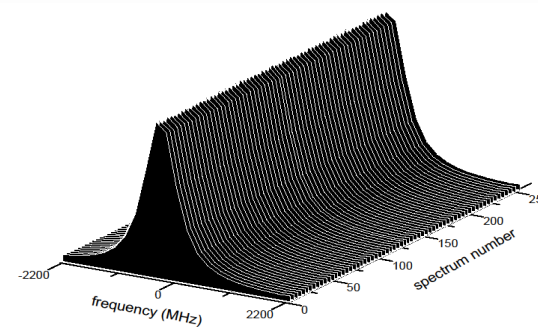


Assessing the precision and accuracy of cavity ring-down spectroscopy measurements

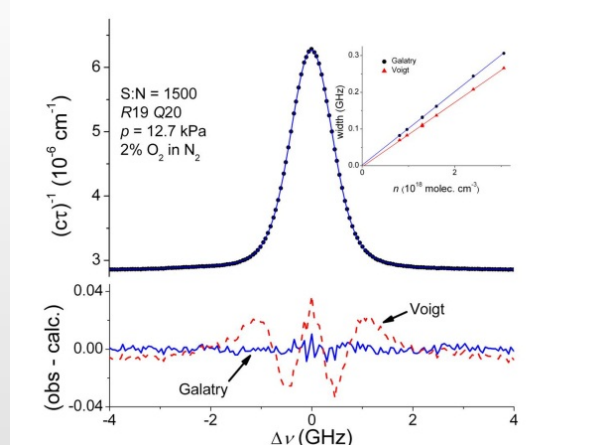
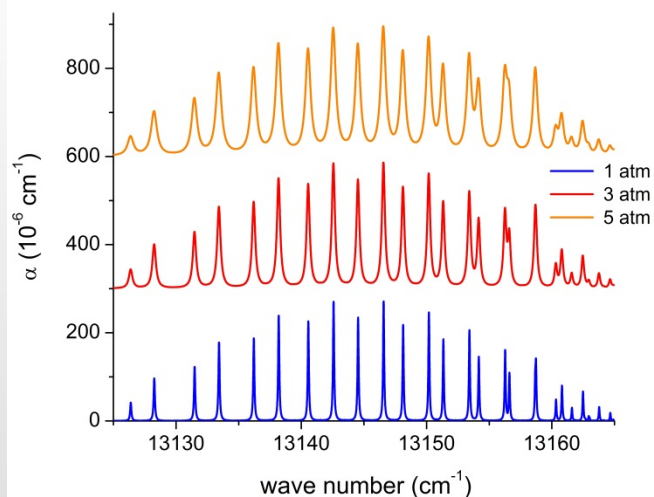
Joseph T. Hodges

Material Measurement Laboratory,
National Institute of Standards and Technology,
Gaithersburg, MD

joseph.hodges@nist.gov



250 spectra in 0.7 s



11th Annual International User Meeting
and Summer School on Cavity-Enhanced Spec
June 16-19, 2015, Boulder CO

Factors affecting the precision of cw-CRDS measurements

Quantum fluctuations in photocurrent (shot noise)

Detector noise & signal digitization

Spurious coupling into high-order transverse modes

Finite beam extinction ratio

Drift and fluctuations in base cavity losses from:

- mirror birefringence & polarization-dependent losses

- coupled-cavity effects (etalons)

- spatially non-uniform losses & gas adsorption at mirrors

Factors affecting the accuracy of cw-CRDS measurements

Poorly constrained spectrum frequency detuning axis

Residual mode beating and improperly weighted fits

Detector/digitizer non-linearity and limited bandwidth

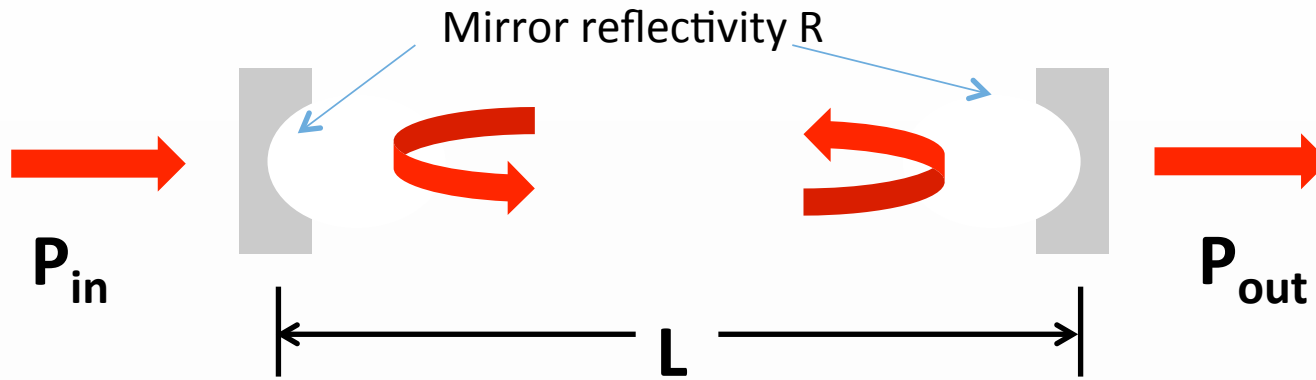
Saturation effects

Overly simplistic line shape models (e.g. Voigt Profile)

Experimental artifacts in spectrum baselines (etalons, birefringence etc.)

Sample characterization (temperature, pressure, molar fraction, wall effects)

Properties of high-finesse resonators



Resonances occur at multiples of $c/2L$

comb-like structure, may provide spectrum "ruler"

$$2L/(\Delta\nu_{mode}) = \pi/(1 - R)$$

cavity finesse

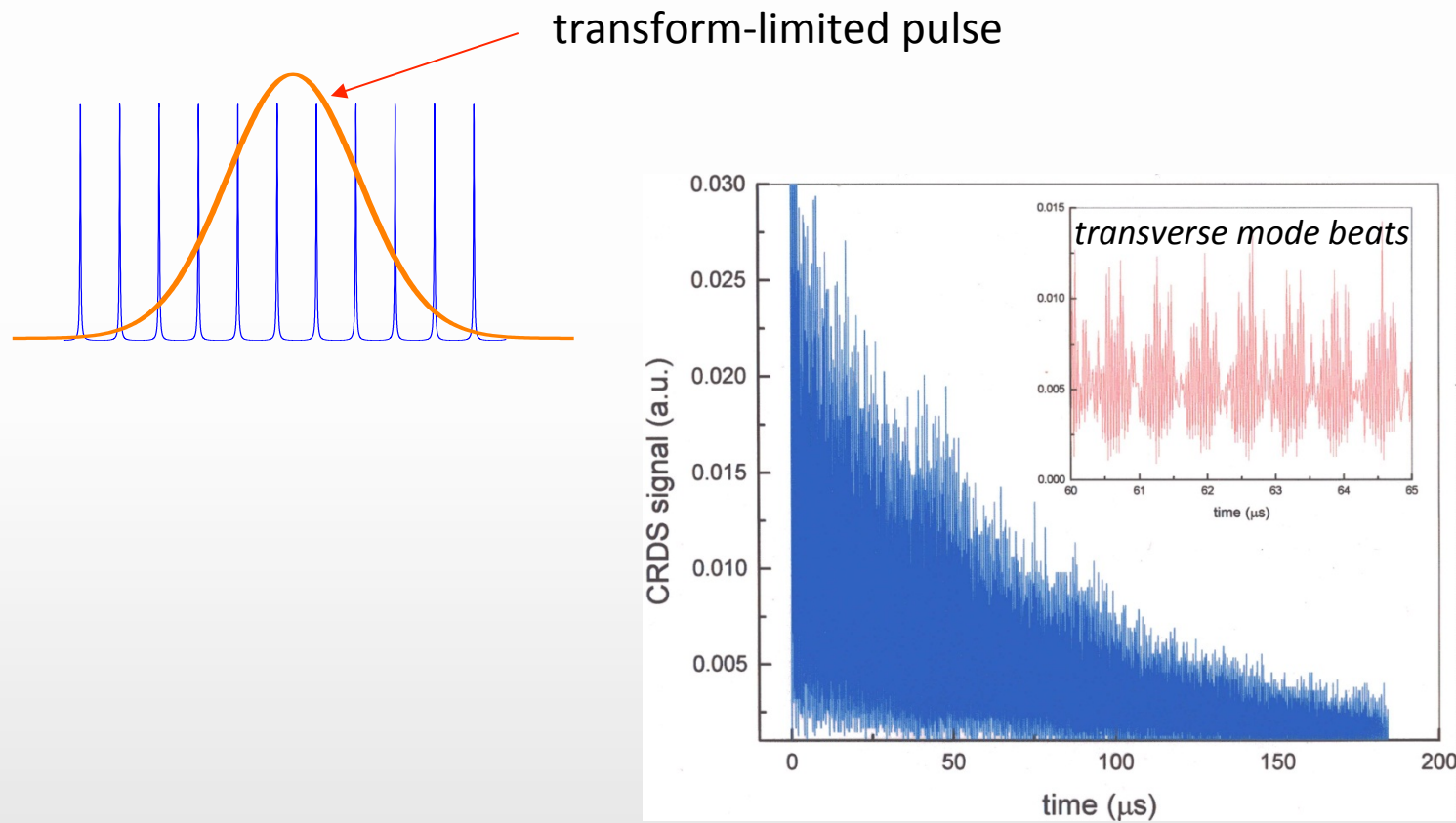
Resonance width is $\Delta\nu_{mode} = (c/2L)/F$

exceptionally good frequency filter, [typically ~ 1 to 50]

Effective interaction path length is $L_{eff} = (F/\pi)*L$ yields high-sensitivity to light absorption by cavity medium

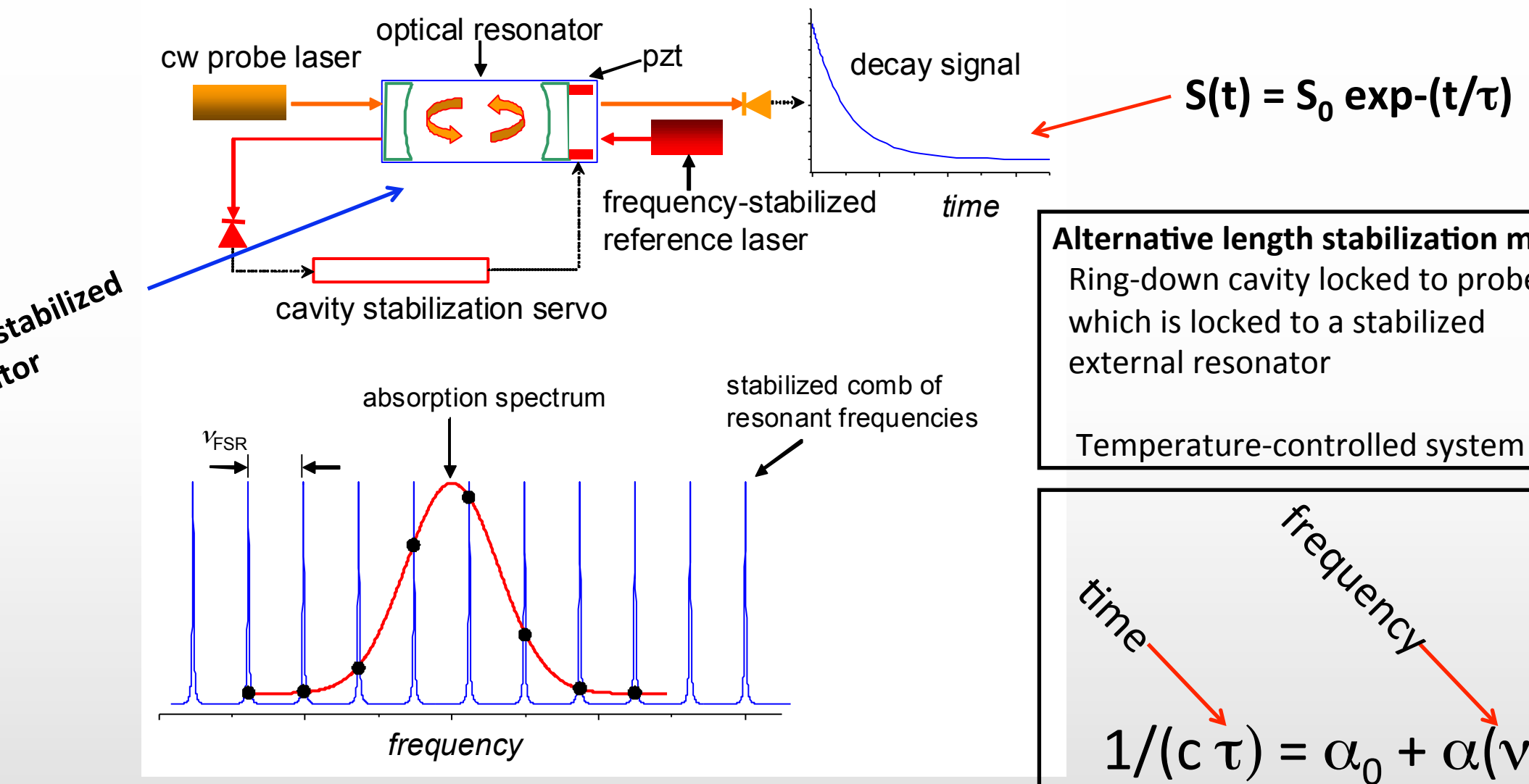
Resonator can be interrogated via cw transmission or by observing passive decays (ring-down)

A little history ... multi-mode CRDS signal (pulsed excitation)



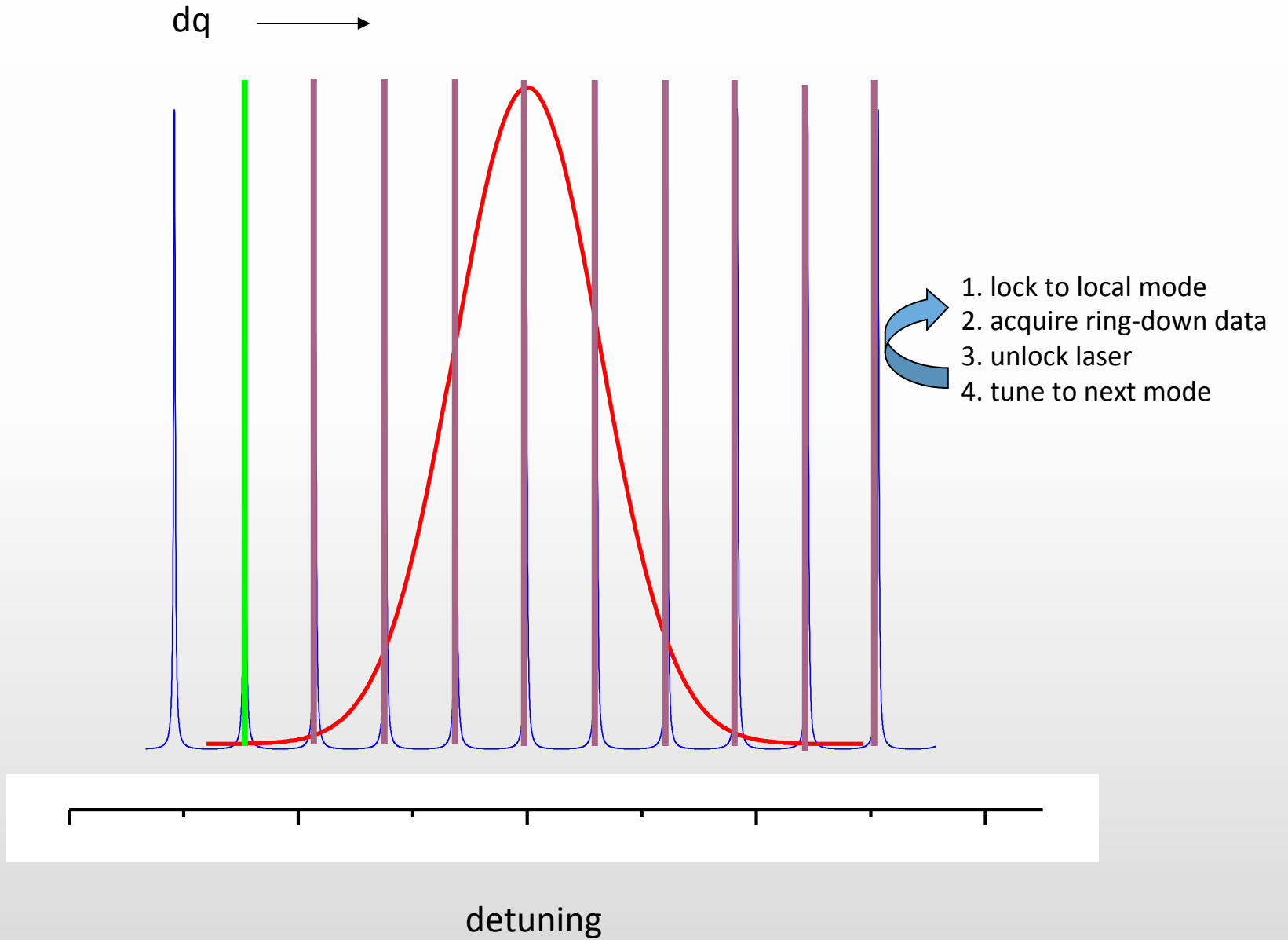
Signals were dominated by transverse and longitudinal mode beating effects, resulting in suboptimal statistics and severely compromised frequency resolution.

