLA19
1	'NO CALL TO 'COMPRS'' BEFORE---', IT, IX, IY, XXX, YYY	DDSPLA20
	CALL SYSTEM(52, LINE)	DDSPLA21
	ENDIF	DDSPLA22
	ENDIF	DDSPLA23
	IF(IT.LT.-2 .OR. IT.GT.38) STOP 'CODE>38'	DDSPLA24
	KNT=KNT+1	DDSPLA25
	IF(IT.EQ.-1) THEN	DDSPLA26
	CALL DDEND	DDSPLA27
	ELSEIF(IT.EQ.-2) THEN	DDSPLA28
	CALL DDFR	DDSPLA29
	ELSEIF(IT.EQ.0) THEN	DDSPLA30
	READ(5) N, M, (TEXT(I:I), I=1, M)	DDSPLA31
	CALL DDINIT(N, TEXT)	DDSPLA32
	ELSEIF(IT.EQ.1) THEN	DDSPLA33
	CALL DDBP	DDSPLA34
	ELSEIF(IT.EQ.2) THEN	DDSPLA35
	CALL DDVC	DDSPLA36
	ELSEIF(IT.EQ.10) THEN	DDSPLA37
	CALL SCMPX	DDSPLA38
	ELSEIF(IT.EQ.11) THEN	DDSPLA39
	CALL MX1ALF(IX, IY)	DDSPLA40
	ELSEIF(IT.EQ.12) THEN	DDSPLA41
	CALL MX2ALF(IX, IY)	DDSPLA42
	ELSEIF(IT.EQ.13) THEN	DDSPLA43
	IF(XXX.LE.0.0) THEN	DDSPLA44
	PRINT *, 'HEIGHT OF ZERO!!'	DDSPLA45
	XXX=.15	DDSPLA46
	ENDIF	DDSPLA47
	CALL HEIGHT(XXX)	DDSPLA48
C	ELSEIF(IT.EQ.20) THEN	DDSPLA49
	COMPCL=.FALSE.	DDSPLA50
	CALL COMPRS	DDSPLA51
	ELSEIF(IT.EQ.21) THEN	DDSPLA52
	CALL GRACE(IX, IY)	DDSPLA53
	ELSEIF(IT.EQ.22) THEN	DDSPLA54
		DDSPLA55
		DDSPLA56
		DDSPLA57

CALL PHYSOR(IX,IY)	DDSPLA58
ELSEIF(IT.EQ.23) THEN	DDSPLA59
CALL PAGE(IX,IY)	DDSPLA60
ELSEIF(IT.EQ.24) THEN	DDSPLA61
CALL SCLPIC(IX)	DDSPLA62
ELSEIF(IT.EQ.25) THEN	DDSPLA63
IF(IX.NE.0 .OR. IY.NE.0) STOP 'ERROR 1'	DDSPLA64
READ(5) A,B,C,D,E,F,XAXIS,YAXIS	DDSPLA65
CALL XREVTK	DDSPLA66
CALL YREVTK	DDSPLA67
CALL INTAXS	DDSPLA68
CALL TITLE(A,B,C,D,E,F,XAXIS,YAXIS)	DDSPLA69
ELSEIF(IT.EQ.26) THEN	DDSPLA70
CALL FRAME	DDSPLA71
ELSEIF(IT.EQ.27) THEN	DDSPLA72
READ(5) W,X,Y,Z	DDSPLA73
CALL GRAFB(IX,IY,W,X,Y,Z,XAXIS,YAXIS)	DDSPLA74
ELSEIF(IT.EQ.28) THEN	DDSPLA75
CALL MARKER(IX)	DDSPLA76
ELSEIF(IT.EQ.29) THEN	DDSPLA77
IF(IX.GT.LIMPTS) CALL SYSTEM(52,'N>LIMPTS')	DDSPLA78
READ(5) (XV(I),I=1,IX),(YV(I),I=1,IX)	DDSPLA79
CALL CURVE(XV,YV,IX,IY)	DDSPLA80
ELSEIF(IT.EQ.30) THEN	DDSPLA81
CALL ENDPL(IX)	DDSPLA82
ELSEIF(IT.EQ.31) THEN	DDSPLA83
CALL DONEPL	DDSPLA84
ELSEIF(IT.EQ.32) THEN	DDSPLA85
CALL XTICKS(IX)	DDSPLA86
ELSEIF(IT.EQ.33) THEN	DDSPLA87
CALL YTICKS(IX)	DDSPLA88
ELSEIF(IT.EQ.34) THEN	DDSPLA89
CALL MYJACT(IX)	DDSPLA90
ELSEIF(IT.EQ.35) THEN	DDSPLA91
CALL MYJACT('NUMBERS')	DDSPLA92
IDEL=IX	DDSPLA93
NMBS=IY	DDSPLA94
ELSEIF(IT.EQ.36) THEN	DDSPLA95
CALL NOBRDR	DDSPLA96
ELSEIF(IT.EQ.37) THEN	DDSPLA97
CALL DASH	DDSPLA98
ELSEIF(IT.EQ.38) THEN	DDSPLA99
READ(5) S	DDSPL100
CALL RESET(S)	DDSPL101
ENDIF	DDSPL102
ENDIF	DDSPL103
C	DDSPL104
IF(IT.NE.3) GO TO 10	DDSPL105
READ(5) IOR,N,M,(TEXT(I:I),I=1,M)	DDSPL106
CALL DDTEXT(N,TEXT)	DDSPL107
C	DDSPL108
20 PRINT 20,(TEXT(I),I=1,N)	DDSPL109
FORMAT(8A10)	DDSPL110
GO TO 10	DDSPL111
C	DDSPL112
100 PRINT *,'NUMBER OF VECTORS=',KNT,IT	