Single-mode cavity ring-down spectroscopy

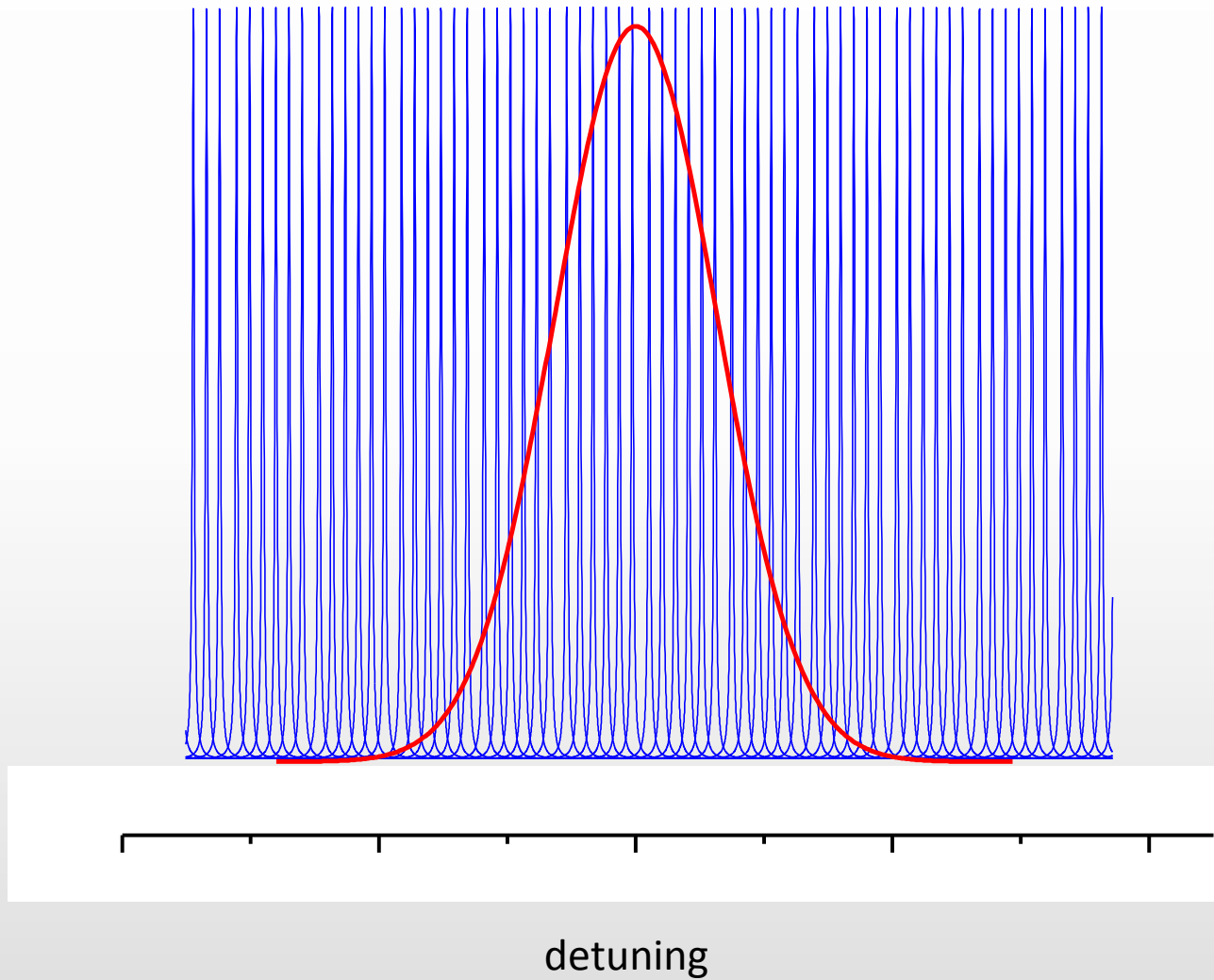


With length-stabilization, single-mode excitation enables high-fidelity and high-sensitivity measurements of transition areas, widths & shapes, positions and pressure shifts

Spectral scans (mode jumping)



Spectral scans (shifting of frequency comb)



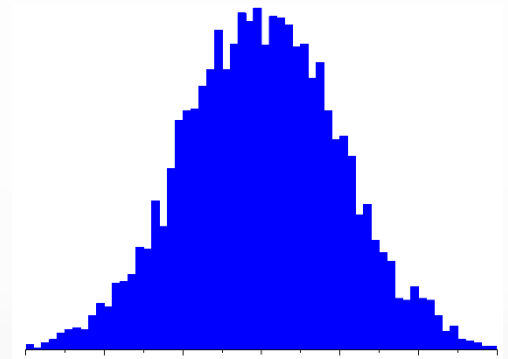
1. lock to local r
2. acquire ring-
3. shift comb wi
4. laser tracks c

Noise-Equivalent Absorption Coefficient (NEA)

corresponds to the standard error in the cavity losses
at a 1 s averaging time (units: $\text{cm}^{-1}/\text{Hz}^{1/2}$)

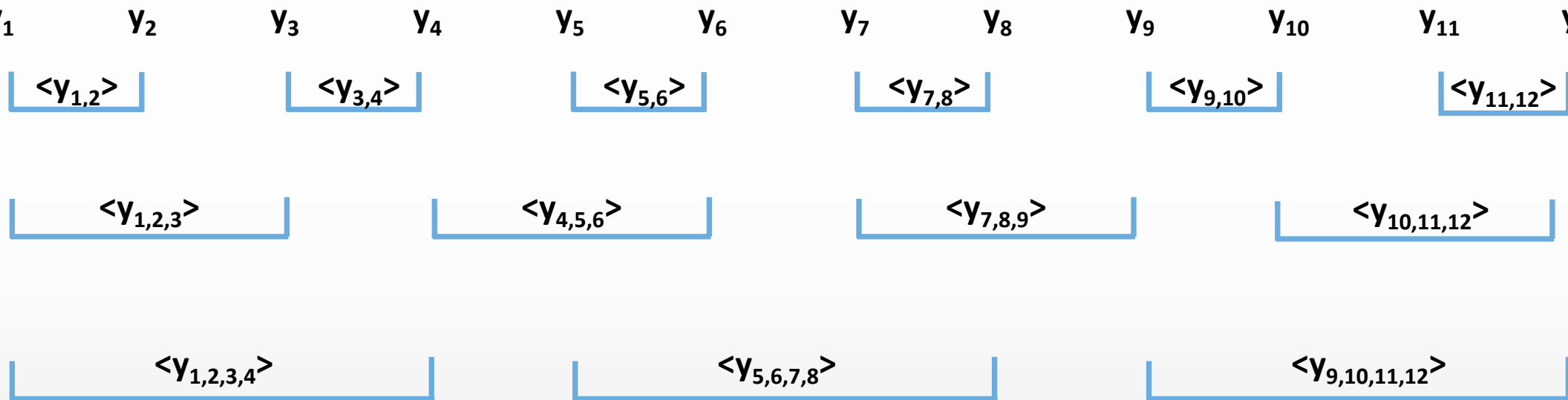
$$\alpha_{min} = \frac{\sigma_{\tau}}{\tau} \frac{L_{mirr}}{\ell} \frac{1}{\sqrt{N_{dec}}} = \frac{\sigma_{\tau}}{\tau} \frac{L_{mirr}}{\ell} \frac{1}{\sqrt{f_{acq} \Delta t_{av}}}$$

$$NEA = \alpha_{min} \sqrt{\Delta t_{av}} = \frac{\sigma_{\tau}}{\tau} \frac{L_{mirr}}{\ell} \frac{1}{\sqrt{f_{acq}}}$$



Distribution of measured
time constants with mean
value, τ and standard
deviation, σ_{τ} .

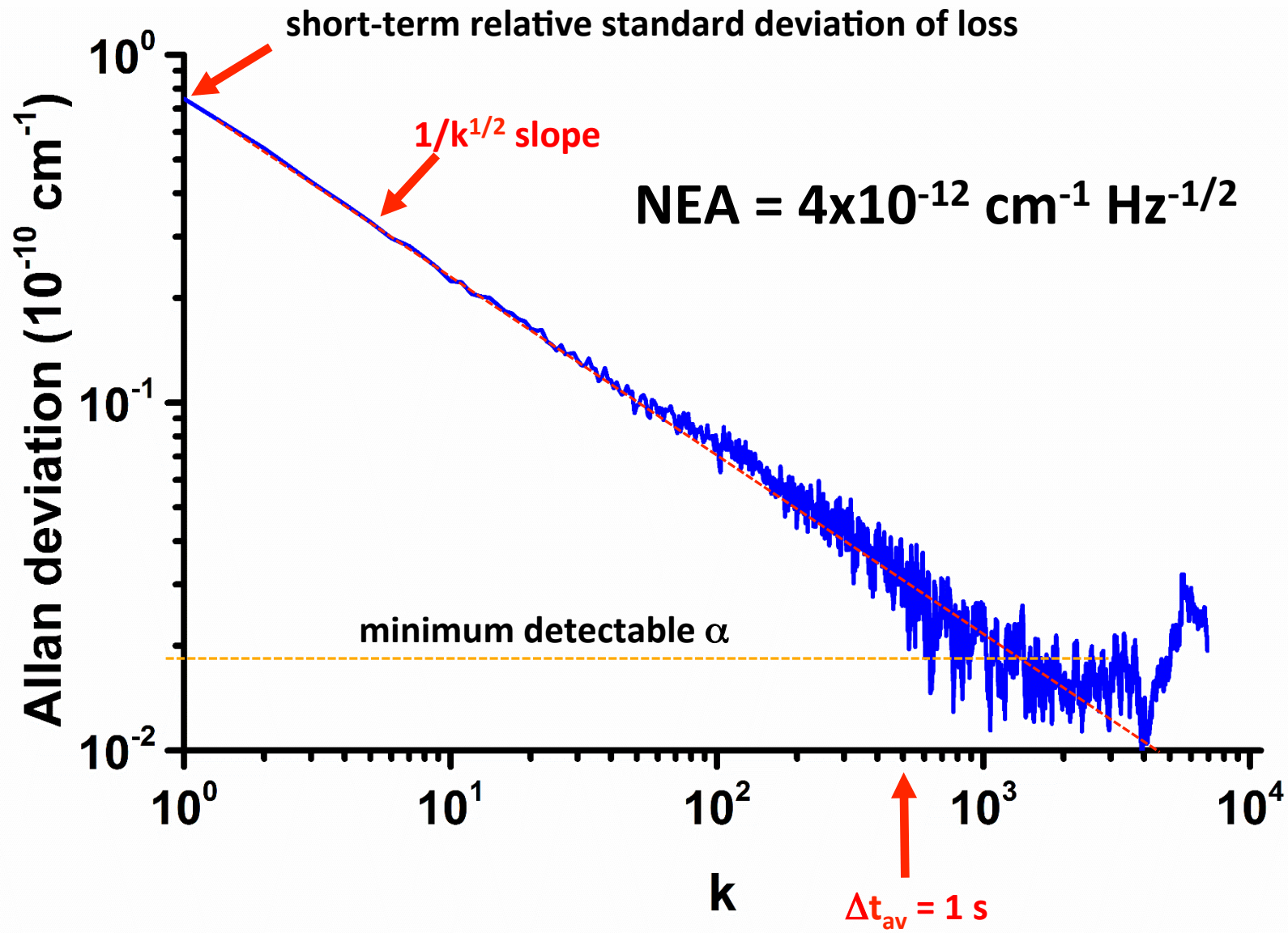
Allan Variance



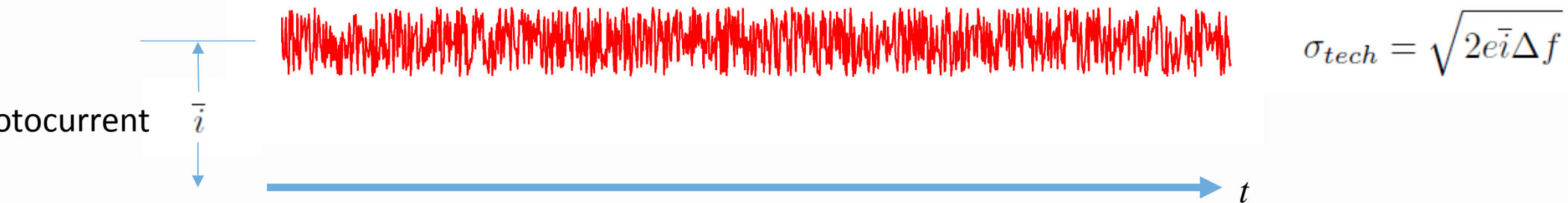
an upper bound on the time scale over which the measurements are statistically stationary

to specify the noise-equivalent absorption coefficient in ($\text{cm}^{-1} \text{Hz}^{-1/2}$) and minimum detectable ab

Allan Deviation Plot



Shot Noise for CW signals



$$SNR = \frac{\bar{i}}{\sigma_{tech}} = \sqrt{\frac{\bar{i}^2}{2e\bar{i}\Delta f}} = \sqrt{\frac{\bar{i}\Delta t_s}{e}} = \sqrt{N_e}$$

The signal-to-noise ratio corresponds to the square root of the number of photo-electrons, N_e in the sampling time interval, Δt_s

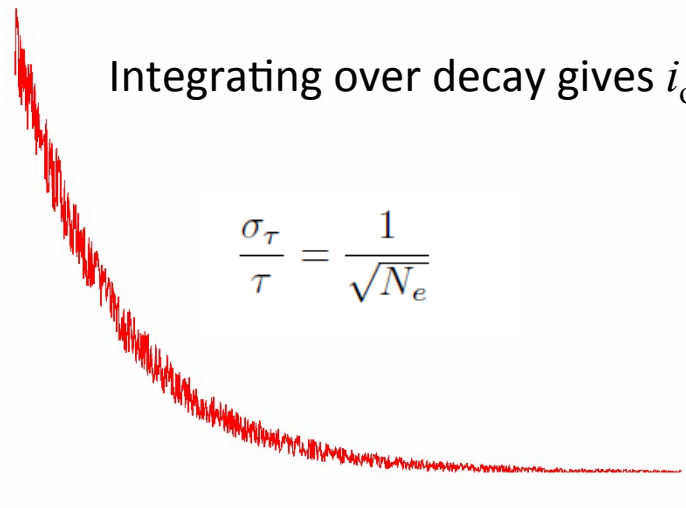
Noise limits for CRDS signals

Shot noise

RMS of noise decays exponentially with time constant of $\tau/2$

Integrating over decay gives $i_0\tau$ photoelectrons, N_e .

$$\frac{\sigma_\tau}{\tau} = \frac{1}{\sqrt{N_e}}$$

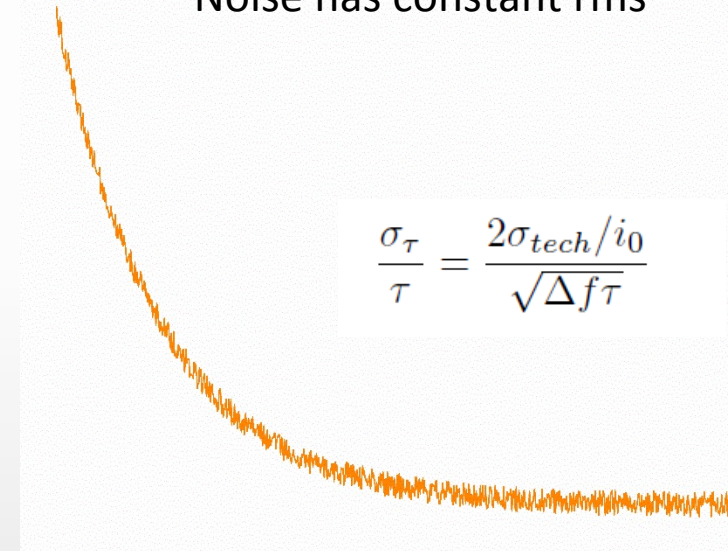


Must be weighted to avoid bias in fitted τ

Technical noise

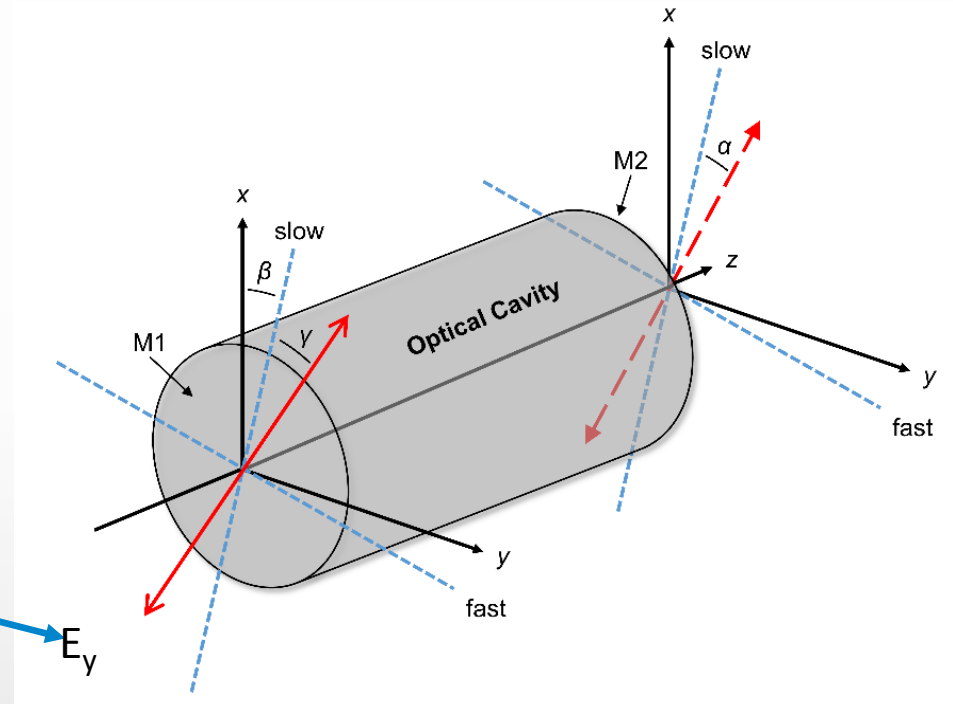
Noise has constant rms

$$\frac{\sigma_\tau}{\tau} = \frac{2\sigma_{tech}/i_0}{\sqrt{\Delta f\tau}}$$



No weighting required

Effect of birefringence and polarization-dependent loss



Can define effective “slow” and “fast” axes for the cavity

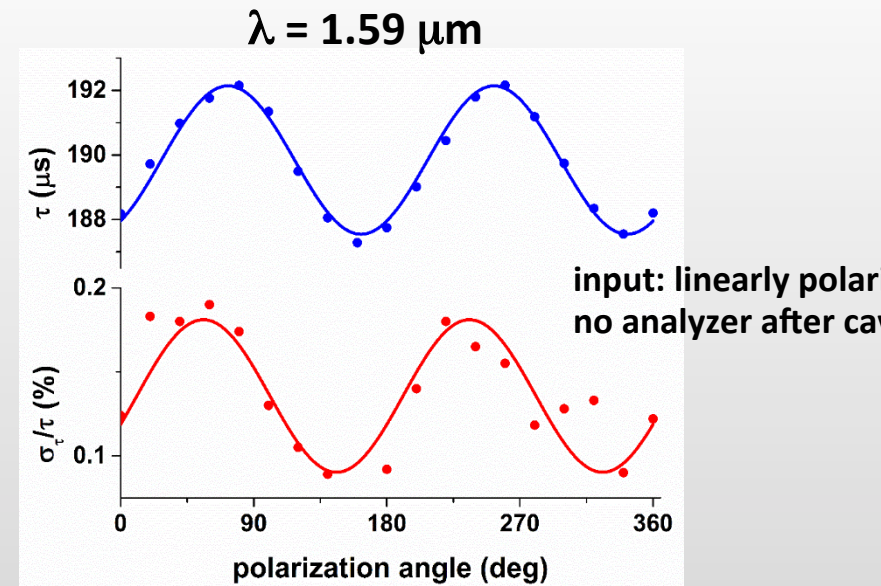
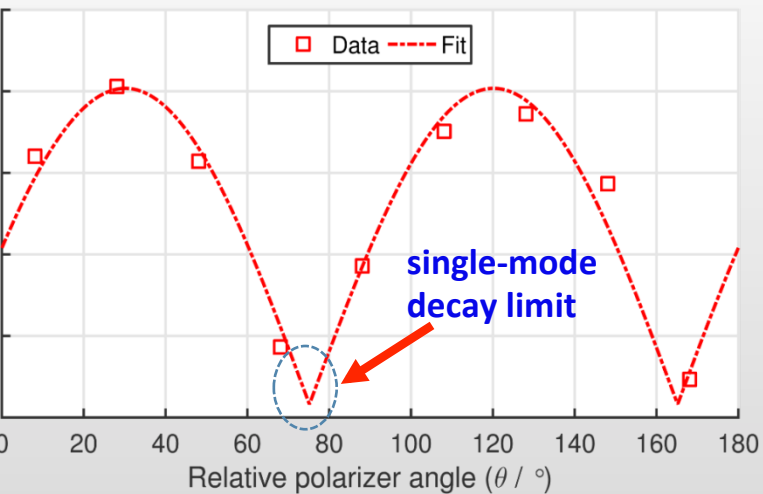
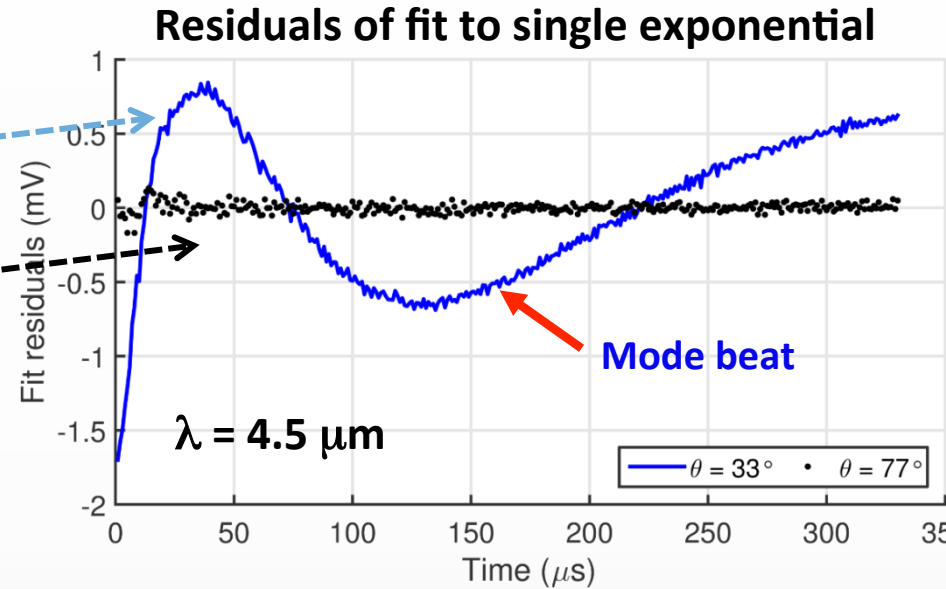
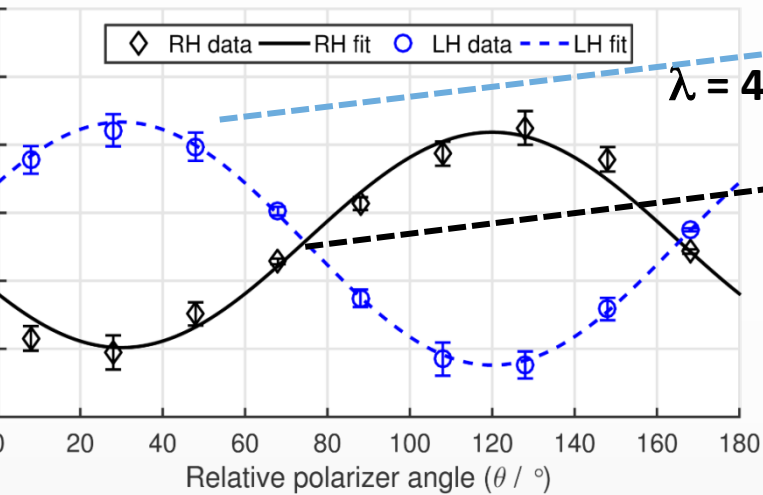
Difference in round-trip time for the two orthogonal polarizations leads to slightly different resonant frequencies for the TEM_{00} mode

$\Delta\nu \sim \Delta n \cdot \text{cavity free spectral range}$

Causes non-exponential decays & statistical broadening of measured time constant

Birefringence and polarization-dependent losses

input: circularly polarized
with analyzer after cavity



High Order Transverse Modes

$$\nu_{qmn} = \frac{c}{2\ell} \left[q + \frac{2}{\pi} \tan^{-1} \left(\frac{\ell}{\sqrt{\ell(2r - \ell)}} \right) (m + n + 1) \right]$$

$\ell = 157 \text{ cm}, r = 100 \text{ cm}$

Δ_{mn} (MHz)	Δq (MHz)	-12	-11	-10	-9	-8	-7	-6	-5	-4	-3	-2	-1	0
		Transverse Mode Beat Frequency (MHz)												
0		-1146	-1050	-955	-859	-764	-668	-573	-477	-382	-286	-191	-95	0
1		-1080	-984	-889	-793	-698	-602	-507	-411	-316	-220	-125	-29	67
2		-1013	-918	-822	-727	-631	-536	-441	-345	-250	-154	-59	37	133
3		-947	-852	-756	-661	-565	-470	-374	-279	-183	-88	8	103	199
4		-881	-786	-690	-595	-499	-404	-308	-213	-117	-22	74	169	265
5		-815	-719	-624	-528	-433	-337	-242	-147	-51	44	140	235	331
6		-749	-653	-558	-462	-367	-271	-176	-80	15	111	206	302	398
7		-683	-587	-492	-396	-301	-205	-110	-14	81	177	272	368	464
8		-616	-521	-425	-330	-234	-139	-43	52	147	243	338	434	530
9		-550	-455	-359	-264	-168	-73	23	118	214	309	405	500	596
10		-484	-389	-293	-198	-102	-7	89	184	280	375	471	566	662
11		-418	-322	-227	-131	-36	60	155	250	346	441	537	632	728
12		-352	-256	-161	-65	30	126	221	317	412	508	603	699	795
13		-286	-190	-95	0.93	96	192	287	383	478	574	669	765	861
14		-219	-124	-28	67	163	258	354	449	544	640	735	831	927

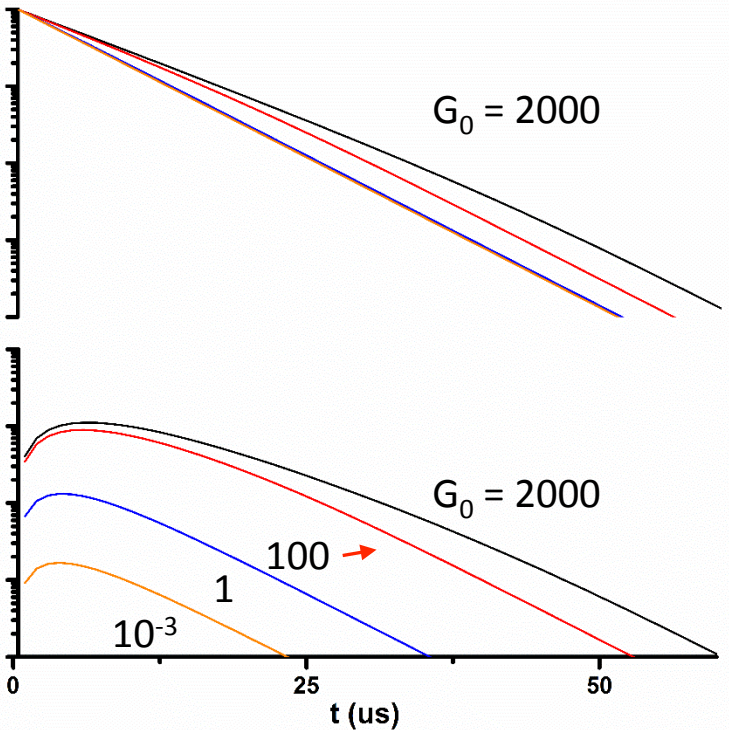
TEM_{6,7}

Saturation in CRDS

Inhomogeneously broadened case

$$G(t) = G_0 e^{-t/\tau_c} f(t; G_0, \tau_c, \tau_{abs})$$

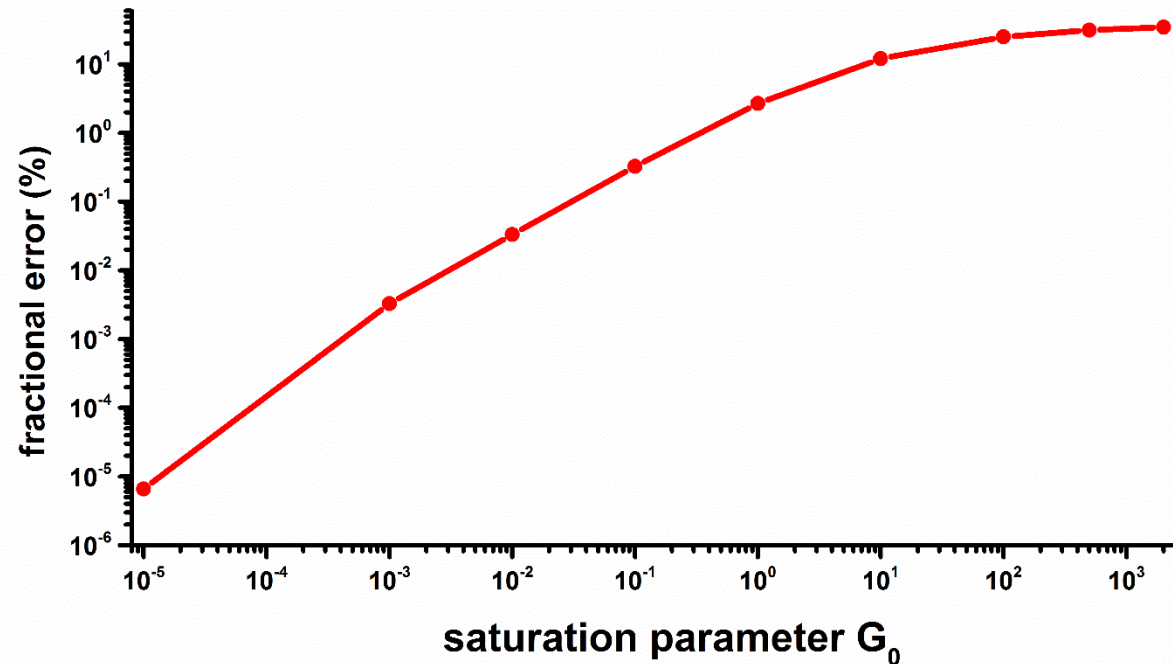
$$\frac{df}{dt} = \frac{-2f(t)/\tau_{abs}}{1 + \sqrt{1 + G_0 e^{-t/\tau_c} f(t)}}, f(0) = 1$$



$$P_{\text{sat}} = T w^2 h c \Gamma_1 \Gamma_2 k^3 / (8 \pi A_{21}) : \text{saturation power}$$

$$G_0 = P_{\text{circ}} / P_{\text{sat}} : \text{saturation parameter}$$

Γ_1 : population relaxation rate
 Γ_2 : dephasing rate

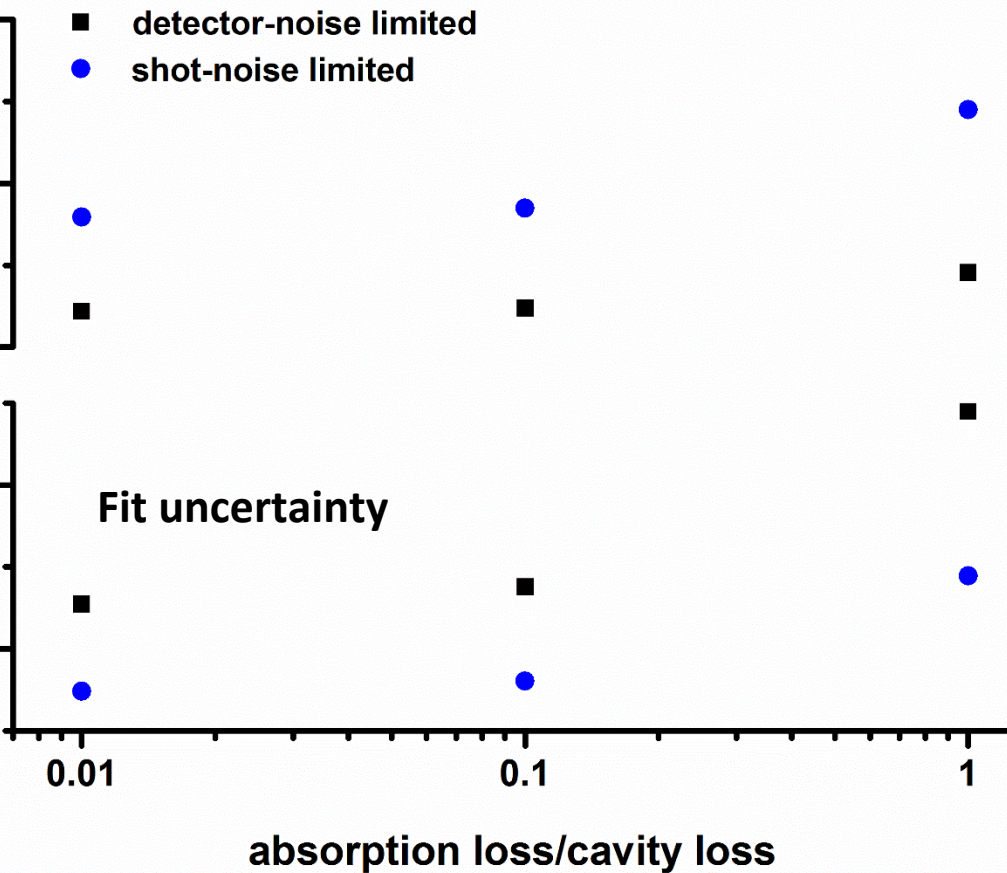


$\tau_c = 0.4$
 μs

Cancio et al, "Saturated-absorption cavity ring-down (SCAR) for high-sensitivity and high-resolution molecular spectroscopy in the mid-IR," Chap. 4, Cavity-enhanced spectroscopy & sensing, eds. Gagliardi & Loock, p. 143 (2014).

Sensitivity of SCAR method

Inhomogeneous broadening case



Theoretical advantage:

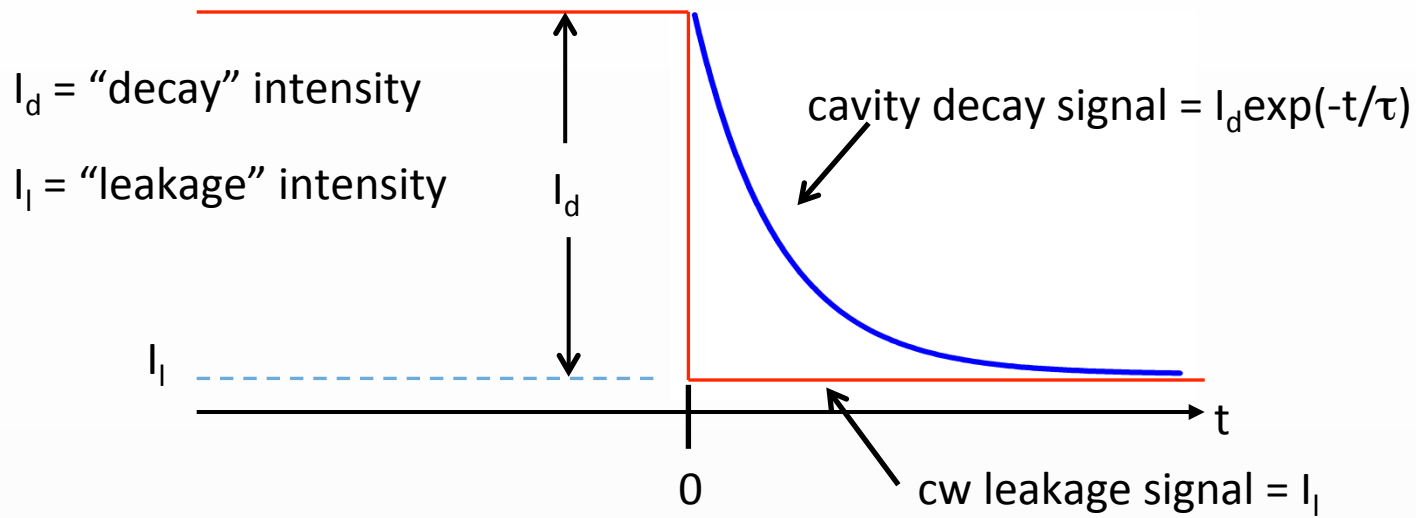
Can measure empty-cavity and absorption in a single decay

In practice:

Parameter correlations lead to relatively large uncertainties in fitted values

Must measure at optimal saturation parameter value, thus restricting useful range of the technique

$$\text{Extinction ratio} = 10 \log(I_d/I_l)$$



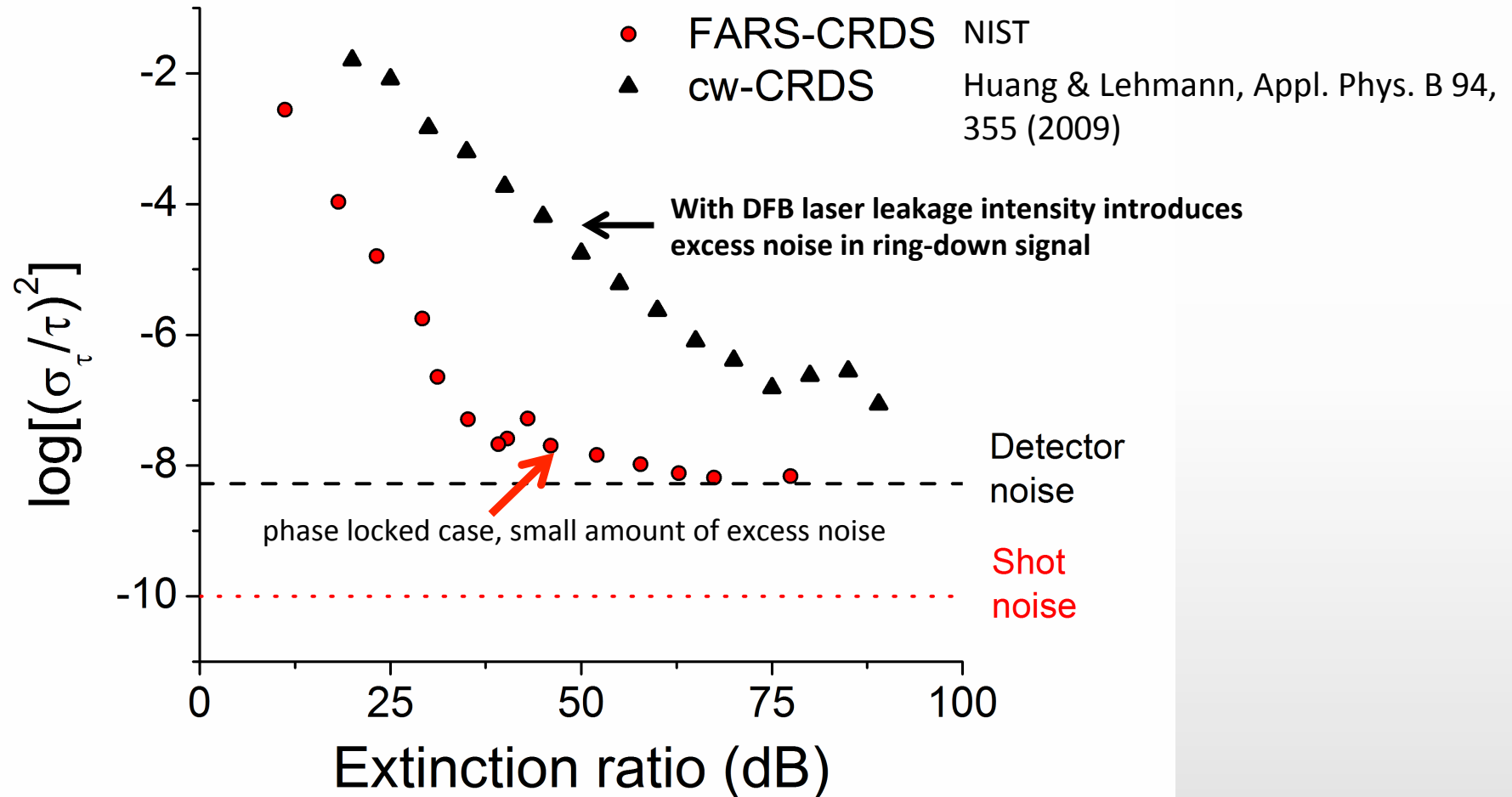
Ideal case (infinite extinction ratio): $I_l = 0$, \rightarrow exponential decay