	STOP	DDSPL113
	END	DDSPL114
	SUBROUTINE MYJSUB(IPAR,ITY,IMYJ)	DDSPL115
	COMMON/SUPNEG/IDEL,NMBS	DDSPL116
	DATA IDEL,NMBS/0,100000/	DDSPL117
C		DDSPL118
C	WE ARE INTERESTED ONLY IN NUMERICAL VALUES CAUSED BY	DDSPL119
C	A CALL MYJACT('NUMBERS')(IMYJ=5)	DDSPL120
C		DDSPL121
	IF(ITY.GE.0 .OR. IMYJ.NE.5) RETURN	DDSPL122
C		DDSPL123
	IF(IDEL.GT.0) IDEL=IDEL-1	DDSPL124
C		DDSPL125
	IF(IDEL.LE.0.AND.NMBS.GT.0) THEN	DDSPL126
	NMBS=NMBS-1	DDSPL127
	IPAR=IABS(IPAR)	DDSPL128
	ENDIF	DDSPL129
	END	DDSPL130
	SUBROUTINE DDINIT(N,TEXT)	DDSPL131
C		DDSPL132
	COMMON/PLOTCH/NPLOT,INABLE,FX,FY,OFFX,OFFY	CPLLOT 2
	DATA OFFX,OFFY/0.0,0.0/	DDSPL134
	DATA NPLOT,INABLE,PLOTSZ,XAXIS,YAXIS/0,0,7.5,11.,8.5/	DDSPL135
C		DDSPL136
C	NO RE-INITIALIZATIONS BEFORE ENDPL'S	DDSPL137
	IF(INABLE.GT.0) RETURN	DDSPL138
C		DDSPL139
	IF(NPLOT.GT.0) GO TO 10	DDSPL140
C		DDSPL141
	CALL COMPRS	DDSPL142
	FY=PLOTSZ/1024.	DDSPL143
	FX=FY	DDSPL144
C		DDSPL145
10	NPLOT=NPLOT+1	DDSPL146
	INABLE=1	DDSPL147
	CALL NOBRDR	DDSPL148
	CALL PAGE(XAXIS,YAXIS)	DDSPL149
	CALL PHYSOR(0.0,0.0)	DDSPL150
	CALL AREA2D(XAXIS,YAXIS)	DDSPL151
	CALL GRACE(0.0)	DDSPL152
	RETURN	DDSPL153
	END	DDSPL154