Actual case:

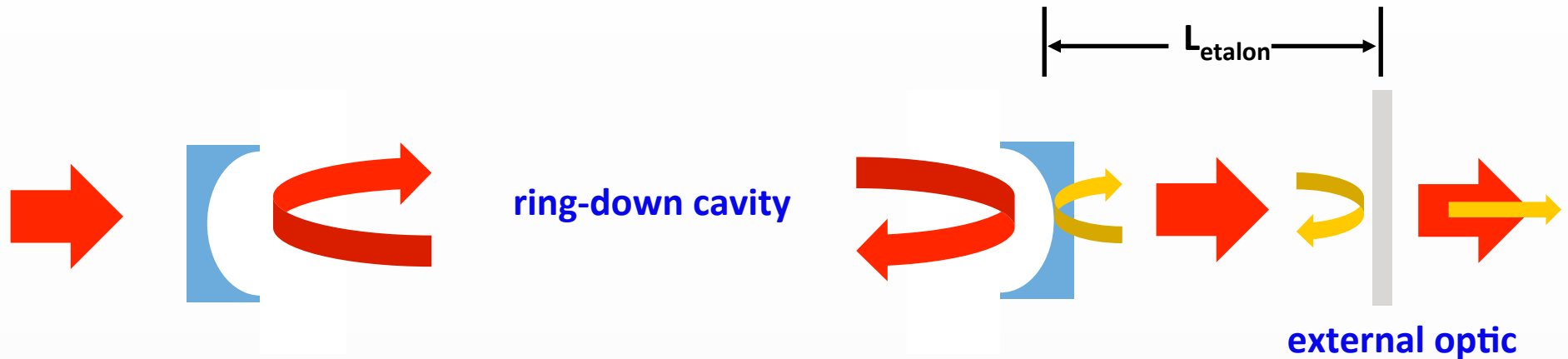
**leakage intensity interferes with decay signal
to yield noisier and/or non-exponential decay**

$$y(t) = y_0 + A[e^{-t/\tau} + 2\sqrt{I_l(t)/I_d} e^{-t/(2\tau)} + I_l(t)/I_d]$$

Effect of extinction ratio on the precision of measured τ



Coupled Cavities



Coupled cavities (“etalons”) are caused by reflections between normal incidence optics exterior to primary cavity and the nearest ring-down cavity mirror

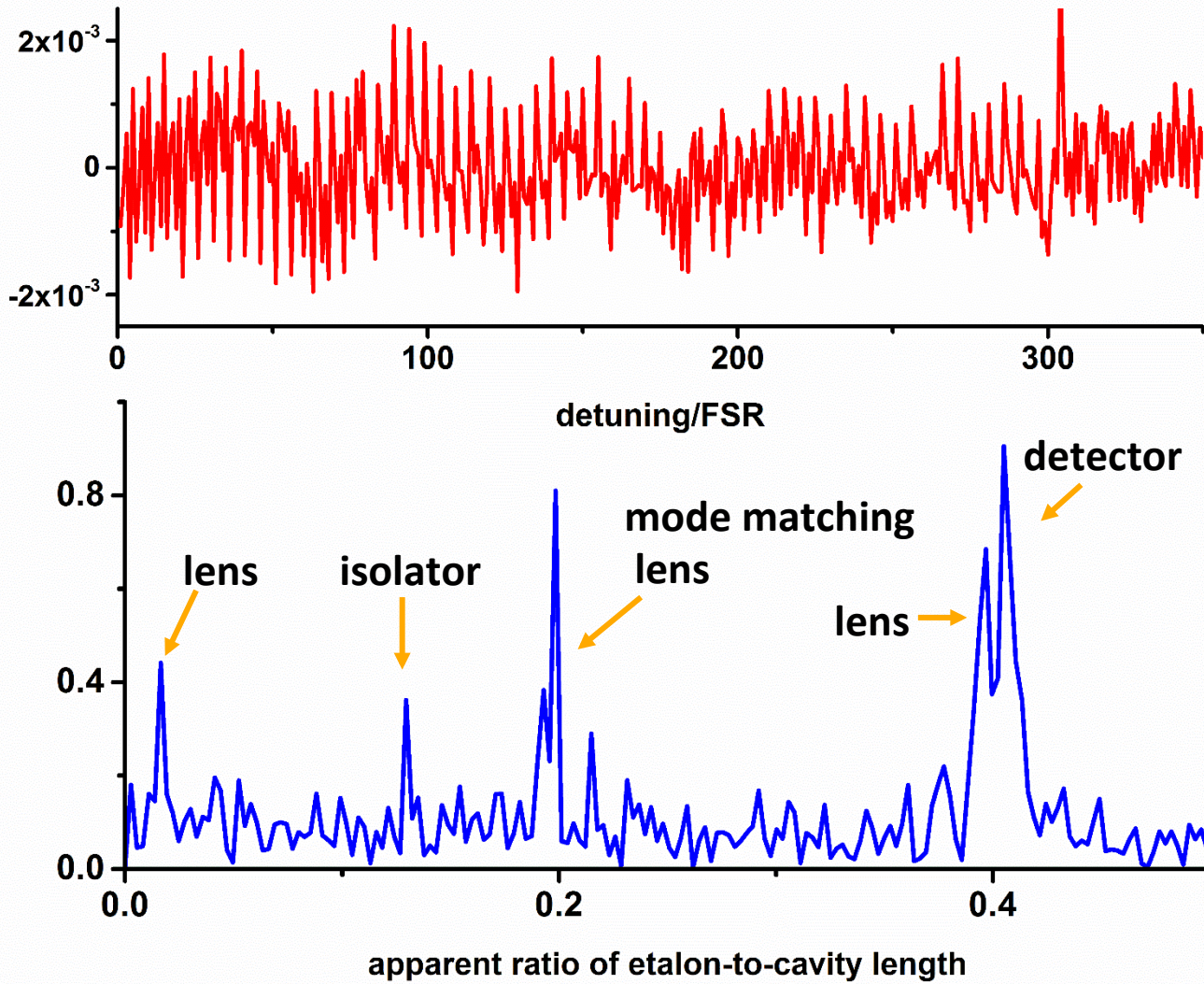
They lead to weak modulation of base losses with a spectrum period of $c/2L_{\text{etalon}}$

Poorly characterized, time-dependent etalons often limit the precision of CRDS spectral baselines

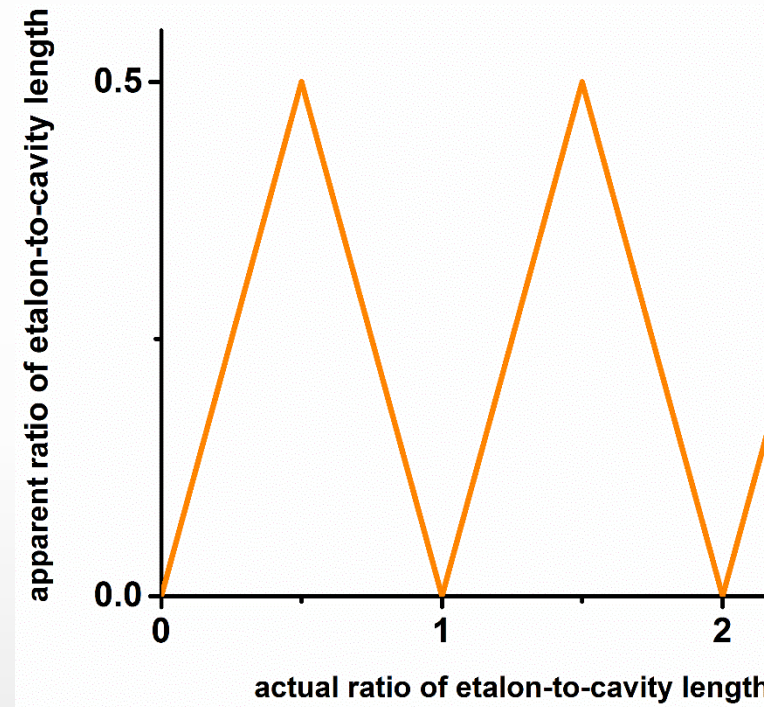
They can be reduced using isolators, low-reflectivity optics and by tilting components

Assigning Etalons

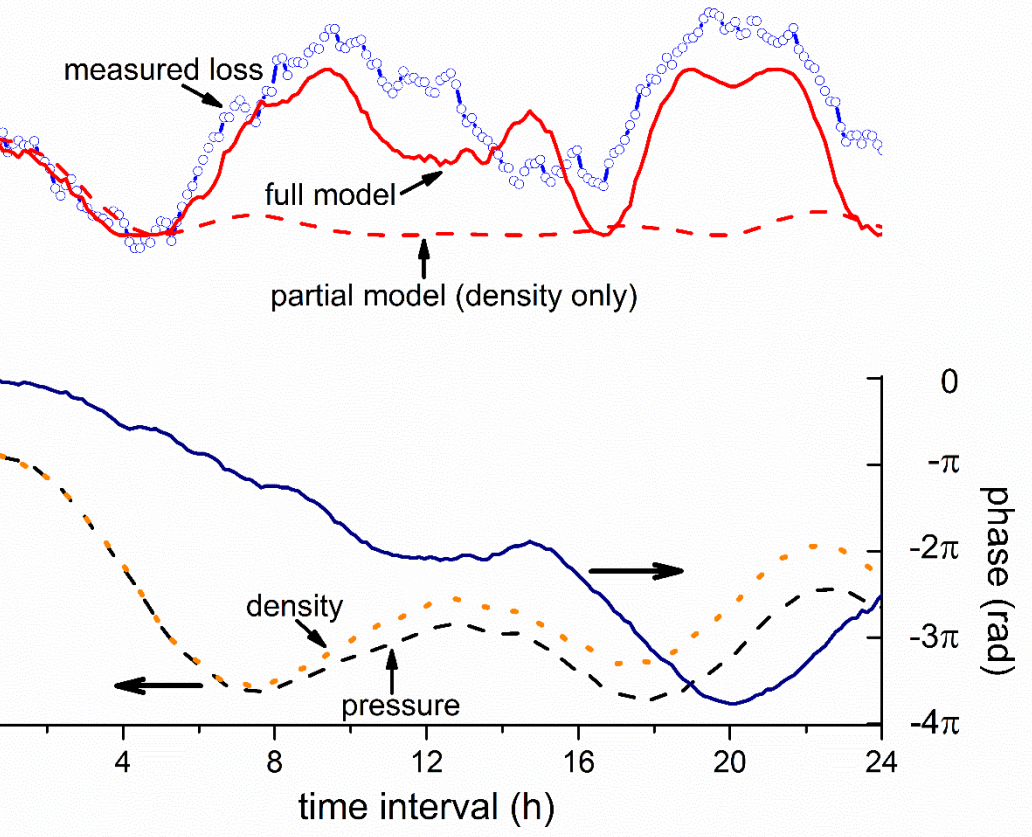
Spectrum of empty-cavity losses



Aliasing Effect



Drift in losses for a length-stabilized cavity



Modeled by two mechanisms:

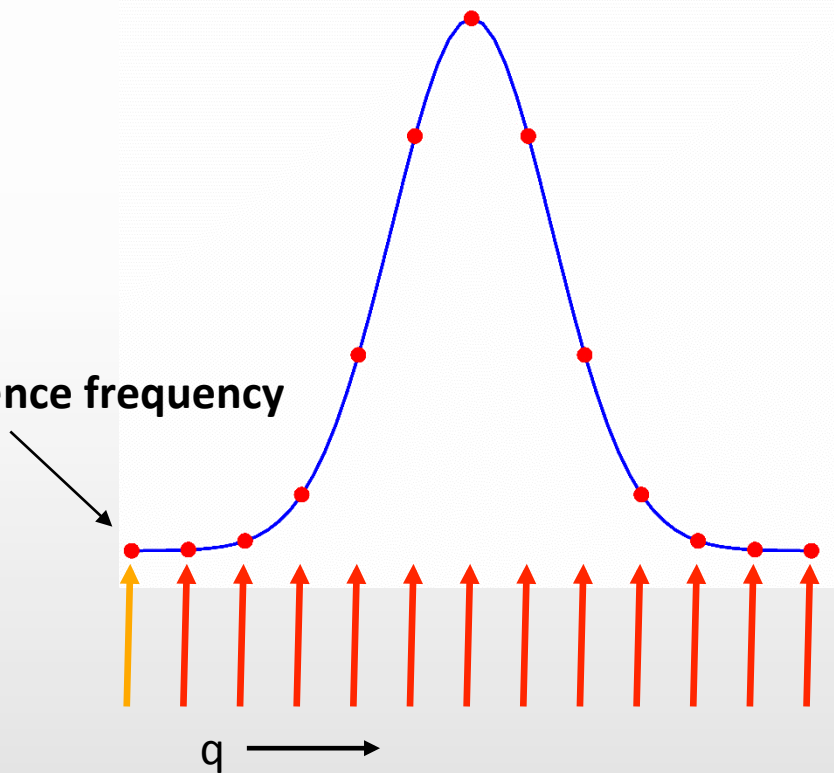
Density dependent changes in refractive index of laboratory air

Thermal expansion of optical table

Differential Cavity Ring-Down Spectroscopy

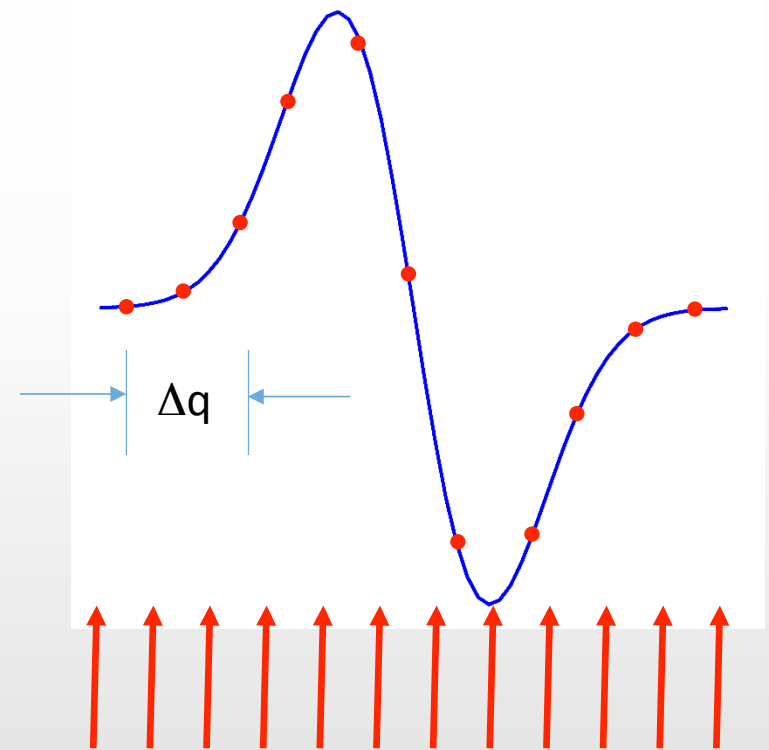
fixed reference mode¹

$$\Delta L_q = L(\nu_q) - L(\nu_0)$$

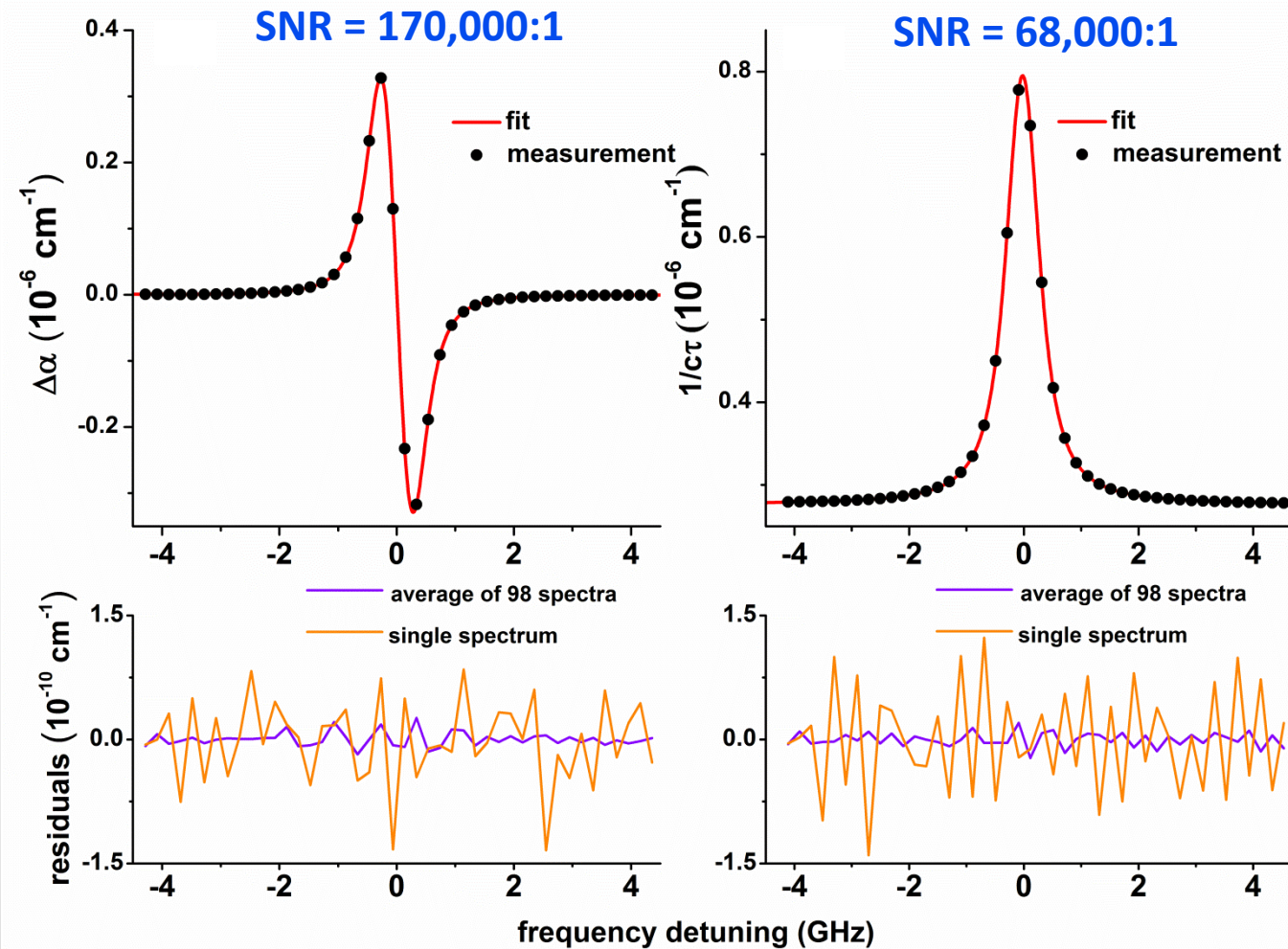


fixed frequency difference²

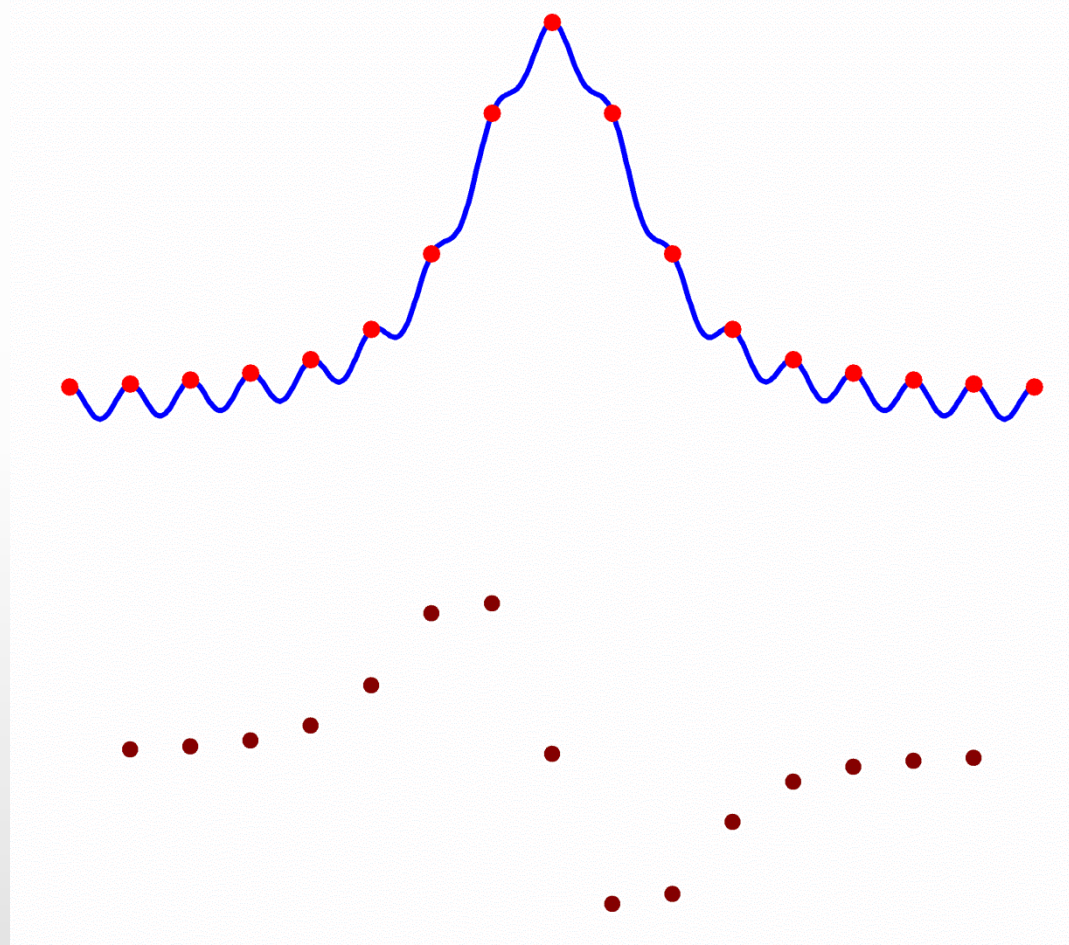
$$\Delta L_{q,q+\Delta q} = L(\nu_{q+\Delta q}) - L(\nu_q)$$



Improved signal-to-noise ratio (SNR) with differential-CRDS method



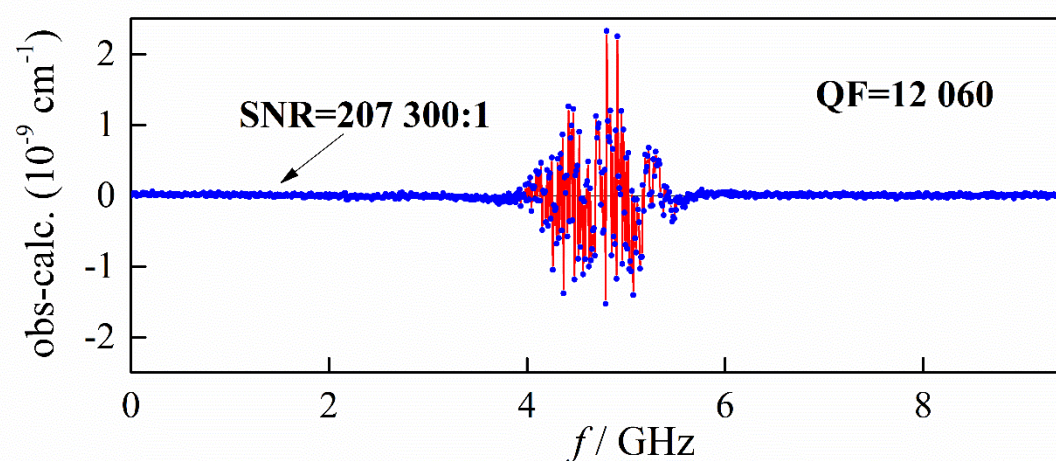
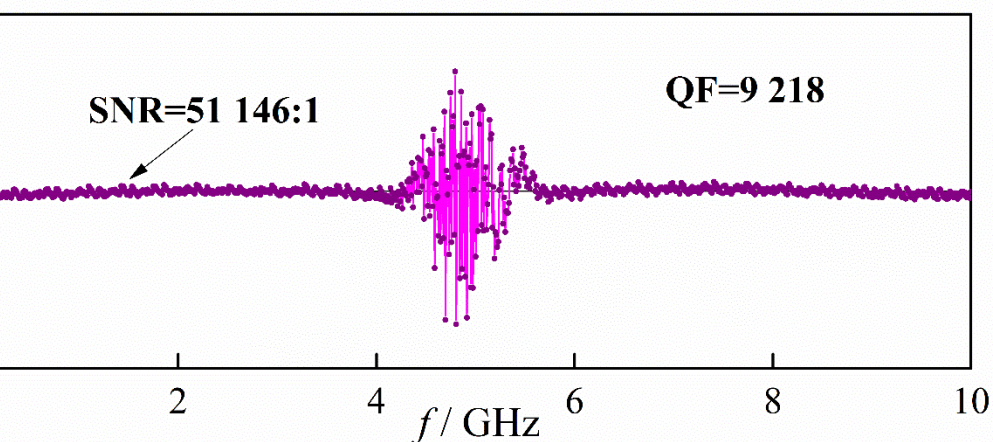
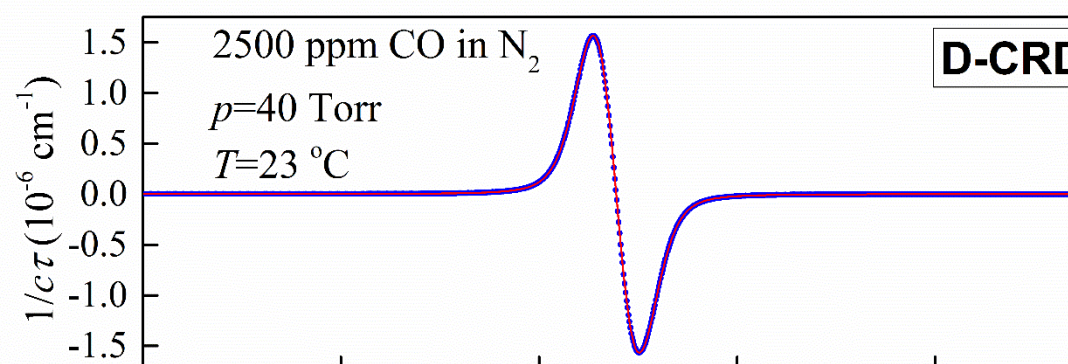
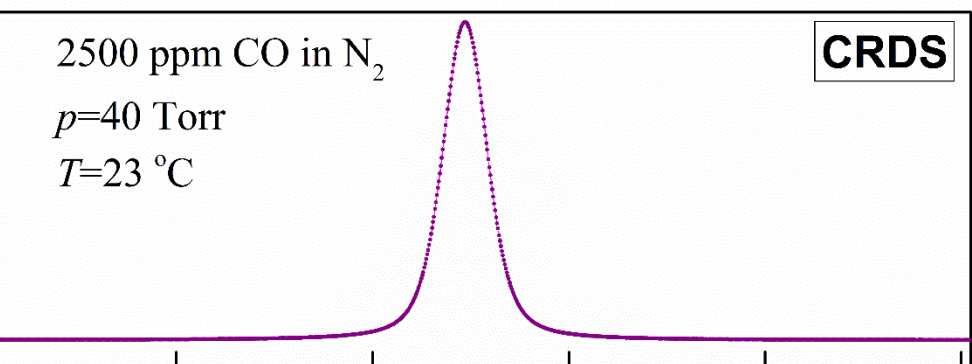
Etalon suppression with differential CRDS method



spectrum with baseline etalon

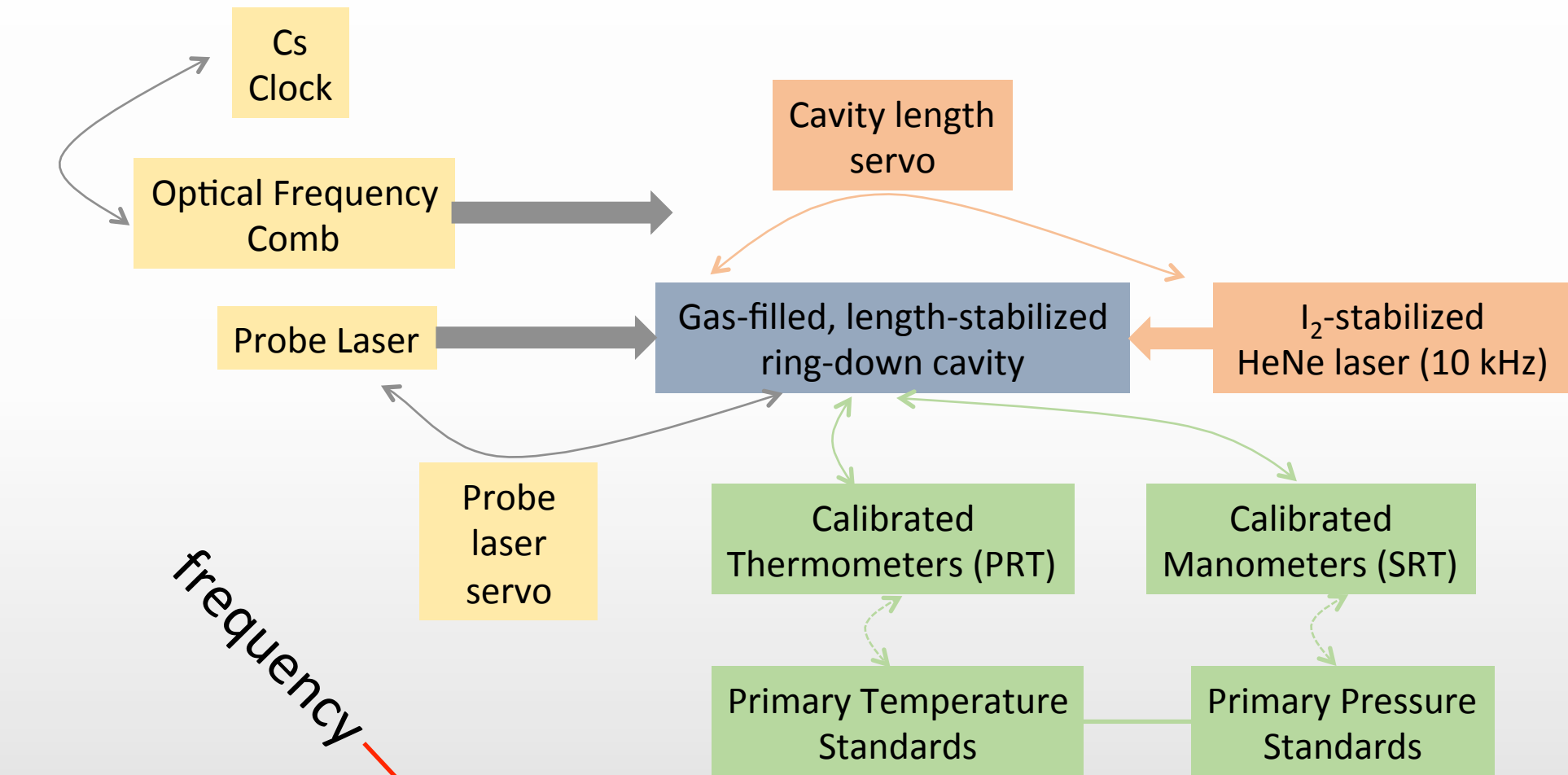
**differential CRDS spectrum
suppresses the etalon**

Using Differential CRDS to compensate for changes in mirror losses: Scanned-cavity case



Measuring line shapes and intensities

Linking measured line parameters to the SI



$$\alpha(\nu) = \alpha_0 + \alpha(\nu)$$

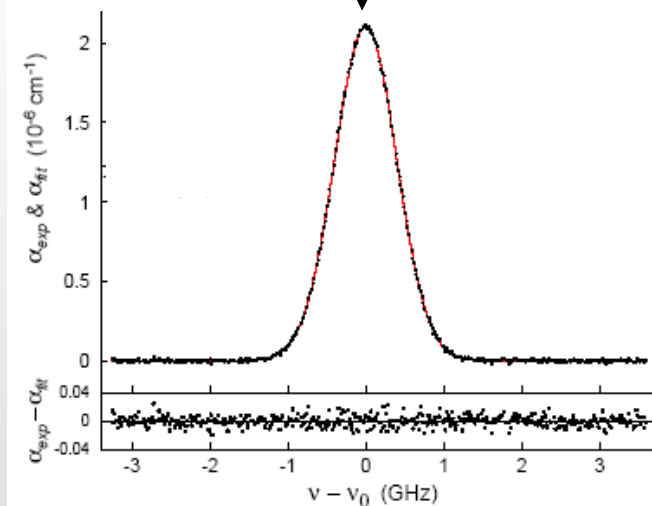
Measurement of Line Intensity (S) and Absorber Concentration (n)

$$S = \int \alpha(\nu) d\nu / \left\{ n \int g(\nu) d\nu \right\} = A/n$$

measured
absorption coefficient

line profile
(unity area)

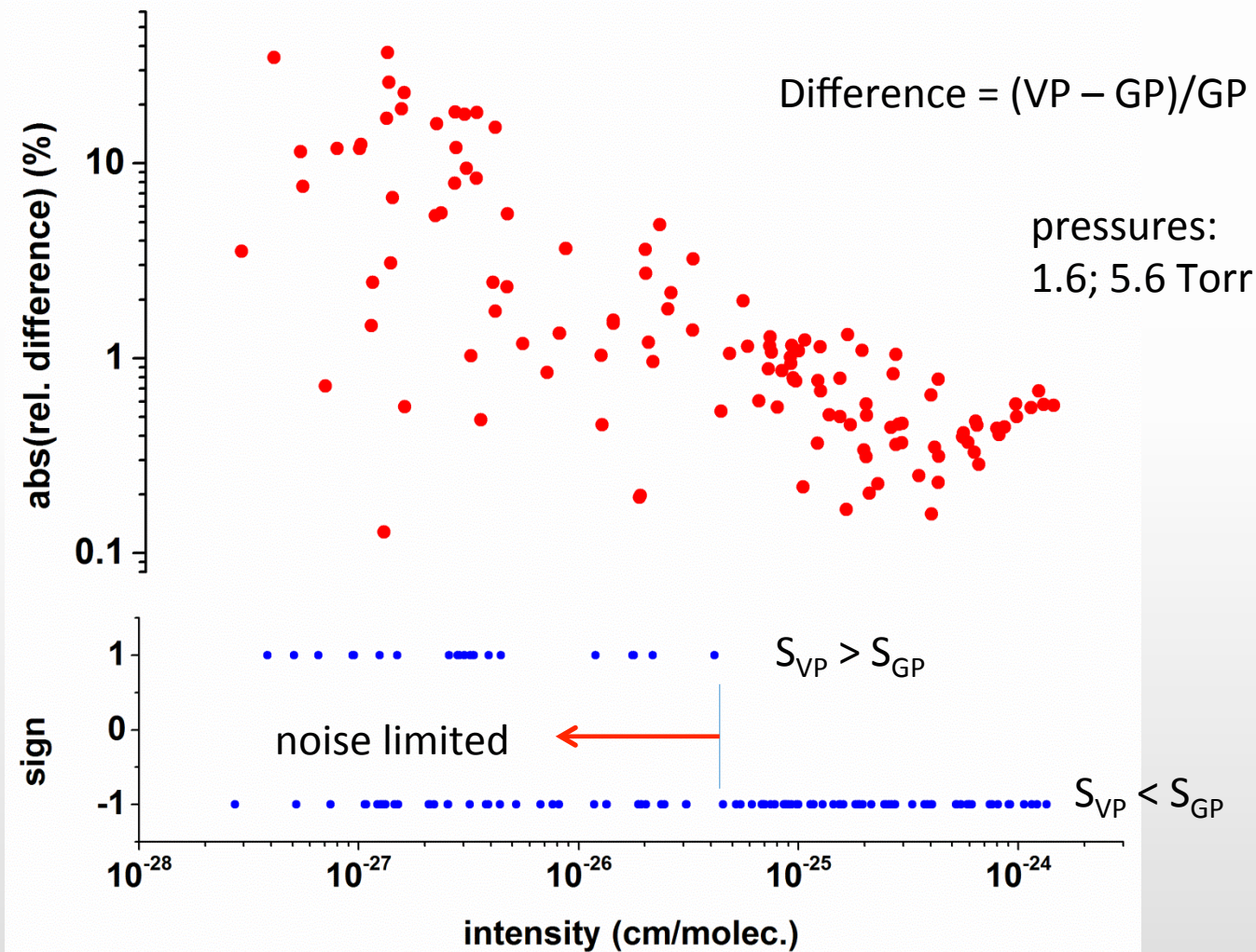
fitted spectrum area



Once the intrinsic property S is known, then

$$n = A/S$$

Dependence of fitted line profile area: Voigt vs. Galatry (H₂O transitions, 1.28 um region)