	SUBROUTINE DDBP	DDSPL155
	COMMON/PLOTCH/NPLOT, INABLE, FX, FY, OFFX, OFFY	CPLLOT 2
	COMMON/DD/IN, IOR, IT, IS, IC, ICC, IX, IY	CDDCOM 2
C		DDSPL158
C	"DDPLOT" DOES NOT REQUIRE RE-INITIALIZATION AFTER EACH FRAME	DDSPL159
C	BUT "DISPLA" DOES SO WE USE THE STATUS OF "INABLE" TO TELL US	DDSPL160
C	WHERE WE ARE.	DDSPL161
	IF(INABLE.EQ.0) CALL DDINIT(-1,0)	DDSPL162
	CALL STRTPT(OFFX+IX*FX,OFFY+IY*FY)	DDSPL163
	RETURN	DDSPL164
	END	DDSPL165

	SUBROUTINE DDVC	DDSPL166
	COMMON/PLOTCH/NPLOT, INABLE, FX, FY, OFFX, OFFY	CPLLOT 2
	COMMON/DD/IN, IOR, IT, IS, IC, ICC, IX, IY	CDDCOM 2
C		DDSPL169
C	SEE "DDBP" FOR THE REASON FOR THIS TEST.	DDSPL170
	IF(INABLE.EQ.0) CALL DDINIT(-1,0)	DDSPL171
	CALL CONNPT(OFFX+IX*FX,OFFY+IY*FY)	DDSPL172
	RETURN	DDSPL173
	END	DDSPL174

	SUBROUTINE DDEND	DDSPL175
	COMMON/PLOTCH/NPLOT, INABLE, FX, FY, OFFX, OFFY	CPLLOT 2
C	CHECK SYNCH, DDFR SHOULD HAVE BEEN CALLED BY NOW	DDSPL177
	IF(INABLE.GT.0) CALL ENDPL(0)	DDSPL178
C		DDSPL179
	CALL DONEPL	DDSPL180
C		DDSPL181
	INABLE=0	DDSPL182
	RETURN	DDSPL183
	END	DDSPL184

	SUBROUTINE DDTEXT(N,TEXT)	DDSPL185
	COMMON/PLOTCH/NPLOT, INABLE, FX, FY, OFFX, OFFY	CPLLOT 2
	COMMON/DD/IN, IOR, IT, IS, IC, ICC, IX, IY	CDDCOM 2
C		DDSPL188
	IF(INABLE.EQ.0) CALL DDINIT(-1,0)	DDSPL189
	IF(IOR.EQ.0) CALL ANGLE(0.0)	DDSPL190
	IF(IOR.NE.0) CALL ANGLE(90.0)	DDSPL191
	CALL MESSAG(TEXT,N*10,OFFX+IX*FX,OFFY+IY*FY)	DDSPL192

	RETURN	DDSPL193
	END	DDSPL194
	 SUBROUTINE DDTAB	
	RETURN	DDSPL195
	END	DDSPL196
		DDSPL197
	 SUBROUTINE DDFR	
	COMMON/PLOTCH/NPLOT, INABLE, FX, FY, OFFX, OFFY	DDSPL198
	IF(INABLE.GT.0) CALL ENDPL(0)	CPLLOT 2
	INABLE=0	DDSPL200
	RETURN	DDSPL201
	END	DDSPL202
		DDSPL203
	 SUBROUTINE SETDDOF(IXF,IYF)	
C	SETS RASTOR RANGE TO: -IXF TO 1023-IXF	DDSPL204
C	AND -IYF TO 1023-IYF.	DDSPL205
	COMMON/PLOTCH/NPLOT, INABLE, FX, FY, OFFX, OFFY	DDSPL206
	OFFX=IXF*FX	CPLLOT 2
	OFFY=IYF*FY	DDSPL208
	END	DDSPL209
		DDSPL210
	 SUBROUTINE GRAFB(XORIG,XSTP,XMAX,YORIG,YSTP,YMAX,XAXIS,YAXIS)	
C	CALL GRAF(XORIG,XSTP,XMAX,YORIG,YSTP,YMAX)	DDSPL211
	CALL XNONUM	DDSPL212
	CALL YNONUM	DDSPL213
	CALL XGRAXS(XORIG,XSTP,XMAX,XAXIS,' ',-1,0.0,YAXIS)	DDSPL214
	XR=XMAX-XORIG	DDSPL215
	XAX=AINT(XR/XSTP)*XSTP*(XAXIS/XR)	DDSPL216
	PRINT *,XORIG,XMAX,XSTP,XAXIS,XAX	DDSPL217
	CALL YGRAXS(YORIG,YSTP,YMAX,YAXIS,' ',-1,XAX,0.0)	DDSPL218
	CALL RESET('XNONUM')	DDSPL219
	CALL RESET('YNONUM')	DDSPL220
	END	DDSPL221
		DDSPL222
		DDSPL223

```
C  SUBROUTINE TITLEW(A,B,C,D,E,F,G,H)          DDSPL224
    DUMMY ROUTINE ALLOWING SUBSTITUTION OF ALTERNATE TITLE PROGRAMS  DDSPL225
    CALL TITLE(A,B,C,D,E,F,G,H)              DDSPL226
    END                                        DDSPL227
```