Voigt tends to underestimate line area

Partially correlated quadratic-speed-dependent Nelkin-Ghatak Profile (Hartmann-Tran Profile)

$$\mathcal{D}_{\text{DNG}} = \frac{\tilde{I}_{\text{qSDV}}(u; B_w \Gamma_0 / \omega_D + \tilde{z})}{1 - \pi \tilde{z} \tilde{I}_{\text{qSDV}}(u; B_w \Gamma_0 / \omega_D + \tilde{z})} \quad \text{Complex profile}$$

$$\tilde{\nu}_{\text{opt}} / \omega_D = [\nu_{\text{eff}} - \eta(\Gamma_0 + i\Delta_0)] / \omega_D \quad \text{Complex, normalized narrowing frequency}$$

$$\mathcal{B}_w(x) = 1 + a_w(x^2 - 3/2)$$

$$\mathcal{B}_s(x) = 1 + a_s(x^2 - 3/2)$$

Quadratic approximation to speed dependence

Correspondence between pCqSDHC and pCqSDNGP parameters

$$a_w = \Gamma_2 / \Gamma_0$$

$$a_s = \Delta_2 / \Delta_0$$

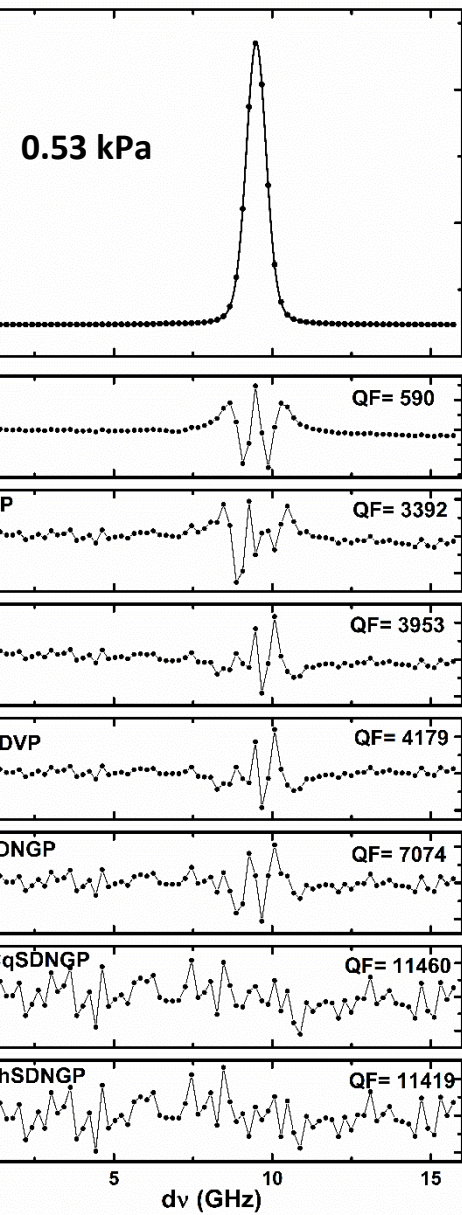
$$\text{Re}[\tilde{\nu}_{\text{opt}}] = \nu_{\text{vc}} - \eta \Gamma_0$$

$$\text{Im}[\tilde{\nu}_{\text{opt}}] = -\eta \Delta_0$$

Mechanisms: 1) collisional narrowing (hard-collision model), 2) speed-dependent broadening and shifting, partial correlations between velocity-changing and dephasing collisions

H₂O line shape study

single-spectrum fit



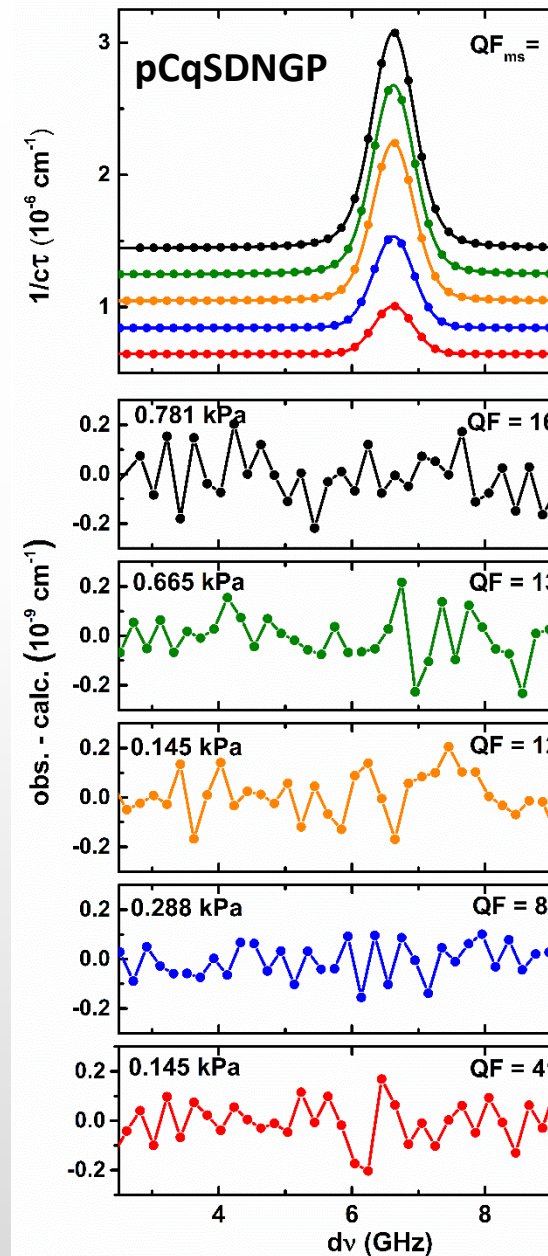
Need to include:

1. collisional narrowing
2. speed dependent effects
3. partial correlation between velocity-changing and dephasing collisions

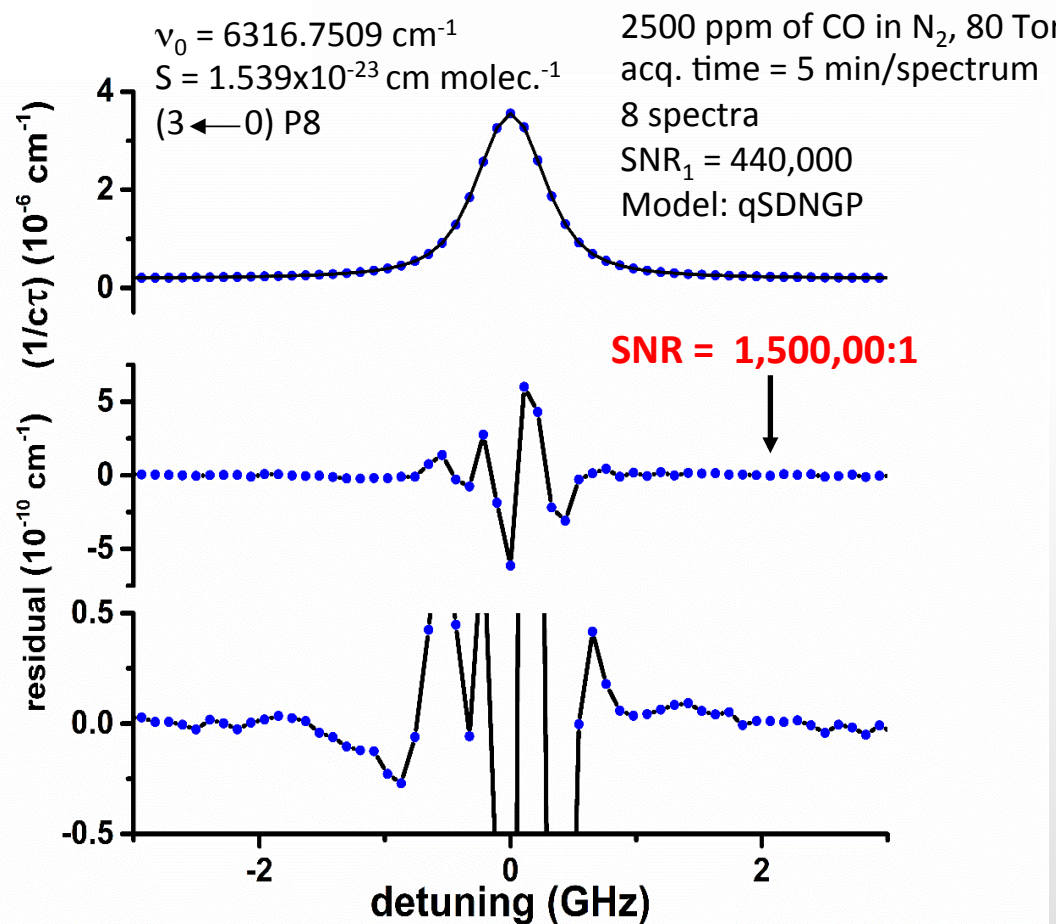
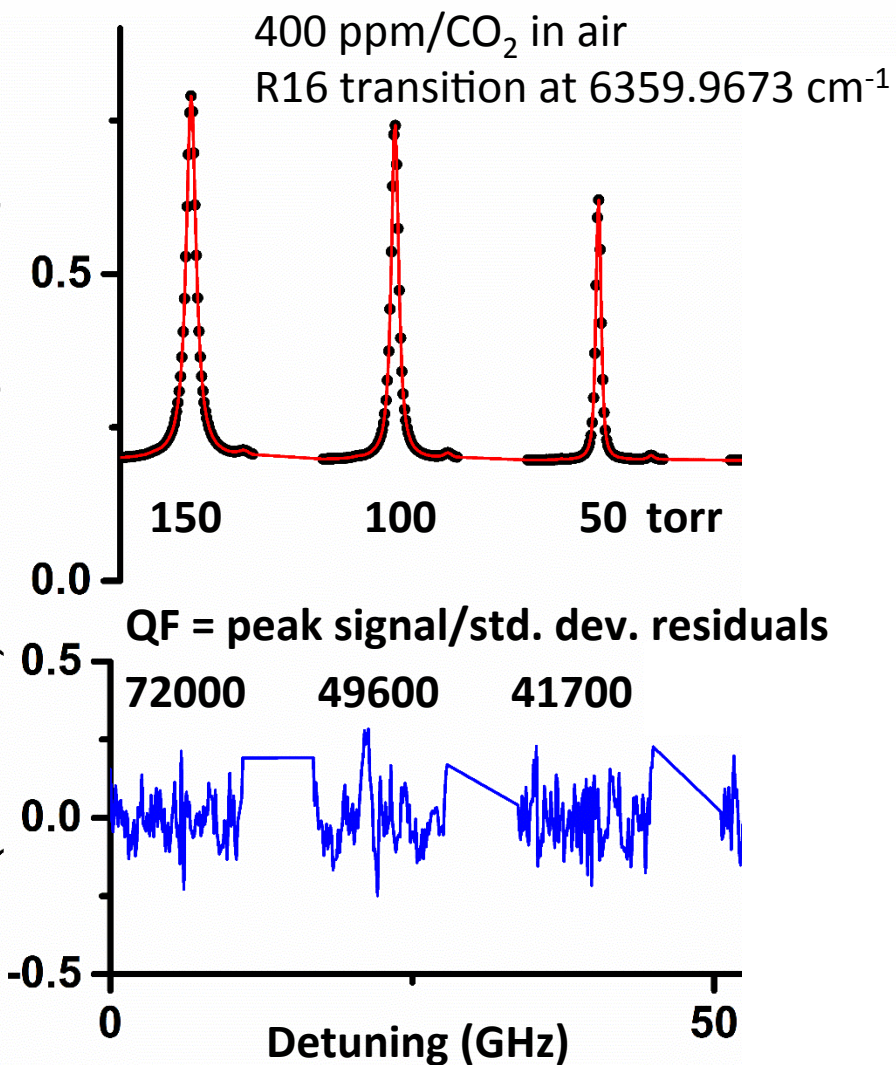
7892.3021 cm⁻¹
 $S = 1.89 \times 10^{-25}$ cm molec.⁻¹
 (002) - (000)
 (15 5 6) - (9 2 7): Q' - Q''

7799.9970 cm⁻¹
 $S = 2.58 \times 10^{-25}$ cm molec.⁻¹
 (002) - (000)
 (10 4 6) - (9 3 7): Q' - Q''