SUBROUTINE DDBP	DDALT
COMMON/DD/IN,IOR,IT,IS,IC,ICC,IX,IY	DDALT
C INSERT YOUR OWN ROUTINE TO DEFINE A VECTOR ORIGIN AT IX,IY	DDALT
RETURN	DDALT
END	DDALT

SUBROUTINE DDVC	DDALT
COMMON/DD/IN,IOR,IT,IS,IC,ICC,IX,IY	DDALT
CINSERT YOUR OWN ROUTINE TO PLOT A STRAIGHT LINE WITH INTENSITY	DDALT
C"IN" FROM THE ORIGIN TO THE END POSITION IX,IY. A SINGLE CALL	DDALT
CTO DDBP FOLLOWED BY SUCCESSIVE CALLS TO DDVC (CHANGING IX,IY)	DDALT
CPLOTS CONNECTED VECTORS.	DDALT
RETURN	DDALT
END	DDALT

SUBROUTINE DDEND	DDALT
C CHECK SYNCH, DDFR SHOULD HAVE BEEN CALLED BY NOW	DDALT
CINSERT YOUR OWN ROUTINE TO EMPTY THE PLOT BUFFER AND RELEASE	DDALT
CTHE PLOTTING COMMAND FILE TO YOUR PLOTTING DEVICE.	DDALT
RETURN	DDALT
END	DDALT

SUBROUTINE DDTEXT(N,NT)	DDALT
COMMON/DD/IN,IOR,IT,IS,IC,ICC,IX,IY	DDALT
CINSERT YOUR OWN ROUTINE TO PLOT A GIVEN ARRAY IN A TABULAR MODE	DDALT
CAFTER INITIALIZING TABULAR PLOTTING WITH DDTAB. NT IS AN ARRAY OF	DDALT
CLENGTH N, CONTAINING "TEXT" FOR TABULAR PLOTTING. SEE APPENDIX C.	DDALT
RETURN	DDALT
END	DDALT

SUBROUTINE DDTAB	DDALT
COMMON/DD/IN,IOR,IT,IS,IC,ICC,IX,IY	DDALT
CINSERT YOUR OWN ROUTINE TO INITIALIZE TABULAR TEXT PLOTTING	DDALT
C SPECIFY IOR,IS,IX,IY. TEXT WILL BEGIN AT IX,IY.	DDALT
RETURN	DDALT
END	DDALT

```
SUBROUTINE DDFR
CINSERT YOUR OWN ROUTINE TO ADVANCE ONE PLOTTING FRAME, WHEN
CPLOTTING IS COMPLETED.
  RETURN
  END
```

```
DDALT
DDALT
DDALT
DDALT
DDALT
```

## APPENDIX E. ERRATA FOR NOAA TECH. MEMO. ERL-WPL 103

A versatile three-dimensional Hamiltonian ray-tracing computer program for acoustic waves in the atmosphere.

by R. M. Jones, J. P. Riley, and T. M. Georges

NOAA Tech. Memo. ERL WPL-103

On page 9, the term  $k_{\phi} r \sin \theta d\phi/dP'$  in equation (3.17) should read  $k_{\phi} r \sin \theta d\phi/dP'$ .

On page 10, the denominator in the last fraction in equation (3.18) should be  $C_{ref} \partial H/\partial \omega$  instead of  $C \partial H/\partial \omega$ .

On page 16,  $\partial \omega/\partial r$  in (4.27) should be  $\partial \Omega/\partial r$ .

On page 45, the last line in the caption for Figure 9 should read:  
\*\*\*\*See Table 29 for details.

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