multi-spectrum fit

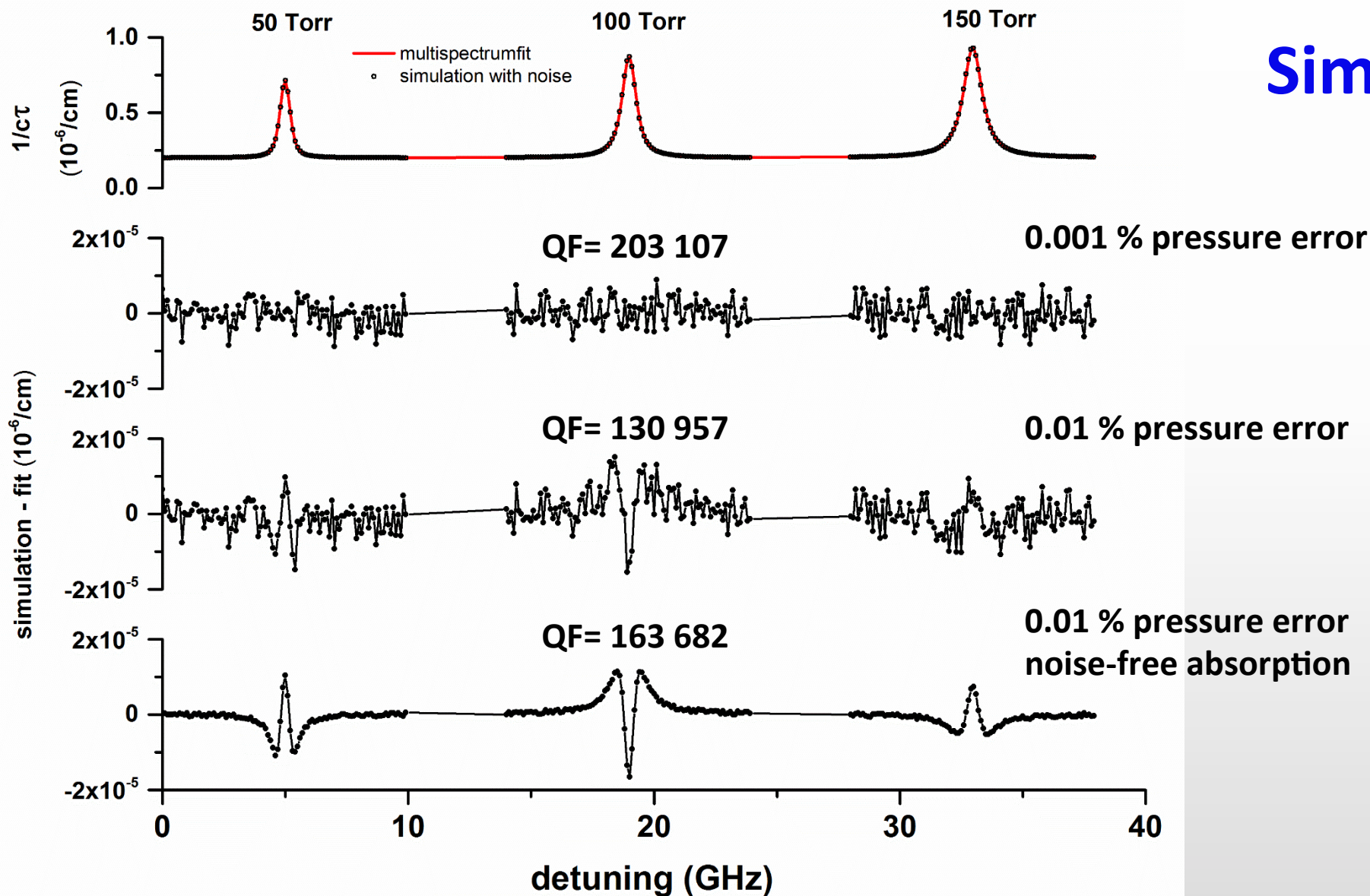


High precision line shape measurements

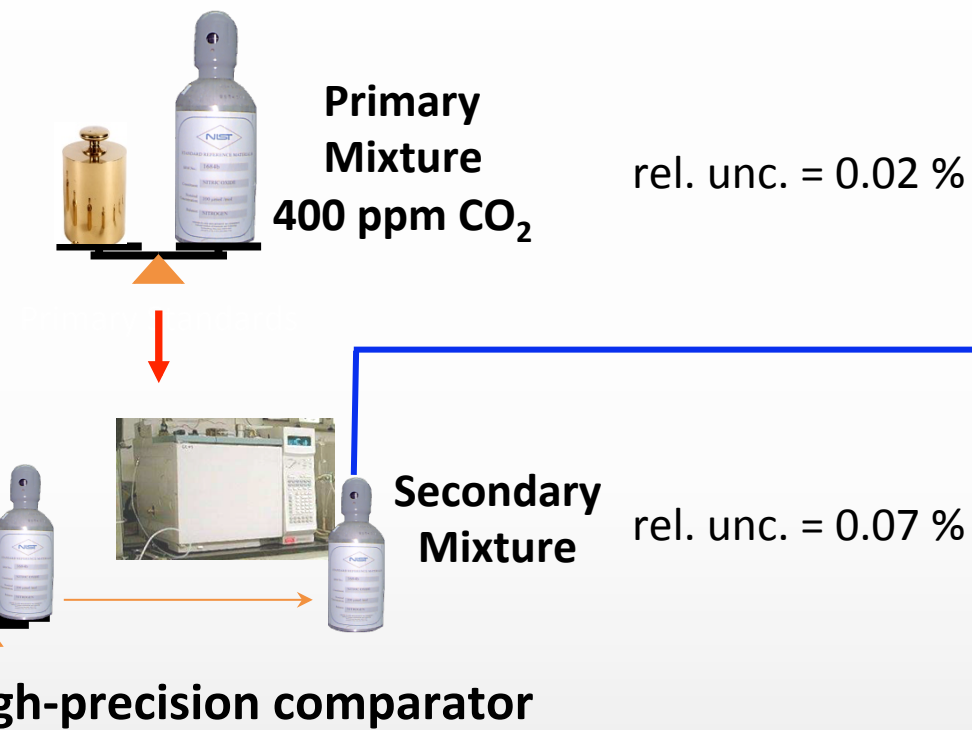


Sensitivity of multispectrum fits to error in pressure measurement

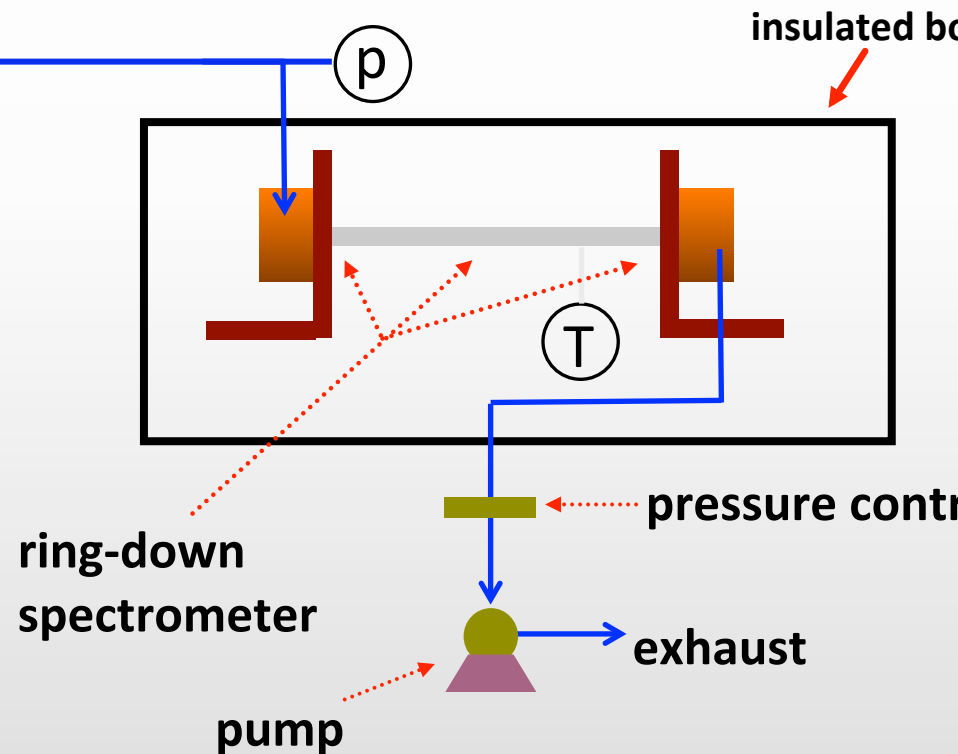
Simulation



CO₂-in-air sample preparation

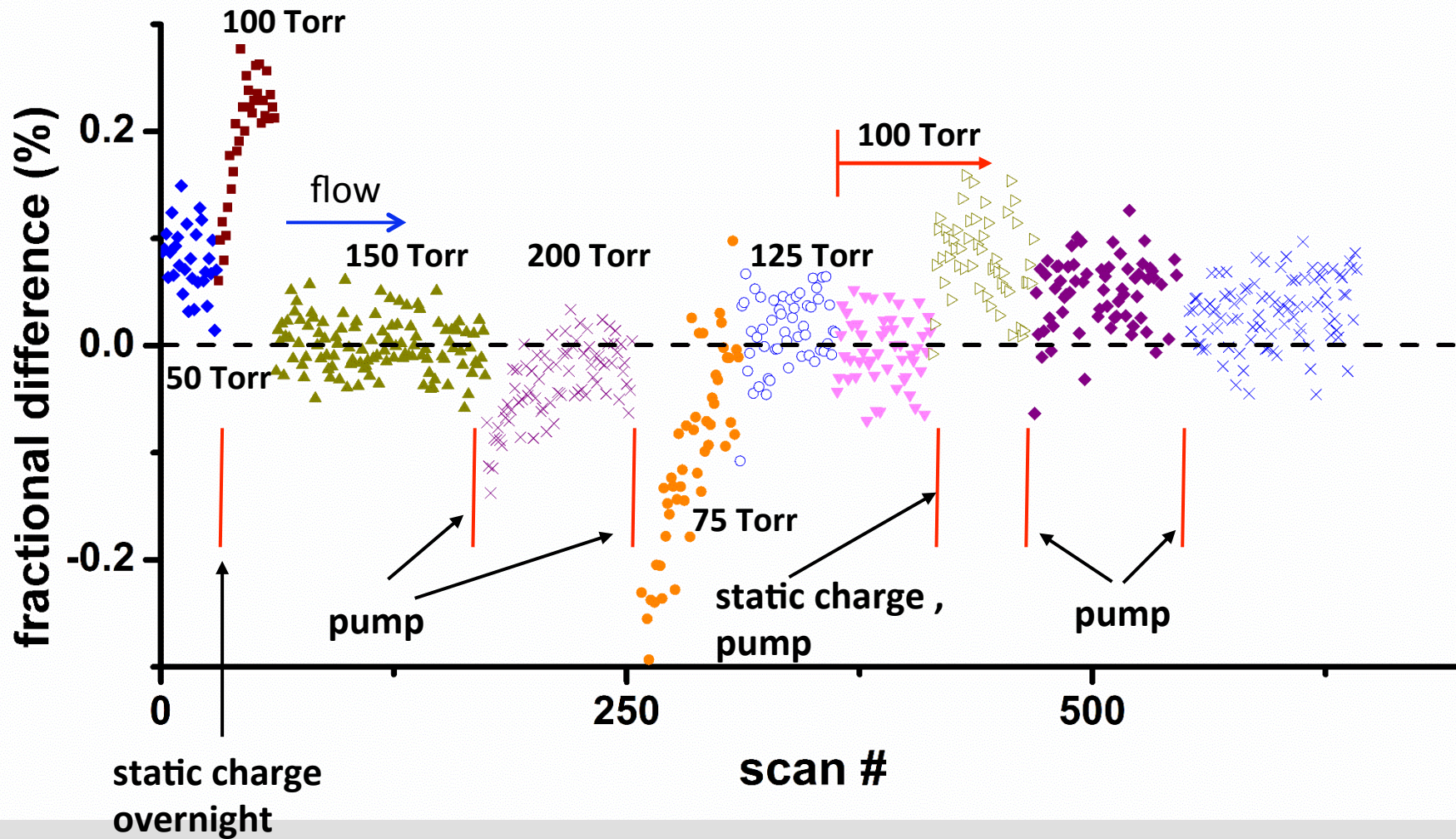


**Need steady flow of sample gas
mitigate wall effects**



CO₂ outgassing effects

2 % CO₂/air 387 ppm CO₂/air



Accuracy of CO₂ intensity measurements: 1.6 um region

Uncertainties

relative uncertainty (%)

0.05 0.10

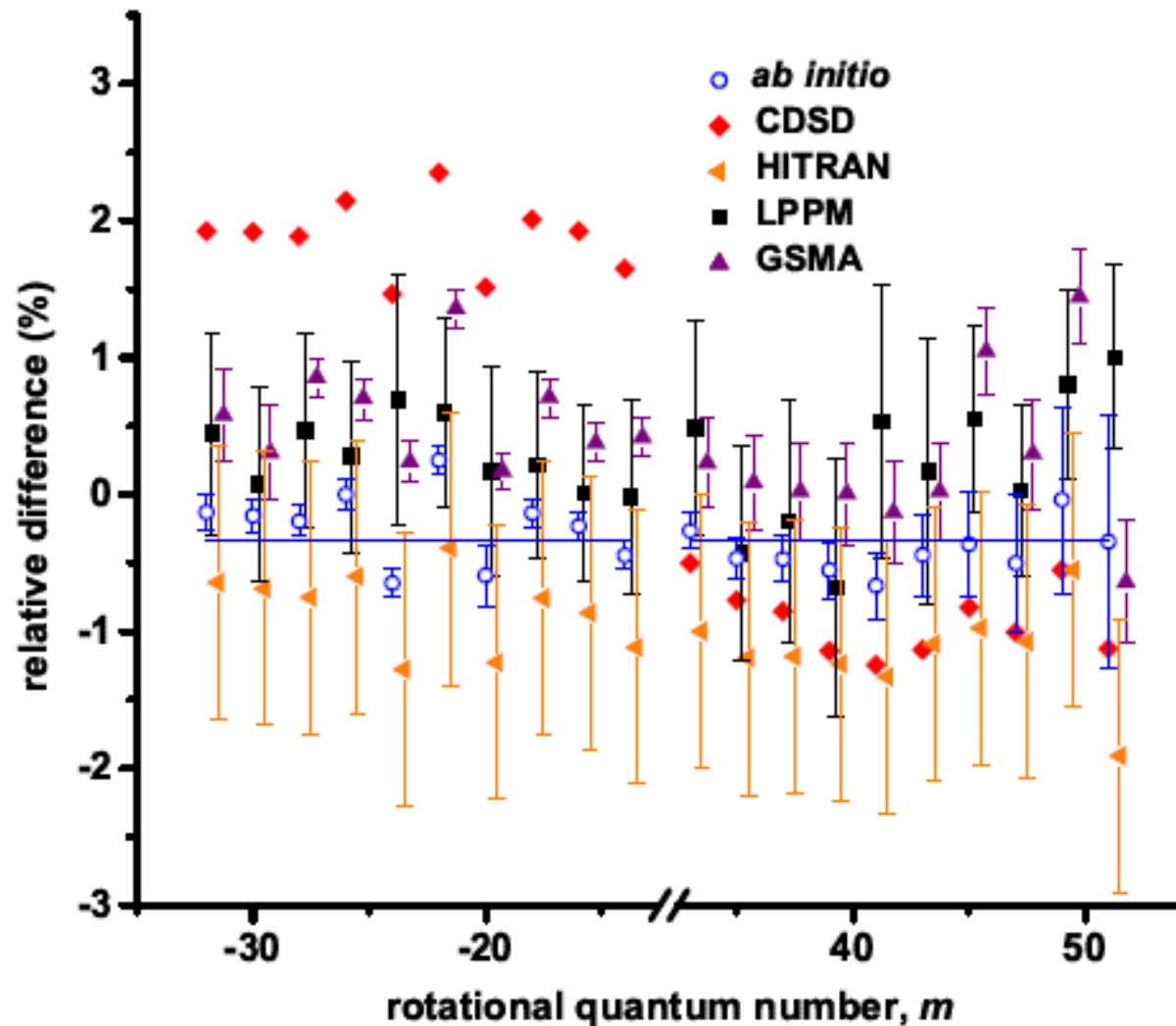
fit + residual area

isotopic composition

etalon

T, p, mole fraction

Total (quadrature sum)

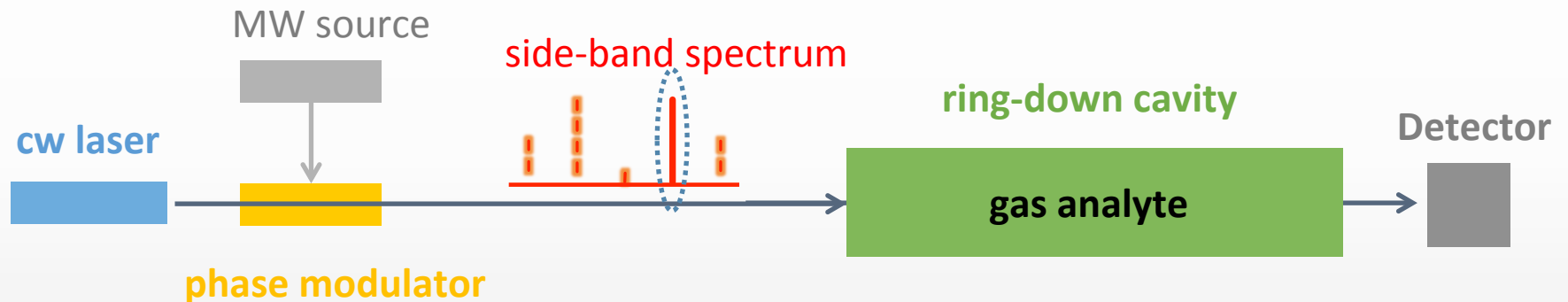


New measurement strategies

Frequency-agile, rapid scanning (FARS) spectroscopy

Method:

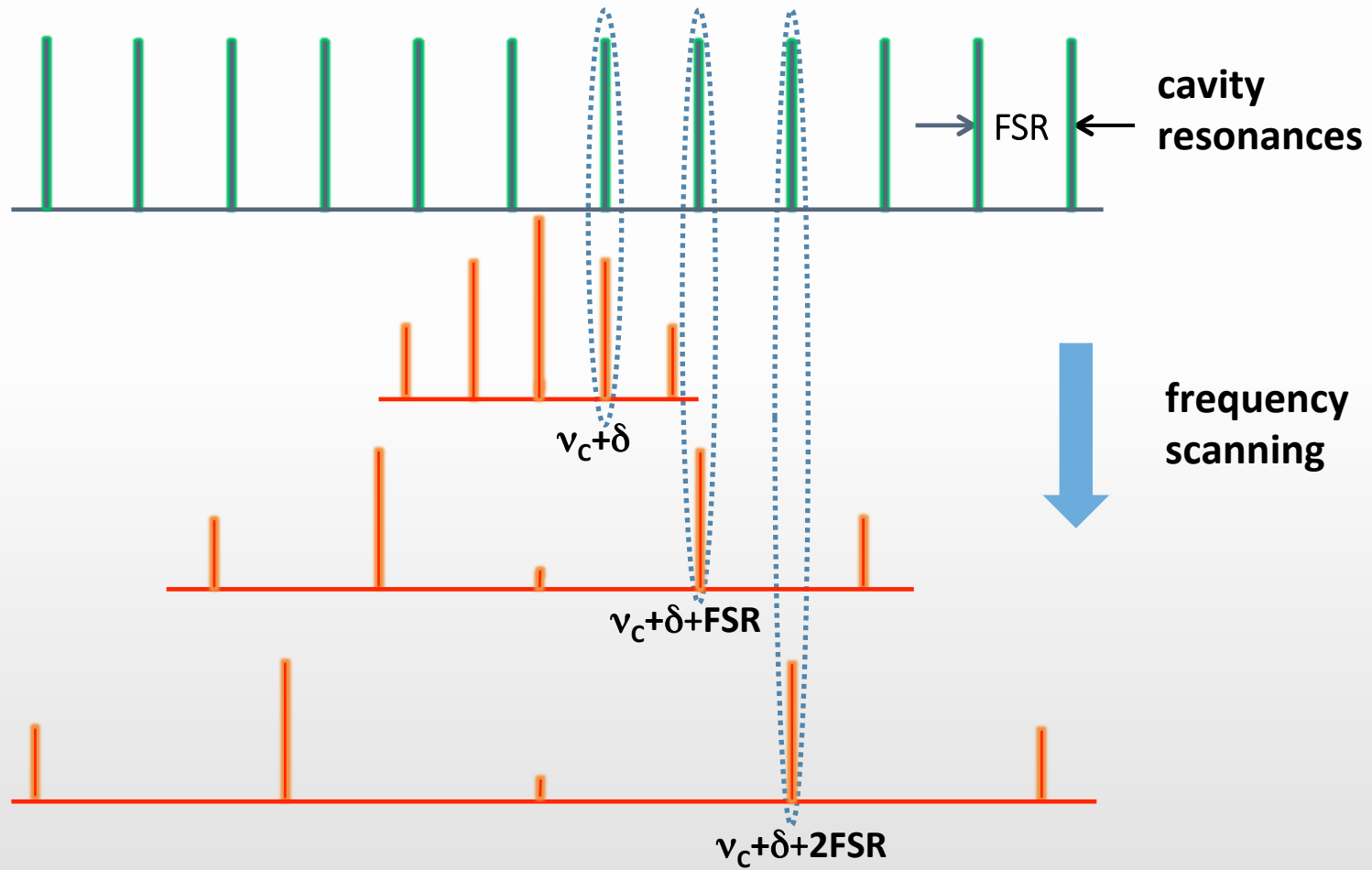
- Use waveguide electro-optic phase-modulator (PM) to generate tunable sidebands
- Drive PM with a rapidly-switchable microwave (MW) source
- Fix carrier and use ring-down cavity to filter out all but one selected side band



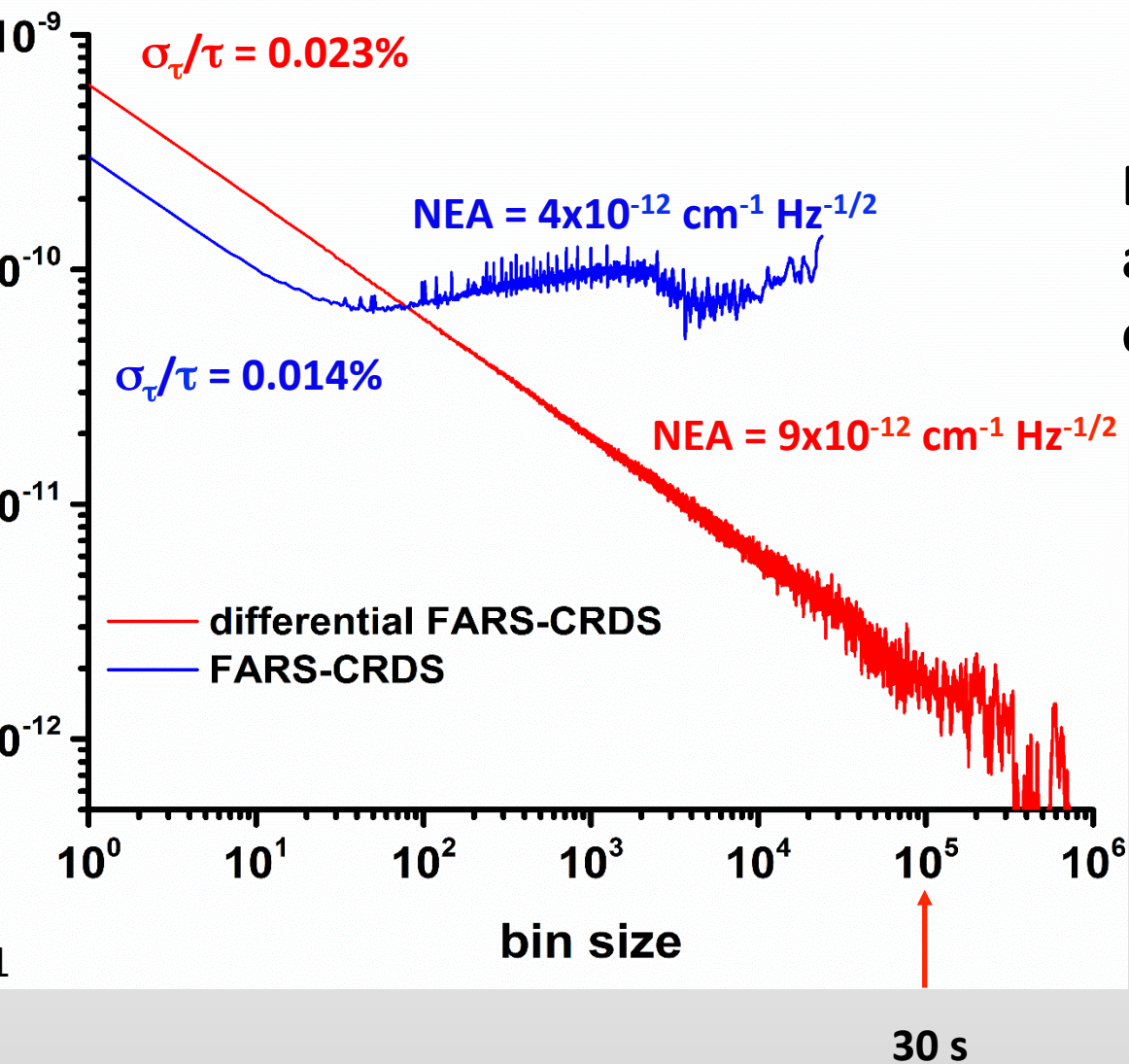
Advantages:

- Overcomes slow mechanical and thermal scanning
- Links optical detuning axis link to RF and microwave standards
- Wide frequency tuning range ($> 90 \text{ GHz} = 3 \text{ cm}^{-1}$)

FARS measurement principle

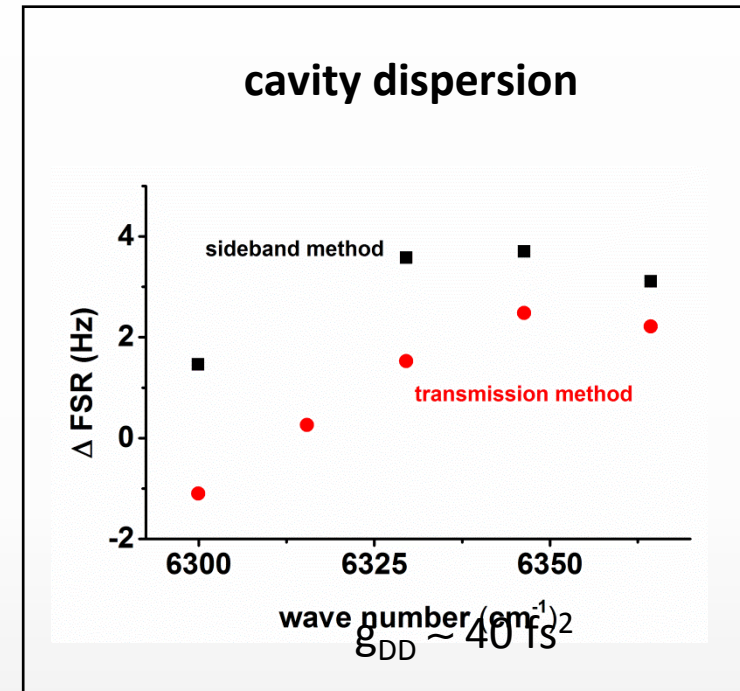
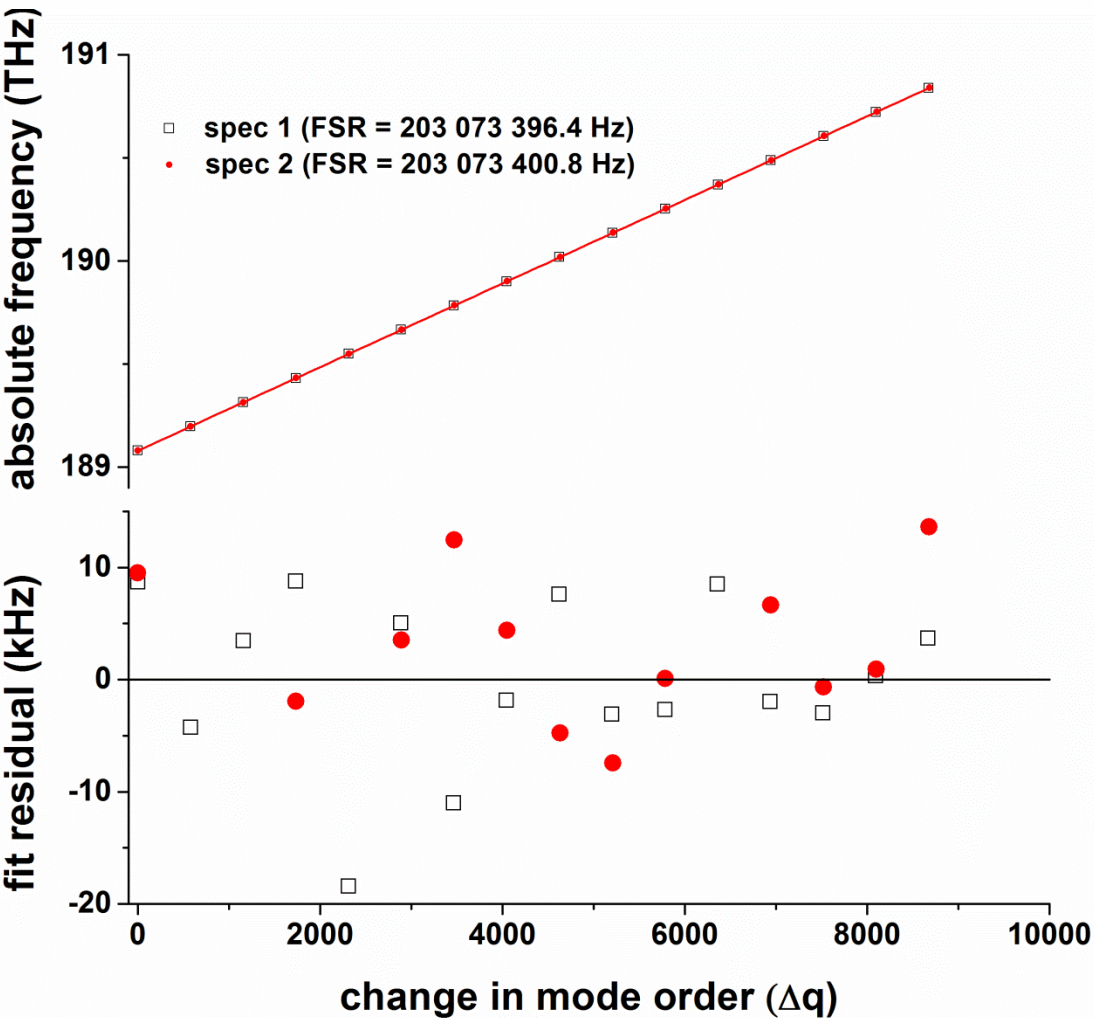


Averaging Statistics: Standard FARS-CRDS vs. Differential FARS-CRDS



Differential approach increases optimal averaging time by more than three orders of magnitude

FARS-CRDS with OFC-referenced frequency axis

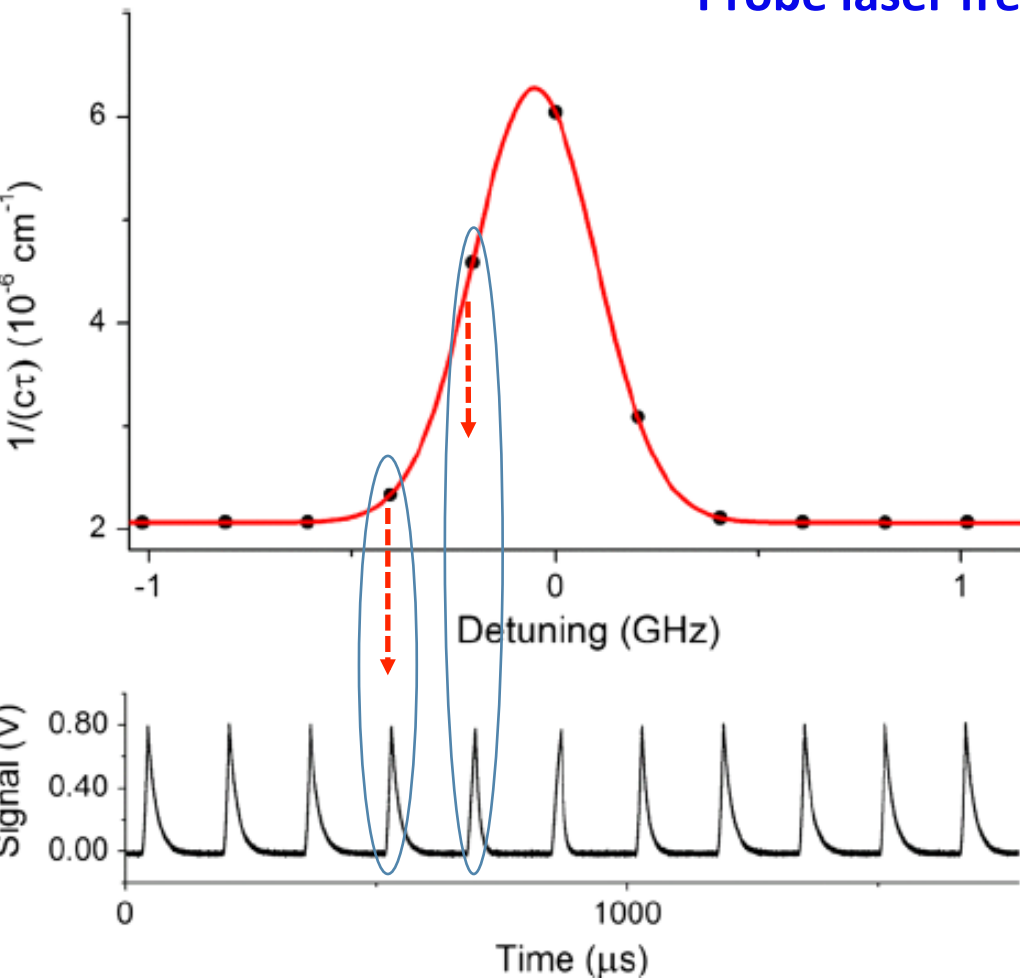


System includes:

- Ring-down cavity locked to I_2 -stabilized HeNe
- Probe laser PDH-locked to cavity
- Optical frequency comb (OFC) for absolute ref

FARS eliminates “dead-time” in CRDS scans

Probe laser frequency can be tuned and relocked to next cavity during the previous decay event



rel. unc. in τ base cav. loss

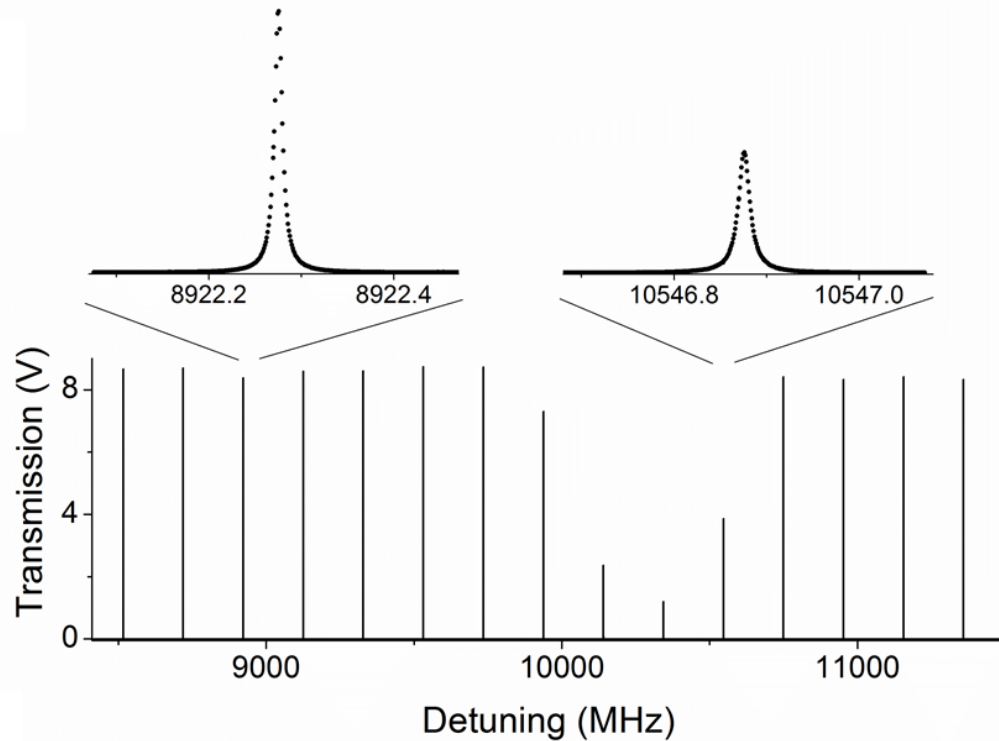
$$\text{NEA} = 80 \text{ ppm} * 150 \text{ ppm} / [(74 \text{ cm} * (8 \text{ kHz})^{1/2})]$$

$$= 1.7 \times 10^{-12} \text{ cm}^{-1} / \text{Hz}^{1/2}$$

cav. length acq. rate

Long et al., *Frequency-agile, rapid scanning spectroscopy: absorption sensitivity of $2 \times 10^{-12} \text{ cm}^{-1} \text{ Hz}^{-1/2}$ with a tunable diode* Appl. Phys. B **114**, 489-495 (2014)

Measuring losses in terms of cavity line width



With PDH-locked FARS-CRDS can measure the shape and width of individual cavity resonances

The width of the resonances provides an equivalent measure of the absorption in the frequency domain,

$$\alpha = \Delta\omega_{1/2}/c$$

~130 Hz relative laser linewidth

Uncertainty of the fitted resonance frequency ~1 Hz

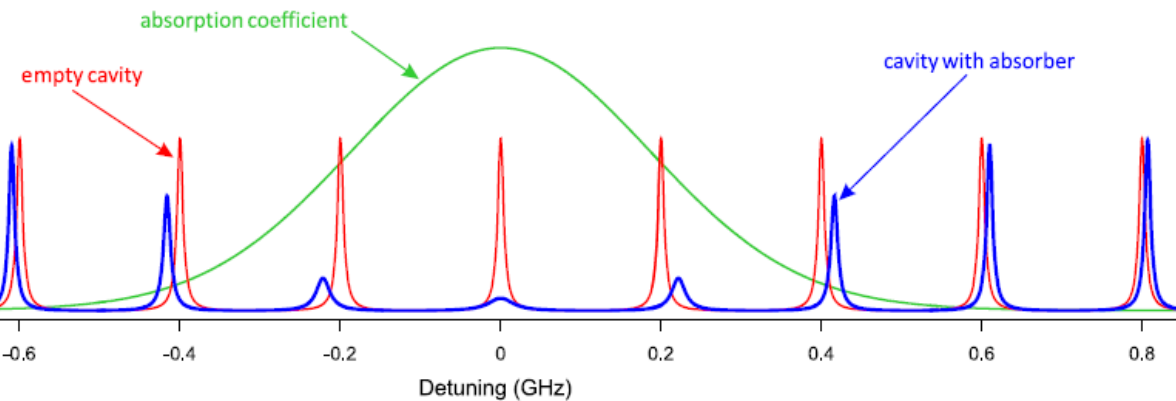
Uncertainty of the fitted width of the resonances ~0.04%

Absorption spectrum measured by observations of frequency for both the x and y axes.

et al., *Frequency-agile, rapid scanning spectroscopy: absorption sensitivity $10^{-12} \text{ cm}^{-1} \text{ Hz}^{-1/2}$ with a tunable diode laser*, Appl. Phys. B **114**, 489-495 (2014)

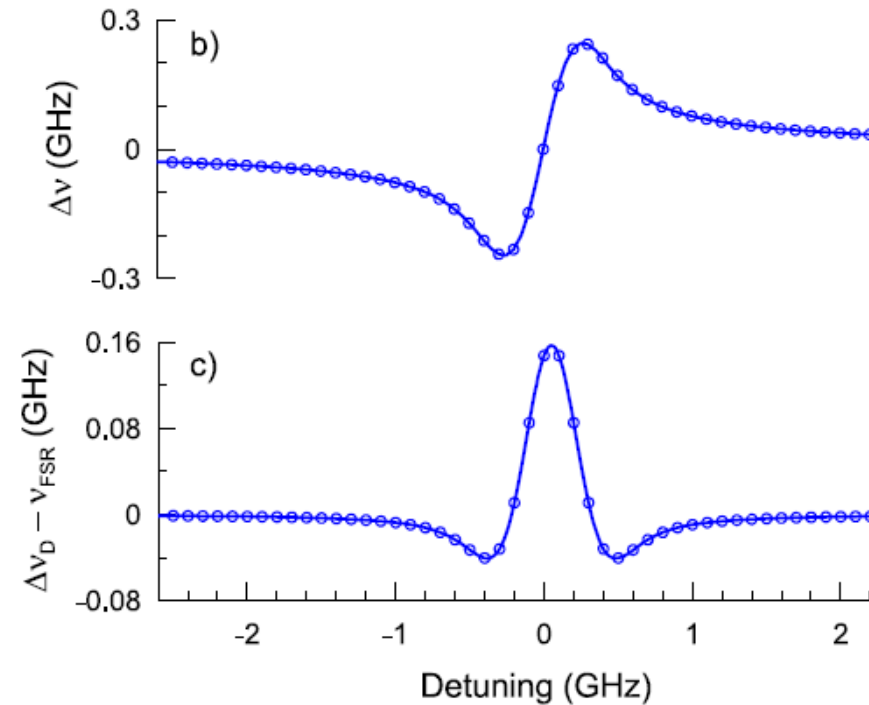
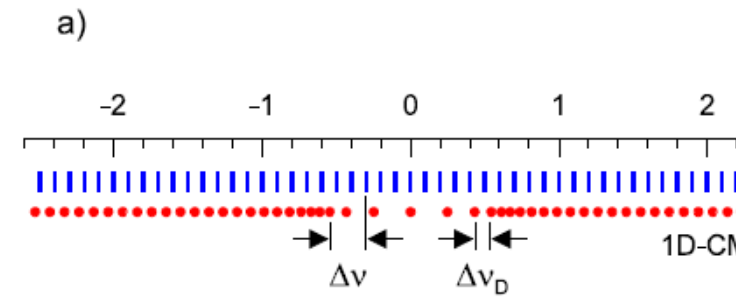
et al., *Cavity mode-width spectroscopy with widely tunable ultra narrow laser*, Opt. Expr. **21**, 29744-29754 (2013)

One-dimensional frequency-based spectroscopy



...tion spectra (both x and y axes) obtained exclusively
...s of frequency measurements

...e potential for quantifying systematic uncertainty by
...rison to standard CRDS and mode-width measurements



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